

# UNDERSTANDING LUNG ACINAR MICROMECHANICS IN HEALTH AND DISEASE: LINKING QUANTITATIVE IMAGING AND ORGAN SCALE MECHANICS BY COMPUTATIONAL MODELING

EDITED BY: Matthias Ochs, Bradford Julian Smith and Lars Knudsen  
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# UNDERSTANDING LUNG ACINAR MICROMECHANICS IN HEALTH AND DISEASE: LINKING QUANTITATIVE IMAGING AND ORGAN SCALE MECHANICS BY COMPUTATIONAL MODELING

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# Editorial: Understanding Lung Acinar Micromechanics in Health and Disease: Linking Quantitative Imaging and Organ Scale Mechanics by Computational Modeling

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## Editorial on the Research Topic

### Understanding Lung Acinar Micromechanics in Health and Disease: Linking Quantitative Imaging and Organ Scale Mechanics by Computational Modeling

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The respiration-related dynamic changes in acinar microarchitecture are very complex and not entirely understood. Therefore, the overall goal of this special issue was to present studies of quantitative morphology, lung mechanics, and computational simulations of acinar dynamics under both physiological and pathophysiological conditions. Taken together, this collection of articles includes four reviews, one hypothesis and theory article, and nine publications of original research.

Matuszak et al. summarize the history and technical developments in the field of intravital microscopy which provides two-dimensional images for assessments of dynamic changes of subpleural alveoli *in vivo*. Taking both intravital microscopy and other imaging techniques into account, the authors comprehensively describe the dynamic changes of both the alveolar airspaces and the capillary network within alveolar septa. This highlights the complex three-dimensional architecture of the alveolar capillary network which is subject to dynamic changes during respiration, and developmental related changes that have not been studied in detail before. In a new-born mouse lung Buchacker et al. used Serial Block-Face Scanning Electron Microscopy to create three-dimensional image stacks with nanometer-scale resolution and then segmented the capillary network within alveolar septa. The reconstruction also included feeding arterioles and the draining venules to describe the complete path of blood through this network. Of particular interest for physiology, and potential use for computational modeling, is the finding that the capillary networks of different saccules are highly interconnected and receive blood from several arterioles and, as such, cannot be regarded separately.

While Buchacker et al. were interested in the capillary network, Cremona et al. investigated the development and Schulte et al. effects of aging on the pulmonary airspaces with the goal of linking structure to function. Both of those studies used design-based stereology, the current gold standard for quantitative morphology using any imaging technique. Cremona et al. investigated

the relevance of the integrin  $\alpha 8$  subunit in lung development and found impaired prenatal branching morphogenesis of the conducting airways with reduced lung volume at birth. Postnatal alveolarization was characterized by accelerated formation of secondary septa so that at late time points lung volumes did not differ between wildtype and integrin  $\alpha 8$  subunit-deficient mice (Cremona et al.). The effects of aging on lung structure and organ-scale lung mechanics in mice was further investigated by Schulte et al. Aging was linked with an increase in the volumes of alveolar and ductal airspaces, as well as alveolar number, while organ-scale tissue elastance decreased. These observations indicate an age-related structural remodeling that result in more distensible lungs.

The analytical and computational modeling of Bou Jawde et al. suggests that the age-related reductions in lung stiffness described by Schulte et al. arise from the alterations in alveolar size and alveolar number, not from changes in the properties of the septal tissue itself. By fitting their models to parenchymal stiffness measured in young and old mice, they show that the age-related stiffening of the alveolar septa may be attributed to an increase in stiffness of the load-bearing fibers in the alveolar septa (Bou Jawde et al.). In contrast to that highly detailed analysis of the intra-septal fibers and septal mechanics, Ma et al. present a detailed computational model of the whole human lung that links tissue and biofluid mechanics. Their approach combines different length scales including purely conductive airways that are embedded in parenchymal airspaces which are stabilized by the presence of a dynamic pulmonary surfactant system with realistic physicochemical dynamics. The resulting large system of equations was solved for the healthy human lung using high performance computing techniques and their modeling approach provides a cutting-edge tool for investigating lung dynamics on scales from the molecular to the whole organ.

Perlman presents a conceptual analysis of how increased surface tension affects septal wall mechanics based on imaging studies performed in an *ex-vivo* ventilated and perfused lung system to model different mechanism involved in acute lung injury. An edema filled alveolus suffering from high surface tension leads to a deformation of the intervening and radiating septa of adjacent alveoli. This resulting stress concentration is directly proportional to surface tension and is an important pathogenic force in ventilation-induced lung injury *via* alveolar interdependence. Perlman further discusses therapeutic interventions to reduce surface tension and why surfactant replacement therapy might not be effective in acute lung injury. While these concepts were developed and are most frequently discussed in the context of acute lung injury, Sehlmeier et al. extensively reviewed the roles of two important components of surfactant, Surfactant Protein C (SP-C) and cholesterol, in chronic lung diseases such as pulmonary fibrosis. The authors explore the interactions between SP-C, cholesterol, and lung mechanics in healthy lungs and summarize the current understanding of how abnormalities in either of these components (e.g., SP-C deficiency) might result in a pathway of chronic impairment of alveolar dynamics, elevated mechanical stresses, chronic lung injury, and eventual fibrosis.

These factors play out on an acute timescale during ventilator-induced lung injury as detailed in two experimental studies that describe pathologic structural changes and organ-scale lung mechanics using animal models. Smith et al. subjected mice to injurious mechanical ventilation and investigated acinar microarchitecture at different airway opening pressures to infer abnormalities in alveolar dynamics that correspond with degraded surfactant function and lung mechanics. The authors identified three alveolar fates directly reflected in organ-scale lung mechanical abnormalities: (1) unrecruitable flooded alveoli; (2) unstable alveoli that cyclically recruit and derecruit; and (3) healthy and stable alveoli. Unrecruitable alveoli due to high surface tension (microatelectases) have also been shown to occur in acute bleomycin-induced lung injury and might act as stress concentrators that potentially increase the risk for ventilation-induced lung injury. To investigate these stress concentrations, Albert et al. ventilated bleomycin pre-injured lungs to show that the presence of occult microatelectases was associated with the development of ventilator-induced lung injury as measured in increased blood-gas barrier permeability, interstitial edema and organ-scale tissue elastance (Albert et al.). These data illustrated that regional heterogeneity in lung ventilation due to derecruited alveoli increase the risk of lung injury during mechanical ventilation in rodents.

Herrmann et al. used four-dimensional computed tomography to quantify heterogeneity in regional ventilation and parenchymal tidal strain in a porcine model of acute lung injury. This large animal model allows consideration of the important gravitational effects such as tidal strain in the dependent lung. After injury induction, the authors observed that heterogeneity in ventilation and regional parenchymal deformation could be reduced by means of multi-frequency oscillatory ventilation (MFOV) compared to a conventional single-frequency ventilation protocol. Accordingly, MFOV is a promising lung-protective ventilation strategy for injured lungs due to more uniform stress distribution.

In acute- and ventilator-induced lung injury, derecruitment of lung parenchyma contributes to ventilation-induced lung injury *via* atelectrauma (repetitive tidal recruitment and derecruitment) and volutrauma (overdistension) in the remaining patent airspaces. In this context Mori et al. developed an analytical mathematical model of the dynamics of derecruitment of distal airspaces during the progression of ventilator-induced lung injury. Their model reproduces the time course of tissue elastance measurements by assigning time- and tidal volume-dependent distributions of opening and closing pressures, as well as opening and closing rates, to lung units. Hence, changes in lung elastance after recruitment maneuver can be described by a progressive time- and pressure-dependent derecruitment of airspaces.

The (patho)physiology of the alveoli in acute lung injury, or alveolar micromechanics, is summarized in the context of mechanical ventilation by Kollisch-Singule et al. taking into account imaging studies (e.g., *in vivo* microscopy) and

computational simulations. The authors identify alveolar instability, alveolar size heterogeneity, alveolar interdependence, and alveolar tidal volumes as critical parameters during mechanical ventilation and describe how changes in the ventilation parameters influence alveolar micromechanics. The authors conclude that the choice of the optimal ventilation pattern for an injured lung should take the pathophysiology of the alveoli into account, above all how alterations in the ventilation protocol affect alveolar dynamics through the respiratory cycle. Based on these pathophysiological concepts of the alveolar micromechanics Nieman et al. discuss the challenges of the mechanical ventilation of patients suffering from acute respiratory distress syndrome (ARDS) and introduce different ventilation strategies and related clinical trials which might be able to minimize ventilation-induced lung injury.

We hope that this collection of articles stimulates further research in this exciting and clinically relevant field of pulmonary physiology which very much depends on inter-disciplinary research.

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# Assessment of the Alveolar Capillary Network in the Postnatal Mouse Lung in 3D Using Serial Block-Face Scanning Electron Microscopy

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The alveolar capillary network (ACN) has a large surface area that provides the basis for an optimized gas exchange in the lung. It needs to adapt to morphological changes during early lung development and alveolarization. Structural alterations of the pulmonary vasculature can lead to pathological functional conditions such as in bronchopulmonary dysplasia and various other lung diseases. To understand the development of the ACN and its impact on the pathogenesis of lung diseases, methods are needed that enable comparative analyses of the complex three-dimensional structure of the ACN at different developmental stages and under pathological conditions. In this study a newborn mouse lung was imaged with serial block-face scanning electron microscopy (SBF-SEM) to investigate the ACN and its surrounding structures before the alveolarization process begins. Most parts but not all of the examined ACN contain two layers of capillaries, which were repeatedly connected with each other. A path from an arteriole to a venule was extracted and straightened to allow cross-sectional visualization of the data along the path within a plane. This allows a qualitative characterization of the structures that erythrocytes pass on their way through the ACN. One way to define regions of the ACN supplied by specific arterioles is presented and used for analyses. Pillars, possibly intussusceptive, were found in the vasculature but no specific pattern was observed in regard to parts of the saccular septa. This study provides 3D information with a resolution of about 150 nm on the microscopic structure of a newborn mouse lung and outlines some of the potentials and challenges of SBF-SEM for 3D analyses of the ACN.

**Keywords:** serial block-face scanning electron microscopy, lung, capillary network, 3D reconstruction, segmentation



# 1. INTRODUCTION

The design of the gas-exchange region of the adult mammalian lung combines a large epithelial and endothelial surface area and a thin tissue barrier for optimized gas diffusion (Gehr et al., 1978; Maina and West, 2005). The fetal development of the lung is characterized by the subsequently occurring pseudo-glandular, canalicular, and saccular stages. The saccular phase is the first where sufficient gas exchange is possible and is followed by the alveolar stage during which mature alveoli are formed. Species differences exist with regard to onset of alveolarization before or after birth. In rodents, for example, the alveolar phase starts about 3 days after birth whereas in humans the alveolarization begins around the 36th week of gestation and lasts until postnatal growth has been finished. Parallel to the alveolarization, the maturation of the microvasculature takes place (Burri, 1975; Smith et al., 2010; Schittny, 2017).

During the saccular and early alveolar phase, the alveolar capillary network (ACN) consists of two layers of capillary sheets whereas in the mature lung only one sheet of capillaries forms the ACN in the alveolar septum (Burri, 1975; Caduff et al., 1986). The double-layered ACN in the developing lung has long been regarded as the prerequisite for the formation of new alveoli although lung growth after micro-vascular maturation, i.e., after pneumonectomy, suggests that this may not be a necessity (Hsia et al., 1994; Fehrenbach et al., 2008). Anyway, evidence exists that the vasculature is of particular importance for the development and maintenance of the alveolar septum: Bronchopulmonary dysplasia (BPD) develops as a consequence of preterm birth and interrupted or aberrant lung development (Solaligue et al., 2017). Several authors have hypothesized that the disrupted alveolarization is the result of a disrupted micro-vascular development, the so-called vascular hypothesis of BPD (Klekamp et al., 1999; Bhatt et al., 2001; Maniscalco et al., 2002). Similarly, a vascular hypothesis has been proposed for COPD/emphysema based on the pathological observation that alveolar septa were present in emphysematous lungs which were devoid of capillaries suggesting that loss of capillaries precedes the loss of alveolar septa/epithelium (MacNee, 2005).

The ACN has a complex 3D structure and methods to analyze it comparatively during development and under pathological conditions are needed (Mühlfeld et al., 2018). Ideally, the methods have a high spatial resolution, contain information on the ACN and its micro-environment and are efficient with regards to time and costs. Recently, a formal stereological approach to estimate the number of capillary loops in the ACN was established (Willführ et al., 2015). In addition, a semi-automatic digital tool to generate 3D reconstructions of the ACN from histological sections was developed (Grothausmann et al., 2017). This approach has several limitations, for example the section thickness, sectioning artifacts, and the resolution of the light microscope. Particularly, in the developing lung, the double-layered ACN as well as the proposed mode of angiogenesis (intussusception) (Burri and Djonov, 2002) require a method of higher resolution to image even very thin cellular structures of a few hundred nanometer thickness.

Serial block-face scanning electron microscopy (SBF-SEM) in combination with digital image analysis offers a method to analyze the ACN of newborn lungs. In contrast to serial sectioning, this technique is based on the repetitive scanning of a block face followed by (automatic) removal of an ultra-thin (approximately 80 nm) section (Peddie and Collinson, 2014; Ochs et al., 2016; Schneider et al., 2019). Scans can run automatically over a few days to weeks and are nearly free of sectioning artifacts. Also, the alignment of the sections requires only minimal effort.

Here, we tested the suitability of SBF-SEM and digital image analysis to visualize the capillary network in the newborn mouse lung. Although there are only sacculi at that age, for the sake of convenience we will use the term ACN also for the newborn capillary network. Special aims were to distinguish between single- and double-layered parts of the ACN, to visualize the transition from arterioles into the ACN and to analyze the parts of the ACN that are potentially perfused from a certain entry of an arteriole. According to developmental studies, one mode of enlargement of the ACN is the in-growth of cellular processes within the existing vessels leading to a lateral expansion of the network. This process is known as intussusception (Burri and Djonov, 2002). Therefore, it was tested whether presumed intussusceptive pillars can be identified.

# 2. MATERIALS AND METHODS

## 2.1. Animal and Surgery

A neonatal wildtype mouse (C3B6 F1 C57BL/6 WT mice, Charles River Laboratories, Sulzfeld, Germany) weighing 1.3–1.4 g was deeply anesthetized with an intraperitoneal injection of ketamine and xylazine (120 and 16 mg/kg, respectively) and sacrificed by exsanguination. Lungs were perfusion fixed using an adapted protocol by Vasilescu et al. (2012b). In brief, the trachea was cannulated and lungs were inflated with room air at a constant pressure of 20 cm H<sub>2</sub>O, the pulmonary artery was cannulated via a small incision in the right heart ventricle. A preflush solution consisting of 94.5% isotonic Ringer (with 5% dextran), 5% procaine (10%), and 0.5% heparin was administered via the pulmonary artery at 20 cm H<sub>2</sub>O pressure and allowed to drain through a small incision in the left heart atrium. After 5 ml of preflush perfusion and the lung tissue visually cleared from blood, the perfusion solution was changed to fixative solution containing 1.5% glutaraldehyde and 1.5% paraformaldehyde in a 0.15 M HEPES buffer at pH 7.35. Vascular perfusion fixation was performed for 10 min at constant airway and perfusion pressures. After perfusion fixation the trachea was double-tied with a 5-0 surgical silk, removed and submerged in fixation solution overnight at 4°C. All experiments were approved by the Regierungspräsidium Karlsruhe and were conducted in agreement with national and international guidelines. Mice were housed in a pathogen-free animal facility and had free access to chow and water.

## 2.2. Preparation and Fixation

For 3D SBF-SEM analysis the samples were processed as described in Beike et al. (2019) based on Deerinck et al.

(2010b), in brief: After fixation (0.15 M HEPES buffer with 1.5% glutaraldehyde and 1.5% paraformaldehyde, pH 7.35) small blocks of the samples (edge length 1–2 mm) were stained en bloc applying a rOTO protocol (rOTO: reduced osmium tetroxide “thiocarbohydrazide” osmium tetroxide) with uranyl acetate and lead aspartate to obtain enough contrast and conductivity of the biological structures for SEM imaging. The samples were dehydrated in an ascending acetone series and embedded in Durcupan™ ACM resin (Sigma-Aldrich, St. Louis, USA). To prepare the polymerized resin blocks for SBF-SEM, the embedded samples were roughly trimmed, mounted with conductive epoxy glue (Chemtronics, CircuitWorks, Kennesaw, USA) on an aluminum specimen pin (Gatan, Pleasanton, CA, USA) and precisely retrimmed with glass knives. This was followed by sputter coating of the samples with a 20 nm gold layer.

## 2.3. EM-Acquisition

Five thousand two hundred and forty-six sections were cut with 80 nm section thickness in a Zeiss Merlin VP Compact SEM (Carl Zeiss Microscopy GmbH, Jena, Germany) equipped with a Gatan 3View2XP system (Gatan Inc., Pleasanton, CA, USA) and the block-face was imaged with a field of view of  $525 \times 525 \mu\text{m}$  ( $15,000 \times 15,000$  pixel, 35 nm pixel size, 0.5  $\mu\text{s}$  dwell time) with 3.0 kV acceleration voltage in the variable pressure mode at 30 Pa.

## 2.4. Digital Processing

The digital processing used in this paper is defined and documented in source-code, scripts and Makefiles, their specific dependencies are tracked by `git`. The repository is available at [http://www.gitlab.com/romangrothausmann/17-297e\\_1\\_s02](http://www.gitlab.com/romangrothausmann/17-297e_1_s02). With the Makefiles in this repository it is possible to reproduce data, images, and analyses reported in this article. Based on the segmentations from the semi-automated method described below, GNU Make was used to automate the execution of various programs in accordance to the dependencies defined in the Makefiles. A Supermicro Server (sysGen, Bremen, Germany) was used with 2 Intel Xeon E5-2667 processors yielding a total of 16x2 cores, 512 GB CPU-RAM, equipped with Nvidia TITAN X (12 GB GPU-RAM) graphic cards for GPU-processing and remote visualization through VirtualGL (Commander, 25). GNU/Linux (Debian 9) was used as operating system, making use of various open-source tools, e.g., ITK, VTK, ITKSnap, ParaView, gnuplot, GNU parallel, and many others (Tange, 2011a; Yushkevich et al., 32; ITK development team, 412; Williams et al., 44; ParaView development team, 531; VTK development team, 81).

The image series from the SBF-SEM ( $35 \times 35 \times 80$  nm, 16-bit, approximately 2 TB) was resampled to an isotropic voxel size of 150 nm ( $3,500 \times 3,500 \times 2,797$  voxel, 16-bit, approx. 64 GB), which is sufficient to resolve even the thin diffusion barriers and allows to keep the maximum memory foot-print around the size of the given RAM of 512 GB for the most demanding programs used in this study. The contrast was adjusted slice by slice to a given mean and variance to equalize the variations that occurred over the days of acquisition time.

The digital processing characterizes the sample in the following ways:

- regions of supply of the ACN.
- profile of blood vessel diameter as it transitions from artery to capillary to vein.
- diffusion distances in air and tissue.

These characterizations include the following phases:

- semi-automated segmentation in to blood, air, tissue, and lymph.
- generation of vessel center-line between selected points.
- characterization of vessel radius based on the center-line.
- segmentation of regions of supply.

To ease understanding of the processing descriptions, corresponding figures are referenced where appropriate, possibly in a different order than in section 3.

### 2.4.1. Segmentation

A semi-automated method was used for the segmentation into air, blood, tissue, and lymph segments. An additional label was used to mark regions that were not clearly assignable to one of these not even with the extra context of the 3rd dimension. A morphological 3D watershed segmentation of the gradient magnitude was loaded into a specially extended version of ITKSnap (for detail see <https://github.com/pyushkevich/itksnap/pull/1>), that allows to efficiently assign the over-segmented watershed labels to each of the desired categories. It was necessary to divide the dataset into octants in order to keep the memory-footprint below the given RAM for generating the 3D watershed segmentation. Apart from the special processing described below, holes are filled in the air and blood segmentation because neither tissue, air or lymph are expected to “float” in blood nor tissue, blood or lymph are expected to “float” in air.

Lower and upper bounds of the segmentations were created as described in Grothausmann et al. (2017). These are used to obtain bounds for the quantifications in **Table 1**.

### 2.4.2. Processing the Segmentation of the Air and Blood Space

A 3D distance map is created from the segmentation of the air space (a-dm). This is used in **Figure 7d** to color the air segment according to the shortest distance to tissue in 3D.

Based on the qualitative evaluation of the vasculature contained within the dataset, a point in the artery and the vein

**TABLE 1** | Measurements of relative volumes and relative surfaces.

	$V_{low}$	$V$	$V_{upp}$	$S_{low}$	$S$	$S_{upp}$
B	17.4	18.1	21.8	66.7	69.2	91.5
A	54.3	54.6	55.0	40.8	43.9	42.5
L	1.1	1.1	1.3	3.0	3.3	4.5
T	27.1	26.2	21.8	105.7	111.2	132.9

Relative volume ( $V(x)/V(s)$  [%]) and relative surface ( $S(x)/V(s)$  [ $\text{mm}^2/\text{mm}^3$ ]) of blood (B), air (A), tissue (T) and lymph (L) and their lower and upper bounds. The reference volume of the sample  $V(s)$  is  $0.116 \text{ mm}^3$ .

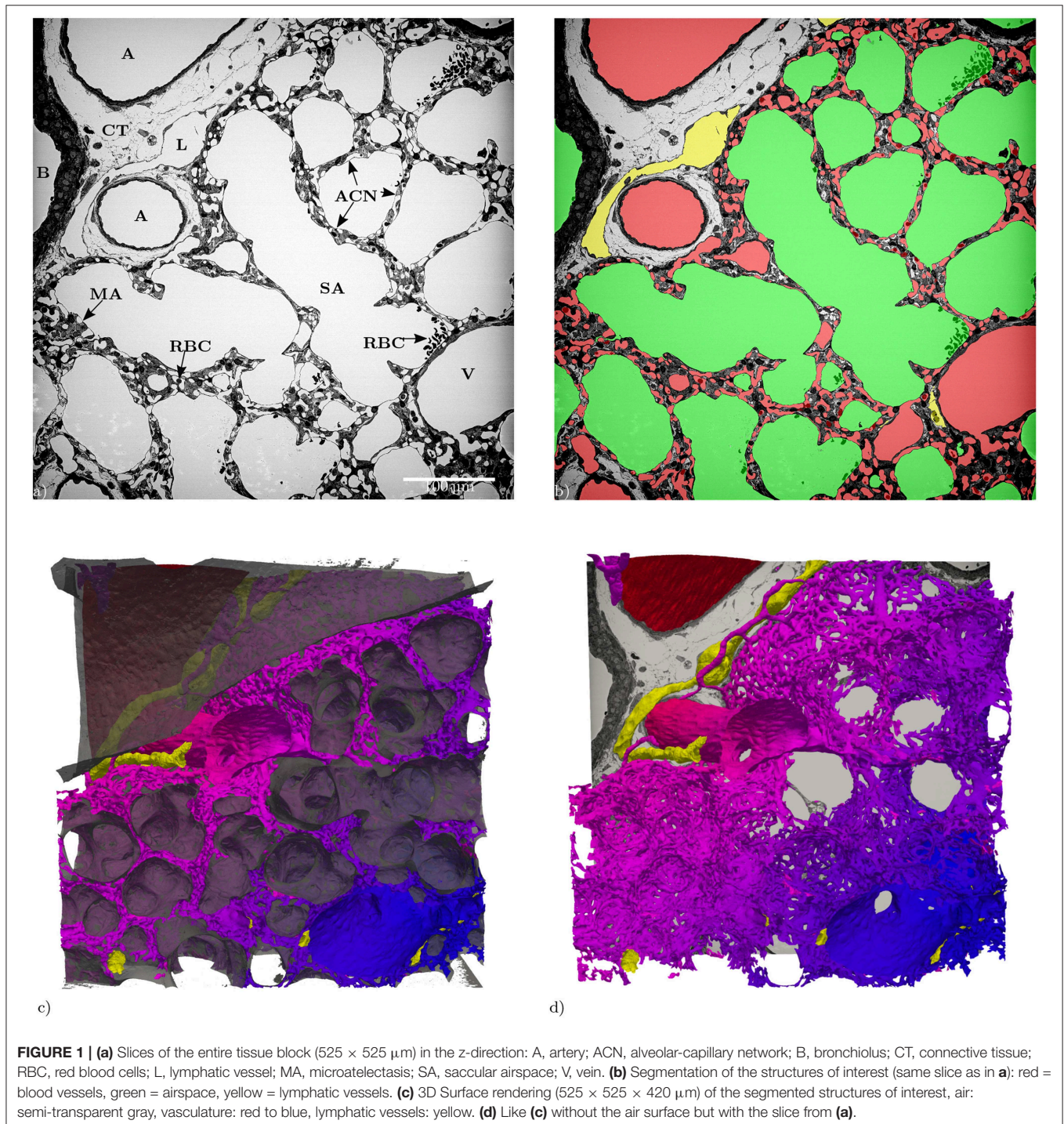


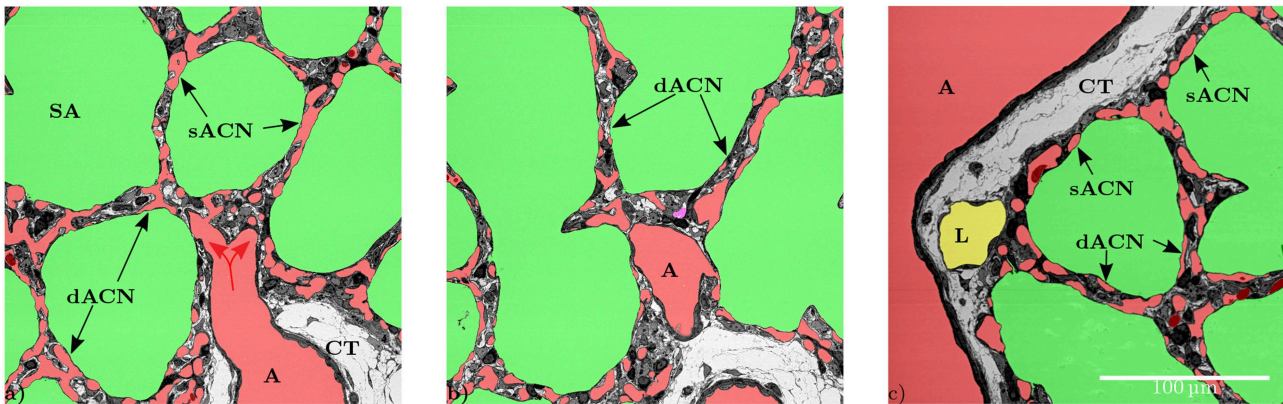
are used as markers. A geodesic distance map is constructed from the manually selected artery-point to all points in the blood segmentation using fast marching (A-fm) (Sethian, 1999). The values of the resulting A-fm can be interpreted as the shortest distance through the vasculature to the artery-point. The same is done for the vein-point yielding V-fm. Then A-fm is subtracted from V-fm, which results in a dataset (V-A-fm) where points that are equally far away from the artery-point and the vein-point

have a value of zero, values closer to the artery-point are positive, those closer to the vein-point are negative.

A signed Euclidean distance map can be generated for the air segmentation and then related to the blood segmentation (t-dm). The resulting dataset can be used to color-code the shortest local distance from the blood surface to the air as in **Figure 3A**.

For further interpretation, a path from the artery-point to the vein-point through the vasculature is found according





**FIGURE 2 |** (a) The artery (A) is surrounded by a single layer of smooth muscle cells and loose connective tissue (CT). The vessel splits into smaller vessels (red arrows) that are no longer surrounded by connective tissue and form the capillary network in the inter-saccular septa. This artery provides blood for several adjacent sacculi. In this slice some parts of the inter-saccular ACN only contain a single layer of capillary vessels (sACN), while other parts contain a double-layered ACN (dACN). (b) Shows the same septa in a different slice, where it can be observed that there also is a double-layered capillary network (dACN) in these septa. The magenta part of the segmentation in the middle of this figure could neither be assigned to the blood vessels, the airspace nor the lymphatic vessel with certainty. (c) Slices where all inter-saccular septa contain a double-layered capillary network (dACN), while the septa that are located between the sacculi and non-parenchymal structures, e.g., lymphatic (L) or artery (A), only contain a single layer of capillaries (sACN).

to Mueller (2008), **Figures 7a,b**. Some modifications to the original code were necessary in this case (for further details see: <https://github.com/InsightSoftwareConsortium/ITKMinimalPathExtraction/issues/61>). The extracted path is not bound to the discretization of the data, it tries to follow the center of the local vessel cross-section while short-cutting on a voxel scale to be as smooth as possible. The path can be guided by way-points, for which two segmented RBCs were chosen. In addition, a binary-image from the maximum-inscribed spheres (ms, **Figures 7a,b**) along the path can be created. As the path is mostly centered in regard to the vessel cross-section, the diameter of the maximum-inscribed spheres can be interpreted as the local minimal diameter of the vessel. If the vessel cross-section is circular, this diameter represents the vessel diameter.

It is possible to straighten each of the above datasets along this path as described in Grothausmann et al., 2017 using a modified version of the code described in Velut (2011). A center slice of the resulting straightened reformatted volume (SRV) then shows the profile of the vasculature and the surroundings along the path. **Figure 7c** shows a center slice of the SRVs of the gray-value dataset with a semi-transparent overlay of the blood, air, and lymph segmentation. The two RBCs used as way-points are centered in the vessel profile. Additionally, the SRV of the ms binary-image is overlaid as well. In regions where this matches the blood segmentation the local circular cross-section is close to circular, in the other regions the difference can be seen as an indicator for non-circular vessel cross-sections.

A slice from the SRVs of V-A-fm, a-dm, and t-dm are shown in **Figure 7d**. Different color look-up-tables (LUTs) were used to indicate the range of distance values according to each dataset. V-A-fm ranges from red (artery-point) to blue (vein-point) over magenta (same distance to artery and vein-point); a-dm ranges from green (proximal) to black (distal); t-dm ranges from yellow (close to air) to black.

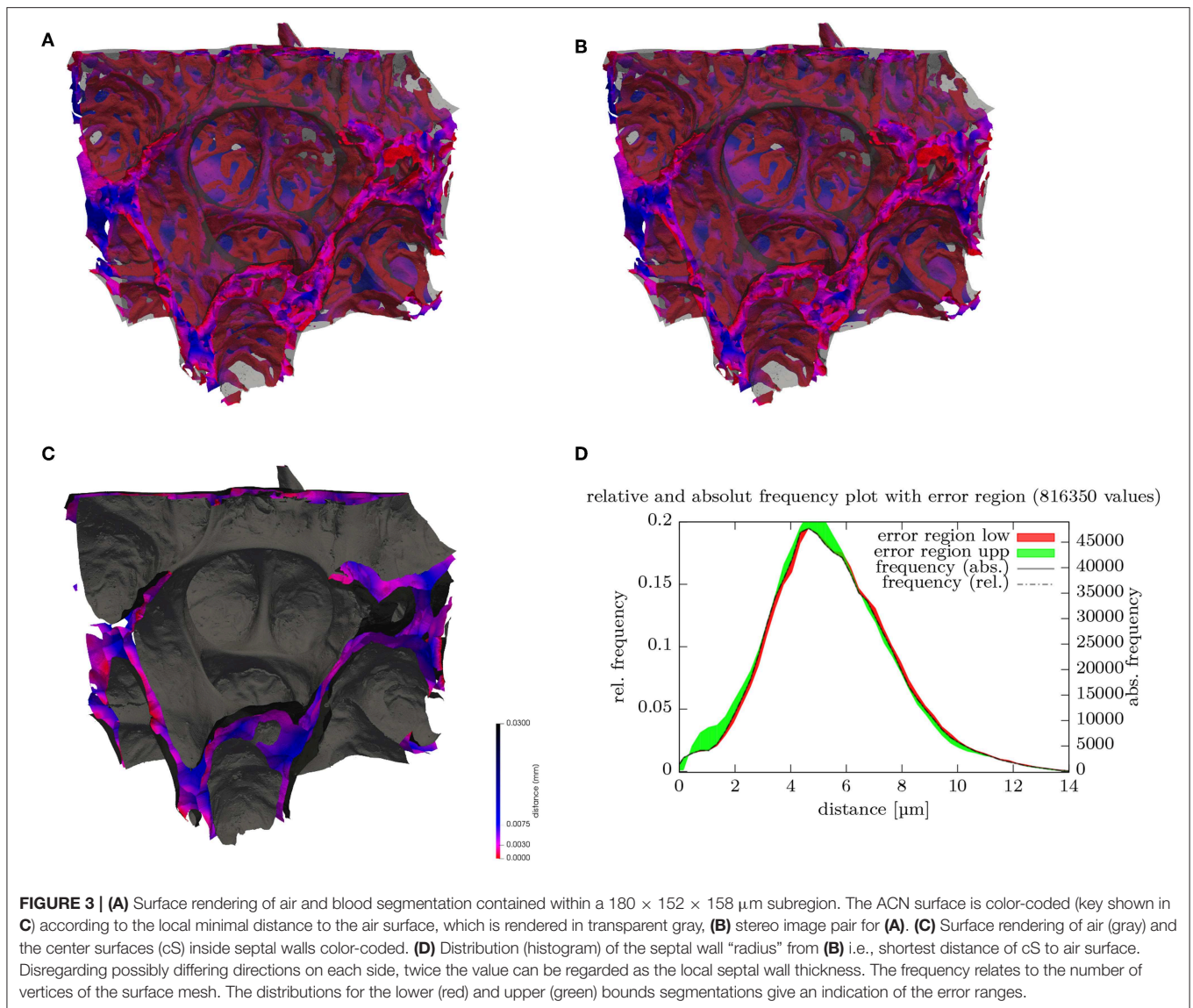
It is possible to separate the larger blood vessels from the ACN with a morphological opening. Regions, a ball with a radius of  $8\ \mu\text{m}$  can reach, are regarded as larger vessels, the rest as ACN. The value of  $8\ \mu\text{m}$  was chosen as a trade-off between removing non-ACN vessels and preserving wider vessel segments contained within the ACN. Labeling the connected components of the ACN binary image (ACN-lcc) shows that there is one main part (consisting of about  $2 \cdot 10^9$  voxel), all other parts have less than about  $4 \cdot 10^6$  voxel (as e.g., the ACN visible in the upper left corner of **Figure 1c**).

There seem to be a few hundred entries from the arterioles into the ACN. Even manual identification of these is difficult. Markers for these were therefore created by using the local maximum inscribed sphere radius as an indication to such entries. These markers were then used for a morphological watershed transform in order to investigate the “region-of-supply” (ROS) of the ACN of each of these entries. The 3D morphological watershed transform basically floods the vasculature in parallel starting from each marker. Then, the region flooded by a marker indicates its ROS. **Figure 6A** shows a few of such ROSs which can vary significantly in size and shape. The relationship between cross sectional area of the ACN and distance to the ROS marker can be examined via the histogram of the geodesic distance map from the ROS markers (similar to A-fm). The count of voxels at each distance is an approximation of the cross sectional area, and the likely bounds on the approximation can be evaluated by comparing the minimal projected area of a voxel (the smallest face) to the maximum projected area (along the voxel diagonal, **Figure 6B**).

#### 2.4.3. Processing the Segmentation of the Septal Walls

A segmentation of the septal walls can be created by combining the segmentation of the tissue with the ACN (and the lymph vessels). These septal walls can then be split into two sides by

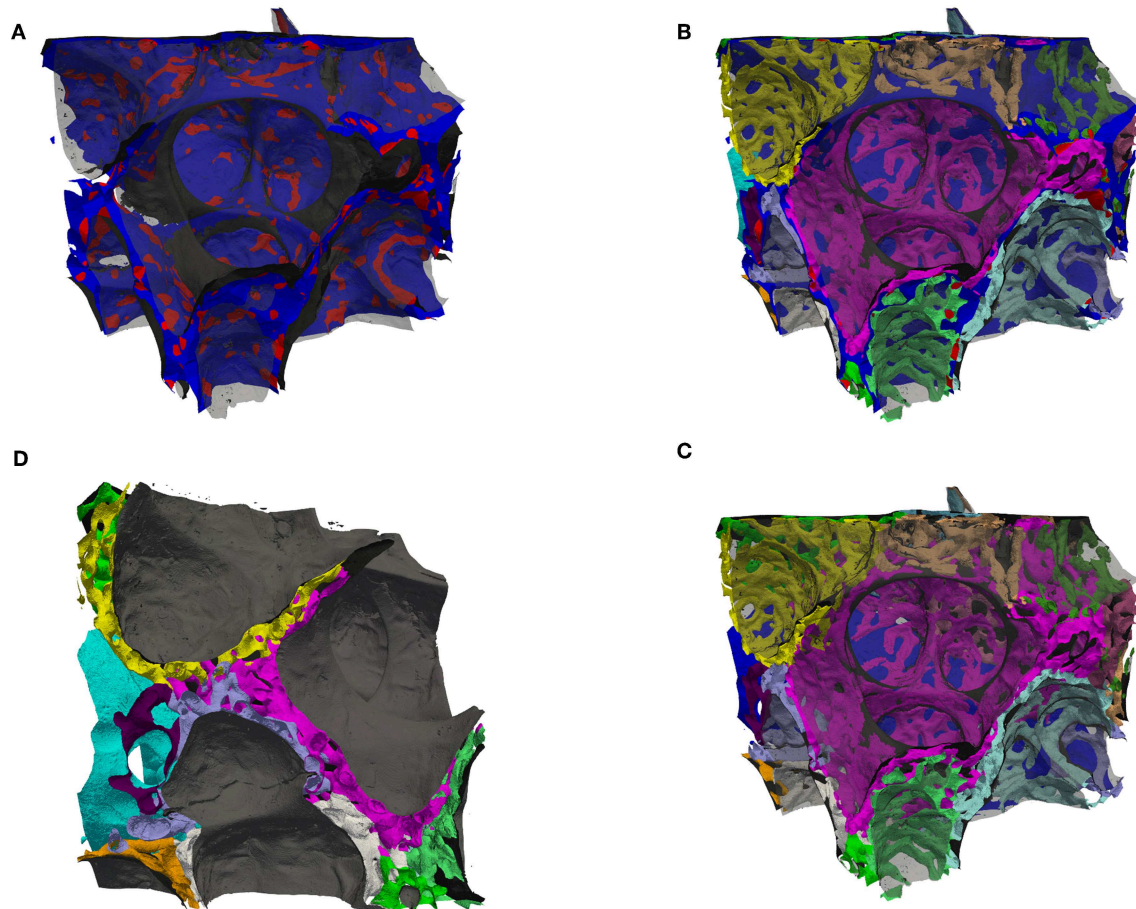




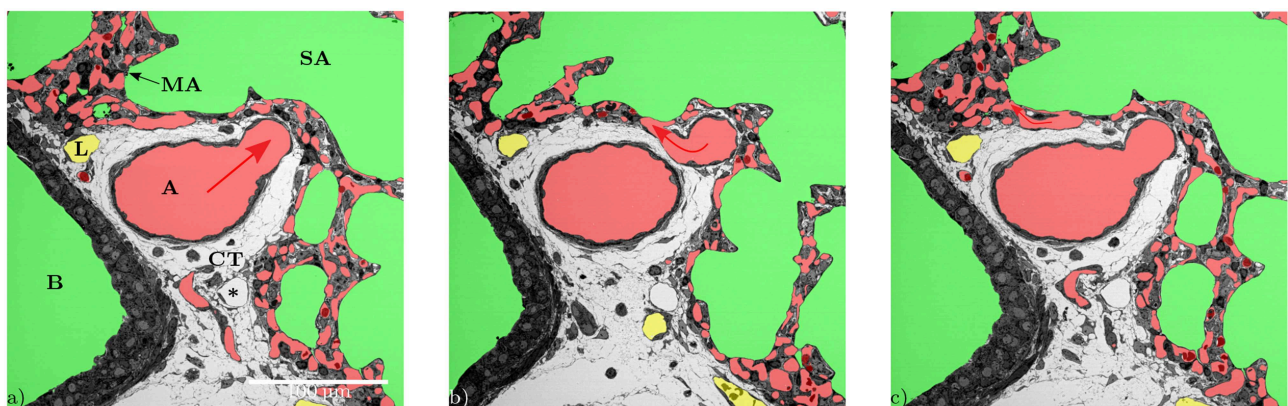
a morphological watershed on the signed distance map of this segmentation. Parts of the borders of these watershed labels lie in the septal walls. These parts are centered in the septa, i.e., they can be regarded as center surfaces (cS) of the septa (Figure 3B)<sup>1</sup>. The cS can be used to split the septa and the ACN. For a double-layered ACN, this should lead to a single-layered ACN for each region (sacculus) (see Figure 4D). Furthermore, the intersection of the double-layered ACN with the cS can be regarded as the inter-communication between the two layers of the ACN, Figure 4A. For a single-layered ACN, the cS would

split each ACN segment into a “half tube.” Whereas, the sides of a double-layered ACN would mostly consist of intact tubes, only the segments connecting both sides would be cut. Therefore, the surface of the cS inside the ACN can be seen as the inter-communication surface, see red regions on the otherwise blue cS in Figure 4A. The ratio of the inner surface (red) to the whole cS surface (red and blue) could be a measure for the inter-communication between two adjacent ACN layers. The ratio is about 20% for the analyzed sub-region. However, this measure is expected not to decrease for a single-layered ACN but to increase because the cS then intersects the whole ACN and not just the inter-communication segments. Examining the ACN at the intersection with the cS, Figures 4B,C, show, that transitions from single to double-layered ACN exist and that inter-communication segments are not necessarily perpendicular to the cS.

<sup>1</sup>This approach for the creation of the cS does not create center surfaces for septa that do not lead to a 3D constriction of sacculus entrances, as can be seen in Figure 4 for the inner septa in the image center. Another way to construct a cS is to use 2D skeletons processed slice by slice. This method does not suffer from the mentioned limitation, but even if done for each spatial direction and combined, it leads to far more inappropriate extrusions than the watershed approach and the cS is likely to have holes.

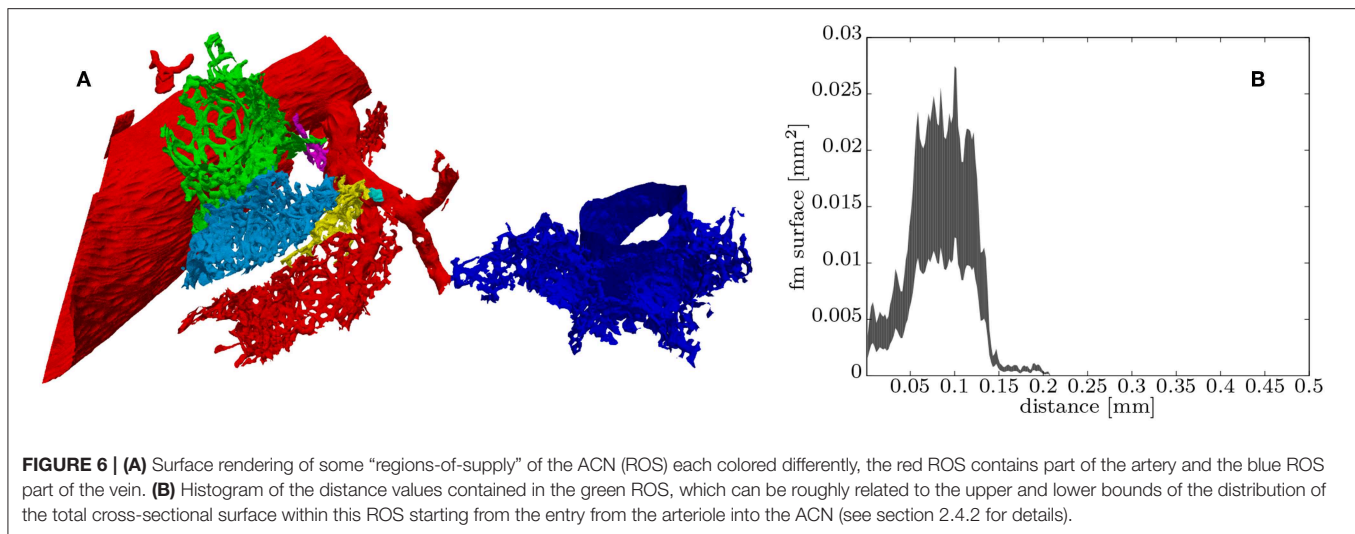


**FIGURE 4 | (A)** Surface rendering of air and the septal center surfaces (cS, as in **Figure 3B**) here colored such that the surface is blue inside tissue and red inside the ACN, i.e., the red regions are the intersection of the cS with the ACN. The air surface is rendered in transparent gray. **(B)** Surface rendering of air (transparent gray), the center surfaces (cS, as in **A**) and the ACN, which is arbitrarily colored such that each side (in regard to cS) has a different color. **(C)** Same as **(B)** but without the cS, instead the vein in blue (partially contained in the back). This view allows to distinguish the single-layered ACN toward the vein and the double-layered ACN mostly in septa separating sacculi. **(D)** Similar to **(B,C)** but viewed from a side, intransparent gray for the air surface to highlight the splitting of the double-layered ACN.



**FIGURE 5 |** Series of different slices from the z-direction showing the division of an artery (A). While the direction of blood flow (red arrows) can be followed as long as the diameters of the off-branching vessels get smaller (**a,b**), it becomes unclear within the ACN, especially when capillaries that branch off flow back together (**c**).





Probing the signed distance map of the septal walls with the cS can be used to visualize the local thickness of the septa (see **Figure 3B**). A histogram of these values then represents the distribution of the septal wall thickness (**Figure 3C**). A visualization of the shortest local diffusion distance from air to blood can be created by probing the signed distance map of the septal walls with the ACN (**Figure 3A**). However, it should be noted that this should be interpreted with caution because its meaning for the inner sides of the double-layered ACN is unclear. Therefore, the distribution of the values is not shown but it can be expected that the distribution would change significantly for a single-layered ACN.

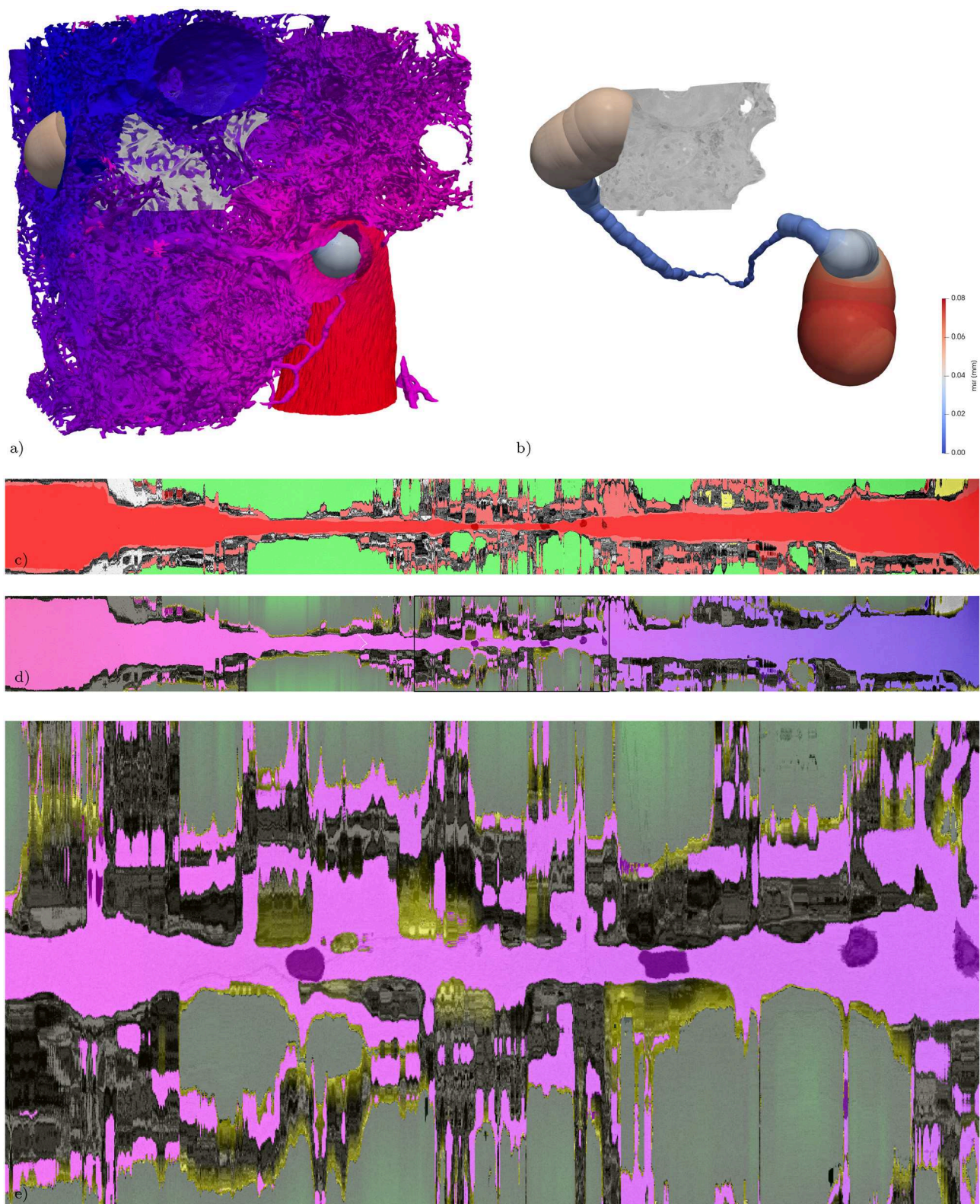
### 3. RESULTS

The data set generated by SBF-SEM had a size of  $525 \times 525 \times 420 \mu\text{m}$  which is approximately  $0.116 \text{ mm}^3$ . The majority of the sample consists of the sacculi and their walls including the capillary network. Most of the capillaries are widely open and contain only very few red blood cells (RBCs, erythrocytes). Although most of the sacculi are well inflated, in some cases microatelectases with one or two collapsed sacculi can sometimes be observed and recognized by the thickened septa and multi-layered capillary network. Some sacculi contain extra-vasated RBCs as a preparation artifact, probably originating from perfusion fixation. In addition to the sacculi and their septa, the sample contains both artery and vein. The artery runs adjacent to a bronchus located at the edge of the tissue block and splits into at least 3 arterioles with a diameter of approximately  $75 \mu\text{m}$  that connect with the ACN. The vein has a diameter of approximately  $100 \mu\text{m}$  and has no connection to a bronchus. **Figure 1** presents a 3D overview of the vascular structures contained in the tissue block and a representative image from the z stack to demonstrate the fixation quality and content of the sample. Arterioles are surrounded by one layer of smooth muscle cells and loose connective tissue, see **Figure 2**.

The next branching generation of approximately  $30\text{--}35 \mu\text{m}$  diameter has only very little surrounding connective tissue and is neighbored by sacculi and their walls. These arterioles branch again into smaller vessels that enter the saccular walls and supply the ACN in various directions. Most parts of the ACN match the concept of a double-layered capillary network **Figures 2–4**, however, in some parts of the septa the ACN is reduced to a single layer. In the saccular walls bordering the non-parenchymal structures, e.g., larger blood vessels, lymphatic vessels or airways, there is usually only a single-layered ACN (**Figures 2, 4**). The two capillary sheets (Fung and Sobin, 1969) of regions with a double-layered ACN have multiple connections between them. Relative volume and surface measurements are listed in **Table 1**. The ratio of blood surface in regard to air surface ( $S(B)/S(A) \approx 1.6$ ) is larger than 1 (compare e.g.  $S_{Vc}/S_{Va}$  in Table 4 of Grothausmann et al., 2017) as expected in the case of a double-layered ACN. **Figure 5** shows another transition of an arteriole into the ACN. The 3D data allows to follow the blood flow from the arteriole into the first capillaries, afterwards the local direction of flow cannot be determined from the structure. The number of possible ways an RBC can take appears nearly unlimited. When investigating the ROS and ACN-lcc datasets, no evidence was found that ROSs are completely separated from each other, overall the connections between neighboring ROSs appear to be the same as within a ROS, see **Figure 6**. This means that, there is no definable part of the ACN that is supplied by a single arteriole because the ACN of multiple sacculi are interconnected and fed by several arterioles. It is not possible to predict the flow direction in the ACN (nor within a ROS) because a point in the ACN can be reached from various arterioles. Examining the SRV dataset as shown in **Figure 7c**, it can be roughly estimated that around 7 sacculi are passed by an RBC following the extracted path.

From a developmental point of view, it is desirable to visualize regions of new septal formation and of angiogenesis. The 3D dataset allows analyzing the sample not only in a certain sectional plane but in any selected direction, like in **Figure 7**.





**FIGURE 7 |** Extracted path from artery to vein and corresponding straightened reformatted volumes (SRVs). **(a)** Surface of the vasculature (as in **Figure 1c**) combined with a rendering of the maximum-inscribed spheres (ms) along the extracted path. In addition the subregion from **Figure 3** is volume rendered in

(Continued)

**FIGURE 7 |** gray-scale. **(b)** Same as **(a)** without the vasculature, revealing the full path indicated by its ms which are colored according to their radius (msr). The path is about 1.2 mm long and the maximum msr along the path is about 76  $\mu\text{m}$  and the minimum msr about 1  $\mu\text{m}$ . **(c)** The SRV of the original data (gray) is overlaid by the segmentation (semi-transparent, air: green; blood: red; lymph: yellow, other: magenta) in addition the voxelization of the locally maximum inscribed spheres is overlaid again in semi-transparent red, giving an indication of local divergence from circular cross-sections. The two RBCs used as way-points for the path extraction are visible as darker spots covered by semi-transparent red along the center line. **(d)** The SRV of the original data (gray) is overlaid by the V-A-fm, a-dm, and t-dm datasets. V-A-fm indicating the distance from the artery to the vein, ranging from red over magenta to blue; a-dm the shortest diffusion distance in the air space towards the surface of the tissue [green (> 50  $\mu\text{m}$ ) to black (0  $\mu\text{m}$ )]; t-dm the shortest diffusion distance from the surface of the tissue to the blood vessels [yellow (0  $\mu\text{m}$ ) to black (> 3  $\mu\text{m}$ )]. **(e)** ACN region marked with a rectangle in **(d)**.

Thus, developing secondary septa, so-called crests or ridges which rise from the primary septa to form new ones, can be looked at in detail, **Figure 8**. Sprouting and intussusception are potential mechanisms of angiogenesis in the developing lung. Intussusception is thought to occur as a cellular bridge between the two sides of a blood vessel which enlarges by ingrowth of a connective tissue core, leading to tissue pillars in the ACN. Such structures can be found in the dataset, see **Figure 9**. However, it is difficult to distinguish between an intussusceptive pillar, indicative of the enlargement of the vascular bed, or a regular tissue pillar of the ACN.

## 4. DISCUSSION

By testing the suitability of SBF-SEM for the analysis of the pulmonary capillary network, the present study has provided new 3D information on the structure of the ACN in the newborn mouse lung. In particular, it could be shown that the so-called double-layered capillary network of developing lungs has to be regarded as a single network extending in all three dimensions rather than two (nearly separated) networks within one septum. However, the network contains segments where only a single-layered “two-dimensional” sheet of capillaries is present. As expected, this was regularly observed at the edges of the sacculi adjacent to larger bronchi or arteries but also within regular septal walls. In addition, the study has shown that the ACN of many sacculi is interconnected and receives inflow from various arterioles which adds to the complexity of understanding the blood flow. Because of the enormous surface area of the ACN, only parts of it are required to meet oxygenation demands at rest which has led to the interpretation that only parts of the ACN are perfused at a given point in time (Wearn et al., 1934; Baumgartner et al., 2004; Wagner et al., 2019), the so-called switching between a perfused and non-perfused state. As the mechanism of perfusion switching remains unknown and *in vivo* ACN perfusion is difficult to analyze, the existence of this phenomenon is controversially debated. The diverse sources of arterial inflow in combination with the interconnection among the capillaries of various sacculi (or alveoli) might offer a complex regulatory system at the level of the arterioles. Another functional aspect of this geometry could be safety: If micro-thrombi from the venous system are transported to the lung and settle in the ACN this will only have minimal effects on oxygenation as gas-exchange is only locally diminished as there is no unique downstream part of the network. It also explains why therapeutic approaches using intravenous application of stem cells do not have major

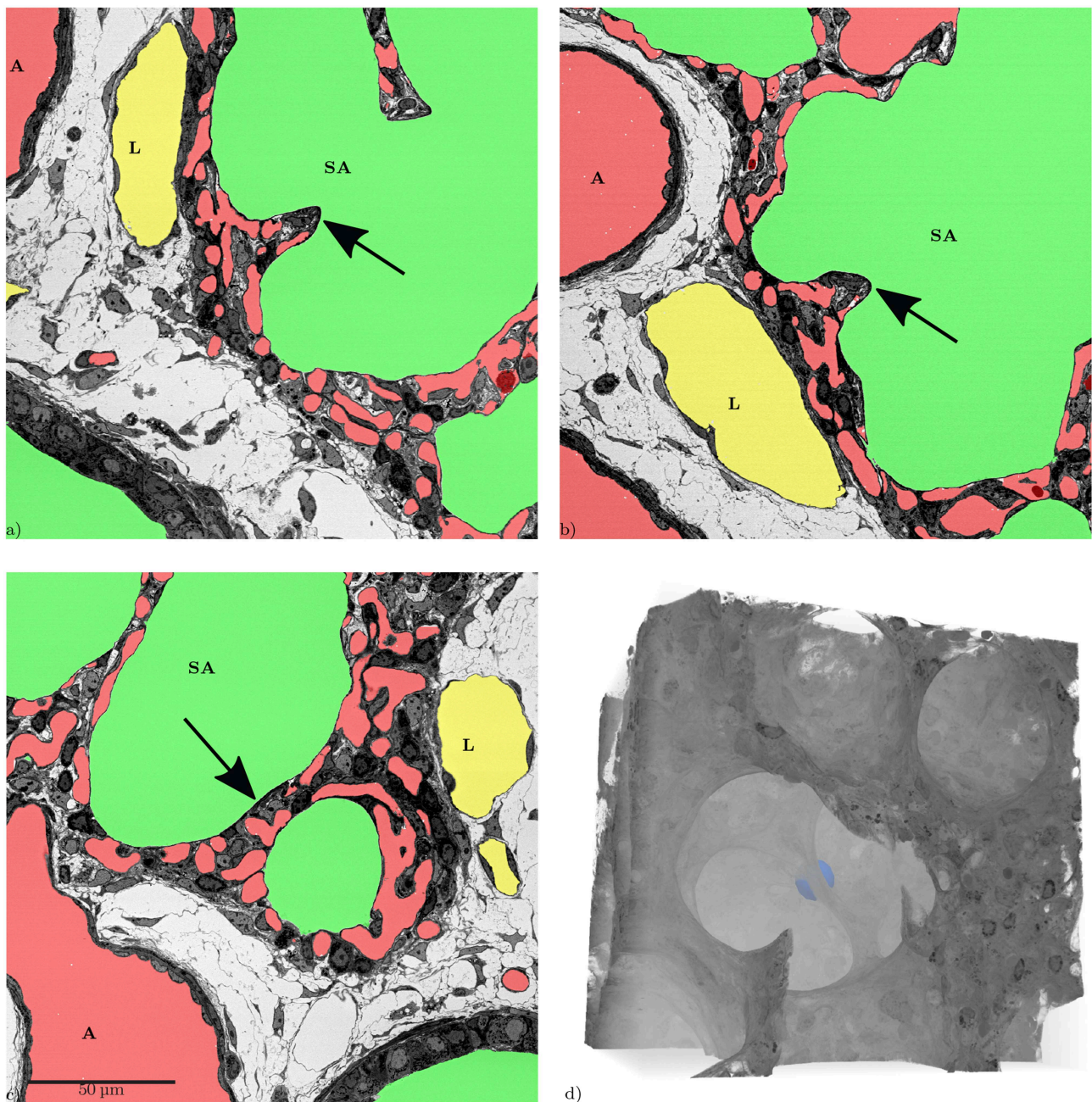
adverse pulmonary effects when stem cells get caught in the ACN (Eggenhofer et al., 2012; Lu et al., 2016).

During the analysis of the segmented microvasculature, emphasis was placed on the identification of structural characteristics that have been described in developmental contexts. One such characteristic are intussusceptive pillars. It was originally believed that the alveolarization requires the existence of a double-layered capillary network as the up-folding of one of the two “layers” is the starting point of secondary septa formation (Burri, 1975; Caduff et al., 1986). This double-layered capillary network is believed to be formed by intussusceptive angiogenesis (Schittny et al., 2008; Ackermann et al., 2013). More recent work has led to the concept that even after micro-vascular maturation, alveolarization continues to take place and that a new layer of the ACN is rather formed by sprouting than intussusception (Schittny et al., 2008; Schittny, 2018). Tissue pillars that match the description of intussusceptive pillars can be found in the presented dataset (**Figure 9**), but their exact role in angiogenesis and lung development is still unclear (Spiegelaere et al., 2012).

Septal up-foldings, so-called ridges that rise from the saccular septa and subdivide the airspace, can easily be identified in the dataset. The reason they often have been described as slender or finger-like protrusions is probably due to their appearance in 2D-analyses (Amy et al., 1975; Zeltner and Burri, 1987), but they appear as long, continuous ridges in 3D that contain a double-layered ACN (Schittny et al., 2008; Branchfield et al., 2016) (**Figure 8**). It was not possible to observe any characteristic differences regarding the ACN in these ridges nor correlation with the occurrence of intussusceptive pillars. The major aim of the present study was to establish SBF-SEM imaging of relatively large samples of lung parenchyma and to test their suitability for the analysis of the pulmonary microvasculature. Therefore, several aspects of the technique are discussed in the following:

In general, the SBF-SEM requires an embedding procedure that differs from classical embedding techniques for SEM or TEM (Deerinck et al., 2010a; Togo et al., 2014). Before starting the automatic SBF-SEM run for obtaining the data set, semi- and ultra-thin sections were generated from several tissue blocks as quality controls. The ultra-thin sections were examined with a transmission electron microscope to make sure that the ROTO embedding protocol with reduced osmium tetroxide, thiocarbonylhydrazide and osmium tetroxide had generated sufficient contrast for further SEM analysis (Ochs et al., 2016). The semi-thin sections were used to select a sample with a well-perfused ACN and a larger artery and vein but without a bronchus in the center of the section. Although



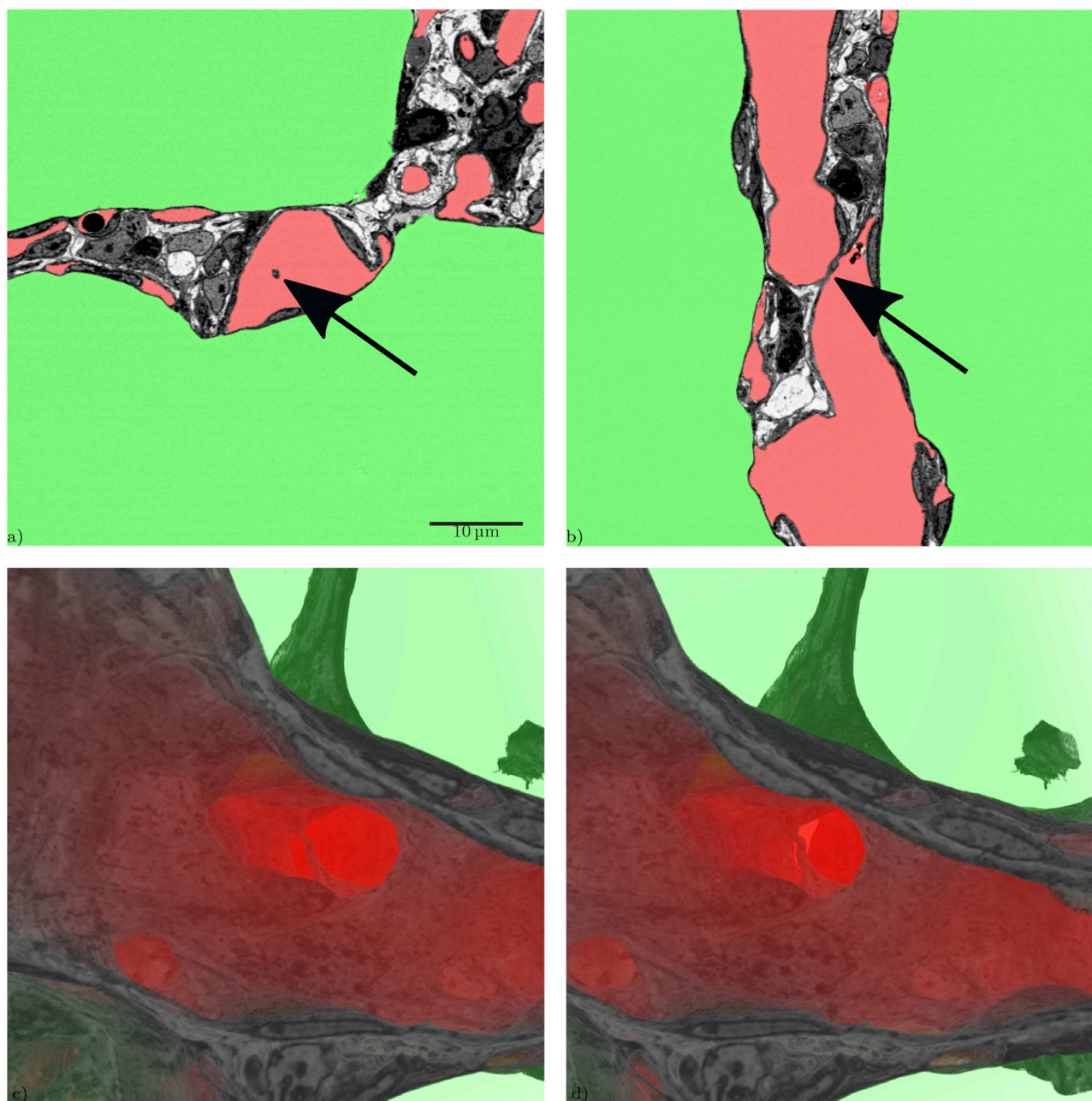


**FIGURE 8 |** Slices from the xyz-directions, showing the same inter-saccular septum (arrows). The structure in **(a,b)** looks like a “finger-like” upfolding of the septum. **(c)** Shows that this structure is a flat septum that can easily appear to be a so-called “crest” when only looking at it in a single slice. **(d)** 3D volume rendering of the same region, the septum shown in the slices is marked by a blue sphere. The 3D-view reveals that there is no “finger-like” upfolding but a continuous ridge.

this procedure helps to find a suitable sample there is no guarantee that the block contains suitable structures in the depth of the sample. Generation of unsuitable data sets due to the unpredictable structural details within the sample is time-consuming and frustrating. Therefore, future studies might benefit from scanning of the sample with a  $\mu$ CT, if available, to make sure the selected block is suited for the intended analysis.

One of the prerequisites of the semi-automatic segmentation used in the present study is the quality of perfusion fixation (Willführ et al., 2015; Mühlfeld et al., 2018). When capillaries are collapsed, the connection of parts of the ACN becomes hardly visible. At the chosen sample size and resolution of the present study, however, even an experienced observer would not be able to identify such lost connections. With the





**FIGURE 9** | Slices through a tissue pillar, possibly an intussusceptive pillar, from two perspectives, **(a)** z-direction, **(b)** x-direction, **(c)** 3D volume rendering of the subregion containing the structure (tissue: hardly transparent black to gray, blood: very transparent red, air: very transparent green), **(d)** stereo image pair for **(c)**, view behind image plane.

described segmentation approach, RBCs contained in the ACN cause interruptions of the ACN segmentation because the RBCs have a contrast similar to the endothelial cells. In the present study, the combination of automatic pre-segmentation and manual post-segmentation to handle remaining RBCs in the segmentation proved to be a convenient yet still time-consuming method. While the computation of the pre-segmentation lies in the range of a few hours, manual post-segmentation including visual quality control took about two weeks, which is about

the same time needed for the SBF-SEM acquisition and for the final digital post-processing. With further advances in machine learning, the recognition and labeling of remaining RBCs could be performed by a trained neural network such that manual interaction could be avoided. Perfusion fixation of neonatal mouse lungs is technically demanding due to the small size of the mouse and its organs. Unfortunately, there is no gold standard for lung fixation (Hsia et al., 2010). Lung fixation is always a compromise and the ideal airway and vascular pressures

in a given experimental setting have to be determined for each experimental purpose. Although the chosen airway inflation and vascular perfusion pressures resulted in a very good preservation of the lung tissue with both inflated airways and widely opened capillaries, the occurrence of a few microatelectases and collapsed capillaries could not be prevented completely.

Several methods to visualize and analyze the ACN have been established over the recent decades. Corrosion casts have the advantage that large parts of the vasculature can be viewed, however, as the technique requires the removal of the surrounding tissue, the cellular environment of the blood vessels cannot be visualized (Caduff et al., 1986; Föhlst et al., 2015). X-Ray computer tomography ( $\mu$ CT) datasets on the other hand prevent the loss of surrounding structures, but still suffer from low resolution that does often not allow the analysis of cellular details (Vasilescu et al., 2012a; Clark and Badea, 2014), however synchrotron CT can provide higher detail (Xu et al., 2012). The present study has shown that SBF-SEM has the potential of having a firm part in the analysis of the pulmonary microvasculature due to its “open view” (all surrounding structures are visible) and its high resolution. A disadvantage of the SBF-SEM approach is the current limitation of the sample volume which is much smaller than with the other techniques and is destructive. Of course, it would be desirable to investigate a complete, closed circuit within the network and perform flow simulations but such a circuit appears to be too large for the SBF-SEM. Possibly, a combination of subsequently applied different techniques, like  $\mu$ CT and SBF-SEM, may help to overcome the shortcomings associated with each method alone.

In summary, the present study has shown that SBF-SEM is a suitable method to analyze the 3D architecture of the pulmonary micro-circulation, particularly the ACN. Digital segmentation helps to visualize and analyze large volumes of the ACN. The high resolution of the images allows viewing small-sized structures like endothelial bridges indicative of intussusceptive angiogenesis. It may be of particular usefulness in the comparative analysis of normal and pathologically altered capillary networks.

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## DATA AVAILABILITY STATEMENT

The git repository containing Makefiles for automated reproduction of the image processing used for this manuscript is available at [http://www.gitlab.com/romangrothausmann/17-297e\\_1\\_s02](http://www.gitlab.com/romangrothausmann/17-297e_1_s02). All used software is open-source and freely available, programs and modifications specifically created for the presented analyses can be found at <http://www.github.com/romangrothausmann/> and <http://github.com/richardbeare/>, docker images of these in the corresponding registry at <http://www.gitlab.com/romangrothausmann/>. The datasets generated for this study are available on request to the corresponding author.

## ETHICS STATEMENT

The animal study was reviewed and approved by Regierungspräsidium Karlsruhe.

## AUTHOR CONTRIBUTIONS

TB, CM, and RG conceived and designed the research, conducted the study, drafted the manuscript, and prepared the figures. WW performed the sample preparation. CW performed the EM-acquisition. RG, RB, and MM performed digital processing and necessary programming. All authors have edited, critically revised, and approved the final version of the manuscript.

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**Conflict of Interest:** MM was employed by Kitware, Inc.

The remaining authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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# Age-Related Structural and Functional Changes in the Mouse Lung

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Lung function declines with advancing age. To improve our understanding of the structure-function relationships leading to this decline, we investigated structural alterations in the lung and their impact on micromechanics and lung function in the aging mouse. Lung function analysis was performed in 3, 6, 12, 18, and 24 months old C57BL/6 mice ( $n = 7-8/\text{age}$ ), followed by lung fixation and stereological sample preparation. Lung parenchymal volume, total, ductal and alveolar airspace volume, alveolar volume and number, septal volume, septal surface area and thickness were quantified by stereology as well as surfactant producing alveolar epithelial type II (ATII) cell volume and number. Parenchymal volume, total and ductal airspace volume increased in old (18 and 24 months) compared with middle-aged (6 and 12 months) and young (3 months) mice. While the alveolar number decreased from young ( $7.5 \times 10^6$ ) to middle-aged ( $6 \times 10^6$ ) and increased again in old ( $9 \times 10^6$ ) mice, the mean alveolar volume and mean septal surface area per alveolus conversely first increased in middle-aged and then declined in old mice. The ATII cell number increased from middle-aged ( $8.8 \times 10^6$ ) to old ( $11.8 \times 10^6$ ) mice, along with the alveolar number, resulting in a constant ratio of ATII cells per alveolus in all age groups (1.4 ATII cells per alveolus). Lung compliance and inspiratory capacity increased, whereas tissue elastance and tissue resistance decreased with age, showing greatest changes between young and middle-aged mice. In conclusion, alveolar size declined significantly in old mice concomitant with a widening of alveolar ducts and late alveolarization. These changes may partly explain the functional alterations during aging. Interestingly, despite age-related lung remodeling, the number of ATII cells per alveolus showed a tightly controlled relation in all age groups.

**Keywords:** pulmonary aging, micromechanics, stereology, late alveolarization, alveolar epithelial type II cells

## INTRODUCTION

Lung aging is accompanied by functional, micromechanical and structural alterations (Chan and Welsh, 1998; Sharma and Goodwin, 2006; Pinkerton et al., 2014). In the elderly ( $>65$  years of age), lung diseases like chronic obstructive pulmonary disease (COPD; Ito and Barnes, 2009; Provinciali et al., 2011), fibrosis/IPF (Raghu et al., 2006; Collard, 2010; Fell et al., 2010; Thannickal, 2013), cancer (Howlader et al., 2019) or acute respiratory distress syndrome (ARDS; Ely et al., 2002; Rubenfeld et al., 2005) occur more frequently and with greater severity than in younger individuals.

These pathologies are also associated with alterations in pulmonary structure and function. For better comprehension of pathological changes with age, it is therefore important to understand the changes of lung function, micromechanics, and structure during normal aging.

Lung function is described by parameters of physiological breathing (Becklake and Crapo, 1991; Pellegrino et al., 2005) that were observed to decline in the elderly (Janssens et al., 1999). For example, studies have shown an increased residual volume (RV) and functional reserve volume (FRV), as well as decreased values of forced expiratory volume in one second (FEV1) in elderly individuals (Kerstjens et al., 1997; Janssens et al., 1999; Turner et al., 2017). Moreover, static lung compliance was found to increase with age (Wahba, 1983; Levitzky, 1984). These changes lead to increased respiratory impairment in the elderly (Vaz Fragoso and Gill, 2012). The mechanical properties of the lung tissue that influence lung function are described by different parameters, such as lung stiffness and elastance (Suki et al., 2011; Suki, 2014; Suki and Bartolák-Suki, 2014). Investigations on age-related changes in lung micromechanics have shown that the elastic recoil pressure decreases in the elderly (Janssens et al., 1999; Turner et al., 2017), possibly due to changes in tissue composition and remodeling (Mercer and Crapo, 1990; Toshima et al., 2004; Subramaniam et al., 2017). Changes in micromechanics are furthermore closely related to structural alterations in the human lung. Structural remodeling and airspace enlargement in aging human lungs was shown qualitatively (D'Errico et al., 1989) as well as quantitatively, by estimation of mean linear intercept [ $L_m$ ] (Verbeken et al., 1992a). In an MRI-based study with hyperpolarized  $^3\text{He}$  gas, Quirk et al. (2016) further confirmed an increase of  $L_m$  as well as decreasing alveolar depth and larger alveolar ductal radius in aging human lungs. These findings show that lung function, micromechanics and structure are closely linked and age-dependent. However, most studies on lung function and micromechanics in humans are cross-sectional and non-invasive and cannot provide the informational quality as research conducted under controlled laboratory conditions. Furthermore, histological samples of healthy human lung tissue are difficult to obtain and often not suited for quantitative structural analysis by means of stereology (Hsia et al., 2010) due to inadequate sample preparation. Thus, studies investigating lung aging are frequently performed under controlled laboratory conditions in animal models to correlate functional and structural parameters in the lung (Zosky, 2015).

In mice, the assessment of lung function and micromechanics is often done by forced ventilation techniques and measurements of pressure-volume changes (Vanoirbeek et al., 2010; De Vleschauwer et al., 2011; Robichaud et al., 2017). Previous studies on lung function over different time courses of maturation and aging provided evidence of an increased inspiratory capacity (IC) (including tidal volume and inspiratory reserve volume) or static lung compliance with age (Huang et al., 2007; Veldhuizen et al., 2019). Major changes in lung function were further found in early adulthood and to a lesser extent later in life (Zosky, 2015; Elliott et al., 2016). Micromechanically, elastic recoil pressure and airway resistance were shown to

decrease with age in mice, whereas lung tissue stiffness tended to increase (Huang et al., 2007; Elliott et al., 2016; Veldhuizen et al., 2019).

Structural changes of the mouse lung with maturation and age included stereological quantification of parameters that are relevant for lung function such as lung volume, alveolar volume and number as well as septal surface area and thickness. However, results on structural changes with age are controversial. For example, Pozarska et al. (2017) found the highest alveolar numbers in 9 months old (mo) mice and biggest alveoli in 22 mo mice in an experimental study covering an age range of 2, 9, and 22 mo mice, whereas another study found no difference in alveolar number in 6 and 24 mo mice (Glassberg et al., 2014). Moreover, little is known about changes in parenchymal airspaces, alveolar septal surface area and volume in the course of aging. These parameters contribute to intact lung function and mechanics and changes may affect the integrity of the lung (Subramaniam et al., 2017; Knudsen and Ochs, 2018). At cellular level, alveolar epithelial type II (ATII) cells play an important role for intact lung function as they produce alveolar surface tension reducing surfactant to prevent alveolar collapsing during breathing (Bachofen and Schürch, 2001). However, no data is available on ATII cell number and size in pulmonary aging. Additionally, although structural investigation by design-based stereology is considered as the gold-standard for morphometric lung research (Hsia et al., 2010), little information is available linking lung functional and micromechanical measurements with profound stereological analyses of the aging mouse lung.

Thus, the aim of this study was to contribute to a comprehensive understanding of age-related structural changes in the mouse lung and linking the findings to functional and micromechanical parameters. As most investigations on lung aging are based on only two age groups (Glassberg et al., 2014; Kling et al., 2017; Veldhuizen et al., 2019), the understanding of gradual changes in lung aging is still limited. The present study investigated age-related changes in lung function, micromechanics and structure in male C57/BL6Jrj mice aged 3, 6, 12, 18, or 24 months to provide a more comprehensive picture of the developmental process from young adulthood to later stages of life.

## MATERIALS AND METHODS

### Animal Model

Male C57BL/6Jrj mice were ordered from Janvier Labs (France) at an age of 3, 6, 12, 18, or 24 months, including 7–8 animals per age group. Before experimental start the animals were allowed to acclimate for 1 week at the local housing facility (Zentrales Tierlaboratorium, Hannover Medical School) with food and water *ad libitum*. The experiments included lung function measurements and quantitative light microscopic analysis (stereology) of the lung. Animal procedures were authorized by the responsible authorities at LAVES (Niedersächsisches Landesamt für Verbraucherschutz und Lebensmittelsicherheit) and are in accordance with the German law for animal protection

(TierSchG; BGBl. I, p. 1206 with corr. on p. 1313) and with the European directive, 2010/63/EU.

## Lung Function and Micromechanics Measurements

Before lung function testing, mice were injected with 80 mg/kg body weight ketamine (Anesketin 100 mg/ml, Eurovet Animal Health B.V.) and 5 mg/kg body weight xylazine (Rompun 2%, Bayer Vital GmbH) intraperitoneally. Under deep anesthesia, tracheotomy was performed and the animals were ventilated by a mechanical ventilation system (flexiVent® FX Module 1 for mice, SCIREQ® Scientific Respiratory Equipment Inc.) at 100 breaths/min and a tidal volume of 10 ml/kg body weight. To suppress spontaneous breathing during lung function measurements, the mice received 0.8 mg/kg body weight pancuronium bromide (Pancuronium-Actavis 2 mg/ml, Actavis GmbH) intraperitoneally. Lung function measurements were taken at a constant positive end-expiratory pressure (PEEP) of 3 cmH<sub>2</sub>O after two recruitment maneuvers. In a different set of animals aged 3, 6, or 18 months ( $n = 7/\text{age}$ ), derecruitability maneuvers were performed with increasing PEEPs of 1, 3, 6, and 10 cmH<sub>2</sub>O. The aim of this experiment was to test for age differences in micromechanical behavior under non-physiological conditions. Static compliance (Cst) was computed by the Salazar-Knowles equation (Salazar and Knowles, 1964). Micromechanical parameters such as tissue resistance (G) and tissue elastance (H) were assessed by forced oscillations following an established protocol (Lutz et al., 2015; Lopez-Rodriguez et al., 2016). Tissue hysteresivity ( $\eta$ ) was computed as the ratio of G/H and hysteresis was calculated as the area between the inflation and deflation limbs of the pressure-volume curve.

## Lung Fixation and Sample Preparation

After lung function measurements mice were killed and the lungs were fixed by tracheal instillation at a pressure of 20 cmH<sub>2</sub>O with aldehyde fixative, containing 1.5% paraformaldehyde (Sigma-Aldrich) and 1.5% glutaraldehyde (Sigma-Aldrich) in 0.15 M HEPES buffer (Merck Millipore). Afterward the heart-lungs-package was excised from the body and stored in the fixative for at least 24 h. Lung volume [V(lung)] was estimated using the Archimedes principle (Scherle, 1970; Schneider and Ochs, 2013). After lung volume measurements, lungs were consecutively sectioned into slices. Every other slice was embedded in glycol methacrylate (Technovit® 7100, Kulzer GmbH), while the remaining samples were subsampled and embedded in epoxy resin (Glycid ether 100 for electron microscopy, SERVA Electrophoresis GmbH). Both embedding protocols were conducted as previously described in detail (Schneider and Ochs, 2014).

From the glycol methacrylate embedded samples 1.5  $\mu\text{m}$  thick sections were cut and stained with toluidine blue (Toluidinblau O, C.I. 52040, Carl Roth GmbH) and eosin-orcein (Eosin G, C.I. 45380, Sigma-Aldrich and Orcein, C.I. Natural Red 28, Sigma-Aldrich),

respectively. From the epoxy resin embedded samples sections with a thickness of 1  $\mu\text{m}$  were cut and stained with toluidine blue.

## Design-Based Stereology

Design-based stereology is the gold standard for quantitative morphometric analyses of the lung due to its accuracy, efficiency, and precision (Hsia et al., 2010) and was applied throughout the entire study. The investigator was blinded to the group identity of the samples during the analysis. The tissue slides were digitalized with a light-microscopic slide scanner (AxioScan.Z1, Carl Zeiss Microscopy GmbH). Systematic uniform random sampling (SURS) (Gundersen and Jensen, 1987; Gundersen et al., 1999; Nyengaard and Gundersen, 2006; Hsia et al., 2010) for stereological analysis was performed with the newCAST™ software (version 5.3.1.1640, Visiopharm®). The following parameters were estimated by stereology: volumes of lung parenchyma, non-parenchyma, septum, parenchymal airspace, alveolar airspace, and ductal airspace. Moreover, septal surface area, number of alveoli, and number and volume of ATII cells were quantified as previously described in detail (Brandenberger et al., 2015).

The estimation of the parenchymal lung volume [V(par,lung)] and non-parenchymal lung volume [V(non-par,lung)] was done by point counting on toluidine blue stained, glycol methacrylate embedded sections. SURS was performed with the Visiopharm® software at a magnification of 5 $\times$  and a sampling fraction of 15–25%. Sampling fractions were dependent on the size of the embedded lung sections and kept constant within one animal. A stereological test grid with 36 sampling points was used (Supplementary Figure 1A). Calculation was done by multiplication of the volume density [V<sub>V</sub>(par/lung)] with the total lung volume [V(lung)] as shown in Eq. 1:

$$V(\text{par,lung}) = \sum P(\text{par}) / \sum P(\text{tot}) \cdot V(\text{lung}) \quad (1)$$

While  $\sum P(\text{tot})$  represents all points falling on lung tissue,  $\sum P(\text{par})$  represents the points on parenchymal tissue. Corresponding calculations were performed for non-parenchymal volume estimation.

Total parenchymal airspace volume [V(airtot,par)], septal volume [V(sept,par)], total septal surface area [S(sept,par)] and mean septal thickness [ $\bar{t}(\text{sept})$ ] were quantified on toluidine blue stained, glycol methacrylate embedded sections, scanned with an objective lens magnification of 20 $\times$ . SURS was performed at sampling fractions of 1.25 to 3.5% per animal using a 20 $\times$  magnification. The stereological test system contained 12 test lines with 24 test points and a length per point [l/p] of 9.4  $\mu\text{m}$  (Supplementary Figure 1B). Point counting was applied to estimate septal volume density [V<sub>V</sub>(sept/par)] and total parenchymal airspace volume density [V<sub>V</sub>(airtot/par)]. Septal volume [V(sept,par)] and total airspace volume [V(airtot,par)] were achieved by multiplying the respective volume densities with V(par,lung).

The septal surface density [ $S_V(\text{sept}/\text{par})$ ] was estimated by counting intersections ( $I$ ) of test lines with the septal surface.  $S(\text{sept},\text{par})$  was calculated by multiplying  $S_V(\text{sept}/\text{par})$  with the reference volume as described previously (Weibel, 1979; Cruz-Orive and Weibel, 1990; Mayhew, 1991; Howard and Reed, 1998; Schneider and Ochs, 2013) and shown in Eq. 2:

$$S(\text{sept},\text{par}) = 2 \cdot \sum I(\text{sept}) / (l/p \cdot \sum P(\text{tot})) \cdot V(\text{par},\text{lung}) \quad (2)$$

Last, the septal thickness [ $\bar{\tau}(\text{sept})$ ] was calculated as shown in Eq. 3:

$$\bar{\tau}(\text{sept}) = 2 \cdot V_V(\text{sept}/\text{par}) / S_V(\text{sept}/\text{par}) \quad (3)$$

To distinguish alveolar airspace [ $V(\text{airalv},\text{par})$ ] and ductal airspace [ $V(\text{airduct},\text{par})$ ], a further investigation was done on toluidine blue stained, glycol methacrylate embedded sections scanned with an objective lens magnification of  $20\times$ . SURS was performed at a sampling fraction of 2.5–6% per animal and a magnification of  $10\times$ . The stereological test grid contained 36 points (**Supplementary Figure 1C**). Calculations of ductal volume density [ $V_V(\text{airduct},\text{par})$ ] and volume  $V(\text{airduct},\text{par})$  were done analogously to parenchymal volume estimations, as shown in Eq. 1. The alveolar airspace volume [ $V(\text{airalv},\text{par})$ ] was calculated by subtraction of  $V(\text{airduct},\text{par})$  from  $V(\text{airtot},\text{par})$ .

For the unbiased estimation of alveolar number [ $N(\text{alv},\text{par})$ ] and ATII cell number [ $N(\text{ATII},\text{par})$ ], the physical disector was used (Sterio, 1983; Ochs, 2006). This method allows the estimation of numbers in a test volume by creating a 3D test system from two planar and parallel cut sections. An unbiased counting frame was used for number estimations (Gundersen, 1977).

Alveoli are assumed to have one entrance to alveolar ducts which is enclosed by a ring of elastin fibers (Mercer and Crapo, 1990; Toshima et al., 2004; Meyerholz et al., 2017). The number of alveoli can be estimated by the Euler number, which describes the connectivity of the alveolar network (Hyde et al., 2004; Ochs et al., 2004). In principle, three topological events are possible to describe a network: bridges, islands, and holes. In the case of alveoli, the Euler number can be reduced to bridges as the other topological items occur very rarely (islands) or never (holes) (Gundersen et al., 1993). Thus, a counting event was the appearance of a closed alveolar elastin “bridge” [ $B(\text{alv})$ ] on one section and two elastin tips (=open alveolar entrance ring) on the other section. For this analysis, glycol methacrylate embedded and eosin-orcein stained sections of two serial tissue sections with a disector height [ $h$ ] of  $3\ \mu\text{m}$  were used (Ochs, 2006). This staining dyes elastin fibers in red-brown and thereby improves the visualization of bridges (Ochs, 2006). The slices were scanned with an objective lens magnification of  $20\times$  and further processed via SURS at a magnification of  $20\times$ . Sampling fractions of 2–4.75% per animal were used. The area of the counting frame [ $A$ ] was  $35,570\ \mu\text{m}^2$

(**Supplementary Figures 2A,B**). Parenchymal reference space was measured using point counting [ $P(\text{par})$ ] on the lower left and upper right corners of the reference section. To increase efficiency, counting was applied in both directions of the image pair. Alveolar number was calculated by multiplying alveolar number density [ $N_V(\text{alv}/\text{par})$ ] by the reference volume as shown in Eq. 4:

$$N(\text{alv},\text{par}) = \sum B(\text{alv}) / (\sum P(\text{par}) \cdot A \cdot h) \cdot V(\text{par},\text{lung}) \quad (4)$$

The number-weighted mean alveolar volume [ $\bar{v}_N(\text{alv})$ ] was calculated as in Eq. 5:

$$\bar{v}_N(\text{alv}) = V(\text{airalv},\text{par}) / N(\text{alv},\text{par}) \quad (5)$$

just like the number-weighted mean alveolar septal surface area [ $\bar{S}(\text{sept}) / N(\text{alv})$ ].

For the quantification of ATII cell numbers, nuclei of ATII cells [ $N(\text{ATII})$ ] were counted for the disector analysis as unique counting events per cell. Cells were counted, if their nucleus only appeared on one section of the disector image pair. Toluidine blue stained tissue sections of epoxy resin embedded samples were cut with a disector height [ $h$ ] of  $3\ \mu\text{m}$ . Slices were scanned with an objective lens magnification of  $40\times$  and further processed via SURS at a magnification of  $40\times$ . Approximately 180 image pairs per animal (60 per slice) were generated and evaluated. The area of the counting frame [ $A$ ] was  $12,000\ \mu\text{m}^2$  (**Supplementary Figures 2C,D**). The number of ATII cells [ $N(\text{ATII},\text{par})$ ] was calculated by multiplication of the ATII cell number density [ $N_V(\text{ATII}/\text{par})$ ] by the reference volume, as shown in Eq. 6:

$$N(\text{ATII},\text{par}) = \sum N(\text{ATII}) / (\sum P(\text{par}) \cdot A \cdot h) \cdot V(\text{par},\text{lung}) \quad (6)$$

Simultaneously, the number-weighted mean volume of ATII cells [ $\bar{v}_N(\text{ATII})$ ] was estimated using the planar rotator (Vedel-Jensen and Gundersen, 1993). Only cells sampled within the disector pairs were subjected to the rotator, using the nucleus as reference point. From the individual estimations, the arithmetic mean was calculated to obtain the number-weighted mean volume of the cells.

## Statistical Analysis

All statistical analyses were performed using SigmaPlot® software, version 13.0.0.83 (SYSTAT® Software Inc.). Data were tested for normality by Shapiro–Wilk test and for equal variance by Brown–Forsythe test. If the data passed both tests, a one-way ANOVA was performed with a pairwise comparison by Bonferroni’s  $t$ -test. If the equal variance or normality test failed, data were  $\ln$  transformed and a one-way ANOVA was performed afterward. For lung function measurements with increasing PEEPs, a repeated measures ANOVA with Bonferroni  $t$ -test was applied. No outlier tests were performed and no data were excluded from the study. Differences were regarded as significant if  $p < 0.05$ .



## RESULTS

### Lung Function and Micromechanics Change Greatest in Early Mouse Adulthood

The greatest changes in lung function such as inspiratory capacity (IC) and static compliance (Cst) were observed in the early period of adulthood, between young (3 mo) and middle-aged (6 and 12 mo) mice. Both, IC and Cst increased by 25% from 3 to 6 mo mice and reached their maximum values at 18 months (Figures 1A,B). However, body weight also increased with age, showing biggest changes between young and middle-aged mice (Table 1) and therefore, Cst and IC per body weight remained quite stable in the course of aging (Figures 1C,D). Only a small but significant increase in IC per body weight was found between 3 and 12 mo mice. Tissue resistance (G) and tissue elastance (H) decreased significantly from 3 to 6 months by 21 and 27%, respectively (Figures 1E,F), but no significant changes were found between middle-aged and old (18 and 24 mo) mice. Hysteresivity ( $\eta$ ) showed no significant changes during aging (Figure 1G), whereas hysteresis increased significantly from 3 and 6 to 18 mo mice by approximately 50% (Figure 1H). All lung function measurement data are further displayed in **Supplementary Table 1**. Results of lung function measurements with increasing PEEPs of 1, 3, 6, and 10 cmH<sub>2</sub>O did not provide any further insights in age-related changes in micromechanics (**Supplementary Figure 3**).

### Lung Parenchyma: Widening of Alveolar Ducts in Old Mice

Pulmonary histology of lung tissue revealed a normal lung parenchyma with absence of any pathological findings such as inflammation or fibrosis. Lung parenchyma from young and middle-aged mice appeared compact with many collateral alveoli surrounding narrow alveolar ducts (Figures 2A–C), whereas parenchyma of old mice appeared less densely packed due to wider alveolar ducts (Figures 2D,E). Stereological quantification revealed that lung volume, parenchymal volume as well as the volume of the parenchymal airspace increased approximately one third from middle-aged to old mice (Figures 2F–H), while the volume densities of these parameters remained almost constant (Table 1). The increase in the volume of the parenchymal airspace during aging was mainly driven by an increase in ductal airspace volume that occurred between 12 (249 mm<sup>3</sup>) and 18 mo (460 mm<sup>3</sup>) mice (Figure 2I), whereas the volume of the alveolar airspace just increased by 16% (Figure 2J). While the volume density of septal tissue remained constant in all age groups, the total septal volume increased from young to old mice (Table 1). Notably, no significant changes in total parenchymal, ductal and alveolar airspace volumes were measured between 18 and 24 mo mice.

### Increasing Number and Decreasing Size of Alveoli in Old Mice

Histology of alveolar structures showed small and densely packed alveoli in young mice (Figure 3A), while the alveoli in middle-aged and old mice were more distended (Figures 3B–E).

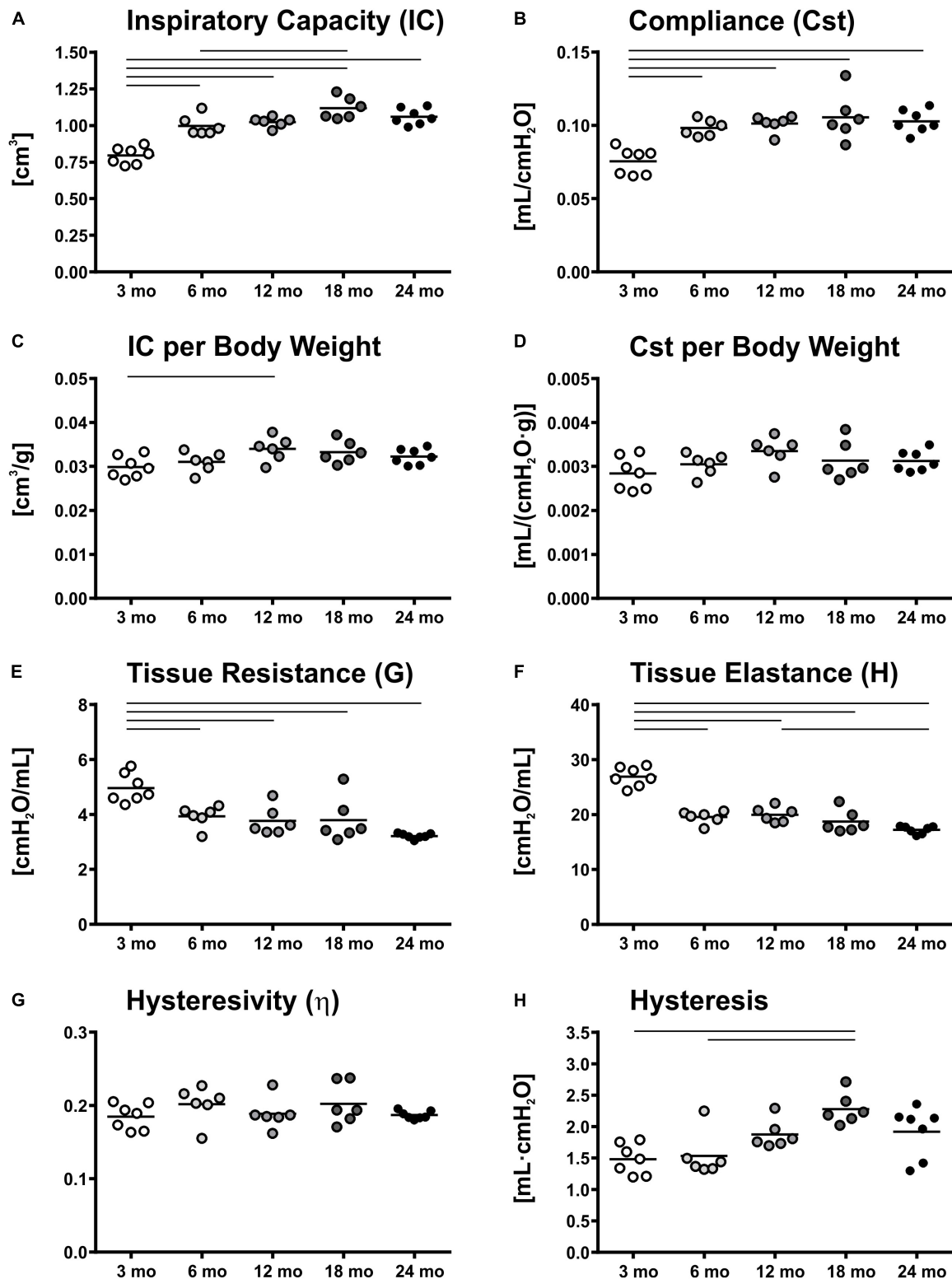
In eosin-orcein stained sections alveolar openings can be well detected due to brown staining of elastin tips at the end of septal borders. The septa oriented toward the alveolar duct thereby appeared shorter in old mice in comparison with middle-aged and young mice (Figures 3A–E). Stereologically, the number density of alveoli showed greatest and significant changes between young and middle-aged mice, decreasing with age (Figure 3F). The absolute number of alveoli on the other hand first decreased from young to middle-aged mice and then increased from middle-aged to old mice by approximately 50% (Figure 3G). The total septal surface area increased significantly from young to middle-aged and to old (18 mo) mice (Figure 3H). However, the septal surface density declined significantly between middle-aged and old (24 mo) mice (Table 1). Accordingly, the mean septal surface area per alveolus was approximately one third bigger in middle-aged compared to young or old (24 mo) mice (Figure 3I). Similarly, the number-weighted mean alveolar volumes were biggest in middle-aged mice ( $\sim 88,000 \mu\text{m}^3$ ) and significantly smaller in young ( $\sim 64,000 \mu\text{m}^3$ ) or old ( $\sim 69,000 \mu\text{m}^3$ ) mice (Figure 3J). The mean septal thickness remained relatively constant over the time course of aging at around  $3 \mu\text{m}$  (Table 1).

### ATII Cell Number Density Remains Constant in Middle-Aged and Old Mice

Representative light micrographs of toluidine blue stained, epoxy resin embedded tissue sections with ATII cells are shown in Figures 4A–E. The ATII cells here are clearly distinguishable due to the metachromatic staining behavior of surfactant storing lamellar bodies. ATII cells were mostly localized in the “corners” of alveoli, near to branching septa and were part of the alveolar septum. Individual cell morphology at light microscopic level remained qualitatively uniform with age. In young mice (Figure 4A), the density of ATII cells was slightly higher compared to older mice (Figures 4B–E). This observation was also supported by stereological findings, as the number density of ATII cells was highest in 3 mo mice and significantly decreased with age, showing an approximately 20% lower density in old mice (Figure 4F). However, the absolute number of ATII cells increased from middle-aged ( $8.8 \times 10^6$ ) to old mice ( $11.7 \times 10^6$ ) (Figure 4G). Interestingly, the number of ATII cells per alveolus remained almost constant at a count of approximately 1.4 over the time course of aging (Figure 4H). The number of ATII cells per septal surface area declined from 3 to 12 months of age and increased again from 12 to 24 mo mice (Figure 4I). The mean volume of ATII cells, estimated by the planar rotator, stayed constant over lifetime at approximately  $280 \mu\text{m}^3$  (Figure 4J).

## DISCUSSION

The aim of this study was to investigate lung aging with respect to structure and function. The results show detailed structural and functional alterations in the mouse lungs over a broad time course from young adult to old mice. In summary, changes in lung function [inspiratory capacity (IC) and static compliance Cst], micromechanics (tissue resistance G and tissue elastance H) and alveolar number and size were greatest in early adulthood



**FIGURE 1 |** Lung function and micromechanics. Inspiratory capacity (IC) (**A**) and static compliance (Cst) (**B**) showed significant increases from young to middle-aged and old mice, respectively. However, IC and Cst corrected for body weight remained rather constant over lifetime (**C,D**). Tissue resistance (G) (**E**) and tissue elastance (H) (**F**) changed most in early mouse adulthood. Hysteresivity ( $\eta$ ) remained constant during aging (**G**), whereas hysteresis increased from 3 and 6 mo mice to 18 mo mice (**H**). Each point represents one animal; bars show means and lines indicate statistically significant differences between age groups (one-way ANOVA with Bonferroni *t*-test,  $p < 0.05$ ).

**TABLE 1** | Data of body weight, lung volume, and stereological parameters regarding parenchymal volumes and alveolar septum.

Parameter	3 mo	6 mo	12 mo	18 mo	24 mo
m(body) [g]	26.7 (1.1)	32.4* (1.5)	29.9* (1.6)	33.8*† (3.0)	32.7* (2.0)
V(lung) [cm <sup>3</sup> ]	0.97 (0.12)	1.01 (0.07)	1.02 (0.05)	1.35*†† (0.14)	1.31*†† (0.07)
V(lung)/m(body) [10 <sup>-2</sup> cm <sup>3</sup> /g]	3.65 (0.53)	3.13 (0.29)	3.42 (0.16)	4.04† (0.54)	4.01† (0.38)
V <sub>V</sub> (par/lung)	0.873 (0.025)	0.856 (0.023)	0.839 (0.034)	0.878 (0.027)	0.855 (0.025)
V <sub>V</sub> (non-par/lung)	0.120 (0.025)	0.139 (0.023)	0.156 (0.034)	0.116 (0.025)	0.140 (0.025)
V <sub>V</sub> (other/lung)	0.0074 (0.0037)	0.0062 (0.0016)	0.0067 (0.0036)	0.0063 (0.0029)	0.0063 (0.0030)
V <sub>V</sub> (airtot/par)	0.906 (0.013)	0.902 (0.012)	0.902 (0.011)	0.914 (0.008)	0.911 (0.012)
V <sub>V</sub> (airduct/par)	0.344 (0.029)	0.296* (0.039)	0.291* (0.016)	0.386†† (0.034)	0.368†† (0.018)
V <sub>V</sub> (sept/par)	0.094 (0.013)	0.098 (0.012)	0.098 (0.011)	0.086 (0.008)	0.089 (0.012)
V(par,lung) [mm <sup>3</sup> ]	847 (101)	865 (71)	858 (69)	1190*†† (130)	1119*†† (77)
V(non-par,lung) [mm <sup>3</sup> ]	117 (30)	140 (24)	158 (31)	157 (35)	182* (31)
V(airtot,par) [mm <sup>3</sup> ]	767 (88)	781 (71)	774 (67)	1087*†† (121)	1019*†† (73)
V(airduct,par) [mm <sup>3</sup> ]	292 (44)	257 (38)	249 (17)	460*†† (74)	413*†† (44)
V(airalv,par) [mm <sup>3</sup> ]	475 (55)	525 (59)	525 (55)	627*†† (66)	606* (34)
V(sept,par) [mm <sup>3</sup> ]	79.9 (16.7)	84.1 (6.5)	83.7 (8.1)	102.5* (13.7)	99.7* (13.7)
S <sub>V</sub> (sept/par) [mm <sup>-1</sup> ]	63.8 (5.5)	65.0 (5.7)	66.6 (5.6)	59.7 (3.4)	56.1†† (6.4)
S(sept,par) [10 <sup>3</sup> mm <sup>2</sup> ]	54.1 (8.7)	56.1 (5.6)	57.0 (5.4)	71.1*†† (10.1)	62.7 (7.8)
τ(sept) [μm]	2.94 (0.22)	3.01 (0.29)	2.95 (0.33)	2.89 (0.19)	3.19 (0.31)

Data are expressed as mean (SD). \**p* < 0.05 for 3 mo vs. 6, 12, 18, 24 mo; †*p* < 0.05 for 6 mo vs. 12, 18, 24 mo; ††*p* < 0.05 for 12 mo vs. 18, 24 mo.

from 3 to 6 mo mice, whereas most other morphological parameters exhibited greatest alterations with progressing age in old mice. Particularly, the ductal airspace volume increased in old mice. Additionally, late alveolarization was observed as well as alveoli with shorter septa and a reduced alveolar depth. The number of ATII cells increased along with alveolar number in old mice.

## Lung Function and Micromechanics in Aging Mice

Greatest changes of lung function and micromechanics were observed in the early adulthood, between 3 and 6 months of age. This has also been shown by others for BALB/c (Ranga et al., 1979) and C57BL/6 mice (Elliott et al., 2016). While Huang et al. suggested a linear decline (Huang et al., 2007), our data supported a non-linear change in lung function and micromechanics in aging C57BL/6 mice, similarly as also shown by Elliott et al. (2016). They observed greatest alterations in early adulthood between 2 and 6 months of age, including increases in IC and Cst by 36% and decreases of G and H by 38% and 34%, respectively, but little changes were observed later in life (Elliott et al., 2016). These findings are consistent with our data showing similar increases for IC (+25%), Cst (+30%), G (−21%), and H (−27%) between 3 and 6 mo mice. Additionally, an increase in hysteresis was found from young and middle-aged (6 mo) to old (18 mo) mice (Figure 1H). Similarly, increases in hysteresis were found in elastase-induced emphysematous mouse lungs (Brewer et al., 2003; Vanoirbeek et al., 2010; Robichaud et al., 2017). Hysteresis is mainly affected by surfactant and the properties of extracellular matrix (ECM) (Suki et al., 2011). Little is known regarding surfactant function in later life, but in a previous study a decrease in septal elastin fibers and an increase in septal collagen fibers were measured between young (3 months) and old (18 months)

mice (Kling et al., 2017), most likely contributing to the changes in pulmonary micromechanics with age.

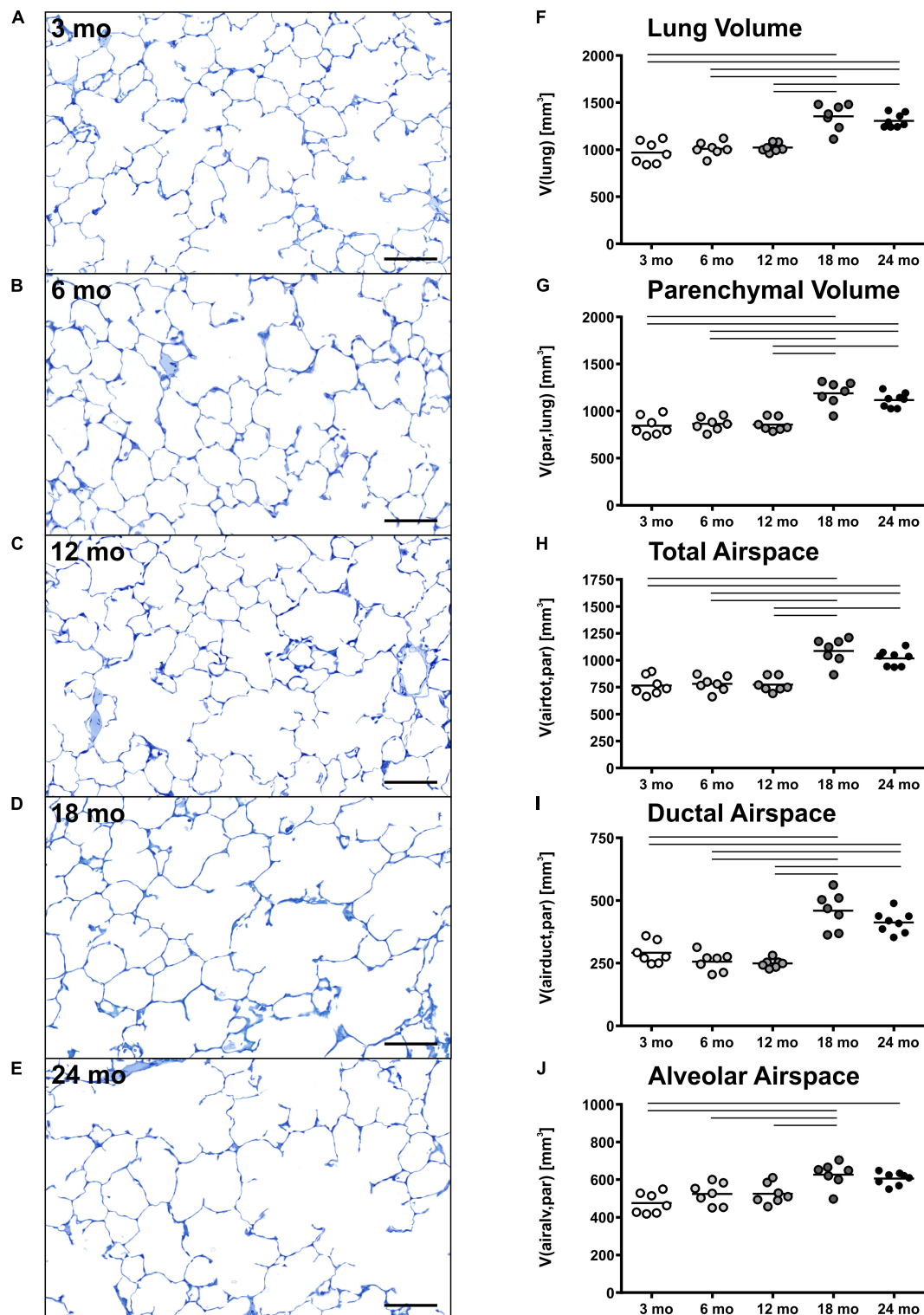
In humans, Sicard et al. (2018) estimated the elastic modulus in different anatomical regions of the lungs via atomic force microscopy and found age-related increases in the stiffness of lung parenchyma and vessels. Furthermore, in humans many lung function parameters such as FEV1, forced vital capacity (FVC) and vital capacity (VC) show a decline with age (Ware et al., 1990; Verbeken et al., 1992b; Janssens et al., 1999; Sharma and Goodwin, 2006), while static lung compliance increases in the elderly (Wahba, 1983; Levitzky, 1984). The inter-species translation of lung function and micromechanics measurements from mice to humans or vice versa is difficult because of the different analytical procedures (Miller et al., 2005; Lopez-Rodriguez et al., 2016). Nevertheless, it seems as lung micromechanics are similarly altered in humans and mice with age.

## Structural Changes in the Lung Parenchyma With Progressing Age

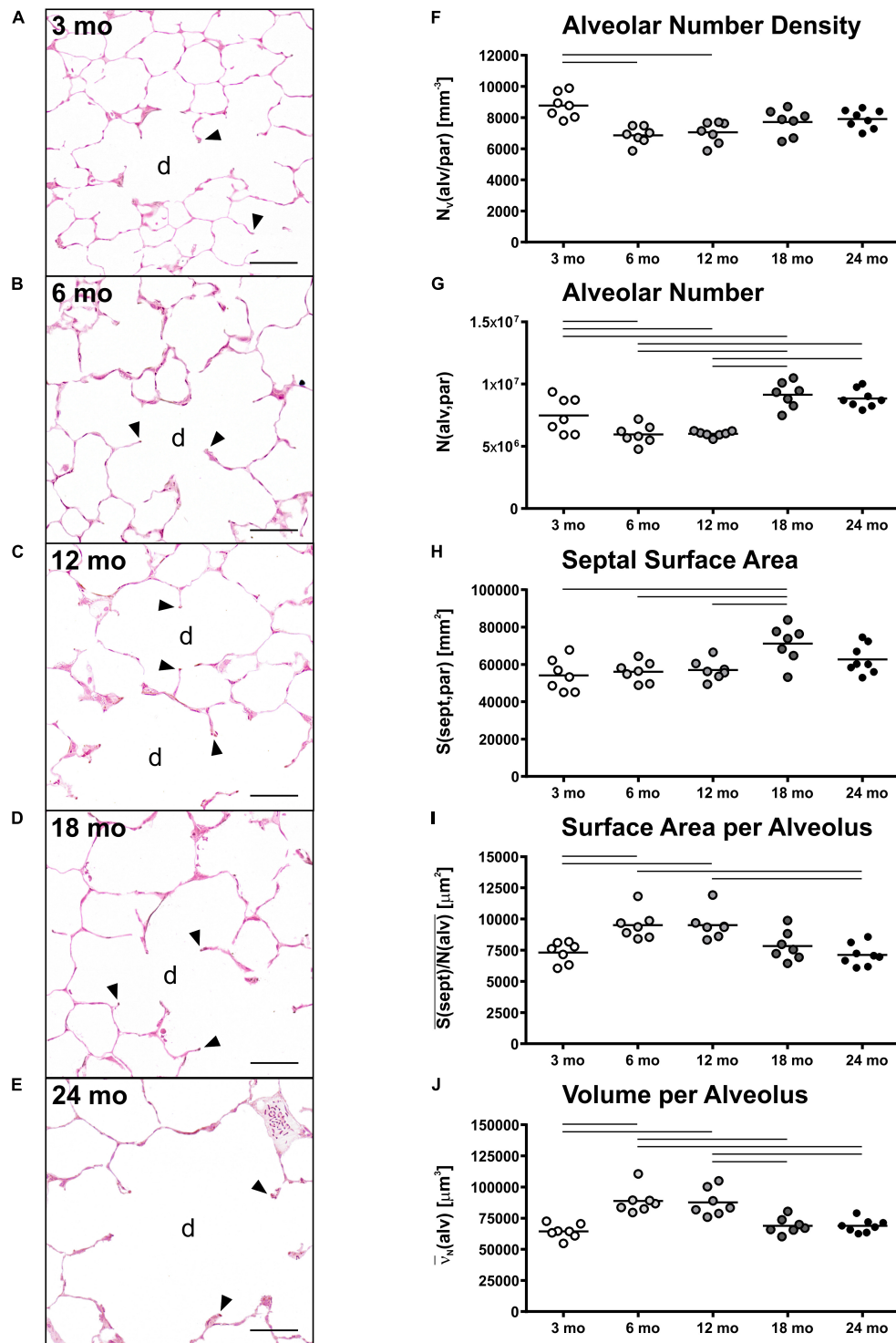
Lung volumes increased with age, particularly in older mice (Figure 2F). This is in line with other studies in mice (Elliott et al., 2016; Pozarska et al., 2017). In humans, lung growth was reported to be mainly restricted to initial lung development and not occurring later in life (de Jong et al., 2006; Copley et al., 2009; Zach et al., 2012; Herring et al., 2014), except after hemipneumectomy (Butler et al., 2012). This finding, however, suggests that lung growth can occur throughout lifetime.

Accompanied by an increase in lung volume in old mice, an enlargement of alveolar ducts was observed (Figure 2I). This has been described before in aging mammalian lungs. Beside qualitative observations (D'Errico et al., 1989; Kerr et al., 1990; Yamamoto et al., 2003; Glassberg et al., 2014), mean linear

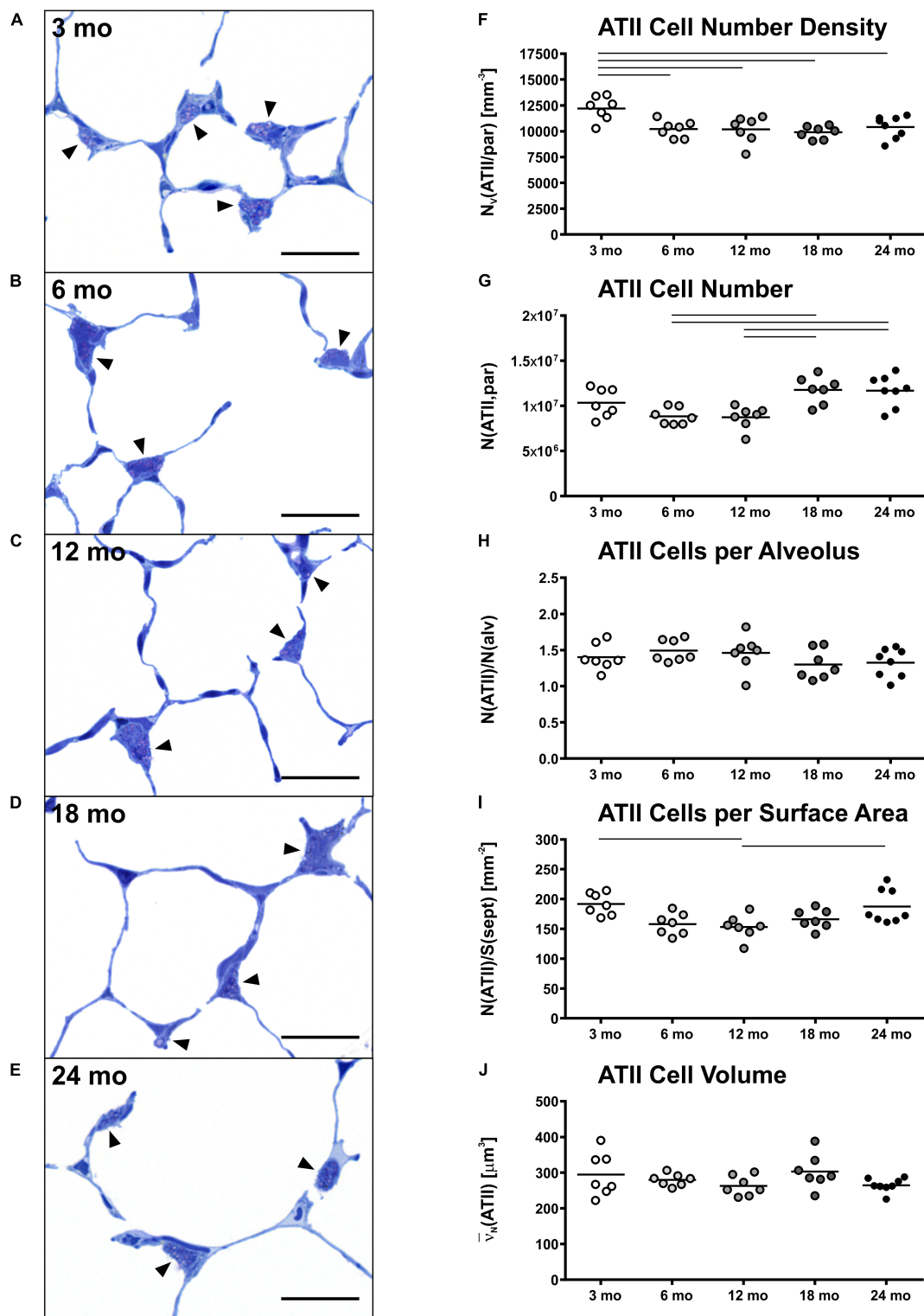




**FIGURE 2 |** Lung parenchymal airspace volumes. **(A–E)** Representative light micrographs of each age group stained with toluidine blue show pulmonary histology. No inflammation or fibrosis was observed qualitatively at any time point. The light micrographs of 3 **(A)**, 6 **(B)**, and 12 **(C)** mo mice show a compact, regular lung parenchyma, whereas the light micrographs of 18 **(D)** and 24 **(E)** mo mice reveal visible widening of alveolar ducts causing a less compact appearance of the parenchyma. Scale bar = 100  $\mu\text{m}$ . **(F–J)** Graphs show lung volume **(F)** and stereological results of parenchymal volume **(G)**, total parenchymal airspace volume **(H)**, ductal airspace volume **(I)**, and alveolar airspace volume **(J)**. Each point represents one animal; bars show means and lines indicate statistically significant differences between age groups (one-way ANOVA with Bonferroni *t*-test,  $p < 0.05$ ).



**FIGURE 3 |** Alveolar changes with age. **(A–E)** Representative light micrographs of each age group show pulmonary histology of eosin-orcein stained lungs. Arrowheads indicate alveolar septal border tips as part of the alveolar entrance ring. Septal border tips are dyed brown by orcein, demonstrating elastin accumulation around the alveolar entrances. Alveolar ducts are indicated by “d.” At 3 months **(A)**, a high density of small alveoli and narrow alveolar ducts can be observed. The light micrographs of 6 **(B)** and 12 **(C)** mo mice show similar narrow alveolar ducts, but alveoli appear less dense. In 18 **(D)** and 24 **(E)** mo mice, the alveolar density seems to remain constant compared to middle-aged mice. The alveolar ducts, however, appear wider and alveolar septal borders seem to be shorter. Scale bar = 50  $\mu\text{m}$ . **(F–J)** Graphs show stereological results of alveolar number density **(F)**, alveolar number **(G)**, total alveolar septal surface area **(H)**, mean septal surface area per alveolus **(I)**, and mean alveolar volume **(J)**. Each point represents one animal; bars show means and lines indicate statistically significant differences between age groups (one-way ANOVA with Bonferroni *t*-test,  $p < 0.05$ ).



**FIGURE 4 |** Alveolar epithelial type II (ATII) cell characteristics. **(A–E)** Representative light micrographs of each age group show pulmonary histology. Tissue sections were stained with toluidine blue. Arrowheads indicate ATII cells, typically located in alveolar “corners”. Intracellular lamellar bodies appear violet due to a metachromatic staining behavior. The ATII cells look quite homogeneous at any age in light microscopic images. However, the cell number density seems to be highest in 3 mo mice **(A)**. Scale bar = 20  $\mu\text{m}$ . **(F–J)** Graphs show stereological results of ATII cell number density **(F)** and ATII cell number **(G)** as well as mean ATII cell number per alveolus **(H)**, mean ATII cell number per alveolar septal surface area **(I)**, and mean ATII cell volume **(J)**. Each point represents one animal; bars show means and lines indicate statistically significant differences between age groups (one-way ANOVA with Bonferroni *t*-test,  $p < 0.05$ ).

intercept  $[L_m]$  is a frequently used parameter to estimate the mean chord length of the complete acinar airspace complex (Verbeke et al., 1992a; Huang et al., 2007; Elliott et al., 2016; Quirk et al., 2016).  $L_m$  is inversely related to  $S/V$  as  $4/L_m$  and expresses the mean free length between two intersections of alveolar septal surface with an unbiased test line system of straight lines (Knudsen et al., 2010). Although this parameter is easy to assess, it cannot reflect different compartments of air-filled spaces. Furthermore,  $L_m$  is susceptible to bias as it does not consider shape and critically depends on the execution of lung inflation, lung volume measurement, and (unbiased) sampling procedures in histological studies, as reviewed in Weibel et al. (2007). Therefore,  $L_m$  cannot be stated as a sufficient parameter for parenchymal airspace alterations (Weibel et al., 2007; Mühlfeld and Ochs, 2013). Only with estimation of alveolar number and by differentiating between alveolar and ductal airspace, the correct and unbiased conclusions can be drawn on changes in alveolar size and ductal airspace (Mühlfeld and Ochs, 2013). Nevertheless, comparing our results of septal surface density  $S_V(\text{sept}/\text{par})$  or, practically,  $S/V$  in older mice with studies in aging C57BL/6 mice estimating  $L_m$  (Huang et al., 2007; Elliott et al., 2016), their findings of increasing  $L_m$  with age is in line with our data of decreasing  $S_V(\text{sept}/\text{par})$ . Considering a concomitant increase in alveolar number density  $N_V(\text{alv}/\text{par})$  with age, this provides evidence of declining alveolar size, which is coherent with enlargement of the alveolar ducts.

## Age-Related Changes in Alveolarization

Alveolarization is mainly a postnatal process and occurs as early “bulk” and a late “continued” alveolarization (Schittny, 2017). Late alveolarization is discussed as the formation of new alveoli after the maturation of the alveolar septum which outlasts later periods of lung development (Burri, 2006; Schittny et al., 2008; Tschanz et al., 2014). Alveolarization has been shown to continue until young adulthood in humans (Narayanan et al., 2012; Herring et al., 2014), rats (Tschanz et al., 2014) and mice (Mund et al., 2008; Pozarska et al., 2017), however, little is known about late alveolarization in the elderly or in aged rodents.

The investigations showed that the number of alveoli increased from middle-aged to old mice, suggesting a late

alveolarization in the old animals. Similarly, a study comparing 3 and 20 mo mice via microCT showed an increased number of alveoli per acinus in old mice (Vasilescu et al., 2012), supporting the idea of late alveolarization as well. In this study, the mean septal surface area per alveolus increased by approximately 15% from 3 to 20 mo mice, which is coherent with our data displaying a slight, non-significant increase of 7% from 3 to 18 mo mice. However, the point in time with the most prominent late alveolarization in our study, occurring from middle-aged to old mice, was not covered in their study. Others also reported different findings. For example, Glassberg et al. (2014) found no age-related changes in alveolar number in 6 and 24 mo female C57BL/6 mice. Furthermore, a study from Pozarska et al. (2017), investigating postnatal lung alveolarization in juvenile and adult mice of both sexes with an age of 2, 9, or 22 months as adult groups, showed highest numbers of alveoli in 9 mo mice. Moreover, the study found alveoli to have greatest volumes in 22 mo mice, whereas our results showed a decrease in alveolar size in old mice. The opposing observations may occur due to strain and sex differences. Furthermore, the study presumably included the total parenchymal airspace volume  $V(\text{airtot}, \text{par})$  comprising alveolar and ductal airspace volumes to estimate the number-weighted mean alveolar volume  $\bar{v}_N(\text{alv})$  (Pozarska et al., 2017). In comparison, we only used the total alveolar airspace volume  $V(\text{airalv}, \text{par})$  without ductal airspace to estimate  $\bar{v}_N(\text{alv})$ . This has a direct impact on the estimation of the mean alveolar volume. By excluding ductal airspace from the estimation of alveolar volume, changes in ductal airspace will have no impact on alveolar volume calculations (Table 2). Here, in our study we therefore found a decrease in number-weighted mean alveolar volume in old mice, while the total number of alveoli was still increasing with age.

The findings of alveolar duct widening and smaller alveoli in old mice compared to middle-aged mice suggest a shortening of alveolar septal borders leading to a reduced alveolar depth, as described previously for aging human lungs (Quirk et al., 2016). The qualitative findings in pulmonary histology support this assumption (Figures 3D,E). As discussed by Quirk et al. (2016), the decreasing alveolar depth is concomitant with an increasing radius of alveolar ducts during aging in

**TABLE 2 |** Data of stereological parameters regarding alveoli and ATII cells.

Parameter	3 mo	6 mo	12 mo	18 mo	24 mo
$N_V(\text{alv}/\text{par}) [10^3 \text{ mm}^{-3}]$	8.77 (0.81)	6.87* (0.57)	7.04* (0.71)	7.72 (0.84)	7.91 (0.59)
$N(\text{alv}, \text{par}) [10^6]$	7.48 (1.44)	5.95* (0.78)	6.00* (0.23)	9.14* <sup>††</sup> (1.05)	8.84* <sup>††</sup> (0.72)
$N_V(\text{ATII}/\text{par}) [10^3 \text{ mm}^{-3}]$	12.21 (1.17)	10.21* (0.81)	10.18* (1.28)	9.88* (0.62)	10.41* (1.07)
$N(\text{ATII}, \text{par}) [10^6]$	10.34 (1.57)	8.82 (0.93)	8.73 (1.26)	11.76* <sup>††</sup> (1.50)	11.68* <sup>††</sup> (1.73)
$\bar{v}_N(\text{ATII}) [\mu\text{m}^3]$	295 (61)	280 (17)	263 (28)	303 (48)	265 (19)
$V(\text{airalv}, \text{par})/N(\text{alv}, \text{par}) = \bar{v}_N(\text{alv}) [10^3 \mu\text{m}^3]$	64.5 (5.9)	88.8* (10.2)	87.7* (11.1)	69.0* <sup>††</sup> (6.5)	68.9* <sup>††</sup> (5.3)
$V(\text{airtot}, \text{par})/N(\text{alv}, \text{par}) [10^3 \mu\text{m}^3]$	104.1 (10.2)	132.2* (12.1)	129.3* (14.7)	119.7 (13.8)	115.7 (8.9)
$S(\text{sept}, \text{par})/N(\text{alv}, \text{par}) = \bar{S}(\text{sept})/N(\text{alv}) [10^3 \mu\text{m}^2]$	7.32 (0.8)	9.51* (1.2)	9.52* (1.2)	7.83 (1.2)	7.12* <sup>††</sup> (0.9)
$N(\text{ATII}, \text{par})/S(\text{sept}, \text{par}) [\text{mm}^{-2}]$	192 (19)	158 (18)	153* (20)	166 (16)	187* <sup>†</sup> (28)
$N(\text{ATII}, \text{par})/N(\text{alv}, \text{par})$	1.40 (0.18)	1.49 (0.15)	1.46 (0.24)	1.30 (0.21)	1.33 (0.20)

Data are expressed as mean (SD). \* $p < 0.05$  for 3 mo vs. 6, 12, 18, 24 mo; <sup>†</sup> $p < 0.05$  for 6 mo vs. 12, 18, 24 mo; <sup>††</sup> $p < 0.05$  for 12 mo vs. 18, 24 mo.



human lungs at 19–71 years of age. It is assumed that these observations correspond with decreasing elastic recoil pressure and increasing shear modulus of the lung tissue (Verbeken et al., 1992a; Subramaniam et al., 2017; Knudsen and Ochs, 2018). Furthermore, alterations in septal elastin and collagen fiber distribution are considered to contribute to these observations in old mice (Toshima et al., 2004; Subramaniam et al., 2017).

It has to be mentioned that age-related changes in mechanical behavior of the lungs, as observed in Cst, could also affect structural parameters such as alveolar size. This holds particularly true, if lungs are instillation fixed under a constant pressure. In our study, Cst increased from 3 mo mice to older mice (Figure 1C), therefore, it is possible that changes in Cst affected alveolar size differences between 3 mo and older mice. However, in middle-aged and old mice Cst remained quite constant (Figure 1C). Hence in these groups, we consider the results in alveolar size measurements comparable, showing an age-related decline in alveolar size in old mice.

## Alterations of ATII Cell Numbers With Progressing Age

ATII cells play an important role for the functionality of the lung, as they serve as progenitor cells for alveolar epithelial type I (ATI) cells, stabilize intra-alveolar surface tension by producing surfactant and have an immunological function (reviewed in Fehrenbach, 2001). While transcriptomics and proteomics were done in ATII cells of young and old mice (Angelidis et al., 2019) and age-related changes were assessed in ATII cells as reviewed in Brandenberger and Mühlfeld (2017), there is no research on the absolute ATII cell number at multiple time points of adulthood yet. Stereological ATII cell quantification is very time consuming due to the necessity of the disector, but is superior to other quantification methods like flow cytometry (Jansing et al., 2017; Dzhuraev et al., 2019) or planimetry (Jansing et al., 2017). Nevertheless, there is a lot of research quantifying ATII cells stereologically in human (Crapo et al., 1982; Stone et al., 1992), rat (Crapo et al., 1980; Stone et al., 1992) and mouse (Stone et al., 1992; Dzhuraev et al., 2019) lungs for one age group.

Our results showed slightly higher total and alveolar surface-related ATII cell numbers for young compared to middle-aged mice (Figures 4F,I). This is in line with investigations in early postnatal rat lung development, showing a decline in ATII cells in the first days of life (Kauffman et al., 1974) and appears biologically consistent, as ATII cells serve as progenitor cells for alveolar epithelial type I (ATI) cells (Evans et al., 1975). From middle-aged to old mice, the ATII cell number density remained quite constant (Figure 4G), whereas, unexpectedly, the total number of ATII cells increased significantly (Figures 4G,I). We hypothesized that ATII cell number would further decrease with age or remain at least constant due to progenitor cell senescence with aging (Alder et al., 2015; Chen et al., 2015). However, our results indicate that ATII cell number concomitantly increased with lung volume in old mice. The constant ratio of ATII cells per alveolus during aging supports this finding (Figure 4H). It appears possible that a constant ATII cell number per alveolus contributes to a maintaining surfactant secretion, preserving lung

function in old mice (Hills, 1999; Fehrenbach, 2001). However, further research is needed to address this hypothesis.

## Developing and Aging of the Mouse Lung

C57BL/6 mice are commonly used for geriatric research (Miller and Nadon, 2000; Huang et al., 2007; Elliott et al., 2016; Kling et al., 2017; Angelidis et al., 2019). The median lifespan of male C57BL/6 mice is approximately 900 days or 29 months (Yuan et al., 2009). Flurkey et al. (2007) recommend using animals aged onto 85–90% of survivorship as oldest group for geriatric research, which would count for approximately 24 mo C57BL/6 mice. We summarized the 5 age groups of this study into 3 groups, because this classification reflected changes of almost all parameters and supported comprehension of the results: one young adult (3 mo), two middle-aged (6 and 12 mo), and two old (18 and 24 mo) mice groups. However, Flurkey et al. (2007) categorized 3–6 mo mice as mature adults and 10–14 mo mice as middle-aged. In recent aging studies with C57BL/6 (Kling et al., 2017; Brandenberger et al., 2018) and BALB/c (Gomez et al., 2007; Chen et al., 2014) mice, 3 and 18 mo groups are frequently used to represent young and old, respectively. Lung development occurs until young adulthood (Schittny, 2017). We found great changes in lung function, micromechanics, and structure between 3 and 6 months of age, suggesting lung development to continue beyond pubertal maturation. Supportively, Miller and Nadon (2000) discussed using mice of 4–6 months of age for young groups to avoid influences of post-pubertal maturation processes. Nevertheless, we considered it important to include also young adult mice of 3 months into our study to have the full range of adult life covered.

## CONCLUSION

In summary, this study provides comprehensive insights on structural alterations in the aging C57BL/6JRj mouse lung, linking it with changes in lung function and micromechanics. Age-related structural alterations mainly appeared between middle-aged and old mice and were characterized by lung growth accompanied by a widening of alveolar ducts. Moreover, late alveolarization occurred, concomitant with decreasing alveolar size, most likely due to reduced alveolar depth. Quite constant relations of ATII cells to alveolar number and alveolar surface area were observed. However, lung function and micromechanics altered most between young and middle-aged mice.

## DATA AVAILABILITY STATEMENT

All datasets generated for this study are included in the article/Supplementary Material.

## ETHICS STATEMENT

The animal study was reviewed and approved by the Niedersächsisches Landesamt für Verbraucherschutz

und Lebensmittelsicherheit (LAVES), Postfach 39 49, 26029 Oldenburg.

## AUTHOR CONTRIBUTIONS

HS, CB, and CM designed the research, interpreted the results of experiments, edited and revised the manuscript, and approved final version of the manuscript. HS and CB performed the experiments, analyzed the data, and prepared the figures. HS drafted the manuscript.

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## SUPPLEMENTARY MATERIAL

The Supplementary Material for this article can be found online at: <https://www.frontiersin.org/articles/10.3389/fphys.2019.01466/full#supplementary-material>

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# Quantifying Regional Lung Deformation Using Four-Dimensional Computed Tomography: A Comparison of Conventional and Oscillatory Ventilation

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Mechanical ventilation strategies that reduce the heterogeneity of regional lung stress and strain may reduce the risk of ventilator-induced lung injury (VILI). In this study, we used registration of four-dimensional computed tomographic (4DCT) images to assess regional lung aeration and deformation in 10 pigs under baseline conditions and following acute lung injury induced with oleic acid. CT images were obtained via dynamic axial imaging (Siemens SOMATOM Force) during conventional pressure-controlled mechanical ventilation (CMV), as well as high-frequency and multi-frequency oscillatory ventilation modalities (HFOV and MFOV, respectively). Our results demonstrate that oscillatory modalities reduce intratidal strain throughout the lung in comparison to conventional ventilation, as well as the spatial gradients of dynamic strain along the dorsal-ventral axis. Harmonic distortion of parenchymal deformation was observed during HFOV with a single discrete sinusoid delivered at the airway opening, suggesting inherent mechanical nonlinearity of the lung tissues. MFOV may therefore provide improved lung-protective ventilation by reducing strain magnitudes and spatial gradients of strain compared to either CMV or HFOV.

**Keywords:** mechanical ventilation, ventilator-induced lung injury, respiratory mechanics, high-frequency oscillatory ventilation, multi-frequency oscillatory ventilation, computed tomography, image registration

## INTRODUCTION

Ventilator-induced lung injury (VILI) may inadvertently occur in critically ill patients receiving mechanical ventilation, due to the harmful stresses and strains associated with gas flows driven under positive pressure (Slutsky and Ranieri, 2013). Patients with injured, inflamed, and/or edematous lungs, such as those with the acute respiratory distress syndrome (ARDS), are especially at risk for VILI due to increased ventilation heterogeneity (Carrasco Loza et al., 2015). Maintaining normal levels of arterial oxygen and carbon dioxide tensions in patients

with ARDS may be extremely difficult using conventional mechanical ventilation (CMV), since increasing the tidal volume or driving pressure to compensate for gas exchange deficiencies may be detrimental to the mechanically overburdened lung (Acute Respiratory Distress Syndrome Network, 2000; Amato et al., 2015; Gattinoni et al., 2016a). The goal of lung-protective ventilation is to provide life-sustaining gas exchange without exacerbating existing injury within vulnerable parenchymal tissues.

In some instances, high-frequency oscillatory ventilation (HFOV) has been proposed as a rescue treatment for refractory hypoxemia in ARDS, given its theoretically ideal qualities for lung-protection: small tidal volumes that mitigate the risk of dynamic strain injury (i.e., volutrauma), and high mean airway pressures that prevent cyclic recruitment/derecruitment (i.e., atelectrauma) (Sklar et al., 2017). Despite an extensive history of scientific and clinical research over several decades, optimal strategies for HFOV initiation and management remain a subject of controversy (Malhotra and Drazen, 2013; Kneyber and Markhorst, 2016; Nguyen et al., 2016). As it is currently delivered, HFOV may not be an appropriate ventilatory modality in many patients with ARDS for several reasons. First, the use of high mean airway pressures may result in hemodynamic compromise due to impaired venous return and low cardiac output (Meade et al., 2017). In addition, high strain rates within the lung tissues during HFOV may also contribute to VILI, by increasing the mechanical power dissipated across the parenchyma (Gattinoni et al., 2016b; Protti et al., 2016; Herrmann et al., 2019b). Finally, high frequency oscillatory flows are distributed in a heterogeneous and frequency-dependent manner, predisposing overventilated regions to excess mechanical strain, and underventilated regions to derecruitment and atelectasis (Amini and Kaczka, 2013; Herrmann et al., 2016).

Multi-frequency oscillatory ventilation (MFOV) has thus also been proposed as an alternative modality for lung-protective ventilation, by delivering multiple frequencies of oscillatory flow and pressure simultaneously (Kaczka et al., 2015; Herrmann et al., 2019b). MFOV has been shown to improve gas exchange and mechanical function compared to traditional “single-frequency” HFOV (Kaczka et al., 2015; Herrmann et al., 2018). Its postulated mechanism of benefit relies on the frequency-dependence of ventilation distribution and gas transport during conventional and oscillatory modes of ventilation (Herrmann et al., 2018), which can be exploited by using flow waveforms with enhanced harmonic content. Given such frequency-dependence of gas flow throughout the airway tree, mechanically disparate regions of an injured lung may thus selectively filter out “less desirable” frequency components of a broadband oscillatory waveform delivered at the airway opening. The corresponding homogenization of intrapulmonary gas transport with MFOV may then contribute to enhanced gas exchange, and simultaneously distribute the mechanical burden of ventilation more uniformly throughout the lung. Nonetheless, specific experimental evidence to support such a mechanism is lacking, and it remains to be seen whether MFOV improves the regional distribution of parenchymal strain throughout the lung compared to CMV or traditional HFOV.

The purpose of this study was to characterize the distribution of regional intratidal lung deformation during conventional and oscillatory modes of ventilation in pigs under baseline conditions and following acute lung injury with oleic acid. We hypothesized that such variations would be less heterogeneous during MFOV, compared to CMV or traditional single-frequency HFOV. Specifically, we quantified intratidal variations in dynamic regional lung aeration, volumetric strain, and volumetric strain rate during CMV, HFOV, and MFOV using frequency-selective four-dimensional computed tomographic (4DCT) image reconstruction (Herrmann et al., 2017) and registration (Zhao et al., 2016).

## MATERIALS AND METHODS

### Animal Preparation

All experimental procedures were approved by the University of Iowa Institute for Animal Care and Use Committee (Protocol Number 5061428). Ten healthy pigs were used in this study, weighing between 9 and 13 kg. Following intramuscular injection of 2.2 mg kg<sup>-1</sup> telazol, 1.1 mg kg<sup>-1</sup> ketamine, and 1.1 mg kg<sup>-1</sup> xylazine, general anesthesia was induced during spontaneous breathing with inhaled isoflurane delivered via nosecone. Each pig was then intubated with a cuffed endotracheal tube (4.5–5.5 mm inner diameter), and mechanically ventilated (Uni-Vent Eagle Model 754, ZOLL Medical Corporation, Chelmsford, MA). Capnography, peripheral oxygen saturation (S<sub>p</sub>O<sub>2</sub>), and electrocardiogram waveforms were obtained using a Philips patient monitor equipped with the M3001A measurement module (Philips Healthcare, Andover, MA). Surgical incision into the neck was performed to allow cannulation of the internal jugular vein and carotid artery, as well as relocation of the endotracheal tube into an incision in the trachea just below the larynx. Endotracheal tubes were manually shortened (to final length 12–15 cm depending on tube diameter) prior to tracheostomy, to reduce apparatus deadspace. Anesthesia was maintained using an intravenous infusion of propofol (7–9 mg kg<sup>-1</sup> hr<sup>-1</sup>), and muscular relaxation was achieved using intermittent intravenous boluses of either rocuronium (1–2 mg kg<sup>-1</sup>) or pancuronium (0.01–0.15 mg kg<sup>-1</sup>).

Lung injury was induced by slow infusion of 0.08 cm<sup>3</sup> kg<sup>-1</sup> oleic acid into the internal jugular vein over 15 min. Maturation of injury required ~90 min, and was confirmed by a ratio of arterial oxygen tension to inspired oxygen fraction (P<sub>a</sub>O<sub>2</sub> : F<sub>i</sub>O<sub>2</sub>) < 300 mmHg during ventilation with 5 cmH<sub>2</sub>O of positive end-expiratory pressure (PEEP). Additional oleic acid (0.04 cm<sup>3</sup> kg<sup>-1</sup>) was administered if P<sub>a</sub>O<sub>2</sub> : F<sub>i</sub>O<sub>2</sub> remained > 300 mmHg 90 min after the initial dose. If necessary, normal systemic arterial blood pressure (systolic/diastolic ≥ 90/60 mmHg) was maintained with intravenous crystalloid solutions and intermittent doses of phenylephrine (1–2 μg kg<sup>-1</sup>).

### Experimental Protocol

All measurements and ventilation modalities were performed under baseline conditions and following lung injury. Each subject was mechanically ventilated with CMV, HFOV, and MFOV in random order over 30-min intervals, using a FabianHFO

hybrid oscillator/ventilator (Acutronic Medical Systems AG, Switzerland). Mean airway pressure ( $\bar{P}_{aw}$ ) was set to 12 cmH<sub>2</sub>O for all modalities. During baseline conditions,  $F_iO_2$  was set to 40%, but was increased to maintain  $S_pO_2 \geq 90\%$  following lung injury. Pressure-controlled CMV was delivered at rates between 20 and 32 min<sup>-1</sup> (0.33 to 0.53 Hz), with inspiratory:expiratory ratio of 1:2. Single-frequency HFOV was delivered at 5 Hz, while MFOV was delivered using a combination of 5, 10, 15, and 20 Hz superimposed sinusoids with uniform flow amplitudes (Kaczka et al., 2015). Example ventilator waveforms are provided in **Supplementary Figures S-1, S-2, S-3**. Sampling frequency for recorded ventilator waveforms was 200 Hz. Ventilator driving pressure or pressure amplitudes were adjusted to obtain arterial CO<sub>2</sub> tension ( $P_aCO_2$ ) in the target range of 30–60 mmHg. Each 30-min experimental interval was followed by an arterial blood gas analysis and 4DCT scan sequence, without interrupting mechanical ventilation (Herrmann et al., 2017). Between each experimental ventilation interval, a 15-min wash-out period of CMV and a 30-s recruitment maneuver to 35 cmH<sub>2</sub>O of airway pressure were used to restore a control mechanical and physiological state. After completion of the experimental protocol, subjects were euthanized with an intravenous solution of pentobarbital sodium and phenytoin sodium (1 mL + 0.2 mL kg<sup>-1</sup>).

## Assessment of Gas Exchange and Mechanics

Oxygenation was assessed using the oxygenation index (OI), defined as (Ortiz et al., 1987):

$$OI = \frac{\bar{P}_{aw} \cdot F_iO_2}{P_aO_2} \quad (1)$$

The efficiency of CO<sub>2</sub> elimination during each modality was assessed using a ventilatory cost function ( $V_C$ ), defined as (Kaczka et al., 2015):

$$V_C = \frac{V_{rms}^2 \cdot P_aCO_2}{Wt} \quad (2)$$

where  $V_{rms}$  is the root mean-square of the volume waveform  $V(t)$  delivered to the airway opening:

$$V_{rms} = \sqrt{\frac{1}{T} \int_0^T [V(t) - \bar{V}]^2 dt} \quad (3)$$

$T$  denotes the time duration over which the integration in Equation (3) is performed (i.e., one breath for CMV or one second during HFOV/MFOV), and  $\bar{V}$  is the mean of the volume waveform over the interval 0 to  $T$ .<sup>1</sup> Peak-to-peak range of volume ( $V_{pp}$ ) was computed as the difference between the largest and smallest values of time-varying volume:

$$V_{pp} = \max_t V(t) - \min_t V(t) \quad (4)$$

<sup>1</sup>The use of  $V_{rms}$  enables comparison between single-frequency modalities, which are typically described by a single tidal volume, and MFOV, which is described by a distinct volume amplitude at each frequency (Kaczka et al., 2015).

Dynamic respiratory system elastance ( $E_{rs}$ ) during pressure-controlled CMV was computed as the quotient of driving pressure ( $\Delta P_{aw}$ ) and tidal volume:

$$E_{rs} = \Delta P_{aw} \cdot V_{pp}^{-1} \quad (5)$$

where:

$$\Delta P_{aw} = \max_t P_{aw}(t) - \min_t P_{aw}(t) \quad (6)$$

Measurements of respiratory impedance ( $Z_{rs}$ ) were obtained under baseline conditions and after maturation of lung injury. A pseudorandom waveform consisting of nine sinusoids ranging in frequency from 0.078 to 8.9 Hz was generated by a digital-to-analog converter (NI USB-6356, National Instruments, Austin, TX), low-pass filtered at 12 Hz (858L8B-2, Frequency Devices, Haverhill, MA), and used as the input driving signal to a custom servo-controlled pneumatic pressure oscillator (Kaczka and Lutchen, 2004). Airway pressure was measured with a transducer placed at the proximal end of the endotracheal tube (Celesco LCVR-0050, Canoga Park, CA), while flow was measured using a screen pneumotach (4700A, Hans Rudolph, Shawnee, KS) coupled to a differential pressure transducer (Celesco LCVR-0002, Canoga Park, CA). The airway pressure and flow signals were sampled at 40 Hz over ~90 s during the application of forced oscillations, allowing for three repetitions of the 25.6-s periodic control signal. Each  $Z_{rs}$  spectrum and its corresponding coherence function ( $\gamma^2$ ) was computed using the Welch periodogram technique (Welch, 1967), with rectangular windowing and 80% overlap. The complex values of  $Z_{rs}$  were evaluated only at the nine frequencies used in the control signal (Suki and Lutchen, 1992). Corresponding resistance  $R_{rs}$  and reactance  $X_{rs}$  spectra were defined by the real and imaginary parts of  $Z_{rs}$ , respectively. The resonant frequency  $f_{res}$  was estimated from the zero-crossing of  $X_{rs}$  using spline interpolation. Each  $Z_{rs}$  spectrum was then characterized by a 4-element constant-phase model consisting of parameters for Newtonian airway and chest wall resistance ( $R$ ), airway inertance ( $I_{aw}$ ), tissue hysteresivity ( $\eta$ ), and tissue elastance ( $H$ ):

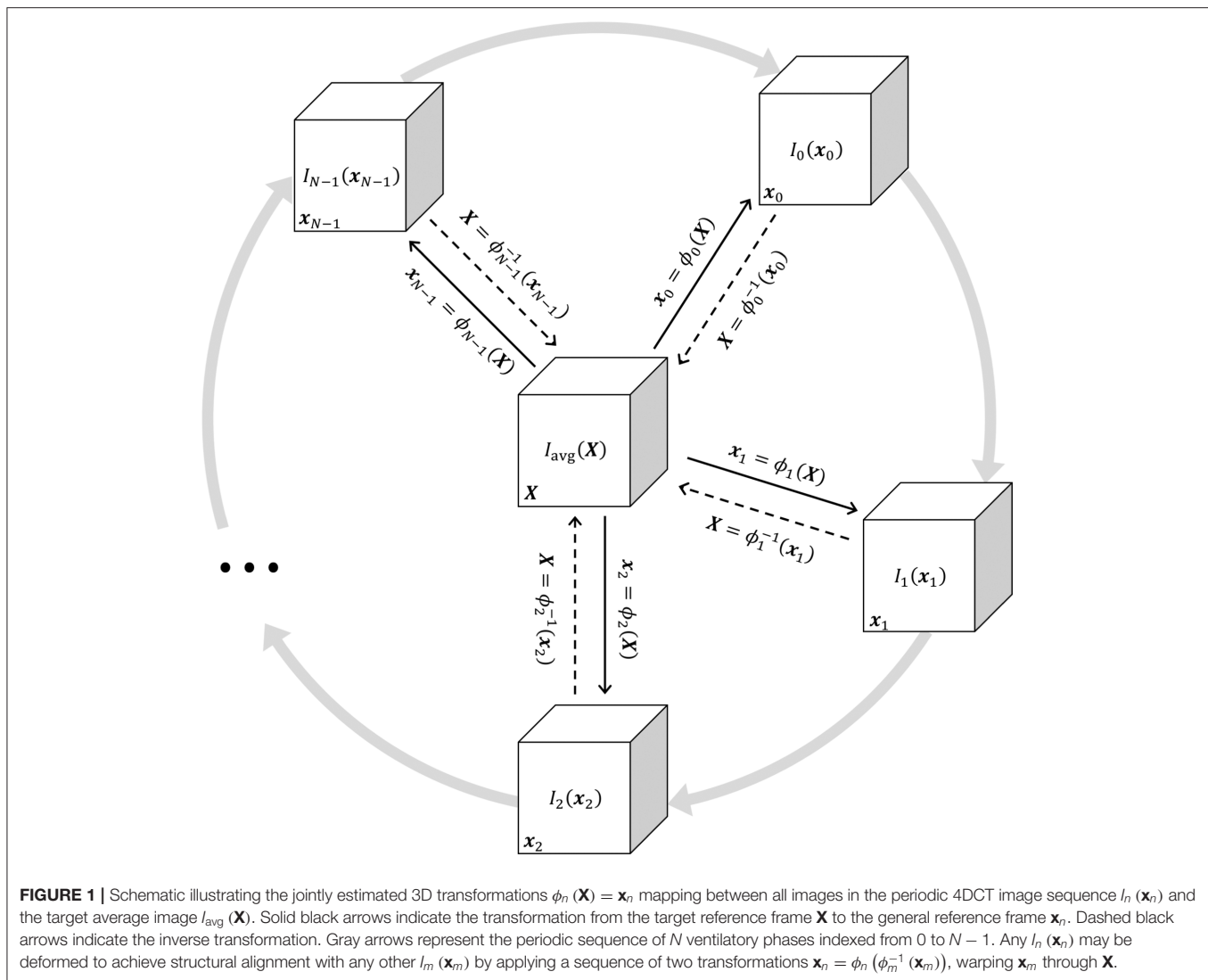
$$\hat{Z}_{rs}(f) = R + j2\pi f I_{aw} + \frac{(\eta - j)H}{(2\pi f)^\alpha} \quad (7)$$

where  $\hat{Z}_{rs}$  denotes the model-predicted  $Z_{rs}$  and  $\alpha = \left(\frac{2}{\pi}\right) \tan^{-1}\left(\frac{1}{\eta}\right)$ . Model parameters were estimated by constrained nonlinear gradient descent technique (MATLAB, Natick, MA).

## Image Acquisition and Processing

CT scans were acquired using a Siemens SOMATOM Force (Siemens Healthineers, Germany) in an axial scanning mode, with 5.76 cm of axial coverage and 0.6 mm slice thickness. Subjects were continuously scanned at 80 kVp tube voltage and 150 mA tube current, with 250 ms scanner rotation period. Each scan lasted a total duration of 30 s, resulting in a radiation exposure of 345 mGy and generating a continuous set of projection images. The 4DCT image sequences were





reconstructed by retrospective binning of x-ray projection data according to mechanical ventilation phase using a frequency-selective reconstruction algorithm (Herrmann et al., 2017), yielding between 13 and 21 volumetric images per 4DCT sequence with isotropic 0.6 mm spatial resolution. The corresponding temporal sampling frequencies for 21-phase image sequences were 7 Hz during CMV with fundamental 0.33 Hz, and 105 Hz during HFOV or MFOV with fundamental 5 Hz. Each sequence was periodic in the temporal (i.e., ventilation phase) dimension, such that the choice of “initial” image in the sequence was arbitrary. Each volumetric image in the temporal sequence was labeled  $I_n(\mathbf{x}_n)$ , where  $n$  indexes the number of images in the sequence 0 through  $N - 1$ , and  $\mathbf{x}_n$  is a vector representing 3-dimensional spatial position. Voxels corresponding to spatial positions within the lungs were identified by a fully automated segmentation algorithm using a deep convolutional neural network (Gerard et al., 2018, 2020), generating a distinct lung mask  $M_n(\mathbf{x}_n)$  for each image phase. The neural network was trained using manually segmented lungs in CT images obtained from multiple datasets of experimental

lung injury models, including a subset of images from the current study.

The periodic motion of respiratory structures was estimated using a deformable 4D image registration technique. This procedure produced  $N$  3-dimensional transformation functions denoted as  $\phi_n(\mathbf{X}) = \mathbf{x}_n$ , where  $\mathbf{X}$  is a vector representing 3-dimensional spatial position within the reference frame of a phase-averaged image  $I_{\text{avg}}(\mathbf{X})$ , and  $\mathbf{x}_n$  represents spatial position in image  $I_n(\mathbf{x}_n)$ . Image  $I_{\text{avg}}(\mathbf{X})$  was used as the target for groupwise image registration of the images  $I_n(\mathbf{x}_n)$ ,  $n = 0 \dots N - 1$ . Thus,  $\phi_n(\mathbf{X}) = \mathbf{x}_n$  is a spatial mapping from the coordinate system of  $I_{\text{avg}}(\mathbf{X})$  to that of  $I_n(\mathbf{x}_n)$ , such that a deformed image  $I_{n \rightarrow \text{avg}}(\mathbf{X})$  was generated with respiratory structures aligned to the target image as:

$$I_{n \rightarrow \text{avg}}(\mathbf{X}) = I_n(\phi_n(\mathbf{X})) \quad (8)$$

**Figure 1** shows a schematic of the transformations mapping between all images in the periodic sequence and  $I_{\text{avg}}(\mathbf{X})$ .



The transformations  $\phi_n(\mathbf{X})$  were coupled together using 4-dimensional cubic B-splines and jointly estimated to ensure smoothness across both spatial and temporal dimensions (Metz et al., 2011). The parameters of the transformation function were iteratively adjusted using the Elastix library (Klein et al., 2010) to minimize the sum of squared tissue volume differences (SSTVD) between each  $I_{n \rightarrow \text{avg}}(\mathbf{X})$  and  $I_{\text{avg}}(\mathbf{X})$ , such that each deformed image preserved the volume of tissue contained within each voxel (Gorbunova et al., 2008; Yin et al., 2009; Zhao et al., 2016). Thus, changes in CT voxel density due to variations in fractional gas content were adjusted using this similarity cost function. Following registration,  $\phi_n(\mathbf{X})$  and its inverse mapping  $\phi_n^{-1}(\mathbf{x}_n)$  were used to align images between arbitrary phases. Deformed images were denoted as  $I_{n \rightarrow m}(\mathbf{x}_m)$ , indicating the  $n$ th image deformed into the  $m$ th spatial reference frame:

$$I_{n \rightarrow m}(\mathbf{x}_m) = I_n(\phi_n(\phi_m^{-1}(\mathbf{x}_m))) \quad (9)$$

For the trivial case of  $m = n$ , Equation (9) simplifies to  $I_{n \rightarrow n}(\mathbf{x}_n) = I_n(\mathbf{x}_n)$ . Conceptually, aligning images from any two phases can be achieved by warping one spatial reference frame to another, passing through the target reference frame  $\mathbf{X}$  (see **Figure 1**). Using this approach, all images were warped to align structures with a single, arbitrarily selected reference phase at  $m = 0$ . Phasic variations in regional aeration and strain could then be associated with the tissue contained within the region of interest at the reference phase. **Figure 2** schematizes the use of a single reference phase to align respiratory structures across several ventilatory phases, thus tracking tissue-correlated changes in aeration and regional volume. Changes in regional aeration were then assessed by the range of voxel intensity values in the deformed image:

$$\Delta I(\mathbf{x}_0) = \max_n I_{n \rightarrow 0}(\mathbf{x}_0) - \min_n I_{n \rightarrow 0}(\mathbf{x}_0) \quad (10)$$

while changes in regional volumetric strain were estimated using the Jacobian matrix ( $\mathcal{J}_{n \rightarrow m}$ ) of transformation spatial derivatives:

$$\mathcal{J}_{n \rightarrow m}(\mathbf{x}_m) = \nabla_{\mathbf{x}_m}(\phi_n(\phi_m^{-1}(\mathbf{x}_m))) \quad (11)$$

where  $\nabla_{\mathbf{x}_m}$  is the spatial gradient operator. Note that  $\mathcal{J}_{n \rightarrow m}$  is expressed in the  $m$ th spatial reference frame and describes the gradient of the “pullback” transformation  $\phi_n(\phi_m^{-1}(\mathbf{x}_m))$ . This pullback transformation is interpreted as “pulling back” point  $\mathbf{x}_n$  in ventilation phase  $n$  to the corresponding point  $\mathbf{x}_m$  in phase  $m$ . Regional volume changes relative to the reference phase (i.e.,  $m = 0$ ) were computed by the determinant of  $\mathcal{J}_{n \rightarrow 0}$ :

$$\frac{V_n(\mathbf{x}_0)}{V_0(\mathbf{x}_0)} = |\mathcal{J}_{n \rightarrow 0}(\mathbf{x}_0)| \quad (12)$$

where  $V_n(\mathbf{x}_0)$  corresponds to the phase-varying volume of a region which, in the reference phase 0, occupies a single voxel centered at position  $\mathbf{x}_0$ . Accordingly,  $V_0(\mathbf{x}_0)$  is everywhere equal to the volume of a single voxel  $\delta V$ , determined by the image spatial resolution. Thus, Equation (12) may be simplified to:

$$V_n(\mathbf{x}_0) = \delta V \cdot |\mathcal{J}_{n \rightarrow 0}(\mathbf{x}_0)| \quad (13)$$

Note that  $|\mathcal{J}_{n \rightarrow 0}| < 1$  when the corresponding region deflates relative to the reference phase,  $|\mathcal{J}_{n \rightarrow 0}| > 1$  when it expands, and  $|\mathcal{J}_{n \rightarrow 0}| = 1$  when there is no volume change (i.e., isovolumetric deformation). **Figure 3** shows an example image sequence for each ventilation modality in one injured subject, demonstrating phase-varying aeration  $I_{n \rightarrow 0}(\mathbf{x}_0)$  and volume change  $V_n(\mathbf{x}_0)$  for each voxel in a sample region of interest in  $\mathbf{x}_0$ . Animated image sequences for one subject under baseline and injured conditions are also provided (**Supplementary Animations S-1, S-2**). Phase-varying strain ( $\varepsilon$ ) for each lung region with respect to its respective minimum inflation state was defined as:

$$\varepsilon_n(\mathbf{x}_0) = \frac{V_n(\mathbf{x}_0) - \min_n V_n(\mathbf{x}_0)}{\min_n V_n(\mathbf{x}_0)} \quad (14)$$

Changes in regional volumetric strain were assessed by the range of  $\varepsilon_n(\mathbf{x}_0)$ :

$$\Delta \varepsilon(\mathbf{x}_0) = \max_n \varepsilon_n(\mathbf{x}_0) - \min_n \varepsilon_n(\mathbf{x}_0) \quad (15)$$

Since the minimum value of  $\varepsilon_n(\mathbf{x}_0)$  is zero by definition, Equation (15) may be reduced to:

$$\Delta \varepsilon(\mathbf{x}_0) = \max_n \varepsilon_n(\mathbf{x}_0) \quad (16)$$

Similarly, regional volumetric strain rate ( $\dot{\varepsilon}$ ) was computed by the temporal rate of change in  $\varepsilon_n(\mathbf{x})$  using the forward difference scheme:

$$\dot{\varepsilon}_n(\mathbf{x}_0) = \frac{\varepsilon_{(n+1) \bmod N}(\mathbf{x}_0) - \varepsilon_n(\mathbf{x}_0)}{\delta t} \quad (17)$$

where  $\delta t$  is the time difference between adjacent phases. The modulo operator is used to indicate the periodicity of ventilatory phase. The value of  $\delta t$  is computed from the ventilatory fundamental frequency ( $f_0$ ) and the number of images in the 4DCT sequence ( $N$ ):

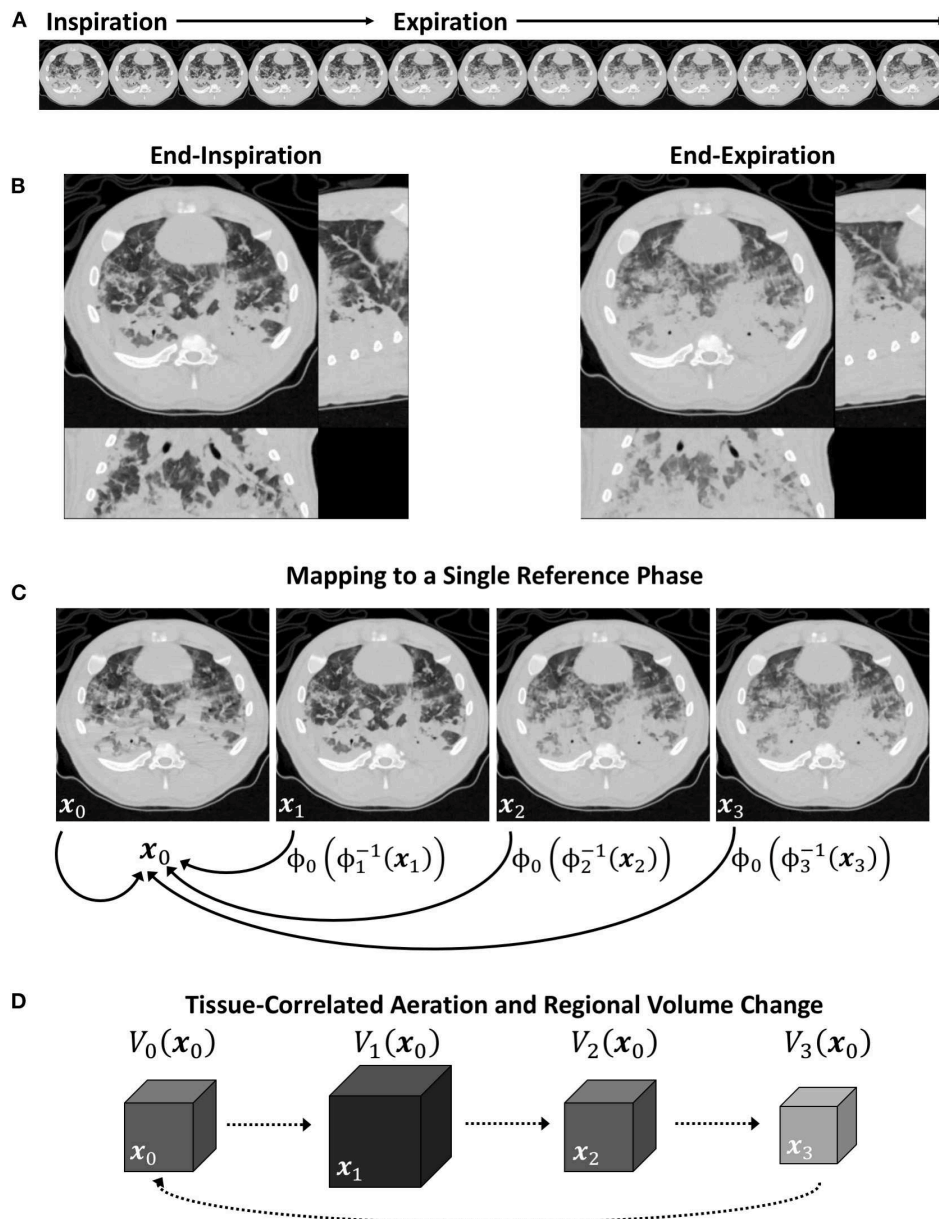
$$\delta t = \frac{1}{f_0 N} \quad (18)$$

Finally, changes in regional volumetric strain rate were assessed by the range of  $\dot{\varepsilon}_n(\mathbf{x}_0)$ :

$$\Delta \dot{\varepsilon}(\mathbf{x}_0) = \max_n \dot{\varepsilon}_n(\mathbf{x}_0) - \min_n \dot{\varepsilon}_n(\mathbf{x}_0) \quad (19)$$

Note that  $\dot{\varepsilon}_n(\mathbf{x}_0)$  generally will be positive during inflation of a specified lung region, and negative during the corresponding deflation. Thus,  $\Delta \dot{\varepsilon}(\mathbf{x}_0)$  will reflect the sum of the fastest inflation and deflation rates of the region.

Voxels within 6.0 mm of the image boundaries along the rostral-caudal axis were excluded from the mask for the purposes of image analysis, due to potential registration artifacts caused by motion of lung tissue into or out of the axial field of view. Regional aeration ( $\Delta I$ ), strain ( $\Delta \varepsilon$ ), and strain rate ( $\Delta \dot{\varepsilon}$ ) were compared across subjects, lung conditions, and ventilation modalities by their mean value throughout the lung mask,

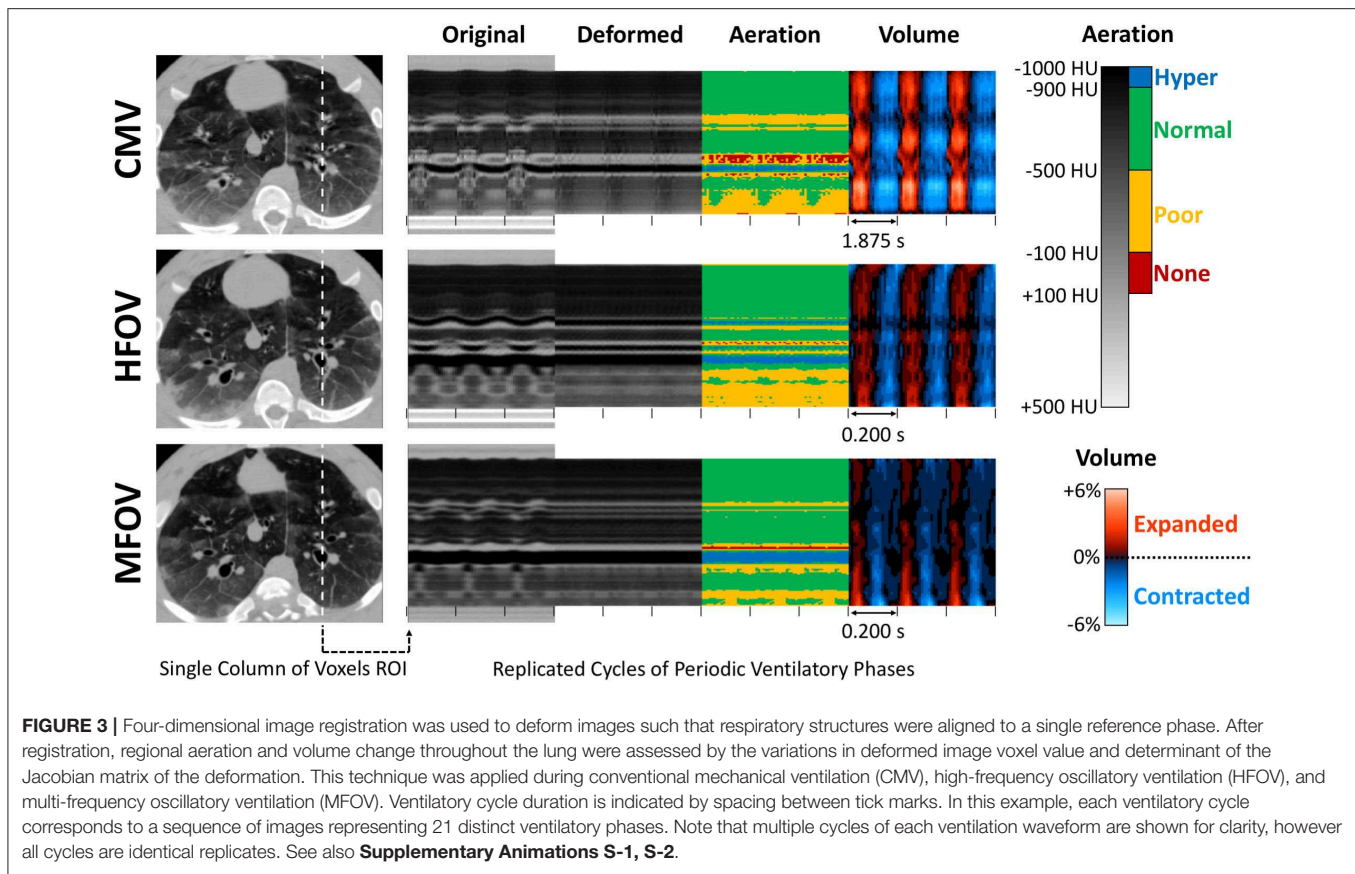


**FIGURE 2 |** Schematic of a periodic 4DCT image sequence during conventional mechanical ventilation **(A)**, with inspiratory and expiratory phases **(B)**. Image registration is used to map each image in the sequence to a single reference phase **(C)**, after which intratidal variations in aeration and regional volume may be associated to specific regions of lung tissue **(D)**.

coefficient of variation, and spatial gradients in the right-left, dorsal-ventral, and rostral-caudal directions. Spatial gradients for each variable were determined from the slopes computed by linear regression with respect to position along each of the principal anatomic axes. Spatial gradients were examined unnormalized and normalized by the spatial mean, in each case comparing both signed values of the gradient (i.e., positive and negative) and gradient magnitude (i.e., absolute value).

Given the harmonic nature of MFOV, the individual frequency components of  $I_n$ ,  $\varepsilon_n$ , and  $\dot{\varepsilon}_n$  were assessed using

the Discrete Fourier Transform (DFT), to relate these periodic time-varying properties at each spatial position into harmonic amplitude and phase components. The regional heterogeneity of volumetric strain ( $\Delta\varepsilon$ ) was assessed using octree and supervoxel decomposition, each of which recursively subdivide regions-of-interest (ROIs) within the lung mask. Both decomposition methods were initialized with a single ROI containing the entire lung mask. At each recursive step, the designated ROI was subdivided into multiple new ROIs if the standard deviation of the contained voxel intensity was greater than a fixed



threshold, set to a standard deviation of mean-normalized  $\Delta\epsilon \geq 0.3$ .<sup>2</sup> Octree decomposition, a three-dimensional extension of quadtree decomposition, was used to partition each ROI into eight octants according to bisecting coronal, sagittal, and transverse planes (Perchiazzi et al., 2014). Supervoxel decomposition was used to partition each ROI into two new ROIs by a weighted  $k$ -means clustering of voxels according to intensity similarity and spatial proximity (Conze et al., 2017). Recursive subdivision was continued until all ROIs either contained below-threshold values of standard deviation, or were  $<0.2\%$  of the lung mask. Regional heterogeneity of  $\Delta\epsilon$  was then quantified by the mean ROI volume ( $\bar{V}_{ROI}$ ) as a fraction of the lung mask.

## Statistics

Non-parametric Kruskal-Wallis rank sum tests were performed for each outcome, testing for main effects of lung condition (i.e., baseline, injured) and ventilation modality (i.e., CMV, HFOV, MFOV) at the 0.05 significance level. The effect of ventilation modality was tested separately under baseline and injured conditions. For outcomes with a significant main effect of ventilation modality, differences among

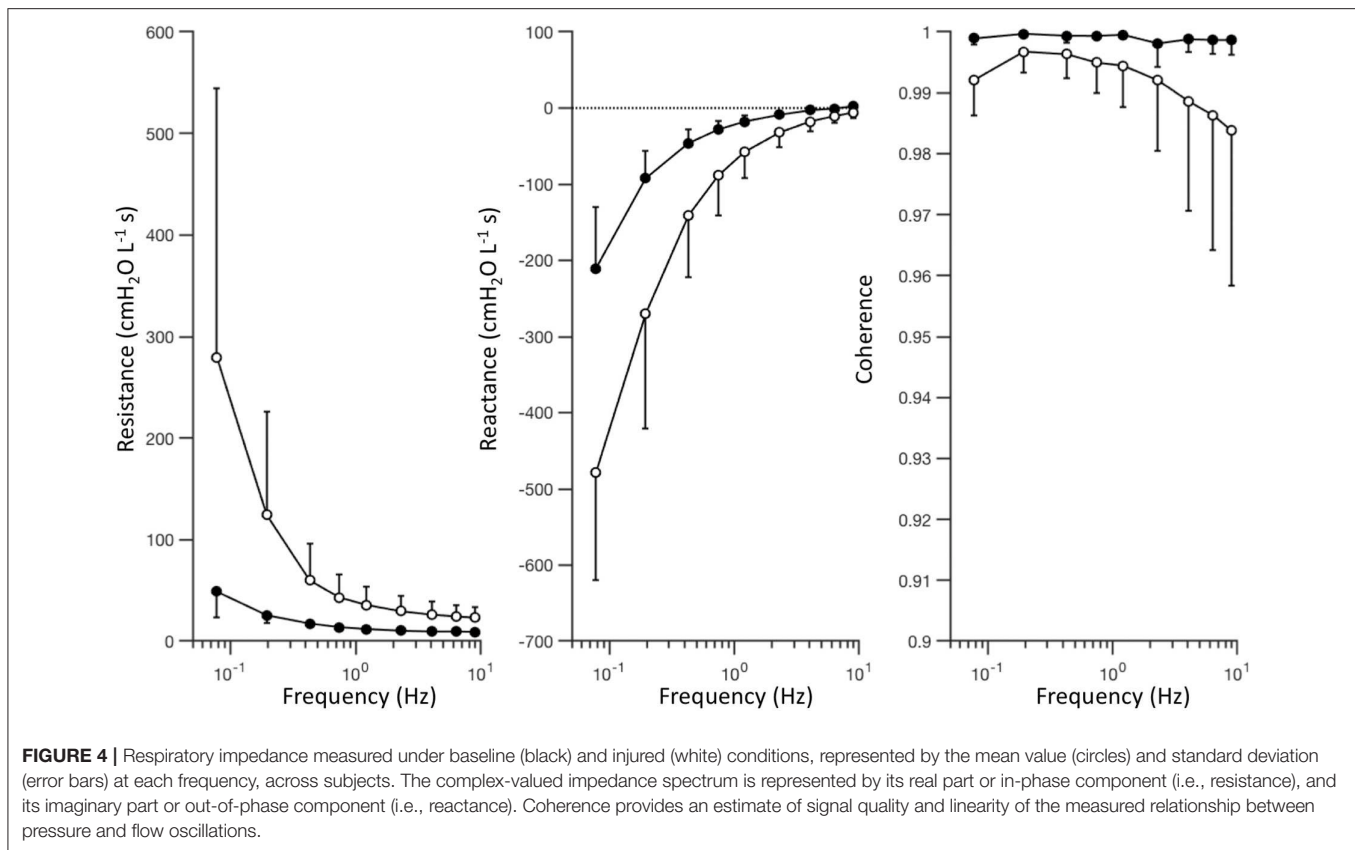
modalities were identified by a Dunn *post hoc* comparison with adjustment for rank ties and further adjustment by the Benjamini-Hochberg procedure for reduced false discovery rate. A web-based tool was used for statistical calculations (Vasavada, 2016).

## RESULTS

**Figure 4** shows a summary of the respiratory impedance spectra  $Z_{rs}$  across all subjects measured under baseline and injured conditions, while **Table 1** provides a summary of the constant phase model applied to  $Z_{rs}$ . Under baseline conditions, average model-based tissue elastance  $H$  was  $121 \text{ cmH}_2\text{O L}^{-1}$  at  $1 \text{ rad s}^{-1}$  ( $0.16 \text{ Hz}$ ) with a coefficient of variation of 0.31. The increase in  $H$  after oleic acid injury was highly variable, resulting in a mean of  $435 \text{ cmH}_2\text{O L}^{-1}$  at  $1 \text{ rad s}^{-1}$  with a coefficient of variation of 0.94. By comparison, measurement of dynamic elastance ( $E_{rs}$ ) during CMV (Equation 5) was  $148.9 \pm 26.9 \text{ cmH}_2\text{O L}^{-1}$  and  $257.5 \pm 64.2 \text{ cmH}_2\text{O L}^{-1}$  under baseline and injured conditions, respectively. Resonant frequency ( $f_{res}$ ) increased after lung injury, in some cases above the measurement range allowed by the sampling parameters. **Table 2** contains a summary of all significant effects identified by non-parametric Kruskal-Wallis tests, as well as *post hoc* comparisons as appropriate. These results are described further in the context of specific figures below.

<sup>2</sup>This threshold value was empirically chosen to be lower than the values of the regional strain coefficient of variation observed across all subjects, to ensure that the recursive subdivision would not be terminated trivially at the level of the entire lung mask, yet high enough to avoid termination at the level of individual voxels. The same threshold was used for all normalized images.





**TABLE 1 |** Respiratory system mechanics.

Condition	$\bar{P}_{aw}^{\S}$	$R$	$I_{aw}$	$\eta$	$H$	$f_{res}^{\ddagger}$	$E_{rs}^{\ddagger}$
Baseline	11.5 ± 0.8	8.9 ± 3.2	0.11 ± 0.03	0.17 ± 9.93	121 ± 38	6.7 ± 1.7	149 ± 27
Injured	12.6 ± 2.9	22.4 ± 13.5	0.13 ± 0.08	0.27 ± 0.04	435 ± 407	9.2 ± 1.3	258 ± 64

$\bar{P}_{aw}^{\S}$  during respiratory impedance measurements.  $f_{res}^{\ddagger}$  interpolation was possible only for nine subjects under baseline conditions and five subjects under injured conditions, due to resonance in other cases occurring above the 12 Hz low-pass filter cutoff frequency.  $E_{rs}^{\ddagger}$  measurements obtained during conventional mechanical ventilation by Equation (5).  $\bar{P}_{aw}$ , mean airway pressure (cmH<sub>2</sub>O);  $R$ , Newtonian airway and chest wall resistance (cmH<sub>2</sub>O L<sup>-1</sup> s);  $I_{aw}$ , airway inertance (cmH<sub>2</sub>O L<sup>-1</sup> s<sup>2</sup>);  $\eta$ , tissue hysteresivity;  $H$ , tissue elastance (cmH<sub>2</sub>O L<sup>-1</sup> at 1 rad s<sup>-1</sup>);  $f_{res}$ , resonant frequency (Hz);  $E_{rs}$ , dynamic respiratory system elastance (cmH<sub>2</sub>O L<sup>-1</sup>).

Figure 5 shows gas exchange outcomes related to mechanical ventilation, including oxygenation index ( $OI = P_aO_2^{-1} \cdot F_iO_2 \cdot \bar{P}_{aw}$ ) and ventilatory cost function ( $V_C = P_aCO_2 \cdot V_{rms}^2 \cdot Wt^{-1}$ ). A significant main effect of lung condition (baseline vs. injured) was found for  $P_aO_2$ ,  $P_aO_2 \cdot F_iO_2^{-1}$ ,  $OI$ , and  $P_aCO_2$  ( $p < 0.001$ ). A significant main effect of ventilation modality was found in  $\Delta P_{aw}$ ,  $V_{pp} \cdot Wt^{-1}$ ,  $V_{rms} \cdot Wt^{-1}$ , and  $V_C$  ( $p < 0.001$ ) for both lung conditions, as well as in  $OI$  for the injured condition ( $p < 0.05$ ). In particular, median  $OI$  increased by 300% for injured subjects compared to baseline ( $p < 0.001$ ), but was 48% lower for injured subjects during MFOV compared to CMV ( $p < 0.05$ ). MFOV and HFOV were associated with lower median  $V_C$  for both baseline and injured conditions compared to CMV (HFOV 84% lower than CMV,  $p < 0.01$ ; MFOV 93% lower than CMV,  $p < 0.001$ ). Pairwise comparison of  $V_C$  for MFOV against HFOV also achieved a statistically significant difference, with 60% lower

median  $V_C$  for MFOV compared to HFOV ( $p < 0.05$ ). Median  $V_{rms} \cdot Wt^{-1}$  was 41% lower for MFOV vs. HFOV ( $p = 0.0505$  baseline;  $p < 0.05$  injured) and 75% lower for MFOV vs. CMV ( $p < 0.001$ ).

Figure 6 shows registration-based estimates of regional ventilation, as intratidal changes in voxel aeration ( $\Delta I$ ), volumetric strain ( $\Delta \epsilon$ ), and volumetric strain rate ( $\Delta \dot{\epsilon}$ ). A significant main effect of condition (baseline vs. injured) was found for  $\Delta I$  spatial mean ( $p < 0.001$ ),  $\Delta \epsilon$  coefficient of variation ( $p < 0.001$ ) and  $\Delta \dot{\epsilon}$  coefficient of variation ( $p < 0.01$ ). A significant main effect of ventilation modality was found for the spatial means of all three variables— $\Delta I$ ,  $\Delta \epsilon$ , and  $\Delta \dot{\epsilon}$ —in both baseline and injured lung conditions ( $p < 0.001$ ). In particular, MFOV and HFOV both produced smaller  $\Delta I$ , smaller  $\Delta \epsilon$ , and larger  $\Delta \dot{\epsilon}$  compared to CMV under baseline and injured conditions ( $p < 0.05$ ). For the injured condition, MFOV resulted

**TABLE 2 |** Statistically significant effects determined by Kruskal-Wallis rank sum test for main effects of lung condition (i.e., baseline, injured) and ventilation modality (i.e., CMV, HFOV, MFOV).

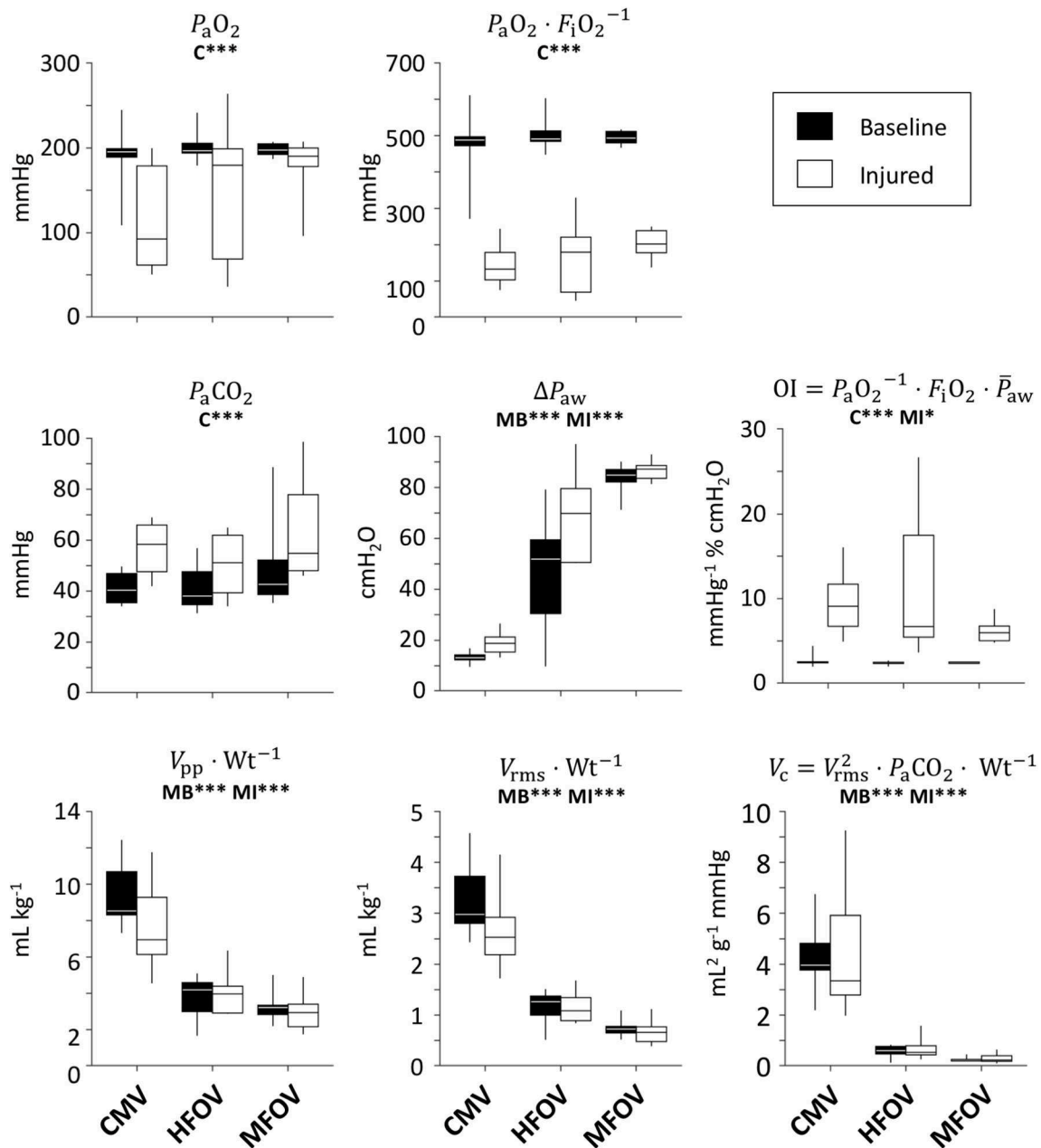
	Condition main effect	Baseline				Injured			
		Ventilation main effect	CMV vs. HFOV	CMV vs. MFOV	HFOV vs. MFOV	Ventilation main effect	CMV vs. HFOV	CMV vs. MFOV	HFOV vs. MFOV
$P_aO_2$	♦♦♦								
$P_aO_2 \cdot F_iO_2^{-1}$	♦♦♦								
$OI$	♦♦♦					♦		♦	
$P_aCO_2$	♦♦♦								
$\Delta P_{aw}$		♦♦♦	♦	♦♦♦	♦♦	♦♦♦	♦♦	♦♦♦	
$V_{pp} \cdot Wt^{-1}$		♦♦♦	♦♦	♦♦♦		♦♦♦	♦♦	♦♦♦	
$V_{rms} \cdot Wt^{-1}$		♦♦♦	♦♦	♦♦♦		♦♦♦	♦	♦♦♦	♦
$V_C$		♦♦♦	♦♦	♦♦♦	♦	♦♦♦	♦♦	♦♦♦	♦
$\Delta I$ Mean	♦♦♦	♦♦♦	♦♦	♦♦		♦♦♦	♦♦♦	♦♦♦	♦♦♦
$\Delta I$ Coef. Var.									
$\Delta I$ Right-Left		♦	♦						
$\Delta I$ Dorsal-Ventral		♦♦♦ ○○○	♦♦ ○	♦♦♦ ○○○					
$\Delta I$ Caudal-Rostral		♦♦♦ ○○○	♦♦♦ ○○○	♦♦♦ ○○○		♦♦ ○○○	♦♦ ○○	♦♦ ○○○	
$ \Delta I $ Right-Left	♦♦♦ ○○○					♦		♦	
$ \Delta I $ Dorsal-Ventral		♦♦ ○○	♦♦ ○○	♦♦ ○		♦ ○		♦ ○	
$ \Delta I $ Caudal-Rostral						♦	♦	♦	
$\Delta \epsilon$ Mean		♦♦♦	♦♦	♦♦♦		♦♦♦	♦	♦♦♦	♦
$\Delta \epsilon$ Coef. Var.	♦♦♦								
$\Delta \epsilon$ Right-Left	♦♦ ○○								
$\Delta \epsilon$ Dorsal-Ventral	♦♦♦ ○○○	♦♦♦ ○		♦♦♦ ○	♦ ○				
$\Delta \epsilon$ Caudal-Rostral	♦♦♦ ○○○	♦♦ ○	♦♦	♦♦					
$ \Delta \epsilon $ Right-Left	♦ ○		♦			♦		♦	
$ \Delta \epsilon $ Dorsal-Ventral		♦♦		♦♦		♦		♦	
$ \Delta \epsilon $ Caudal-Rostral		♦	♦	♦					
$\Delta \dot{\epsilon}$ Mean		♦♦♦	♦♦♦	♦♦♦		♦♦♦	♦♦♦	♦♦	
$\Delta \dot{\epsilon}$ Coef. Var.	♦♦								
$\Delta \dot{\epsilon}$ Right-Left	♦ ○○								
$\Delta \dot{\epsilon}$ Dorsal-Ventral	♦ ○	♦♦ ○○		♦♦ ○○	♦	♦	♦	♦	
$\Delta \dot{\epsilon}$ Caudal-Rostral		♦♦ ○○○	♦ ○○	♦ ○○		♦ ○○		♦ ○○	
$ \Delta \dot{\epsilon} $ Right-Left		♦♦	♦♦	♦♦					
$ \Delta \dot{\epsilon} $ Dorsal-Ventral	♦	♦		♦	♦	♦	♦	♦	
$ \Delta \dot{\epsilon} $ Caudal-Rostral						♦		♦	
$\bar{V}_{ROI}$ Supervoxel									
$\bar{V}_{ROI}$ Octree	♦♦♦								

Post-hoc comparisons for ventilation modality performed using the Dunn method with Benjamini-Hochberg adjustment. (♦ $p < 0.05$ , ♦♦ $p < 0.01$ , ♦♦♦ $p < 0.001$ ). Symbols distinguish unnormalized (♦) and mean-normalized (○) spatial gradients.  $P_aO_2$ , arterial oxygen tension;  $F_iO_2$ , fractional inspired oxygen;  $OI$ , oxygenation index;  $\Delta P_{aw}$ , pressure amplitude;  $V_{pp}$ , peak-peak volume;  $Wt$ , body weight;  $V_{rms}$ , root-mean-square volume;  $V_C$ , ventilatory cost function;  $P_aCO_2$ , arterial carbon dioxide tension;  $\Delta I$ , range of CT value;  $\Delta \epsilon$ , range of volumetric strain;  $\Delta \dot{\epsilon}$ , range of volumetric strain rate;  $\bar{V}_{ROI}$ , mean cluster volume;  $|\dots|$ , absolute value of enclosed argument.

in significantly lower  $\Delta I$  and  $\Delta \epsilon$  compared to HFOV ( $p < 0.05$ ), but no difference for  $\Delta \dot{\epsilon}$  ( $p = 0.20$ ).

**Figure 7** shows unnormalized spatial gradients of  $\Delta I$ ,  $\Delta \epsilon$ , and  $\Delta \dot{\epsilon}$  in the right-left, dorsal-ventral, and caudal-rostral axes. The largest spatial gradient magnitudes observed occurred along the dorsal-ventral axis. In particular, the injured lung condition was associated with significantly more positive dorsal-ventral gradients of  $\Delta \epsilon$  ( $p < 0.001$ ) and  $\Delta \dot{\epsilon}$  ( $p < 0.05$ ). Ventilation modality had a significant effect on all dorsal-ventral gradients under baseline conditions ( $\Delta I$ ,  $p < 0.001$ ;  $\Delta \epsilon$ ,  $p < 0.001$ ;

$\Delta \dot{\epsilon}$ ,  $p < 0.01$ ), with MFOV producing the least negative dorsal-ventral gradients of  $\Delta I$  and  $\Delta \epsilon$ , but the most positive dorsal-ventral gradients of  $\Delta \dot{\epsilon}$ . Although modality was not a significant predictor of variability in the actual value (positive or negative) of any dorsal-ventral gradient for injured subjects, it was a significant main effect for the *magnitudes* of all dorsal-ventral gradients ( $\Delta I$ ,  $p < 0.001$ ;  $\Delta \epsilon$ ,  $p < 0.01$ ;  $\Delta \dot{\epsilon}$ ,  $p < 0.05$ ). In general HFOV and MFOV reduced the dorsal-ventral gradient magnitudes of  $\Delta I$  and  $\Delta \epsilon$  under both baseline and injured conditions, while increasing the corresponding



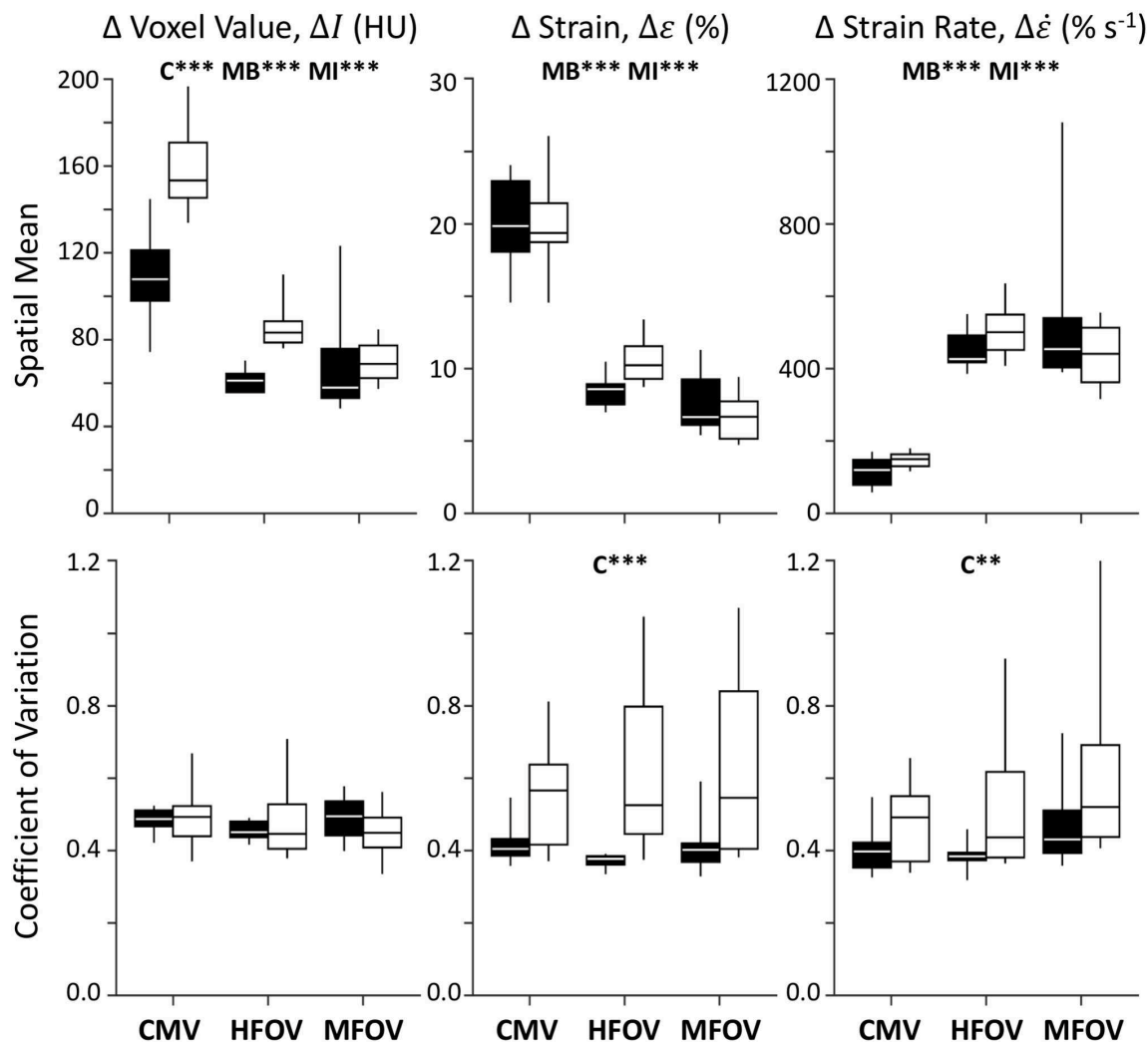
**FIGURE 5 |** Gas exchange outcomes, represented by box plots showing minimum, maximum, and quartiles across subjects under baseline (black) and injured (white) conditions, during conventional mechanical ventilation (CMV), high-frequency oscillatory ventilation (HFOV), and multi-frequency oscillatory ventilation (MFOV). Asterisks indicate significance levels (\* $p < 0.05$ , \*\*\* $p < 0.001$ ) for main effects (C = lung condition, MB = modality for baseline condition, MI = modality for injured condition). See **Table 2** for additional clarification.  $P_{aO_2}$  = arterial oxygen tension;  $F_{iO_2}$  = fractional inspired oxygen;  $P_{aCO_2}$  = arterial carbon dioxide tension;  $\Delta P_{aw}$  = airway pressure amplitude;  $V_{pp}$  = peak-to-peak volume range;  $Wt$  = body weight;  $V_{rms}$  = root-mean-square volume.

$\Delta \epsilon$  gradient. **Figure 8** shows corresponding mean-normalized spatial gradients. In general, normalizing each spatial gradients by the respective spatial mean accounted for much of the variability observed in the unnormalized spatial gradients (**Figure 7**) with respect to varying ventilation modality. This is also evidenced by the loss of significant differences between

ventilation modalities for the corresponding spatial gradients as indicated in **Table 2**.

**Figure 9** shows an example of regions-of-interest defined by recursive supervoxel and octree decomposition performed on mean-normalized  $\Delta \epsilon$  in one subject. Clustered regions are illustrated using contours and filled regions in two-dimensional



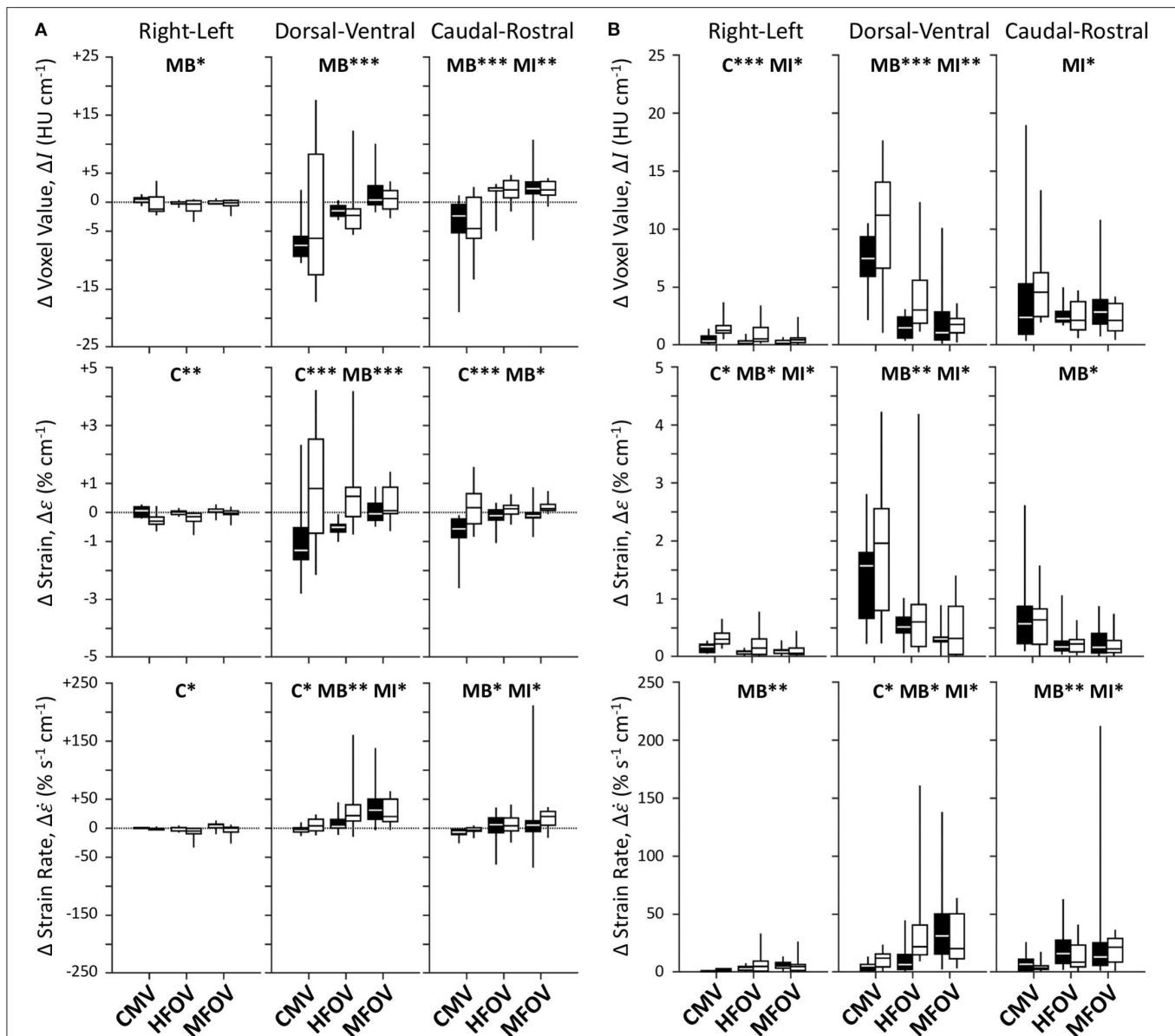


**FIGURE 6** | Summary of image registration-based regional ventilation measures for intratidal changes in aeration ( $\Delta I$ ), volumetric strain ( $\Delta \epsilon$ ), and volumetric strain rate ( $\Delta \dot{\epsilon}$ ). Mean and coefficient of variation throughout the lung mask are shown for each variable, represented by box plots showing minimum, maximum, and quartiles across subjects under baseline (black) and injured (white) conditions, during conventional mechanical ventilation (CMV), high-frequency oscillatory ventilation (HFOV), and multi-frequency oscillatory ventilation (MFOV). Asterisks indicate significance levels (\*\* $p < 0.01$ , \*\*\* $p < 0.001$ ) for main effects (C = lung condition, MB = modality for baseline condition, MI = modality for injured condition). See **Table 2** for additional clarification.

views of a slice, as well as translucent surface renderings in three-dimensional projections. Note that supervoxel decomposition produces larger contiguous ROIs, despite using the same decision criteria for recursive cluster subdivision. **Figure 9** also provides a summary of mean cluster size ( $\bar{V}_{ROI}$ ) across subjects, condition, and ventilation modality. A significant effect of lung condition was found for the octree technique ( $p < 0.001$ ), with 32% smaller median  $\bar{V}_{ROI}$  in injured lungs.

**Figure 10** shows example distributions of strain amplitude and phase at the first four harmonics for CMV, HFOV, or MFOV, computed using the discrete Fourier transform of time-varying Jacobian determinants in aligned images. **Figure 11** provides a summary of the harmonic strain amplitudes during HFOV

and MFOV across all subjects, correlated with corresponding amplitudes of the ventilator volume waveform  $V(t)$ . The oscillatory waveforms were a 5 Hz sinusoid (HFOV) and a combination of 5, 10, 15, and 20 Hz sinusoids with uniform flow amplitudes (MFOV). The relative amplitude distributions in the flow waveforms delivered by the ventilator were largely preserved throughout the lung, according to the registration-based metrics ( $r^2 = 0.78$ ). However, harmonic distortion measurements during HFOV indicated nearly 20% of the spectral power in regional strain was concentrated in the higher-order harmonics of the 5 Hz waveform (i.e., 10, 15, 20 Hz), whereas the ventilator volume waveform exhibited only 5% harmonic distortion (Zhang et al., 1995; Amini et al., 2017).

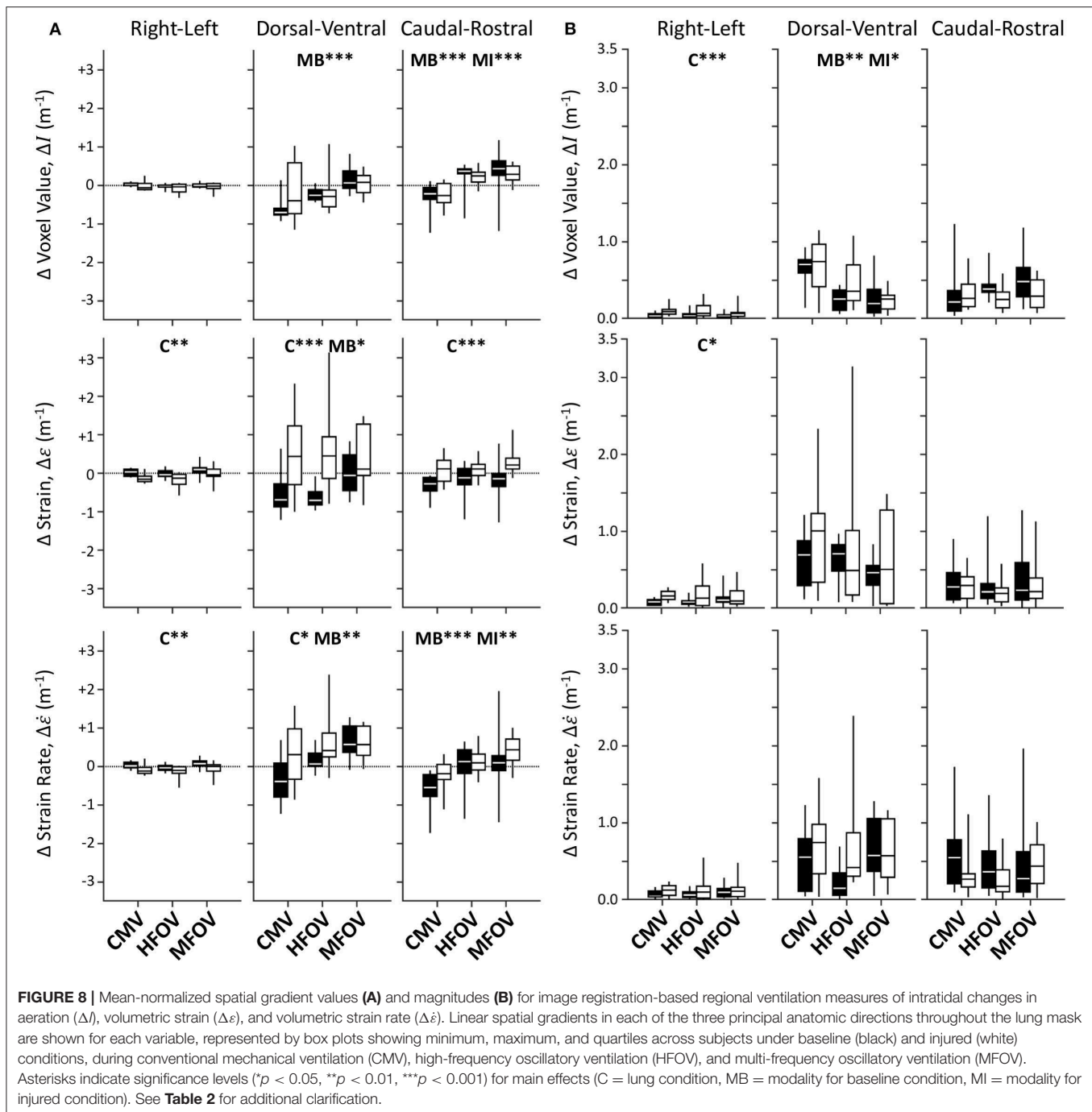


**FIGURE 7 |** Unnormalized spatial gradient values (A) and magnitudes (B) for image registration-based regional ventilation measures of intratidal changes in aeration ( $\Delta I$ ), volumetric strain ( $\Delta \epsilon$ ), and volumetric strain rate ( $\Delta \dot{\epsilon}$ ). Linear spatial gradients in each of the three principal anatomic directions throughout the lung mask are shown for each variable, represented by box plots showing minimum, maximum, and quartiles across subjects under baseline (black) and injured (white) conditions, during conventional mechanical ventilation (CMV), high-frequency oscillatory ventilation (HFOV), and multi-frequency oscillatory ventilation (MFOV). Asterisks indicate significance levels (\* $p < 0.05$ , \*\* $p < 0.01$ , \*\*\* $p < 0.001$ ) for main effects (C = lung condition, MB = modality for baseline condition, MI = modality for injured condition). See **Table 2** for additional clarification.

## DISCUSSION

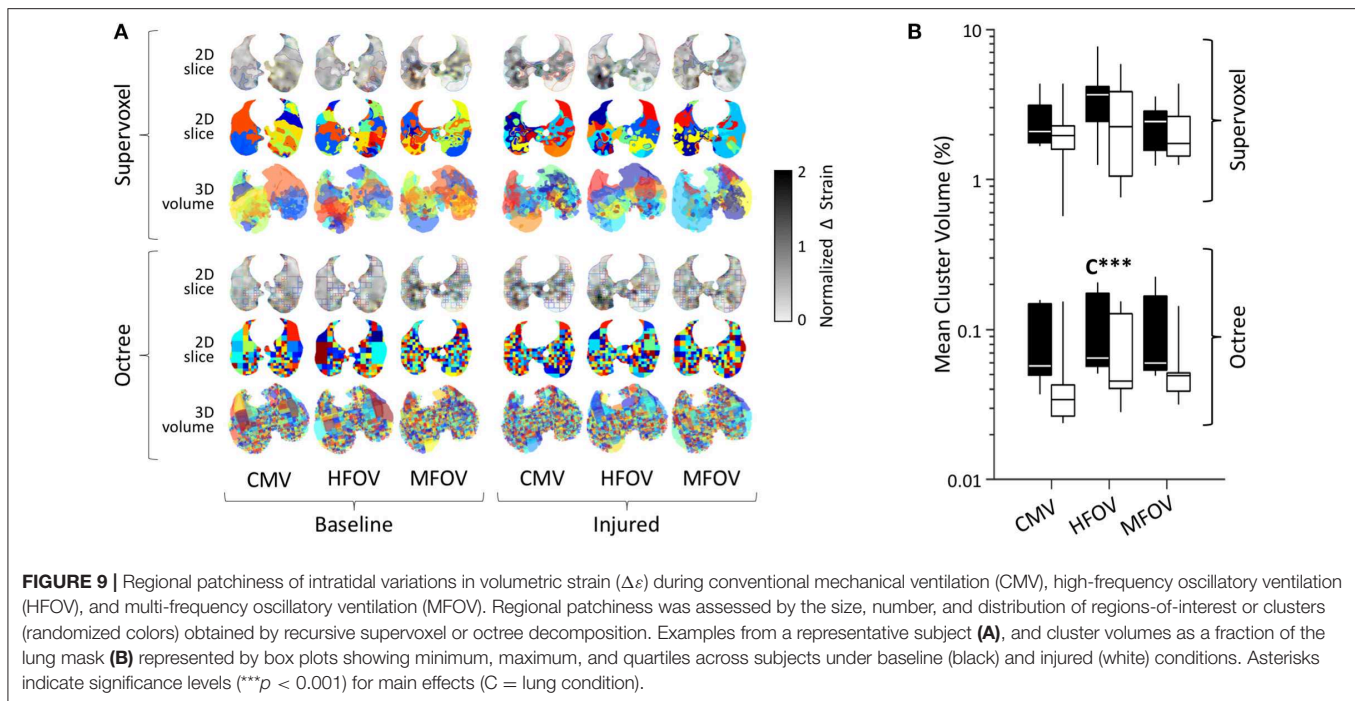
In this study, we demonstrated that oscillatory ventilation improves the average regional lung strain, as well as the spatial gradients of lung strain, compared to a conventional pressure-controlled modality in pigs with heterogeneous lung injury. This study revealed a mechanism by which enhanced harmonic content in MFOV waveforms may improve gas exchange compared to either CMV or single-frequency HFOV waveforms.

The increase in respiratory system elastance following lung injury (i.e., 183% increase in  $E_{rs}$  and 355% increase in  $H$ ) is consistent with substantial lung derecruitment and/or surfactant dysfunction. Consequently, increased driving pressure was required to maintain eucapnia at comparable respiratory rates. Despite similar  $V_{pp} \cdot Wt^{-1}$  and ventilatory cost function ( $V_C$ ), the driving pressure ( $\Delta P_{aw}$ ) after lung injury increased to 18.7  $\text{cmH}_2\text{O}$ , compared to 13.0  $\text{cmH}_2\text{O}$  at baseline (**Figure 5**). Increased  $\Delta P_{aw}$  during CMV after injury exceeded the 15  $\text{cmH}_2\text{O}$  threshold identified by Amato et al. (2015), above



which the mortality odds ratio was greater than unity in patients with ARDS. The use of  $\Delta P_{aw} > 15$  cmH<sub>2</sub>O suggests substantial potential for VILI despite average measured  $V_{pp} \cdot Wt^{-1}$  of 7.5 mL kg<sup>-1</sup> (**Figure 5**). However, such heuristics are only applicable during CMV, for which  $P_{aw}$  fluctuations are well-correlated with lung strain. During oscillatory modes of ventilation,  $\Delta P_{aw}$  as computed from Equation (6) does not represent elastic pressures distending peripheral alveoli, but also includes substantial pressure losses due to resistive and inertial

loads imposed by the endotracheal tube and conducting airways, especially with increasing frequency. The fact that  $\Delta P_{aw}$  was greater during MFOV than HFOV indicates that larger pressure amplitudes were required to overcome the increased resistive and inertial losses at frequencies up to 20 Hz compared to 5 Hz, but does not indicate that these larger airway pressures were transmitted to distal alveoli (Pillow et al., 2002). We found that the spatial mean of strain throughout the entire lung during CMV was unchanged after injury, despite increased  $\Delta P_{aw}$  and



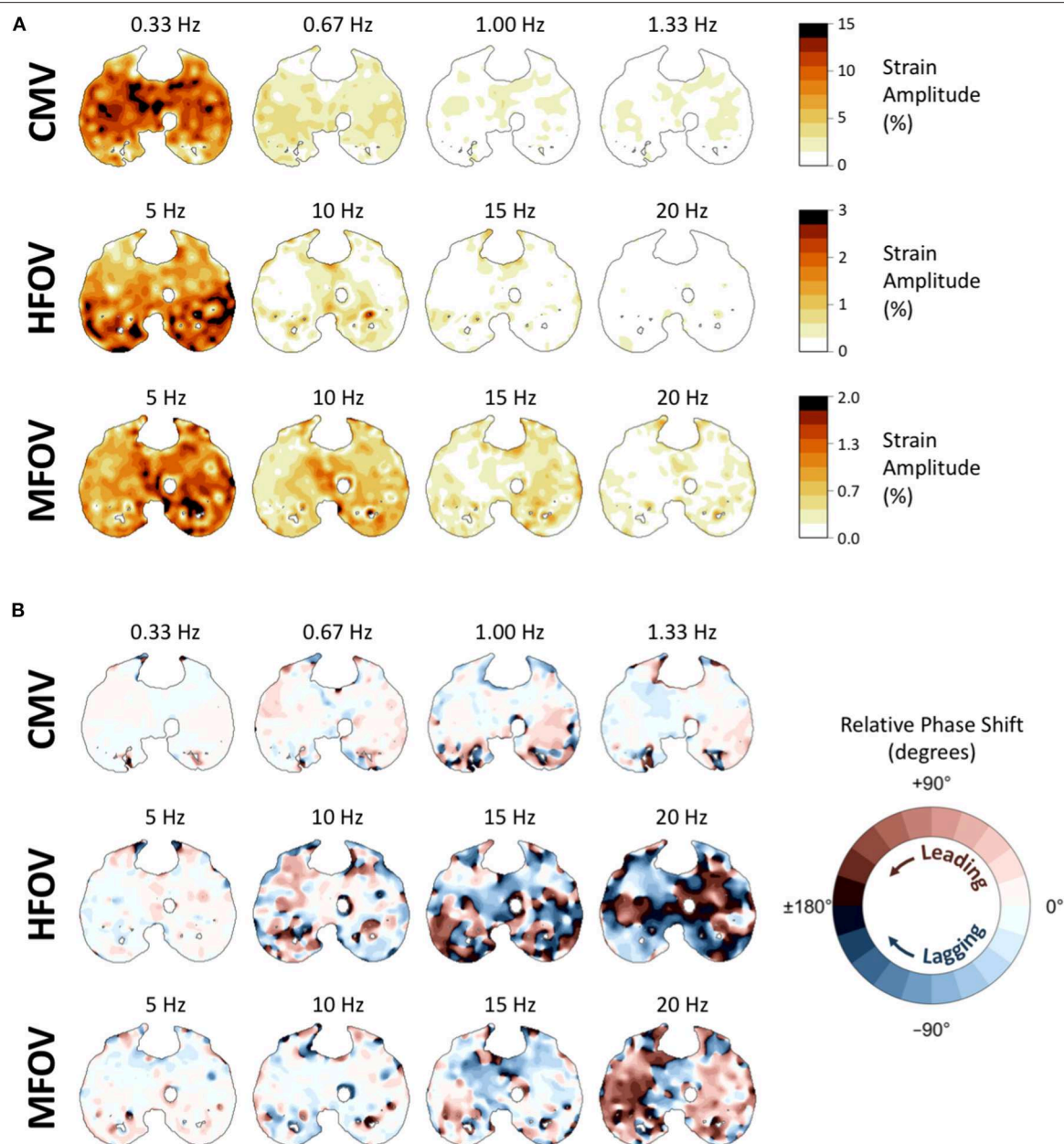
$\Delta I$  spatial mean (Figure 6). Some evidence to reconcile this discrepancy is apparent in the greatly increased coefficient of variation for  $\Delta\epsilon$  (Figure 6). Upon closer examination of the regional strain distributions in injured lungs,  $\Delta\epsilon$  was nearly zero in consolidated regions of the lung with  $I > -100$  HU. By contrast,  $\Delta\epsilon$  was increased by 25% in normally aerated regions (i.e.,  $-900 \text{ HU} < I < -500 \text{ HU}$ ) relative to the average throughout the entire lung mask. Thus, the increased  $\Delta P_{aw}$  required to deliver similar  $V_{pp} \cdot Wt^{-1}$  (Figure 5) resulted in concentrated strains within the recruited lung. This finding is consistent with the concept of the “baby lung,” which describes reduced functional recruited volume in ARDS (Gattinoni and Pesenti, 2005; Gattinoni et al., 2016a).

Spatial gradients of intratidal strain also provide some insight into the redistribution of mechanical flows after lung injury. As expected, the magnitudes of right-left gradients were small relative to those of the dorsal-ventral and caudal-rostral gradients (Figure 7). Most noticeably, lung injury was associated with dramatic changes in dorsal-ventral  $\Delta\epsilon$  gradients. Ventilation in healthy subjects during CMV tended to distribute toward the dorsal and caudal lung regions. However, varying degrees of lung injury resulted in consolidation or derecruitment of the dependent lung, such that dorsal-ventral  $\Delta\epsilon$  gradients were reduced (or even reversed) depending on the extent of edema, particularly for CMV and HFOV. Interestingly, intratidal changes in aeration tended to preserve the dorsal-ventral  $\Delta I$  gradient before and after injury, despite the positive shift observed in dorsal-ventral  $\Delta\epsilon$  gradients. It should be noted that actual spatial distributions of  $\Delta I$  and  $\Delta\epsilon$  are likely not well-described by linear functions of spatial position following lung injury, and may even be non-monotonic (Johnson

et al., 2017). For example, negative dorsal-ventral gradients may be possible in the recruited lung, but counteracted by zero ventilation in the derecruited dependent lung such that the resulting overall linear gradient may be negative, zero, or even positive. Nonetheless compared to either CMV or HFOV, MFOV reduced the magnitude of spatial gradients in ventilation regardless of the lung condition. Other strategies for improving ventilation distribution and eliminating large dorsal-ventral gradients include prone position ventilation (Scholten et al., 2017; Xin et al., 2018), which was not used in this study. Prone posture serves to eliminate large-scale gravitational gradients in lung expansion (Hoffman, 1985), but would not be expected to affect the local, region-to-region mechanical differences which MFOV targets. Finally, both HFOV and MFOV were associated with more positive caudal-rostral  $\Delta I$  gradients compared to CMV, regardless of injured condition ( $p < 0.001$ ). CMV-associated findings indicate that in contrast to oscillatory modalities, CMV preferentially ventilates the basal regions of the lungs, consistent with a previous positron emission tomography study (Venegas et al., 1993).

Much of the variability in spatial gradient magnitudes across different ventilation modalities was due to changes in the spatial means. By contrast, the normalized gradients (i.e., the spatial gradients divided by the spatial mean) exhibited fewer significant differences across modalities (Figure 8, Table 2). This finding indicates that, at least for the particular frequencies and waveforms used in this study, the *relative* spatial gradients were not substantially altered by modality. This may be due in part to the predominance of the 5 Hz component in both HFOV and MFOV waveforms, which was below the resonant frequency in almost every case (Table 1), and therefore

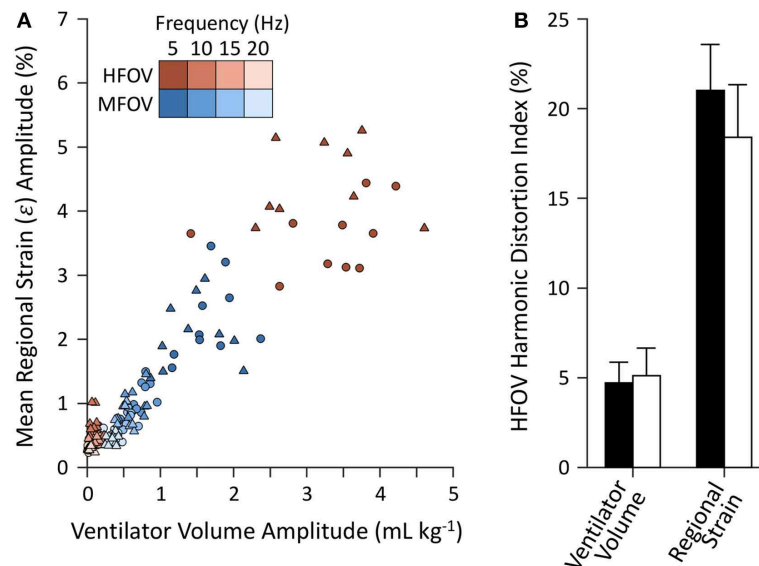




**FIGURE 10 |** Frequency-domain representations of tissue-correlated regional strain amplitude **(A)** and phase variations **(B)** in one subject during conventional mechanical ventilation (CMV), high-frequency oscillatory ventilation (HFOV), and multi-frequency oscillatory ventilation (MFOV). For each ventilation modality, strain amplitudes and phases were obtained from the discrete Fourier transform of time-varying Jacobian determinants within each voxel, using transformations mapped to a single reference image. In each cross-section of the reference image, voxel color in **(A)** indicates the strain amplitude at that frequency, corresponding to the amplitude of volumetric strain relative to the minimum volume of that particular voxel. Voxel color in **(B)** indicates the amount of phase shift (leading or lagging) relative to the median phase of all lung voxels at the specified frequency.

below a threshold frequency for developing regional ventilation heterogeneity due to resonant amplification (Herrmann et al., 2019a). Our results then indicate that broadband MFOV waveforms, while producing the same *relative* ventilation heterogeneity as HFOV, still reduce the average strain and magnitude of strain gradients that are associated with risk for VILI.

Based on our supervoxel and octree analysis, regional strain heterogeneity did not differ greatly across ventilation modality, although the injured lungs did require smaller sizes to describe the spatial clustering of  $\Delta\epsilon$  compared to the baseline conditions (Figure 9). Lung injury may thus result in increased small-scale strain heterogeneity (Kaczka et al., 2011; Perchiazzi et al., 2014). It should be noted that our estimates of regional strain



**FIGURE 11 |** Harmonic amplitudes (A) from imaging-based regional strain measurements and corresponding amplitudes from the ventilator volume waveform measured at the airway opening under baseline (circles) and injured (triangles) conditions. Harmonic distortion index (B) mean and standard deviation for each set of measurements, grouped by baseline (black) and injured (white) lung conditions.

derived from image registration are inherently smooth due to the use of B-splines to define the spatiotemporal deformations. The discrepancy between the supervoxel- and octree-based results may also be due in part to the discrete anatomic structure of lungs, which consist of an assumed continuum of spongy parenchymal tissues penetrated by branching networks of airways and vessels. Airways and vessels are not expected to undergo large volumetric strains during mechanical ventilation, and therefore give rise to irregularities in the spatial field of  $\Delta\epsilon$ . Such irregularities may be approximately contoured by supervoxel boundaries, which are not rigidly constrained. By contrast, octree decomposition is strictly planar, and therefore may require greater degrees of recursive subdivision to isolate such irregular spatial distributions of  $\Delta\epsilon$  (Perchiazzi et al., 2014). The supervoxel decomposition incorporates spatial proximity as well as image intensity, such that reducing the spatial proximity weighting may facilitate the identification of larger clusters albeit with irregular boundaries. Therefore, it is possible that our findings would be altered if smaller airways and blood vessels were further segmented from the lung parenchyma prior to cluster analysis, or if a different spatial proximity weighting was used for the supervoxel decomposition.

Separation of the harmonic content of regional ventilation illustrates a potential influence of nonlinear mechanics during HFOV at 5 Hz (Figure 11). For example, image registration resulted in estimation of  $\dot{\epsilon}$  amplitudes at 10, 15, and 20 Hz of roughly one third those at 5 Hz, despite the ventilator waveform consisting of only 5 Hz oscillation (Supplementary Figure S-4). By contrast,  $\dot{\epsilon}$  amplitudes during MFOV approximated the input distribution of uniform amplitude flow at all four harmonics (Supplementary Figure S-4). Intrapulmonary harmonic distortion of distributed flows during HFOV (with only a

single frequency) may result from the use of larger-amplitude flows exacerbating inherent mechanical nonlinearities, but may also result from the complex interaction of mechanically-interdependent lung tissues (Suki and Bates, 1991; Suki et al., 1991). During MFOV, the use of small-amplitude flows may contribute to relatively linear mechanical behavior of the lung tissues. It is also possible that the observed nonlinearity may be due in part to imaging artifact and errors in image registration resulting in misidentified high-frequency, small-amplitude motion. Assuming that our registration results are accurate however, the  $\dot{\epsilon}$  amplitudes measured at the higher harmonics during HFOV are surprisingly large, almost comparable to those intentionally delivered during MFOV. It is plausible that the mechanisms by which MFOV may enhance gas transport already occur, at least to some extent, within the lung periphery during HFOV. However, MFOV may induce these higher harmonics directly, without incurring the overhead of generating high flow rates at the fundamental frequency. The consequences of such overhead may include, for example, increased spatial gradients of strain and strain rate due to gravitational dependence (Figure 7).

## Limitations

MFOV may improve ventilation distribution and the efficiency gas exchange efficacy (Kaczka et al., 2015; Herrmann et al., 2018, 2019b). However, given the technical limitations of the mechanical ventilator as well as our dynamic CT image reconstruction technique which assumed strict periodicity of motion (Herrmann et al., 2017), the MFOV waveform used in this study comprised only harmonic components of the fundamental frequency. Cardiogenic motion was not synchronized with respiratory motion and therefore presents a source of artifact in the reconstructed 4DCT images of

respiratory motion, depending on the relative periodicity between the ventilator frequency and the heart rate. Such artifact may manifest as rapid oscillations in CT density (Herrmann et al., 2017), which may influence registration-based estimates of strain rate, especially in regions adjacent to the mediastinum.

In addition, the interpretation of regional strain in the proximity of recruitment/derecruitment is challenging for several reasons. Standard image registration techniques (e.g., using a similarity cost function defined as the sum of squared intensity differences) assume a uniform intensity transform to predict voxel-wise correspondence, but cannot account for local changes in intensity associated with changing gas fraction. Consequently, these approaches may result in the prediction of non-physical deformations, such as contraction of non-aerated lung regions. The sum of squared tissue volume differences (SSTVD) similarity cost function used in this study addresses this problem using a non-uniform intensity transform that accounts for local variations in CT intensity that are due to changing proportions of gas-to-tissue content in each lung region during breathing or ventilation (Zhao et al., 2016). Another challenge to registration of injured lungs is the lack of contrast or structural landmarks in consolidated regions, which renders validation of estimated voxel-wise correspondence nearly impossible, especially when large changes in recruitment occur between two images. In this study, high temporal resolution imaging (7–105 Hz) was used to minimize the time between adjacent ventilation phases, which resulted in small deformations and small changes in recruitment between adjacent images being registered. Linear elastic regularization produces plausible predictions of voxel-wise correspondence in regions with little contrast, assuming the lung parenchyma deforms as a linear elastic material. An important limitation of most registration techniques is the assumption of smoothly varying deformation, which may not accurately reflect discontinuous motion at distinct structural boundaries between aerated and non-aerated lung tissue. Due to the limited spatial resolution in this study (0.6 mm), each voxel may contain up to dozens of alveoli. Thus, it is difficult, if not impossible, to distinguish the underlying cause of observed changes in aeration (Cereda et al., 2019). For example, the same change in aeration of a single voxel may represent uniform deflation of its alveoli, complete derecruitment of only a portion of alveoli, or any combination thereof. Thus, prediction of recruitment/derecruitment on the basis of voxel aeration is speculative.

Finally, while our study focused on regional distributions of aeration, strain, and strain rate as the primary indicators of ventilation and VILI, the exact relationship between these mechanical variables and VILI is difficult to ascertain. VILI is a complicated process associated with a diverse range of mechanical stimuli (Hussein et al., 2013; Carrasco Loza et al., 2015; Güldner et al., 2016; Smith et al., 2017; Tonetti et al., 2017). So-called “mechanical power” (i.e., the rate of energy dissipation across parenchymal tissues) may provide a better prediction of VILI compared to either strain or strain rate alone (Gattinoni et al., 2016b; Serpa Neto et al., 2018). However, measurement of regional mechanical power is not practical, given the requirement of regional gas pressure within

the lung for its estimation. Alternatively, VILI may also be assessed using fluoro-deoxyglucose (FDG) uptake (Wellman et al., 2014), serum or alveolar inflammatory cytokines (Liu et al., 2013), protein content in bronchoalveolar lavage fluid (Smith et al., 2017), and histopathology. All of these quantitative measurements of lung injury require extensive durations of mechanical ventilation prior to measurement, some of which may only be obtained *post mortem*.

## Conclusion

In an oleic acid model of porcine ARDS, high-frequency and multi-frequency oscillatory ventilation resulted in improved gas exchange efficiency and reduced regional lung strain compared to conventional mechanical ventilation. MFOV also reduced spatial gradients in lung strain compared to CMV or HFOV, resulting in a more uniform overall distribution of lung strain. By contrast, mean-normalized spatial gradients exhibited less dependence on ventilation modality, indicating that the use of higher harmonic frequencies in MFOV does not substantially alter *relative* ventilation heterogeneity. Thus, the reduced spatial strain gradients observed with MFOV, compared to HFOV or CMV, may be explained by reductions in the *average* parenchymal strain. In summary, MFOV supports gas exchange with reduced lung strain, and may provide additional benefit over HFOV by reducing ventilation heterogeneity associated with spatial gradients in absolute strain, and by reducing the strain associated with conventional ventilation or single-frequency oscillation.

## DATA AVAILABILITY STATEMENT

The datasets generated for this study are available on request to the corresponding author.

## ETHICS STATEMENT

The animal study was reviewed and approved by University of Iowa Institute for Animal Care and Use Committee (Protocol Number 5061428).

## AUTHOR CONTRIBUTIONS

JH and DK conceived the study, collected the data, and wrote the manuscript. JH, SG, WS, MH, JR, GC, EH, and DK analyzed the data and revised the manuscript.

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## SUPPLEMENTARY MATERIAL

The Supplementary Material for this article can be found online at: <https://www.frontiersin.org/articles/10.3389/fphys.2020.00014/full#supplementary-material>

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The remaining authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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## NOMENCLATURE

4DCT	Four-dimensional computed tomography	$\bar{V}_{ROI}$	Mean cluster size after recursive octree or supervoxel decomposition
ARDS	Acute respiratory distress syndrome	$\delta V$	Volume of a single voxel
CMV	Conventional mechanical ventilation	$V_C$	Ventilatory cost function
CO <sub>2</sub>	Carbon dioxide	Wt	Body weight
$E_{rs}$	Dynamic respiratory system elastance	$x_n$	Vector of 3-dimensional spatial coordinates in $n$ th image reference frame
FDG	Fluorodeoxyglucose	$X$	Vector of 3-dimensional spatial coordinates in target image reference frame
$f$	Frequency	$X_{rs}$	Respiratory system reactance
$f_0$	Fundamental frequency	$Z_{rs}$	Respiratory system mechanical impedance
$f_{res}$	Resonant frequency	$\hat{Z}_{rs}$	Model-predicted respiratory system mechanical impedance
$F_{iO_2}$	Fraction of oxygen in inspired gas	$\alpha$	Exponent of frequency in constant phase model
HFOV	High-frequency oscillatory ventilation	$\varepsilon$	Volumetric strain
$H$	Tissue elastance	$\Delta\varepsilon$	Intratidal range of volumetric strain
$I_{aw}$	Airway inertance	$\dot{\varepsilon}$	Volumetric strain rate
$I$	Volumetric CT density image	$\Delta\dot{\varepsilon}$	Intratidal range of volumetric strain rate
$I_{avg}$	Target image for registration, representing the average of deformed images	$\gamma^2$	Coherence spectrum
$I_{n \rightarrow m}$	Result of deforming the $n$ th image into the $m$ th spatial reference frame	$\eta$	Tissue hysteresivity
$\Delta I$	Intratidal range of CT density	$\pi$	Number of radians in a semicircle
$J_{n \rightarrow m}$	Jacobian matrix of the transformation from the $n$ th to $m$ th spatial reference frames	$\phi$	4-dimensional transformation mapping image sequence to target average image
$j$	Unit imaginary number, i.e., $j = \sqrt{-1}$	$\nabla_x$	Spatial gradient operator
$k$	Frequency index		
MFOV	Multi-frequency oscillatory ventilation		
$M$	Lung segmentation mask		
$m$	Image index, corresponding to phase of periodic ventilation cycle		
$n$	Image index, corresponding to phase of periodic ventilation cycle		
$N$	Number of images in periodic sequence		
OI	Oxygenation index		
$P$	Pressure		
$P_{aw}$	Pressure at the airway opening		
$\bar{P}_{aw}$	Mean airway pressure		
$\Delta P_{aw}$	Intratidal range of airway pressure		
$P_aCO_2$	Partial pressure of carbon dioxide in arterial blood		
$P_aO_2$	Partial pressure of oxygen in arterial blood		
PEEP	Positive end-expiratory pressure		
ROI	Region of interest		
$R$	Airway resistance		
SFOV	Single-frequency oscillatory ventilation		
SSTVD	Sum of squared tissue volume differences		
$t$	Time		
$\delta t$	Time step between adjacent image phases		
$T$	Time duration of the ventilatory cycle		
VILI	Ventilator-induced lung injury		
$V$	Volume		
$\bar{V}$	Time-averaged volume over the ventilatory cycle		
$V_{pp}$	Peak-to-peak volume		
$V_{rms}$	Root-mean-square volume		



# An Analytical Model for Estimating Alveolar Wall Elastic Moduli From Lung Tissue Uniaxial Stress-Strain Curves

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The non-linear stress-strain behavior of uniaxially-stretched lung parenchyma is thought to be an emergent phenomenon arising from the ensemble behavior of its microscopic constituents. Such behavior includes the alignment and elongation of randomly oriented alveolar walls with initially flaccid fibers in the direction of strain. To account for the link between microscopic wall behavior and the macroscopic stress-strain curve, we developed an analytical model that represents both alignment and elongation of alveolar walls during uniaxial stretching. The model includes the kinetics and mechanical behavior of randomly oriented elastic alveolar walls that have a bending stiffness at their intersections. The alignment and stretch of the walls following incremental stretch of the tissue were determined based on energy minimization, and the total stress was obtained by differentiating the total energy density with respect to strain. The stress-strain curves predicted by the model were comparable to curves generated by a previously published numerical alveolar network model. The model was also fit to experimentally measured stress-strain curves in parenchymal strips obtained from mice with decreased lung collagen content, and from young and aged mice. This yielded estimates for the elastic modulus of an alveolar wall, which increased with age from 4.4 to 5.9 kPa ( $p = 0.043$ ), and for the elastic modulus of fibers within the wall, which increased with age from 311 to 620 kPa ( $p = 0.001$ ). This demonstrates the possibility of estimating alveolar wall mechanical properties in biological soft tissue from its macroscopic behavior given appropriate assumptions about tissue structure.

**Keywords:** multiscale, alignment, tensile modulus, bond-bending modulus, aging

## INTRODUCTION

The macroscopic mechanical behavior of a biological tissue such as the lung parenchyma arises from the ensemble behavior of its microscopic constituents (Suki and Bates, 2011). This macroscopic behavior is usually very different from the behaviors of the constituents themselves. Furthermore, while macroscopic behavior determines physiological phenotype, disease processes and pharmacotherapies invariably act at the microscale level. It is thus crucial to understand macroscopic mechanical behavior of tissue as an emergent consequence of structure and function at the microscale. In particular, the strain-stiffening behavior of biological soft tissues has been

primarily attributed to the way in which load-bearing fibers are recruited via alignment and/or straightening within the extracellular matrix (ECM) (Wuyts et al., 1995; Suki et al., 2005; Suki and Bates, 2011). The progressive recruitment of collagen fibers with increasing strain has been modeled specifically for lung parenchymal tissue (Maksym and Bates, 1997), human vein, fascia, tympanic membrane, rabbit papillary muscle (Decraemer et al., 1980), and ligament (Liao and Belkoff, 1999). Both recruitment and fiber reorientation were simultaneously taken into account by Lanir (1979). Nevertheless, the stress-strain behavior of the individual tissue constituents themselves must also be taken into account for a complete understanding of tissue mechanics. Determining this behavior experimentally is challenging because of the tiny length scales involved, but Sacks was able to determine fiber orientation using small-angle light scattering and numerically solved the constitutive equations to estimate the stress-strain behavior of individual collagen fibers (Sacks, 2003). Furthermore, these fibers do not act in isolation. They interact with each other and with other components of the ECM through electrostatic forces arising, for example, from negatively charged proteoglycans (PGs) that exert repulsive forces on each other (Cavalcante et al., 2005; Ritter et al., 2009).

These models, however, all fail to capture the foam-like structure of lung parenchyma comprised of alveoli and alveolar ducts. Models based on 3-dimensional alveolar geometry have been proposed (Denny and Schroter, 2006; Parameswaran et al., 2011; Pidaparti et al., 2013), but these all assume constitutive properties for the alveolar wall and predict tissue behavior on this basis. Here we seek to do the reverse, namely to infer alveolar wall properties from the macroscopic mechanical behavior of lung parenchyma. Most models of lung tissue that have been proposed to date are limited in this regard because they are numerical (Maksym et al., 1998; Cavalcante et al., 2005; Takahashi et al., 2014), and are thus computationally expensive. Also, the insights provided by numerical models are limited to the particular parameter sets used to calculate examples of model behavior. Analytical models, in contrast, have the potential to provide general insight that is not bound by particular exemplars. Analytical models can also usually be solved much more quickly than numerical models, which makes them more suited to the present inverse modeling application, although they invariably require significant simplifying assumptions in order to be tractable.

Accordingly, the goal of this study was to develop an analytical multi-scale model that links the elastic stiffness and the alignment mechanism of the alveolar walls to the macroscopic mechanical stress-strain behavior of the lung tissue itself. We test the predictions of this model by comparing its macroscopic stress-strain curves to those made by a previously developed numerical model. We also tested model predictions against experimental data obtained in parenchymal tissue strips under uniaxial stretching. These conditions modulate fiber stretching and alignment without being confounded by other phenomena operative in the 3-dimensional expansion of lungs *in situ* such as volumetric expansion, shear, and surface tension (Wilson and Bachofen, 1982; Bachofen and Schürch, 2001; Denny and Schroter, 2006). This enabled us to focus exclusively on the

mechanical properties of the tissue fibers and how they change with age, the latter being known to principally affect the fibers (Kohn et al., 2015; Panwar et al., 2015).

## METHODS

### Model Development

We assume that a 2-dimensional strip of lung tissue with length  $L$  and width  $W$  is held in place at one end and stretched uniaxially from the other in a sequence of equal increments. The tissue strip is modeled as a network of hexagonal alveoli. Each of the  $N$  alveolar walls in the strip (**Figure 1A**) has a tensile Young's modulus  $Y_a$ , while adjacent walls are bonded together at intersections that have bond-bending modulus  $Y_b$  that resists changes in angle between neighboring walls. The volume fraction of the tissue comprised of alveolar walls is  $\delta_{V,w}$ , so the effective tensile and bond-bending moduli of the tissue are  $Y_{ae} = Y_a \delta_{V,w}$  and  $Y_{be} = Y_b \delta_{V,w}$ , respectively (assuming that whatever fills the alveolar lumen makes no contribution to either). At incremental stretch step  $s - 1$ , the  $n^{\text{th}}$  alveolar wall has length  $l_{n,s-1}$  and strain  $\varepsilon_{n,s-1}$  and is oriented at an angle  $\theta_{n,s-1}$  with respect to the direction of tissue stretch (**Figure 1B**).

An incremental displacement  $x$  of the right-hand end of the alveolar wall in the direction of tissue stretch will, in general, cause the wall itself to undergo some combination of alignment and elongation (**Figure 1C**). Elongation of the wall increases its elastic energy, while alignment alters the elastic energy stored within its wall-wall bonds (**Figure 1D**). The configuration of the various walls within the tissue at any time step  $s$  will be that which minimizes the sum of all these energies. The stress within the tissue is then the derivative of the energy density of the system with respect to macroscopic strain. To establish the global stress-strain equation for the tissue, we further assume

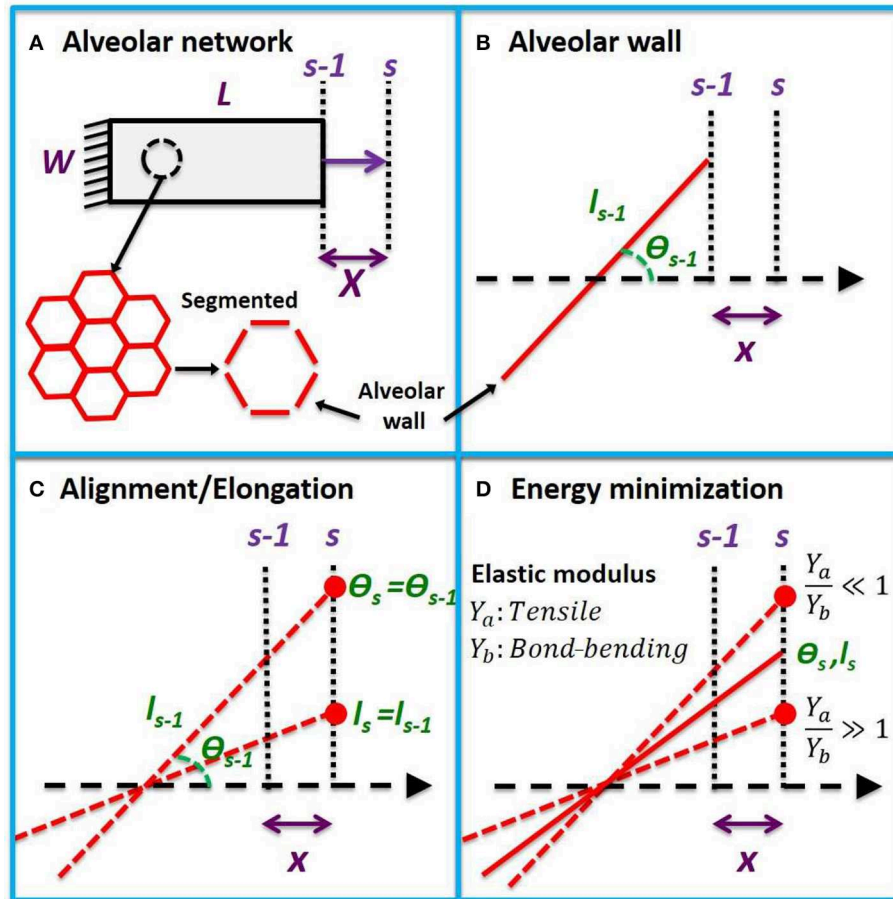
- constant tensile and wall-bending moduli,
- affine tissue deformation characterized by the microscopic incremental tissue strain ( $d\epsilon_x$ ) due to the microscopic incremental displacement  $x$  being equal to the macroscopic incremental strain ( $d\epsilon_x$ ) due to the macroscopic incremental displacement  $X$  ( $d\epsilon_x = d\epsilon_X$ ),
- extension and alignment of the alveolar wall bear a linear relationship to each other when strained incrementally,
- boundary effects are minimal (i.e.,  $L \gg l_{s-1}$  and  $W \gg l_{s-1}$ ).

These assumptions lead to the following equation relating macroscopic tissue stress  $\sigma_T$  at the current stretch step  $s$  to the alveolar wall constitutive properties, the current strains, angles, and initial angles  $\theta_{n,0}$  for all walls ( $n = 1, \dots, N$ ), and the incremental tissue strain (see **Appendix A** for a detailed derivation):

$$\sigma_T(s) = Y_{ae} \frac{1}{N} \sum_{n=1}^N \frac{d\epsilon_X + \varepsilon_{n,s-1} + (1 + \varepsilon_{n,s-1}) (\theta_{n,0} - \theta_{n,s-1}) \tan(\theta_{n,s-1})}{1 + \frac{Y_{ae}}{Y_{be}} (1 + \varepsilon_{n,s-1})^2 \tan^2(\theta_{n,s-1})} \quad (1)$$

In the limit of large macroscopic stretch, all the alveolar walls become aligned, the denominator of the above equation tends to 1, and the last term of the numerator tends to 0. At this point, the equation reduces to the description of an arbitrary number of





**FIGURE 1 |** Uniaxial model development. **(A)** Uniaxial stretching of a tissue strip from step  $s - 1$  to  $s$  with an incremental macroscopic displacement  $X$ . The tissue is composed of a hexagonal network which can be partitioned into alveolar wall segments. **(B)** A single wall segment with length  $l_{s-1}$  and angle  $\theta_{s-1}$  with respect to the direction of stretch at step  $s - 1$ . A microscopic displacement  $x$  will cause the wall to align by rotation and stretch. **(C)** The alveolar wall will follow the microscopic displacement between two extremes of pure elongation and pure rotation. **(D)** When the tensile modulus of the wall is much larger than its bond-bending modulus ( $Y_a > Y_b$ ), it will rotate, and when its bond-bending modulus is much larger ( $Y_b \gg Y_a$ ), it will elongate in order to minimize energy. The new angle ( $\theta_s$ ) and length ( $l_s$ ) at step  $s$  will lie between these two extremes at a location that minimizes the total elastic energy.

linearly elastic walls in parallel thus:

$$\sigma_T = Y_{ae}(d\epsilon_X + \bar{\epsilon}_{s-1}) \quad (2)$$

where  $\bar{\epsilon}_{s-1}$  is the mean wall strain. The slope of this stress-strain relationship is independent of angle because, at full alignment, the bond-bending energy remains constant. The asymptotically linear portion of the stress-strain curve at high strain thus depends only on  $Y_{ae}$ . In general, however, the macroscopic stress-strain relationship expressed by Equation 1 involves the two elastic moduli  $Y_{ae}$  and  $Y_{be}$ , which can be estimated by fitting Equation 1 to experimental measurements of  $\sigma_T$  and  $\epsilon_X$ . Finally, if the average fiber volume fraction ( $\delta_{V,f}$ ) within the alveolar wall is known, and assuming that the fibers are the major contributors to the wall tensile modulus, then the average elastic modulus of a single fiber ( $Y_f$ ) can be estimated as.

$$Y_f \cong \frac{Y_a}{\delta_{V,f}} \cong \frac{Y_{ae}}{\delta_{V,w}\delta_{V,f}} \quad (3)$$

## Computational Model Validation

We compared the predictions of the above model to stress-strain relationships generated by a previously described numerical model. The numerical model, introduced by Cavalcante et al. (2005), consists of a hexagonal cell network representing a strip of lung parenchyma, where each hexagonal cell represents an alveolus in cross-section and each hexagonal segment represents an alveolar wall. (Figure 9A in Appendix B). Each wall is modeled as a spring with spring constant  $k$  in units of [N/m]. The relative rotation of two alveolar walls about their point of intersection is hindered by a bond-bending spring with an elastic constant  $b$  in units of [Nm/rad<sup>2</sup>]. When  $b$  is zero, the hexagonal structure is unstable and collapses upon shear or uniaxial stretch, while when  $b$  is very high the symmetric configuration of the hexagon strongly resists a change in shape. In any case, the walls each align and elongate in such a way that the total energy of the network is minimized at each strain step. In this way, the model of Cavalcante et al. (2005) takes into consideration the deformation

energy stored within all the individual alveolar walls and all the bonds between their respective neighboring walls in a network.

In contrast, the analytical model developed above considers the tensile and bending energies of alveolar walls in isolation (i.e., it does not take into account how the presence of neighboring walls might affect a given wall's configuration). Both models, however, should predict the same total elastic energy in the tissue strip at each tissue strain. When their respective expressions for total energy are equated (see **Appendix B** for details), we find that

$$Y_{ae} = u \frac{9}{4} l_o^2 k \quad (4)$$

$$Y_{be} = u 18b \quad (5)$$

where  $l_o$  is the mean initial length of the walls in the numerical model, and  $u$  is a unity constant that ensures both sides of Equations 4 and 5 have the same dimensions.

### Experimental Model Validation

We tested the predictions of the analytical model against three different sets of experimental data. The first set comprised the stress-strain measurements made in excised rat lung slices ( $n = 5$  per group) published by Cavalcante et al. (2005). Measurements were made while the strips were bathed in normal, hypertonic, and hypotonic saline in order to modulate the charge densities on the proteoglycans in the tissue, which affects tissue stiffness due to altered repulsive forces acting on alveolar walls. Because the surface charges on elastin and collagen are significantly lower than those on proteoglycans (Maroudas and Bannon, 1981; Chalmers et al., 1999), altering saline tonicity is expected to mainly affect  $Y_{be}$  with relatively little influence on  $Y_{ae}$ .

The second test data set was comprised of quasi-static stress-strain curves measured in mice published by Shiwen et al. (2015). We used data from both wild-type mice (WT,  $n = 6$ ) and from age-matched mice in which myocardin-related transcription factor-A (MRTF-A) had been knocked out (KO,  $n = 6$ ). MRTF-A is known to lead to a reduction in type I collagen deposition, leading to tissue softening, and indeed these investigators showed that KO had reduced tissue stresses compared to WT. The reduction in stress was attributed to both a decrease in collagen content and a decrease in fibril diameter from  $97 \pm 24$  nm in WT to  $58 \pm 9$  nm in KO. It is thus expected that both  $Y_f$  and  $Y_{ae}$  should be reduced in the KO mice, with minimal alterations to  $Y_{be}$ .

The third data set was collected in our laboratory in a study approved by the Institutional Animal Care and Use Committee of Boston University. We investigated the effects of aging on alveolar wall tensile and bond-bending moduli by fitting lung tissue stress-strain curves obtained in young ( $n = 5$ ; 5 months) and old ( $n = 6$ ; 19, and 24 months) mice. The young mice were obtained from Charles River Laboratories (Boston, MA). The mice were anesthetized by intraperitoneal injection of pentobarbital sodium (80 mg/kg), tracheostomized and cannulated with an 18-gauge steel needle in the supine position followed by median abdominal incision and sternotomy under deep anesthesia. Euthanasia was obtained during exsanguination by cutting the abdominal aorta and inferior vena cava while the

pulmonary artery was flushed with phosphate buffered saline (PBS). For the aged mice, isolated lungs were obtained from Brigham and Women's Hospital, Harvard Medical School. The left lung in each group was cut into strips with dimensions of  $5 \times 2 \times 1$  mm, and used to obtain tissue strip mechanics. Uniaxial quasi-static stress-strain curves were obtained as previously described (Cavalcante et al., 2005). Briefly, the system consists of a computer-controlled lever arm (Aurora Scientific, Ontario, Canada) and a sensitive force transducer (model 300B; Aurora Scientific, Ontario, Canada) both attached to an acrylic base housing a 24 mL tissue bath maintained at a temperature of 37°C. Small metal plates were glued to each end of the strip with cyanoacrylate. The plates were attached to the force transducer and lever-arm via steel wires and the strip was submerged in the tissue bath containing PBS. The strips were preconditioned by applying three consecutive triangular displacement signals peaking at 60% uniaxial macroscopic strain at a rate of 2 %/s. After a 5-min equilibration period, force-displacement data were collected. Stress and strain were calculated as the force divided by the initial cross-sectional area and the displacement divided by the initial length of the strip, respectively.

### Model Fitting and Statistical Analysis

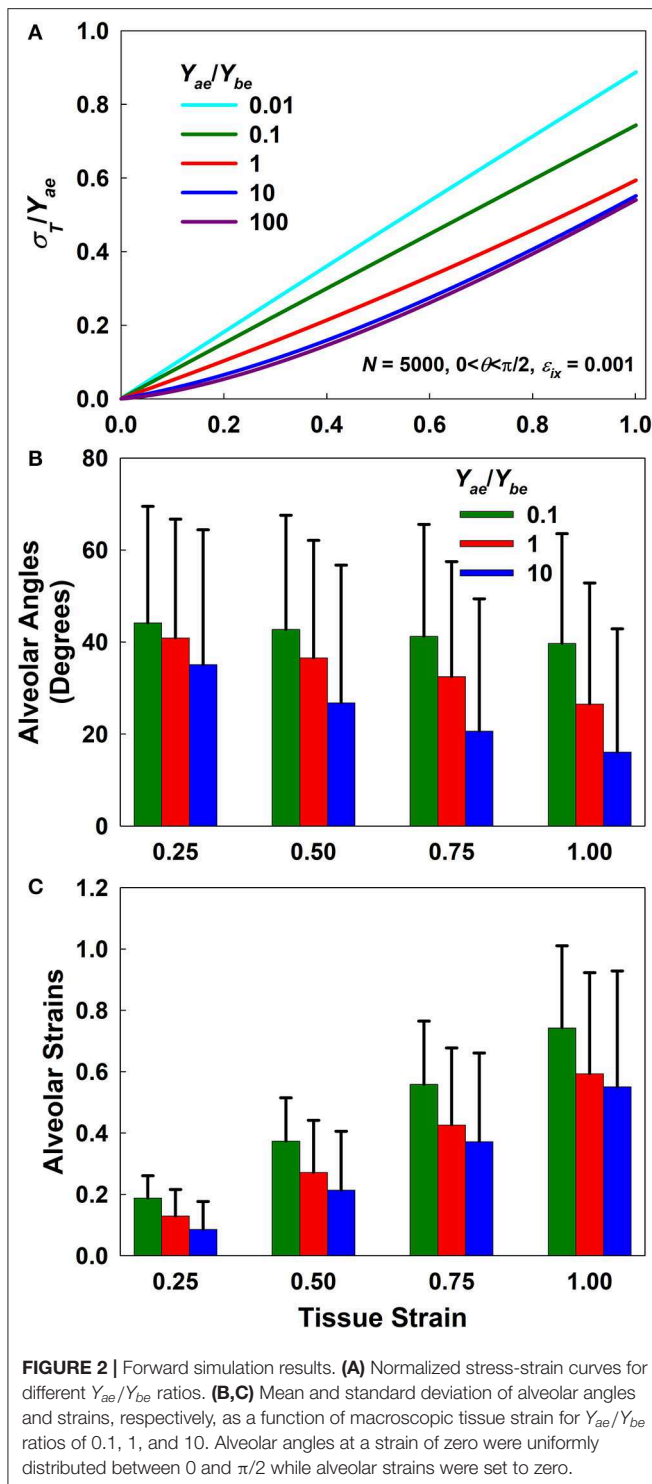
Data simulation and curve fitting were performed using either MATLAB R2015a or R2018b (MathWorks, CA), while statistical tests were performed using SigmaPlot 11.0 (Systat Software, CA). A paired  $t$ -test was applied for the rat tissue slices bathed in different tonicities, while a  $t$ -test was used for the collagen knockout and aging study. Statistical significance was accepted at  $p < 0.05$ .

The *nlinfit* function in MATLAB was used to fit the model to data. The *nlinfit* solver was provided with initial guesses for  $Y_{ae}$  and  $Y_{be}$  and an initial uniform distribution of 5,000 alveolar wall angles between 0 and  $\pi/2$  was assumed. The initial alveolar strains were set to zero. Since the model predictions (Equation 1) are based on the assumption of small incremental strains, while in most cases the experimental strain steps were large, we iteratively calculated the alveolar wall strains and angles as well as the total tissue stress for strains ranging from zero up to the maximum experimental strain, in strain steps of 0.001. The predicted model tissue stress was then compared to the experimental stress values at the experimental strains, the predicted values of  $Y_{ae}$  and  $Y_{be}$  were updated, and the process was repeated. Further investigations with the model indicated that at least 2,000 alveolar walls and an incremental strain of  $<0.01$  are required for the model to converge—see **Appendix C**.

## RESULTS

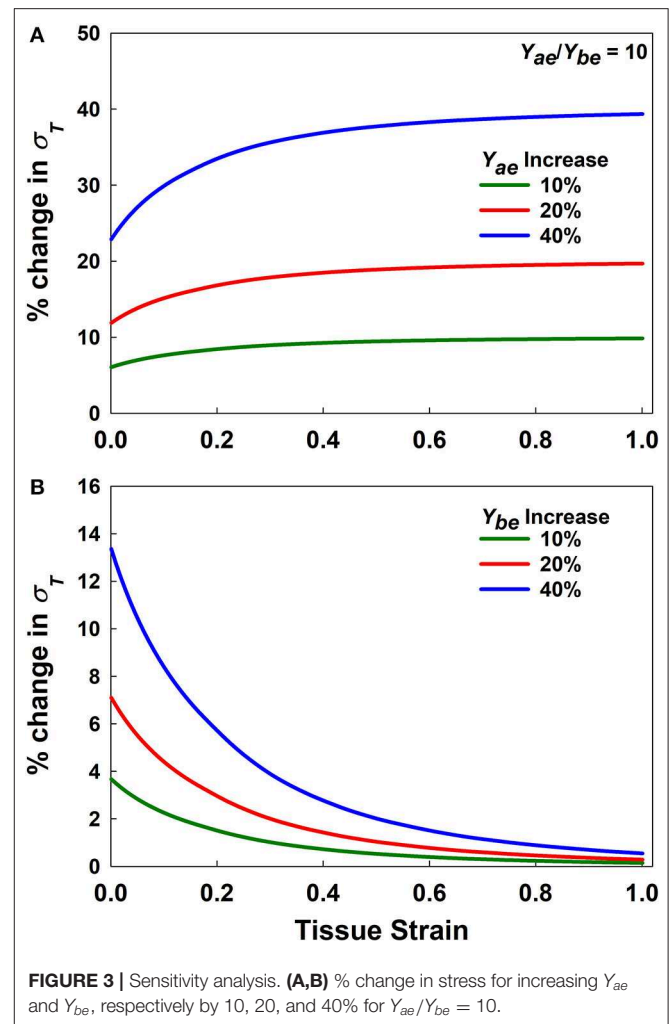
### Model Behavior

**Figure 2** plots the normalized stress-strain curves for five different  $Y_{ae}/Y_{be}$  ratios (**Figure 2A**) as well as the means and standard deviations of the alveolar angles and strains for ratios of 0.1, 1, and 10 (**Figures 2B,C**, respectively). The normalized stress-strain relationship for a ratio of 0.01 is essentially linear (**Figure 2A**) while the mean wall angle of  $\pi/4$



**FIGURE 2 |** Forward simulation results. **(A)** Normalized stress-strain curves for different  $Y_{ae}/Y_{be}$  ratios. **(B,C)** Mean and standard deviation of alveolar angles and strains, respectively, as a function of macroscopic tissue strain for  $Y_{ae}/Y_{be}$  ratios of 0.1, 1, and 10. Alveolar angles at a strain of zero were uniformly distributed between 0 and  $\pi/2$  while alveolar strains were set to zero.

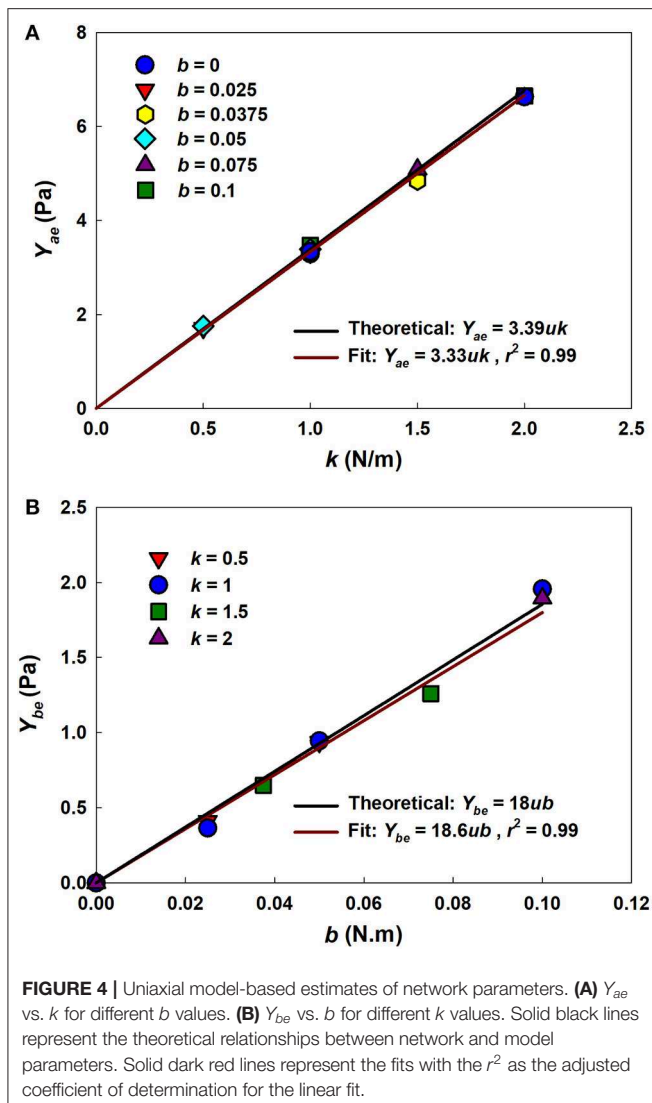
shows that alignment was minimal, demonstrating that strain was accommodated almost entirely through wall elongation. As  $Y_{ae}/Y_{be}$  increases, however, the stress-strain relationships (Figure 2A) become progressively more non-linear and thus similar to the experimentally observed stress-strain curves, while the mean wall angles depart increasingly from  $\pi/4$ , indicative of



**FIGURE 3 |** Sensitivity analysis. **(A,B)** % change in stress for increasing  $Y_{ae}$  and  $Y_{be}$ , respectively by 10, 20, and 40% for  $Y_{ae}/Y_{be} = 10$ .

an increasing degree of wall alignment with macroscopic stretch. Above a  $Y_{ae}/Y_{be}$  ratio of 100 the macroscopic stretch of the tissue was accommodated almost entirely by wall alignment. Additional investigations of the effects of alveolar number and incremental strain are presented in Appendix C.

Figure 3 presents a sensitivity analysis of the effects of variations in  $Y_{ae}$  and  $Y_{be}$  on model stress for a  $Y_{ae}/Y_{be}$  ratio of 10. The effects of these two parameters are opposite; increasing  $Y_{ae}$  causes stress to increase (Figure 3A), while increasing  $Y_{be}$  causes stress to decrease (Figure 3B) with strain. Furthermore, variations in  $Y_{ae}$  have a stronger impact at high strains, while the opposite is true for  $Y_{be}$ . Clearly, once strain is high enough to bring the alveolar walls into alignment,  $Y_{be}$  has no further effect on the stress-strain curve, so with further strain there is a linear relationship between  $Y_{ae}$  and stress. In contrast, a linear relationship between  $Y_{be}$  and stress is not possible. Figure 3 also shows that the rate of change of stress with either  $Y_{ae}$  or  $Y_{be}$  is greatest at low stress. This indicates that fitting the stress-strain relationship predicted by the model to experimental data over a range of strains from 0 to 30% should be sufficient to reliably estimate both elastic moduli.



## Model Validation

**Figure 4** shows that estimates of  $Y_{ae}$  and  $Y_{be}$  from the analytical model (Equations 4 and 5, respectively) agree closely with those used in the numerical network model over a range of parameter values, with  $r^2$  values of 0.99. This supports the utility of the analytical model as a computationally much faster alternative to the numerical model.

The distributions of alveolar wall angle and wall strain at four different tissue strains for the analytical and numerical models are compared in **Figure 5**. There is generally good agreement between the two models in terms of wall angle (**Figures 5A,C,E,G**), although alveolar walls align with the direction of strain somewhat more rapidly in the analytical model because interactions between the nodes of the network model resist alignment to some degree. In particular, the analytical model assumes that the alveolar wall ends rotate according to the macroscopic strain; however, in the network model each node pulls on another wall which delays the alignment with strain.

The strain distributions from the two models (**Figures 5B,D,F,H**) are less consistent than the angle distributions, although both models exhibit similar ranges of strain values. An important difference between the two models that may account for the discrepancies seen in the strain panels of **Figure 5** is that while alveolar walls can only increase in length with macroscopic strain in the analytical model, in the network model it is possible for two adjacent nodes in the network model to approach each with increasing strain if the nodes are aligned perpendicular to the direction of strain (as illustrated in **Figure 10B**, **Appendix B**). The network model considers such shortened walls to be flaccid, thus making no contribution to the strain energy.

**Figure 6** shows fits from the analytical model to stress-strain measurements in rat lung tissue strips made under different tonicity conditions (**Figure 6A**) and between WT and MRTF-A KO mice (**Figure 6B**). The fitted model parameters are shown in **Table 1**. Alterations in tonicity had no statistically significant effect on  $Y_{ae}$ , but  $Y_{be}$  increased by 211% between normal and hypotonic conditions ( $p = 0.03$ ) and showed a nearly significant ( $p = 0.09$ ) decrease between normal and hypertonic conditions. On the other hand,  $Y_{ae}$  decreased significantly ( $p = 0.014$ ) between WT and MRTF-A KO mice, while there was no significant change in  $Y_{be}$ . These differential effects of changes in tonicity vs. MRTF-A KO are as expected on the basis of altered proteoglycan charge density vs. reduced collagen I deposition in the tissue.

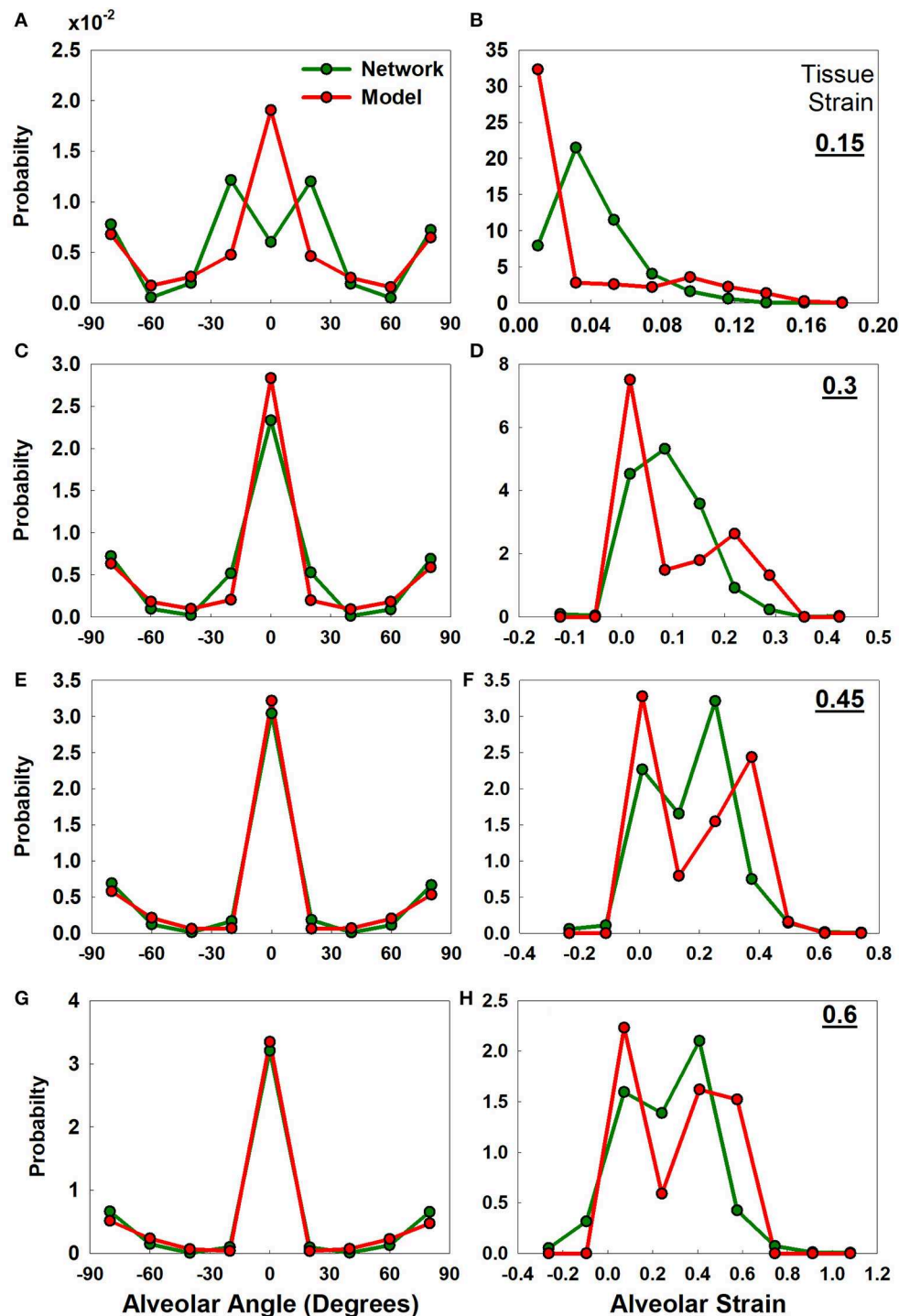
**Figure 7** shows that age increases parenchymal tissue stiffness, and that the analytical model recapitulates this effect. The elastic moduli obtained by fitting the model to the young and old stress-strain relationships are given in **Table 2**. Values for  $Y_a$  and  $Y_b$  as well as the fiber tensile elastic modulus ( $Y_f$ ) were estimated using literature values for the density of wall tissue in a parenchymal strip ( $\delta_{V,w}$ ) and the density of fibers in an alveolar wall ( $\delta_{V,f}$ ) obtained by Huang et al. (2007) in 2 and 20 month old C57BL/6 mice. They found that the tissue fraction was 35% independent of age, while the total fiber content (collagen plus elastin) decreased with age from 4 to 2.75%. The values of  $Y_{be}$  estimated by the analytical model did not change with age, but  $Y_{ae}$  increased by 34.4% from 4.4 to 5.9 kPa ( $p = 0.043$ ).  $Y_f$  increased with age by 99.4% from 311 to 620 kPa ( $p = 0.001$ ).

## DISCUSSION

In this study, we developed an analytical model of lung parenchymal tissue mechanics that links uniaxial stress-strain behavior at the level of the tissue strip to the alignment and elongation of alveolar walls. By modeling this behavior, we were able to separate and estimate the tensile and bond-bending moduli of alveolar walls under different experimental conditions and biological processes such as aging.

The model replicated experimental stress-strain data from a variety of sources and provided average estimates of the tensile modulus of an average alveolar wall and the bond-bending modulus of the junction between walls (**Tables 1, 2**). Investigations of model behavior (**Figures 2, 3**) suggest that the





**FIGURE 5 |** Uniaxial analytical and the network model-based alveolar angle and strain distributions. The graphs show alveolar angle probability distribution functions (**A,C,E,G**) and alveolar strain probability distribution functions (**B,D,F,H**) from the analytical model and the network at four levels of tissue strains (0.15, 0.3, 0.45, and 0.6). Initial alveolar strains are zero. Initial angle distribution is shown in **Appendix B, Figure 9B**.

ratio of the tensile to the bond-bending elastic moduli must exceed 1 in order to account for the experimentally observed strain-stiffening properties of lung tissue (Fung, 1984; Karlinsky,

1992; Pinart et al., 2011; Suki and Bates, 2011; Yi et al., 2016; Polio et al., 2018). The stress-strain relationships predicted by the model become increasingly non-linear as the modulus ratio

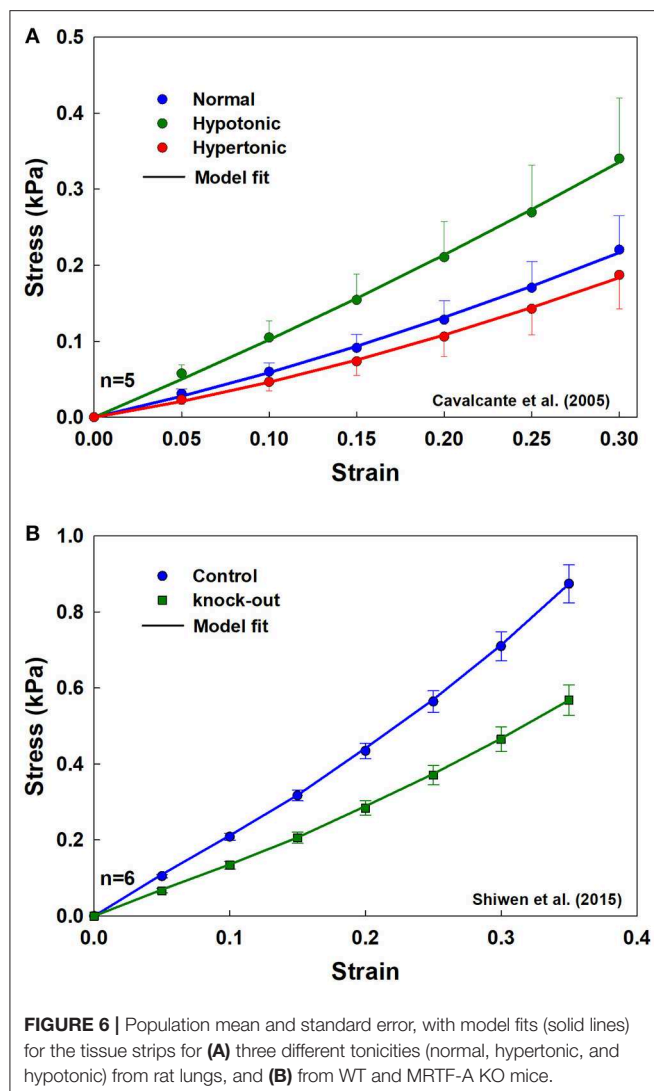
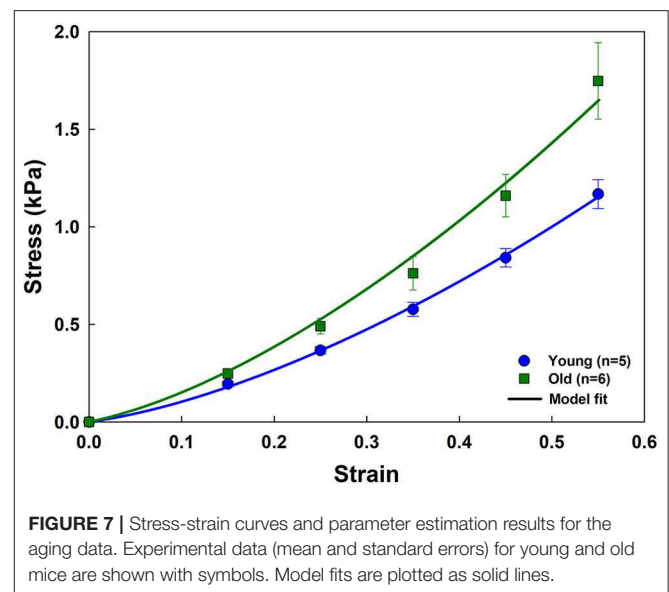


TABLE 1 | Model validation experimental results.

	$Y_{ae}$ (kPa)	% $\Delta$	p-value	$Y_{be}$ (kPa)	% $\Delta$	p-value
<b>Tonicity—Rat Tissue Strips</b>						
Normal	$1.94 \pm 1.07$			$0.27 \pm 0.14$		
Hypotonic	$3.28 \pm 1.75$	69	0.11	$0.84 \pm 0.41$	211	0.03
Hypertonic	$1.78 \pm 1.03$	-8	0.11	$0.11 \pm 0.11$	-60	0.09
<b>Collagen Knockout—Mouse Tissue Strips</b>						
Control	$5.96 \pm 1.39$			$1.28 \pm 0.42$		
Knock-out	$3.94 \pm 0.93$	-34	0.014	$0.84 \pm 0.58$	-34	0.165

$Y_{ae}$  and  $Y_{be}$  values are mean  $\pm$  standard deviation. % $\Delta$  is the percent difference with respect to the normal control.

increases. This is consistent with the notion that the alveolar walls and the embedded fibers are the main load bearing elements in the lung parenchyma (Romero et al., 1998; Yuan et al., 2000;



Maina and West, 2005; Yi et al., 2016), and is supported by our finding that reducing collagen in the wall reduces tissue stiffness (Figure 6B). Furthermore, since the elastic modulus of an alveolar wall in the model is constant with stretch, the non-linearity of the predicted stress-strain relationships arises purely from alignment that allows the walls to align with the direction of macroscopic strain, which is essentially a recruitment process. Alignment also implies a certain capacity of the wall to oppose being stretched, something that is modulated by the ratio of  $Y_{ae}$  to  $Y_{be}$ . The higher the ratio, the stiffer the alveolar wall and the faster the alignment (Figure 2B). Ratios larger than 1 were obtained from the fitting (Tables 1, 2) which is expected on physiological grounds since the function of the wall, and particularly the fibers within it, is to provide a mechanically resilient structure within a very thin layer to support structural integrity and gas exchange (Weibel, 2009; Maina and West, 2005).

The estimated values of  $Y_{ae}$  ( $\sim 5$  kPa) and  $Y_f$  ( $\sim 300$  kPa) for the young mice) obtained by fitting the analytical model to experimental stress-strain relationships match those reported in literature (Table 2). For example, Polio et al. (2018), measured  $Y_{ae}$  in porcine lung using cavitation rheology ( $6.1 \pm 1.6$  kPa), small amplitude oscillatory shear rheometry ( $3.3 \pm 0.5$ ), micro-indentation ( $1.4 \pm 0.4$ ), and uniaxial tension ( $3.4 \pm 0.4$ ) and showed that all these techniques provided values in the same range. Using AFM, Liu and Tschumperlin (2011) estimated a value around 5 kPa for mice, while Jorba et al. (2019) obtained values around 10 kPa at low strain in rats. Cavalcante et al. (2005) used their network model to estimate the effective alveolar wall stiffness to be  $\sim 5$  kPa. Assuming that collagen fibers are the primary load bearing constituents of the wall, they also estimated fiber tensile elastic modulus to be  $\sim 300$  kPa, which is similar to the average modulus in mice provided by our analytical model (Table 2) even though our estimate is an ensemble value including both elastin and collagen fibers. Furthermore, the elastic modulus of single elastin fibers is around 410 kPa (Aaron

**TABLE 2 |** Aging results showing mean and standard errors with respective *p*-values for young and old mice.

Modulus (kPa)	Young ( <i>n</i> = 5)	Old ( <i>n</i> = 6)	<i>p</i> -value
$Y_{ae}$	4.36 ± 0.45	5.86 ± 1.35	0.043
$Y_{be}$	0.114 ± 0.001	0.161 ± 0.066	0.77
$Y_a$	12.44 ± 1.14	15.49 ± 3.53	0.094
$Y_b$	0.42 ± 0.25	0.46 ± 0.17	0.77
$Y_f$	311 ± 29	620 ± 131	0.001

Model fitted values for  $Y_{ae}$  and  $Y_{be}$  were used to derive  $Y_a$ ,  $Y_b$ , and  $Y_f$ .  $Y_a$  = average alveolar tensile elastic modulus;  $Y_b$  = average alveolar wall bond-bending elastic modulus;  $Y_f$  = average fiber tensile elastic modulus.

and Gosline, 1981). This is similar to the values of  $Y_f$  we obtained in mice in the present study (Table 2), perhaps because the delayed recruitment of flaccid collagen fibers causes elastin to be the primary determinant of stress at low strain (Mead, 1961).

The elastic moduli of the alveolar wall and the load-bearing fiber estimated by the analytical model both increased with age (Table 2), as did the stiffness of the tissue itself (Figure 7). Thus, even though the fiber content of the alveolar wall was reduced in the older mice, the fibers themselves were actually stiffer, something that can be attributed to the increased protein fiber cross-linking that is known to occur with age (Reiser et al., 1987; Snedeker and Gautieri, 2014). This implies that the increased lung compliance that occurs with age (Knudson et al., 1977; Suki and Bartolák-Suki, 2015) must be a reflection of age-related increase in airspace dimensions (Thurlbeck, 1967). More importantly, however, this finding also suggests that cells in the aging lung will experience an increased stiffening of the ECM substrate upon which they live, which has implications for cellular signaling and senescence (Suki and Bartolák-Suki, 2015).

Our analytical model thus recapitulates key experimental observations made in lung tissue strips and provides estimates of constitutive tissue properties that are consistent with experimental measurement and prediction by other models. These findings must nevertheless be viewed in light of the model limitations, which relate principally to the assumptions inherent in it. For example, a fundamental assumption of the model, made in the interests of mathematical tractability, is that alveolar walls can be represented as components that do not interact except insofar as to collaborate in the generation of bond-bending forces through their relative orientations. In other words, the orientation of a given wall is assumed not to influence the orientations of any of the neighboring walls to which it is connected. While this might seem open to question, the estimates of elastic modulus obtained by fitting the model to data generated by a numerical model compare well both to the parameters (Figure 4) and to wall angles and strains (Figure 5) in the numerical model even though the analytical model is not capable of recapitulating network effects that can take place in the numerical model.

Concerning validation by comparing the model to another model, we note the following. If an analytical model is developed with simplifying assumptions, it is often the case

that such a model is compared to a more sophisticated numerical model that accounts for mechanisms that are necessarily omitted from the analytic approach. Since Cavalcante et al. (2005) did verify their model experimentally, we chose this model to investigate how network effects influenced the current model.

Another important simplifying assumption in the analytical model is that the stress-strain behavior of the alveolar wall is linear with a constant elastic modulus. A recent study used atomic force microscopy (AFM) to measure alveolar septal wall stiffness in decellularized rat lung tissue and found that indentation stiffness increased from about 10 kPa at 0 strain to about 80 kPa at 0.3 strain (Jorba et al., 2019). While the mechanism underlying this non-linear behavior remains unclear, one possibility is that it reflects the progressive straightening of flaccid fibers (Sobin et al., 1988; Mercer and Crapo, 1990; Toshima et al., 2004). Elastin fibers are generally presumed not to be flaccid under any conditions, so the flaccid fibers are probably collagen (Mercer and Crapo, 1990; Chen et al., 2013; Chow et al., 2014). Another possible explanation for the AFM results is geometric; the opposing force on a probe pushing perpendicular to a fiber under tension is due to the vector component of the tension in the fiber that is generated against the probe as the fiber bends. It is also possible that the stress-strain behavior of the fiber itself is actually non-linear. This behavior could be incorporated into the model at the expense of increased model complexity. As an example, the elastic moduli could be modeled using a polynomial equation to capture waviness or fiber stiffening. Even though this additional complexity might not have an analytical solution and thus would need to be solved numerically, the same geometrical considerations and energy minimization principles still hold and are applicable. Thus, in relation to the present study, it must be noted that the modulus parameters estimated by the analytical model represent averages of the tensile and bond-bending moduli of a large population of alveolar walls.

The analytical model also assumes affine kinematics, meaning that microstrains occurring in small parcels of tissue mirror the macrostrains of the tissue as a whole. This does not, however, apply to individual alveolar walls, which move according to their respective initial orientations. These orientations vary widely throughout the tissue, as they do in the numerical network model (Cavalcante et al., 2005), and also as found experimentally; alveolar wall segments violate the affine deformation assumption during uniaxial stretching (Brewer et al., 2003).

In summary, we have developed an analytical model that establishes a link between the mechanical behavior of lung tissue at the macroscopic tissue level and alveolar wall scale. Matching the model predictions to experimental data provides realistic values for the tensile and bond-bending moduli of individual alveolar walls, as well as their changes with age, collagen content, and matrix charge density. The model thus provides a potential platform upon which to understand how disease processes and aging affect lung function, and how interventions such as mechanical ventilation might be optimized to avoid damaging the tissue or avoid aberrant mechanotransduction of the cells contained within it.

## DATA AVAILABILITY STATEMENT

The datasets generated for this study and the model as an executable file are available on request to the corresponding author.

## ETHICS STATEMENT

The animal study was reviewed and approved by Institutional Animal Care and Use Committee of Boston University.

## AUTHOR CONTRIBUTIONS

SB, BS, and JB contributed to model development. AT collected data for the young and old mouse study. SB contributed to forward simulations and experimental data fitting. SB and BS contributed to data analysis. SB, BS, and JB

contributed to writing the manuscript. All authors approved the submitted manuscript.

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## SUPPLEMENTARY MATERIAL

The Supplementary Material for this article can be found online at: <https://www.frontiersin.org/articles/10.3389/fphys.2020.00121/full#supplementary-material>

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**Conflict of Interest:** The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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# A Physiologically Informed Strategy to Effectively Open, Stabilize, and Protect the Acutely Injured Lung

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Acute respiratory distress syndrome (ARDS) causes a heterogeneous lung injury and remains a serious medical problem, with one of the only treatments being supportive care in the form of mechanical ventilation. It is very difficult, however, to mechanically ventilate the heterogeneously damaged lung without causing secondary ventilator-induced lung injury (VILI). The acutely injured lung becomes *time* and *pressure* dependent, meaning that it takes more time and pressure to open the lung, and it recollapses more quickly and at higher pressure. Current protective ventilation strategies, ARDSnet low tidal volume (LVt) and the open lung approach (OLA), have been unsuccessful at further reducing ARDS mortality. We postulate that this is because the LVt strategy is constrained to ventilating a lung with a heterogeneous mix of normal and focalized injured tissue, and the OLA, although designed to fully open and stabilize the lung, is often unsuccessful at doing so. In this review we analyzed the pathophysiology of ARDS that renders the lung susceptible to VILI. We also analyzed the alterations in alveolar and alveolar duct mechanics that occur in the acutely injured lung and discussed how these alterations are a key mechanism driving VILI. Our analysis suggests that the *time* component of each mechanical breath, at both inspiration and expiration, is critical to normalize alveolar mechanics and protect the lung from VILI. Animal studies and a meta-analysis have suggested that the time-controlled adaptive ventilation (TCAV) method, using the airway pressure release ventilation mode, eliminates the constraints of ventilating a lung with heterogeneous injury, since it is highly effective at opening and stabilizing the *time*- and *pressure*-dependent lung. In animal studies it has been shown that by “casting open” the acutely injured lung with TCAV we can (1) reestablish normal expiratory lung volume as assessed by direct observation of subpleural alveoli; (2) return normal parenchymal microanatomical structural support, known as alveolar interdependence and parenchymal tethering, as assessed by morphometric analysis of lung histology; (3) facilitate regeneration of normal surfactant function measured as increases in surfactant proteins A and B; and (4) significantly increase lung compliance, which reduces the pathologic impact of driving pressure and mechanical power at any given tidal volume.

**Keywords:** ARDS, VILI (ventilator induced lung injury), mechanical ventilation, APRV, alveolar mechanics

## INTRODUCTION

Acute respiratory distress syndrome (ARDS) was initially thought to be a lethal double pneumonia and was identified as a syndrome by Ashbaugh et al. (1967). Unfortunately, in the 50 years since ARDS was identified, only a few treatments have been used, with the mainstay being supportive in the form of mechanical ventilation (Slutsky and Ranieri, 2013). However, mechanical ventilation constrained to the limitations of a heterogeneously injured lung can cause unintended tissue damage, referred to as ventilator-induced lung injury (VILI), which can significantly increase mortality (~40%) as compared to lung protective ventilation (~31%) (Acute Respiratory Distress Syndrome Network, 2000). Initial randomized controlled trials (RCTs) attempting to reduce VILI by lowering tidal volume (Vt) failed to reduce mortality (Stewart et al., 1998; Brower et al., 1999). It was not until the ARDS Network (ARDSnet) conducted the seminal ARMA study, published in 2000, that a reduction in mortality was shown (Acute Respiratory Distress Syndrome Network, 2000). However, most (Phua et al., 2009; Villar et al., 2011; Caser et al., 2014; Bellani et al., 2016; Laffey et al., 2016; Villar et al., 2016; Maca et al., 2017; Raymonds et al., 2017; Rezoagli et al., 2017; Fan et al., 2018; McNicholas et al., 2018; Pham et al., 2019; Shen et al., 2019) but not all (Brun-Buisson et al., 2004; Fan et al., 2005; Putensen et al., 2009; Petrucci and De Feo, 2013; Shen et al., 2019) of the recent statistical- and meta-analyses have shown that ARDS mortality has not been reduced below the 31% “gold standard” of the 2000 ARMA study but rather remains unacceptably high at ~40% (**Figure 1**). Despite these disappointing results, the low-Vt ARDSnet method is still recommended as the standard-of-care protective ventilation strategy for ARDS patients (Fan et al., 2017, 2018; Papazian et al., 2019).

Since outcome data for ARDS patients has not improved for almost 20 years, it is imperative to (1) ascertain the mechanisms of dynamic alveolar and alveolar duct volume change during mechanical ventilation (elastic, viscous, or viscoelastic), (2) characterize ARDS-induced changes in alveolar mechanics (i.e., the dynamic change in alveolar size and shape during mechanical ventilation) (Grune et al., 2019) that drive VILI-induced tissue damage, (3) identify the role of airway pressure and the duration at both inspiration and expiration on alveolar mechanics in the acutely injured lung (Kollisch-Singule et al., 2014a, 2018), and (4) use this knowledge to develop novel ventilation strategies to better reduce VILI and protect the lung. Although pulmonary inflammation (biotrauma) also plays a critical role in ARDS and VILI pathogenesis, the focus of this review will be the mechanical injury to tissue caused during ventilation.

## CONSTRAINTS OF VENTILATING THE ACUTELY INJURED LUNG

The current concept is that ARDS causes heterogeneous injury in three general lung compartments that are layered by gravity (**Figure 2**). The first compartment, or the non-dependent area, contains a small number of normal compliant alveoli that remain

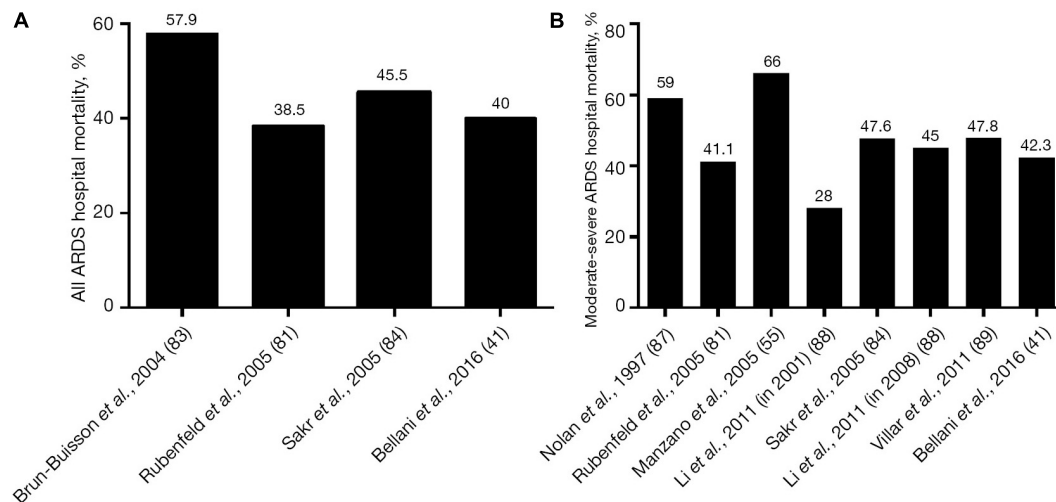
inflated at end-expiration—functional residual capacity (FRC)—and is referred to as the “baby lung” (Gattinoni and Pesenti, 2005). The second compartment consists of alveoli in the dependent areas that are collapsed and/or edema filled. The third compartment consists of alveoli that remain in the transition zone between healthy and unstable, due to loss of surfactant function, and that open and collapse with every breath.

Consequently, the ARDSnet low-Vt and plateau pressure (Pplat) strategy is constrained to ventilating this heterogeneous lung tissue without causing VILI using a three-tiered approach: (1) *protect* the baby lung by not overdistending the compliant tissue that is open at FRC, (2) *rest* the dependent collapsed and edema-filled tissue by keeping it out of the ventilatory cycle, and (3) *stabilize* the tissue in between by applying positive end-expiratory pressure (PEEP), usually adjusted by oxygenation (**Figure 2**) (Acute Respiratory Distress Syndrome Network, 2000; Del Sorbo et al., 2017).

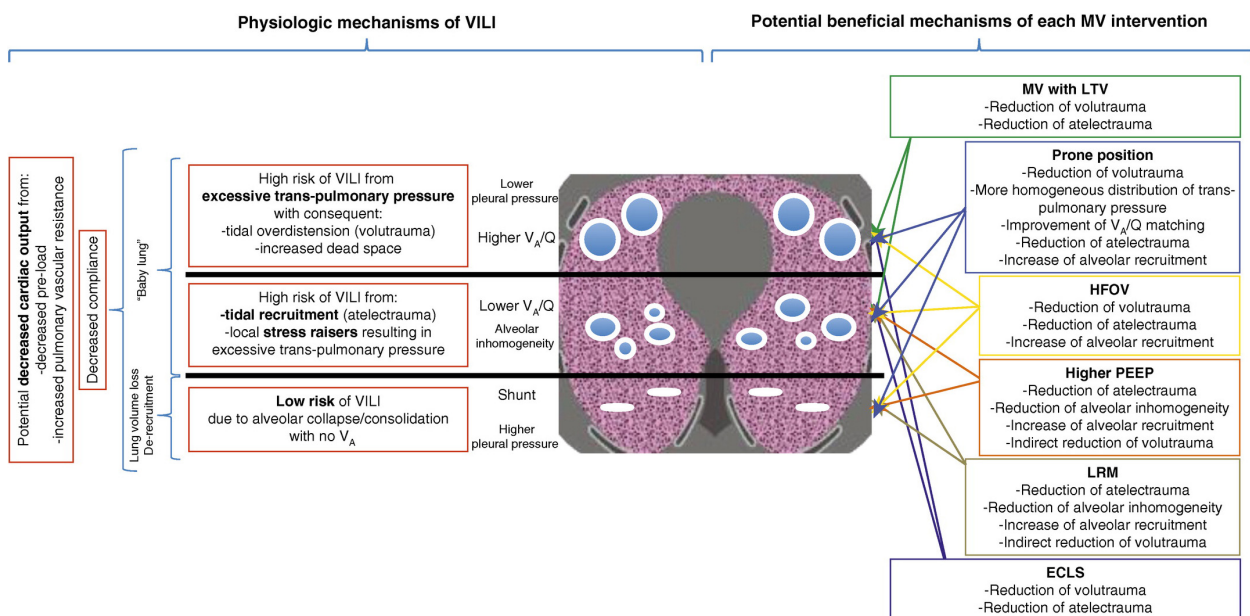
## Problems With Protecting the Baby Lung

Since the baby lung is believed to be a small volume of normal tissue (Gattinoni and Pesenti, 2005), its overdistension has been postulated to be a primary VILI mechanism (Brower et al., 2004). However, in studies in which normal lungs were subjected to excessively high airway pressures (>30 cm H<sub>2</sub>O) and strain (2.5 ratio), overdistension-induced VILI did not occur as long as this excessive strain was nearly static. This suggests that overdistension of normal tissue with high volume and pressure is not a primary VILI mechanism unless there is also a large dynamic strain (Seah et al., 2011; Protti et al., 2013b; Jain et al., 2017). It is possible that the baby lung is injured not by overdistension of the normal tissue, but rather by the recruiting and recollapse of unstable tissue in the adjacent collapsed regions (Gattinoni et al., 1995). Thus, lowering Vt and Pplat to reduce overdistension in the open lung tissue, which is surrounded by a large volume of collapsed and unstable tissue of very low compliance, may not reduce VILI. Regional instability and inflammation occur throughout the entire lung, including in tissue that appears to be normal on computed tomography (CT) scan or chest X-ray, and serve as pathologic focal points from which VILI-induced tissue damage expands (Wellman et al., 2014, 2016; Cereda et al., 2016b, 2017). This suggests that to protect the normal lung tissue regional instability must be eliminated.

However, others have shown that overdistension is a major component of VILI pathophysiology in injured lungs (Guldner et al., 2016). Guldner et al. (2016), in a porcine ARDS model, showed that extreme conditions of overdistension resulted in more lung inflammation than did extreme lung collapse, suggesting that static stress and strain are major VILI mechanisms. Although this study clearly showed that volutrauma increased inflammation, histopathology was not measured, and there was no difference in pulmonary edema as measured by lung weight. Thus, it is not clear whether the increase in inflammation caused any lung pathology. In addition, recalculation of the data showed that the average mechanical power in the volutrauma group was 17.12 J/min, more than double that of the atelectrauma group (7.13 J/min) (Tonetti et al., 2017). Others have also



**FIGURE 1 | (A)** Hospital mortality (%) in the main epidemiological studies for all three American-European Consensus Conference (AECC) classifications of acute respiratory distress syndrome (ARDS – mild, moderate, and severe) and **(B)** mortality (%) for only moderate and severe ARDS. The mean and standard deviation for mortality in all of the studies following the 2000 ARMA study (Acute Respiratory Distress Syndrome Network, 2000) is  $45.4 \pm 9.5$  (Rezoagli et al., 2017). Permissions obtained from AME Publishing Company, License ID 1017423-1.



**FIGURE 2 |** Gravity dependent three-compartment model of acute respiratory distress syndrome (ARDS) pathology: **Left** – Physiological mechanisms of ventilator-induced lung injury (VILI) and **Right** – Potential beneficial mechanisms of various protective ventilation strategies to minimize VILI. Open alveoli are shown as blue circles similar in size (top), unstable alveoli as smaller circles of various sizes (middle), and collapsed alveoli as solid white lines (bottom). The ARDSnet low tidal volume (LTV) method is designed to *protect* compliant open alveoli in the non-dependent lung and *rest* the collapsed tissue in the dependent portion of the lung by keeping it unventilated. Positive end-expiratory pressure (PEEP) is added in an attempt to *stabilize* the alveoli in between (Acute Respiratory Distress Syndrome Network, 2000). High-frequency oscillatory ventilation (HFOV) and lung recruitment maneuvers (LRMs) have been shown ineffective in reducing ARDS mortality (Brower et al., 2004; Meade et al., 2008; Mercat et al., 2008; Ferguson et al., 2013; Young et al., 2013; Cavalcanti et al., 2017; Hodgson et al., 2019). Prone position has been shown effective at reducing mortality (Guerin et al., 2013) by a mechanism of reducing regional alveolar strain and inflammation (Motta-Ribeiro et al., 2018; Xin et al., 2018). VILI, ventilator-induced lung injury; MV, mechanical ventilation; LTV, low tidal volume and inspiratory pressure; PEEP, positive end-expiratory pressure; ECLS, extracorporeal life support; HFOV, high-frequency oscillatory ventilation; LRM, lung recruitment maneuver; Q, perfusion;  $V_A$ , alveolar ventilation;  $V_A/Q$ , ventilation/perfusion ratio; baby lung, functional residual capacity (FRC) (Del Sorbo et al., 2017). Permissions to publish obtained from ATS.



shown that increasing airway pressure in an acutely injured lung will cause a rapid progression of injury in a “rich-get-richer” power-law fashion, supporting the findings in the Guldner study (Hamlington et al., 2018). Combined, these studies suggest that high static stress and strain are associated with volutrauma in acutely injured lung tissue but not in normal lung tissue.

## Problems With Resting the Collapsed Lung

When the lung is allowed to collapse below normal FRC, atelectatic, and edema-filled *resting* tissue (1) does not exchange gas; (2) is susceptible to the development of pneumonia (Huynh et al., 2019; Li Bassi et al., 2019); (3) will become fibrotic if not reopened (Burkhardt, 1989; Cabrera-Benitez et al., 2014; Lutz et al., 2015); (4) initiates patient-ventilator dyssynchrony, which is caused by the firing of mechanical stretch, PO<sub>2</sub>, PCO<sub>2</sub>, and pH receptors (Solomon et al., 2000; Manning and Mahler, 2001; Widdicombe, 2001; Mellott et al., 2009; Burki and Lee, 2010; Yu, 2016; Yoshida et al., 2017) and which is associated with high mortality (Blanch et al., 2015); and (5) creates a stress-focus in the adjacent open alveoli and alveolar ducts, greatly amplifying the forces applied to these parenchymal tissues during tidal ventilation (Mead et al., 1970; Gattinoni et al., 2012; Cressoni et al., 2014; Makiyama et al., 2014; Retamal et al., 2014). It has been shown that letting the lung *rest* in obese bariatric surgery patients is associated with worse oxygenation, longer post-anesthesia care unit stay, and more post-operative pulmonary complications as compared with patients in which the atelectatic *resting* lung was opened and ventilated (Talab et al., 2009). Although, the phrase *resting* the lung sounds protective, the lung is not meant to function in a deflated state, and as listed above, such a state is associated with numerous pathologies. If the lung is to be *rested*, meaning that parenchymal tissue is to be kept from being damaged by mechanical ventilation, the better strategy would be to *rest* it in the natural inflated state (Nieman et al., 2018).

## Problems With Stabilizing the Lung

There is no consensus on how best to set PEEP to effectively *stabilize* lung tissue (Coruh and Luks, 2014; Gattinoni et al., 2017; Nieman et al., 2017a; Bergez et al., 2019). The current ARDSnet method for setting PEEP uses a sliding scale of oxygenation (Acute Respiratory Distress Syndrome Network, 2000), but increased oxygenation does not correlate well with an increase in alveolar stability (Andrews et al., 2015), a key VILI mechanism (Wellman et al., 2014, 2016; Cereda et al., 2016b, 2017). Many methods have been used in an attempt to titrate the PEEP to stabilize lung tissue. These methods include using dead space, lung stress and strain, lung compliance, CT, pressure-volume curve inflection points, and electrical impedance tomography, but there is no current bedside technique to determine whether the set PEEP has actually stabilized the lung (Nieman et al., 2017a). The above problems with the ARDSnet *protect*, *rest*, and *stabilize* method may partially explain the lack of improved outcome in ARDS mortality over the last 20 years (Figure 1) (Brun-Buisson et al., 2004; Phua et al., 2009; Villar et al., 2011;

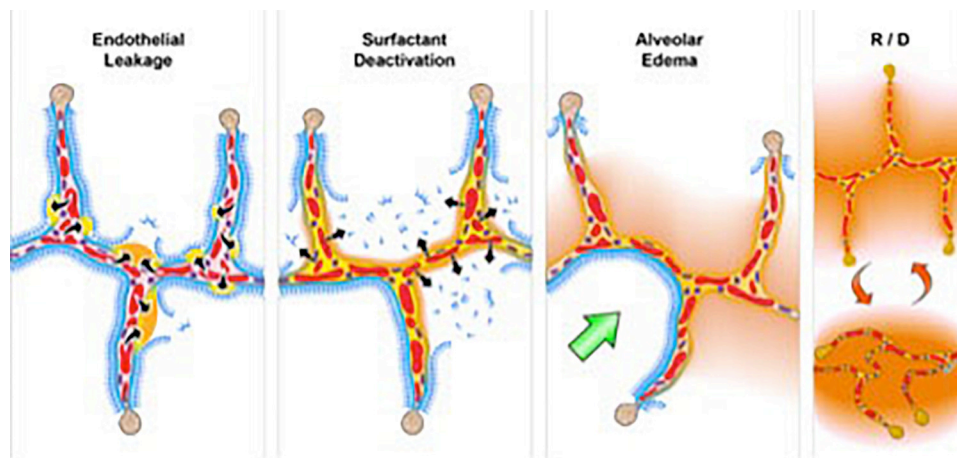
Caser et al., 2014; Bellani et al., 2016; Laffey et al., 2016; Villar et al., 2016; Maca et al., 2017; Raymonds et al., 2017; Rezoagli et al., 2017; Fan et al., 2018; McNicholas et al., 2018; Pham et al., 2019). By allowing the lung to remain heterogeneously collapsed, the *protect*, *rest*, and *stabilize* method is unintendedly preserving the constraints of ventilating the heterogeneously injured lung, which is nearly impossible to do without causing some degree of VILI.

## Open Lung Approach (OLA) as a Protective Strategy

The goal of the open lung approach (OLA) is to eliminate the constraints of ventilating a heterogeneously injured lung by normalizing all three pathologic compartments (Figure 2). The aim is to reinflate the collapsed tissue using a recruitment maneuver (RM) and to keep it open by using an appropriate level of PEEP. If the entire lung could be recruited and recollapse prevented, the main VILI mechanical mechanisms (dynamic strain and overdistension of alveolar walls in areas of stress-focus) would be eliminated (Nieman et al., 2017b). An RM is an acute event performed by raising the airway pressure (30–40 cm H<sub>2</sub>O) and holding it for ~40 s (Fan et al., 2008) or by greatly increasing PEEP (25 cm H<sub>2</sub>O) and combining it with 15 cm H<sub>2</sub>O of driving pressure above the PEEP (Borges et al., 2006). In the latter strategy, PEEP is increased in 5 cm H<sub>2</sub>O increments up to 45 cm H<sub>2</sub>O until the lung fully recruits, which was confirmed when PaO<sub>2</sub> + PaCO<sub>2</sub> > 400 mmHg (Borges et al., 2006).

Following the RM, PEEP is titrated downward to find the lung recollapse point (usually by a sharp fall in lung compliance), and then PEEP is set 2 cm H<sub>2</sub>O above this collapse pressure, following a second RM. However, multiple RCTs testing the OLA in ARDS patients have failed to show significant benefits over standard of care (Brower et al., 2004; Meade et al., 2008; Mercat et al., 2008; Cavalcanti et al., 2017; Hodgson et al., 2019). Reasons for these failures include the following: (1) timing of OLA application [early (Borges et al., 2006) vs. late (Gattinoni et al., 2006)] (2) one-size-fits-all RM strategies, (3) PEEP set inappropriately to keep the recruited lung open, (4) recruiting pressures insufficient to open all of the lung, (5) a patient population of responders (lung recruits) and non-responders (lung does not recruit) (Gattinoni et al., 2006), and (6) application of OLA not as a continuous treatment but rather as a one-time event with a long time period before a second application or with no second application at all (Goligher et al., 2017; Lu et al., 2017; Bhattacharjee et al., 2018; Cui et al., 2019; Hodgson et al., 2019; Kang et al., 2019; van der Zee and Gommers, 2019; Zheng et al., 2019). Most (Bhattacharjee et al., 2018; Cui et al., 2019; Hodgson et al., 2019; Kang et al., 2019; Zheng et al., 2019) but not all (Goligher et al., 2017; Lu et al., 2017) meta-analyses have shown no decrease in ARDS-related mortality associated with the OLA.

To further reduce ARDS mortality and acute lung injury, two pathologic processes must be understood: (1) the pathophysiology of ARDS that predisposes the lung to a secondary VILI and (2) the mechanisms of VILI in the microenvironment (i.e., the terminal airspaces, alveoli, and alveolar ducts). This knowledge informs the design of a



**FIGURE 3 |** The *pathologic tetrad* of acute respiratory distress syndrome (ARDS). Alveolar walls contain pulmonary capillaries (red circles) and are lined with a liquid hypophase (blue layer inside each alveolus), with an intact pulmonary surfactant layer (small blue ball with tail) layered on the hypophase. The systemic inflammatory response syndrome (SIRS) secondary to sepsis, trauma, burns, pneumonia, and so on increases pulmonary capillary permeability. **Endothelial leakage:** increased microvascular permeability allowing pulmonary edema to move into the alveolus (black arrows and tan edema blebs) (Martin and Brigham, 2012). **Surfactant deactivation:** the continuous layer of pulmonary surfactant molecules is disrupted as the edema blebs expand causing surfactant deactivation (surfactant sluffing off into the alveolar space). Edema usurping surfactant from the alveolar surface, the proteins in the edema fluid deactivating the surfactant (Taeusch et al., 2005), and improper mechanical ventilation (Albert, 2012) causing further surfactant disruption all combine to exacerbate surfactant loss. **Alveolar edema:** increased capillary permeability (Martin and Brigham, 2012) and high alveolar surface tension combine to flood alveoli with edema fluid (tan). **Recruitment/derecruitment (R/D):** loss of surfactant function results in increased alveolar surface tension causing loss of alveolar stability (i.e., causing alveolar R/D with each breath). Alveoli in the top frame of R/D are fully inflated but collapse during expiration in the bottom R/D frame. Alveolar R/D, known as atelectrauma, is another key VILI mechanism (Cressoni et al., 2017). **Stress-focus:** edema-filled or collapsed alveoli adjacent to air-filled alveoli create a stress-focus causing the alveolar wall to bend toward the fluid-filled alveolus (green arrow), which can cause stress failure at the alveolar wall (Perlman et al., 2011). Stress-focus is another key mechanism of VILI (Perlman et al., 2011; Chen et al., 2014; Makiyama et al., 2014; Retamal et al., 2014). Thus, the *pathologic tetrad* sets up a vicious cycle of high microvascular permeability → edema → surfactant deactivation → high alveolar surface tension → more edema → alveolar R/D → further increase in microvascular permeability → severe ARDS (Nieman and Bredenberg, 1985).

protective mechanical breath that will allow the lung to heal by eliminating the constraints present when ventilating a heterogeneously injured lung (Nieman et al., 2018).

## ARDS PATHOPHYSIOLOGY THAT PREDISPOSES THE LUNG TO VILI

### ARDS Is a Pathologic Tetrad

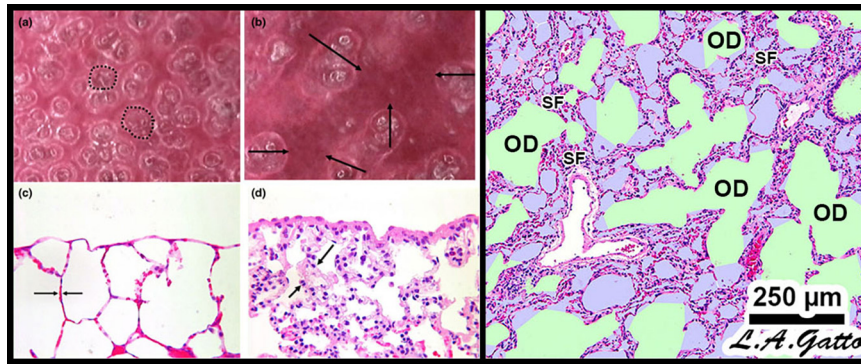
To investigate the relationship between ARDS and VILI, we need to understand the pathology of acute lung injury. Although ARDS is a complex syndrome, it features four well-accepted central components (Thompson et al., 2017) known as the “pathologic tetrad” (Figure 3) (Nieman et al., 2018). The components of the tetrad include *increased pulmonary capillary permeability* (Figure 3, Endothelial Leakage), which if unchecked will lead to *loss of surfactant function* (Figure 3, Surfactant Deactivation) (Lewis et al., 1993). The resultant high alveolar surface tension will exacerbate the permeability-induced increase in *alveolar flooding* with edema fluid (Figure 3, Alveolar Edema) (Nieman and Bredenberg, 1985). Surfactant dysfunction will alter alveolar mechanics, resulting in alveolar *recruitment/derecruitment (R/D)* with each breath (Figure 3, R/D) (Schiller et al., 2001). Each component of the tetrad has a profound impact on alveolar mechanics. Surfactant deactivation sets the stage for a secondary VILI by promoting heterogeneous

lung tissue instability and collapse. In addition, surfactant secretions from type II cells would be inhibited in collapsed areas that are not being stretched during ventilation (Wirtz and Dobbs, 1990; Majumdar et al., 2012). Reduced surfactant secretion would exacerbate and perpetuate the already reduced surfactant function caused by alveolar flooding with edema.

## VILI MECHANISMS: HETEROGENEOUS ALVEOLAR INSTABILITY AND COLLAPSE

The hallmark of ARDS is a heterogeneous lung injury encompassing normal, collapsed, edematous, and unstable tissues (Figure 2). This pathology alters pulmonary microanatomy and dynamic alveolar inflation physiology, generating three basic VILI mechanisms: *volutrauma* (overdistension of airways), *atelectrauma* (R/D of alveoli), and *biotrauma* (inflammation) (Thompson et al., 2017). From an engineering perspective, volutrauma is caused by excessive static strain and atelectrauma by excessive dynamic strain (Seah et al., 2011; Protti et al., 2013a,b, 2014). In this review we do not discuss biotrauma but rather focus on the unintentional mechanical damage to the pulmonary parenchyma caused during mechanical ventilation.

Mechanical ventilation of the acutely injured lung with altered alveolar opening and collapse time constants can cause tissue



**FIGURE 4 |** Mechanical mechanisms of ventilator-induced lung injury (VILI) in the microenvironment: Left – *In vivo* subpleural alveoli in an acutely injured rat lung at inspiration (a) and expiration (b). Lung histology in the same rat lung injury model fixed at inspiration (c) and expiration (d) (Pavone et al., 2007). *Alveolar recruitment/derecruitment (R/D)* causing atelectrauma can be seen as fully recruited alveoli filling the microscopic field (white circles, two of which are highlighted with black dotted line) (a) that collapse during expiration (red atelectatic areas highlighted by arrows) (b). Histology shows open alveoli at inspiration with a shared alveolar wall highlighted by arrows (c) that collapse with expiration by alveolar wall folding, identified by arrows. Right – *Stress-focus (SF)* in areas with collapsed alveoli. SF adjacent to open alveolar ducts, causing alveolar duct *overdistension (OD)*. SF-induced OD causes excessive mechanical stress and strain on alveolar duct walls, resulting in damage to pulmonary parenchymal cells (Ghadiali and Gaver, 2008). Loss of surfactant function results in alveolar instability (Figure 3, R/D). Histology at exhalation in a rat Tween-induced surfactant deactivation model with a tidal volume of 6 ml/kg and a PEEP of 5 cm H<sub>2</sub>O. Note the heterogeneous collapse of alveoli causing areas of stress-focus (SF). Adjacent to these areas of SF are overdistended (OD) alveolar ducts (Kollisch-Singule et al., 2014b). Summary – R/D causes excessive normal or “peeling” stress as the adhered alveolar walls peel apart during inflation; both R/D and SF cause OD in adjacent open stable tissue. This excessive stress and strain on alveolar walls results in lung parenchymal cell death and is a major VILI mechanism. Permissions obtained to reuse panels (a–d) (Pavone et al., 2007). Springer Nature license number 4766000130978.

stress-failure by the following mechanisms: (1) alveolar R/D-induced excessive stress on the epithelial cells as the alveolar walls in apposition peel apart (Bilek et al., 2003), (2) stress-focusing in areas of open alveoli adjacent to collapsed or edema fill alveoli (Gattinoni et al., 2012; Cressoni et al., 2014; Retamal et al., 2014), and (3) collapsed tissue stretching and overdistending the shared walls of patent alveoli, as alveolar walls are interconnected (Figure 4) (Nieman et al., 2017b). Theoretically, if it were possible to minimize or prevent all of the above VILI mechanisms, ARDS associated mortality would be significantly reduced.

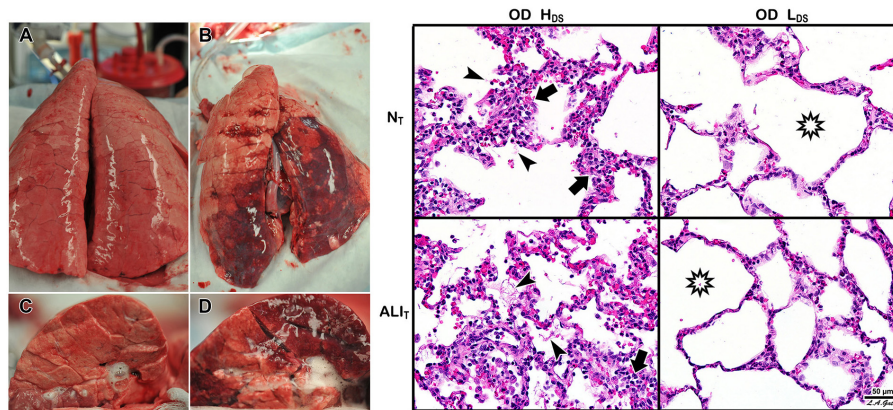
In normal pigs ventilated for 54 h, Protti et al. (2013b) examined the impact of high static strain and several levels of dynamic strain. They demonstrated that *high static strain*, using elevated PEEP and minimal Vt, caused little damage, but when PEEP was reduced, producing a *high dynamic strain*, it caused pulmonary edema and death. In subsequent work they showed that high static strain did not merely act as a dam to prevent edema formation by altering the Starling forces (i.e., increasing the pulmonary interstitial pressure) (Effros and Parker, 2009) but rather preserved the integrity of the alveolar-capillary membrane (Figure 3, Endothelial Leakage) (Protti et al., 2013a). These findings were supported by Jain et al. (2017) using a porcine heterogeneous lung injury model. They subjected two study groups to high static strain (Pplat = 40 cm H<sub>2</sub>O) that was believed to be more than sufficient to cause volutrauma-induced VILI (Acute Respiratory Distress Syndrome Network, 2000; Sahetya et al., 2017). Following heterogeneous lung injury, the animals in the second group were also subjected to high dynamic strain. High static strain did not injure normal open tissue (baby lung), nor did it exacerbate acutely injured tissue. However, combining high static strain with high dynamic strain caused significant

damage to both of these tissues (Figure 5). Further support for the contention that volutrauma of normal lung tissue is not a primary VILI mechanism comes from the Bates group, who showed that 4 h of mechanical ventilation in mice with high static strain was not associated with lung injury, but when it was combined with high dynamic strain, it caused VILI-induced tissue damage (Seah et al., 2011).

Protti et al. (2014) showed that a large dynamic strain (atelectrauma) is much more harmful to the normal lung than a large static strain (volutrauma), and when combined, the two work additively or synergistically to greatly accelerate tissue damage (Seah et al., 2011; Hamlington et al., 2016; Ruhl et al., 2019). In addition, the heterogeneous injury caused by ARDS establishes many areas of *stress-focus* between the open tissue and collapsed or unstable tissue and have been shown to double the stress and strain calculated for the entire lung (Cressoni et al., 2014). The impact that areas of stress-focus have on the forces generated on alveolar walls during ventilation was first described by Mead et al. (1970) and was more recently analyzed by Makiyama et al. (2014) using computer-simulated alveolar walls. This latter group demonstrated that a Pplat at the upper end of the “safe” level (30 cm H<sub>2</sub>O) could result in a local stress-focusing in individual alveolar walls of up to 48 cm H<sub>2</sub>O and could concentrate stress in an individual alveolar wall as much as 16-fold (Figure 6).

In summary, ARDS results in a heterogeneous loss of surfactant function (Figure 3, Surfactant Deactivation) and airway flooding (Figure 3, Alveolar Edema) that cause the lung to become *time and pressure dependent*, which means that the lung will collapse in a relatively short time at atmospheric pressure and will require a longer period of time to open





**FIGURE 5 |** Heterogeneous Tween Injury in pigs ventilated for 6 h. A bronchoscope was used to deliver Tween to the dependent areas of the diaphragmatic or caudal lung lobes. Thus, the upper lobes would be normal homogeneously inflated tissue (i.e., would simulate the baby lung), and the dependent areas of the caudal lobe would model acutely injured tissue that would be either collapsed or unstable during tidal ventilation. Using this injury model we can determine whether a ventilation strategy protects either normal tissue ( $N_T$ ) or acutely injured lung tissue ( $AL_T$ ), protects neither, or protects both. Two groups were studied. Both groups were subjected to a high static strain ( $P_{plat} = 40$  cm  $H_2O$ ) hypothesized to be sufficient to cause overdistension (OD)-induced VILI to the baby lung (Acute Respiratory Distress Syndrome Network, 2000). One group was also subject to high dynamic strain ( $H_{DS}$ ) and the other to low dynamic strain ( $L_{DS}$ ). The dynamic strain was adjusted using the airway pressure release ventilation (APRV) mode by changing the expiratory duration, which changed tidal volume size. Left – Gross photographs of the whole lung (A,B) and cut surface (C,D) of the diaphragmatic lung lobe. The  $L_{DS}$  group (A,C) showed minimal damage in both  $N_T$  and  $AL_T$  lung tissue (i.e., no dark red hepatized atelectasis). This was in contrast to the  $H_{DS}$  group, in which there was severe injury in both the  $N_T$  and  $AL_T$  lung tissues (B,D). Right – In the OD +  $H_{DS}$  group (OD +  $H_{DS}$ ), widespread histopathology typical of ARDS was seen, with inflammatory cell infiltration (arrows) and fibrin deposits (arrowheads) in both the  $N_T$  and  $AL_T$  lung tissue. In the OD +  $L_{DS}$  group, minimal histopathology was seen, and alveoli remained open (stars) in both  $N_T$  and  $AL_T$  lung tissue. These data support Protti et al.'s (2013b) work and demonstrate that normal lung tissue is highly resistant to static strain-induced volutrauma. In addition, this study showed that acutely injured lung tissue is also resistant to volutrauma as long as dynamic strain remains low. Both normal and acutely injured lung tissue are highly susceptible to high alveolar R/D-induced VILI when under high inflation pressure (Jain et al., 2017). These data support the rapid progression of lung injury in a power-law fashion when high static and dynamic strain are combined (Hamlington et al., 2018).

even at high inflation pressures (Takahashi et al., 2015). Mechanical ventilation can exacerbate the initial ARDS-induced inflammatory injury (Figure 3, Endothelial Leakage, Surfactant Deactivation, and Alveolar Edema) by generating excessive stress and strain on alveolar and alveolar duct walls resulting from a collapsing and reopening of alveoli and heterogeneous areas of stress-focusing in open tissue adjacent to collapsed or edema-filled tissue (Figure 4).

It is important to note that parenchymal overdistension following acute lung injury is a regional phenomenon and occurs only in open alveoli and alveolar ducts that are adjacent to the unstable or collapsed tissue (Figure 7, PEEP 16, PEEP 5, APRV 10%); it does not occur in homogeneously inflated acutely injured lung tissue (Figure 7, APRV 75%) (Nieman et al., 2017b). It has been shown that combining high pressure with alveolar instability greatly exacerbates tissue tearing in a rich-get-richer fashion (i.e., the larger the initial tear in the epithelial membrane the more that this tear will be expanded by increased airway pressure) (Figure 8) (Hamlington et al., 2016; Ruhl et al., 2019).

## VENTILATING WITHIN THE CONSTRAINTS OF AN ACUTELY INJURED LUNG

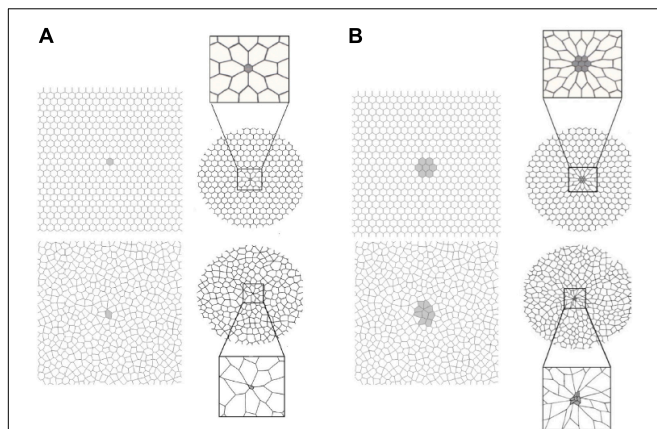
The ARDSnet method is a logical physiologically based lung ventilation strategy within the constraints of protecting a

heterogeneously injured lung. The better strategy would be to eliminate these constraints by opening and stabilizing the acutely injured lung or, better yet, by applying a protective ventilation strategy early and never letting the lung collapse (Satalin et al., 2018). Gattinoni and Pesenti stressed that in a patient with ARDS the  $V_t$  should not be set by body weight ( $V_t/kg$  ratio) but rather by the size of the remaining normal open tissue at FRC: the baby lung ( $V_t/baby$  lung volume ratio) (Gattinoni and Pesenti, 2005). They hypothesized that the baby lung was the small amount of open tissue at end-expiration (i.e., FRC) surrounded by a large volume of collapsed tissue with very low compliance. Since the specific elastance [ $E_{spec} = \text{transpulmonary pressure (Ptp)}/V_t \times \text{baby lung volume}$ , which is the airway pressure at which expiratory lung volume or FRC or baby lung volume doubles in size (i.e., when  $V_t/baby$  lung volume = 1)] if the baby lung is postulated to be normal, there would be a greater potential for overdistension in normal lung tissue because of the high compliance at any given level of static strain (Gattinoni and Pesenti, 2005). Both the potential of excessive stress (Ptp) to cause volutrauma and of excessive strain ( $V_t/\text{end-expiratory lung volume}$ ) to cause atelectrauma are linked with the following equation:

$$Ptp(\text{stress}) = E_{spec} \times (V_t/baby \text{ lung volume}).$$

(Eq. 1) (Gattinoni and Pesenti, 2005) (1)

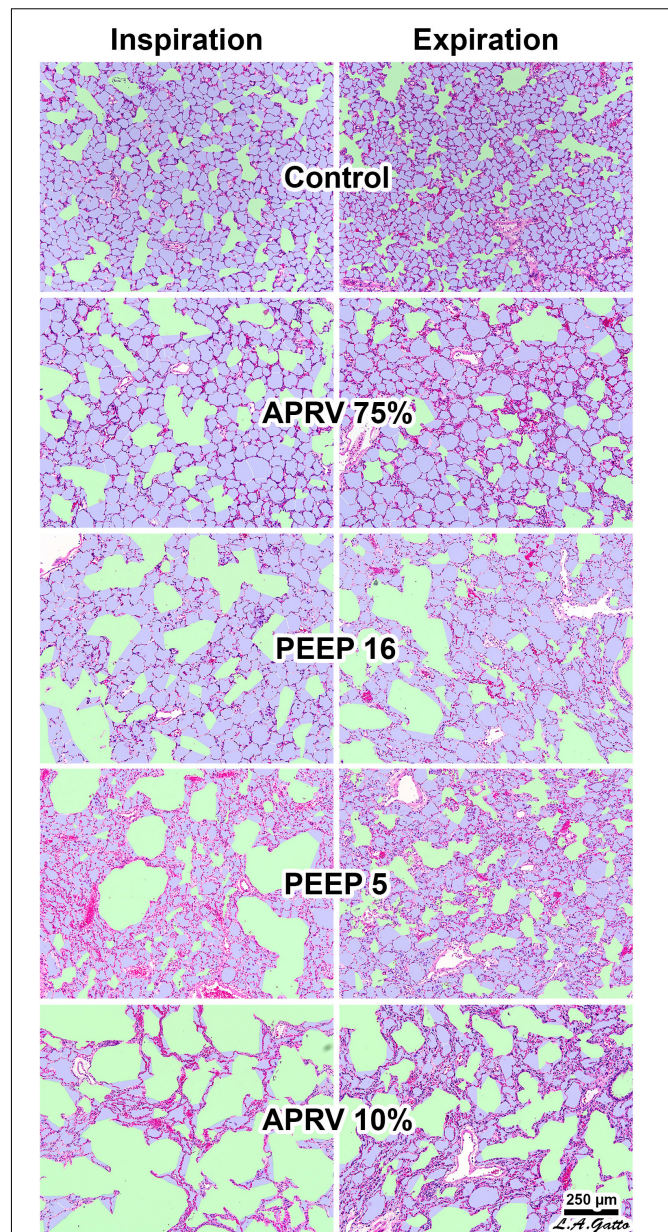




**FIGURE 6 |** A two-dimensional finite element computational model of interconnected alveolar walls to study the impact of areas of stress-focus (S-F) on stress-strain relationships. Both a hexagonal honeycomb (top) and Voroni honeycombs (bottom) were studied with areas of S-F created by increasing the stiff regions in one (A) or nine (B) cells. These stiff regions simulate collapsed alveoli adjacent to open alveoli that create an S-F in acute respiratory distress syndrome (ARDS) patients (Figure 4) (Cressoni et al., 2014). The entire honeycomb structure was expanded and exposed to strains of 15, 30, 45, and 55% above the resting geometry. Some of the alveolar walls in the Voroni honeycomb were exposed to a S-F  $\sim 16$  times greater than that applied to uniformly expanded areas. This suggests that ventilation pressures considered safe in ARDS patients ( $<30$  cm H<sub>2</sub>O) (Acute Respiratory Distress Syndrome Network, 2000) could be causing local stress concentration on some alveolar walls of approximately 48 cm H<sub>2</sub>O, with even higher stress in areas of S-F (Makiyama et al., 2014). Permissions obtained from Elsevier. License 4699410294890.

Gattinoni and Pesenti further concluded that the above equation suggests the baby lung must be treated gently, using low V<sub>t</sub>, low P<sub>tp</sub>, and proning so as not to cause volutrauma. Gently ventilating the lung should be protective, within the constraints of a heterogeneously injured lung (i.e., high E<sub>spec</sub> and low baby lung volume).

The current strategy of lung protection is designed to minimize normal tissue overdistention (low V<sub>t</sub>) and to stabilize (PEEP) injured tissue. Although the current hypothesis is that the primary mechanism of VILI is overdistention of the baby lung (Acute Respiratory Distress Syndrome Network, 2000), recent studies have demonstrated that high P<sub>tp</sub> does not result in injury to normal lung tissue (Seah et al., 2011; Protti et al., 2013a,b, 2014; Jain et al., 2017). Since much of the lung remains collapsed and unstable using the ARDSnet method, there are numerous areas of stress-focus, as PEEP adjusted by changes in oxygenation may not be adequate to prevent R/D (Baumgardner et al., 2002; Boehme et al., 2015). Even with low V<sub>t</sub>, tissue injury may occur regionally, since overdistention is not global but occurs in the microenvironment. Specifically, alveolar and alveolar duct overdistention occurs in open tissue surrounding a collapsed area of stress-focus or adjacent to areas of alveolar instability (Figures 4, 6, 7) (Mead et al., 1970; Cereda et al., 2011, 2013, 2016a; Kollisch-Singule et al., 2014b, 2018; Makiyama et al., 2014; Nieman et al., 2017b; Ruhl et al., 2019). Indeed, it has been shown that atelectasis, not high V<sub>t</sub>, causes overdistention



**FIGURE 7 |** Rat lungs fixed at inspiration and expiration in normal lungs (Control) and in a Tween lavage ARDS model with four ventilation strategies: (1) the TCAV method setting airway pressure release ventilation (APRV) with the expiratory flow termination (E<sub>FT</sub>) at 75% of expiratory flow peak (E<sub>FP</sub>) (E<sub>FT</sub>/E<sub>FP</sub> = 75%) (APRV 75%) (Habashi, 2005; Jain et al., 2016); (2) E<sub>FT</sub>/E<sub>FP</sub> = 10% (APRV 10%), which significantly increased expiratory time; (3) controlled mandatory ventilation (CMV) with low tidal volume (6 mL/kg) with 5 cm H<sub>2</sub>O positive end-expiratory pressure (PEEP 5); or (4) CMV with low tidal volume (6 mL/kg) with 16 cm H<sub>2</sub>O PEEP (PEEP 16). APRV 10% (not the TCAV method) significantly increased expiratory duration, allowing sufficient time for alveoli to collapse. The conducting airways are depicted in green; alveoli in lilac; and remaining interstitium, blood vessels, and lymphatics in magenta. The size of each microanatomical area was quantified using computer image analysis. In the Control group all alveoli were inflated surrounding normally distended alveolar ducts. Following Tween-induced ARDS, alveolar ducts in all ventilation groups were increased in size. In the CMV groups alveolar ducts were overdistended at both inspiration and

(Continued)

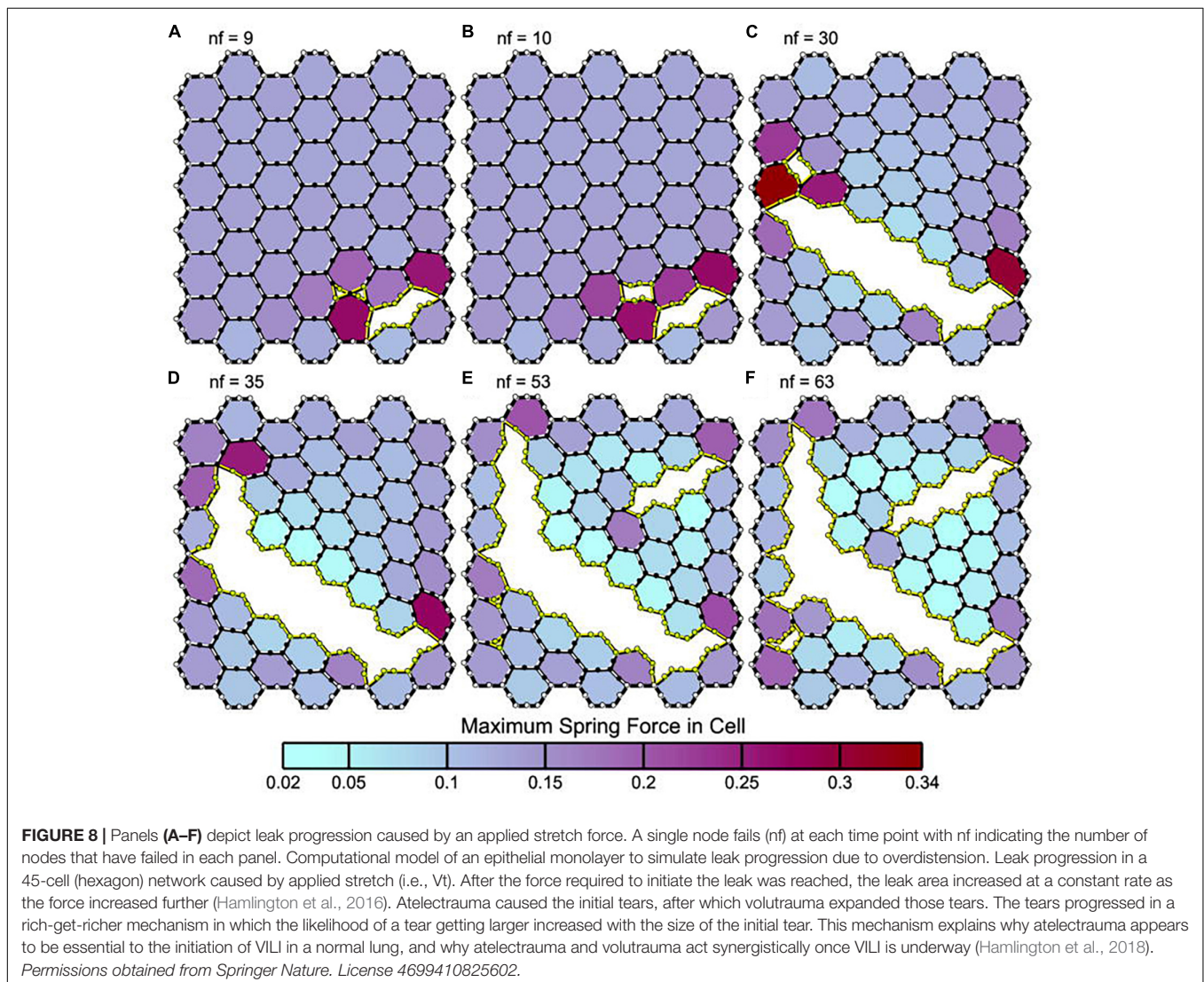


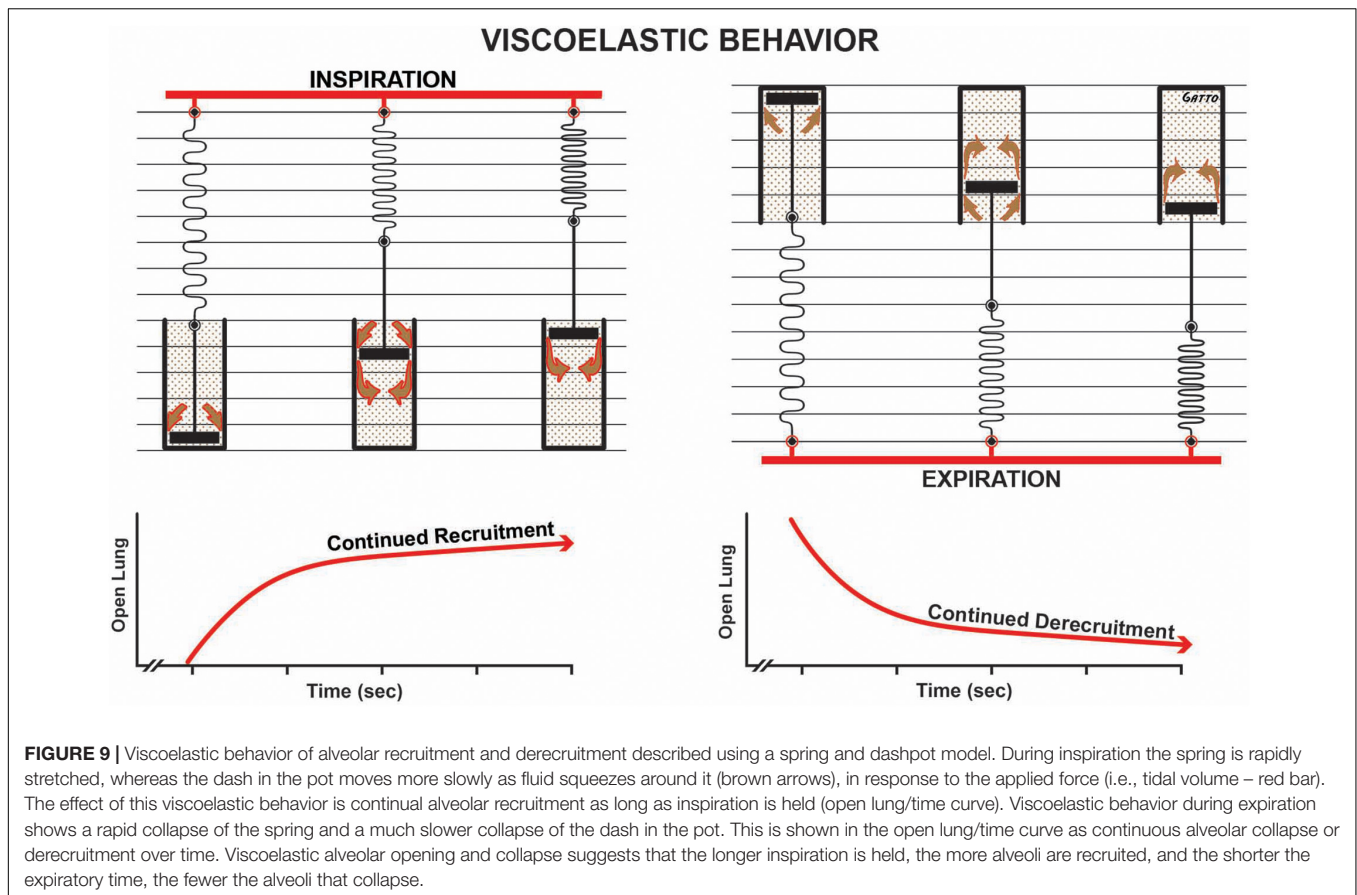
**FIGURE 7 | Continued**

expiration in **PEEP16**. In the **PEEP5** group alveolar ducts were relatively normal size at expiration but greatly overdistended at inspiration with areas of alveolar collapse (i.e., high dynamic strain) at both inspiration and expiration. **APRV 10%** resulted in highly overdistended alveolar ducts at both inspiration and expiration with large areas of collapsed alveoli. **APRV 75%** (i.e., the TCAV method) resulted in the smallest increase in alveolar duct size, with uniformly open, homogeneously ventilated alveoli that were closest to those seen in the **Control** group (Kollisch-Singule et al., 2014b). Permissions obtained from Elsevier. License 4732510649425.

in the adjacent patent alveoli and that alveolar size actually decreases with increased airway pressure (i.e., PEEP) if lung tissue is recruited by a mechanism of gas redistribution (Cereda et al., 2011, 2013, 2016a). It has also been shown that gas redistribution in the microenvironment is not only *pressure* dependent but also *time* dependent (i.e., the longer the pressure is applied, the better the gas redistribution) (**Figure 7**) (Kollisch-Singule et al., 2014b).

Animal studies have shown that the OLA can protect the lung from VILI even if  $\Delta P$  is not reduced (Tojo et al., 2018). Recruiting the lung with PEEP has been shown to reduce tissue damage secondary to spontaneous breathing (SB) by two mechanisms: (1) the intensity of the SB is reduced via neuromechanical uncoupling, and (2) the reduced amount of atelectatic tissue decreases the volume of stress-focus areas (Morais et al., 2018). Other studies using animal models have also shown the physiologic and pathologic benefit of opening the acutely injured lung (Faridy et al., 1966; Webb and Tierney, 1974; Dreyfuss et al., 1988; Muscedere et al., 1994; Nakazawa et al., 2007; Nieman et al., 2015; Magalhaes et al., 2018). Additionally, animal studies have shown that to successfully implement the OLA, the RM and subsequent PEEP level must be applied properly, or the approach may actually increase lung damage. Farias et al. (2005) showed that an RM increased lung pathology if PEEP was not set sufficiently high to prevent recollapse of the newly opened tissue, a finding that is supported by direct *in vivo* observation of subpleural alveoli (Halter et al., 2003). In light of





this evidence, discarding the OLA does not seem logical, since it is unclear whether the RCTs testing the OLA actually opened and stabilized the lung. A better strategy might be to identify ventilation strategies that are most likely to accomplish the goals of the OLA (Sahetya and Brower, 2017).

## A PHYSIOLOGICALLY INFORMED STRATEGY TO EFFECTIVELY OPEN AND STABILIZE THE LUNG

Surfactant deactivation and edema flooding with acute lung injury cause alveolar collapse; the result is very “sticky” and does not reopen easily (**Figure 3**) (Crotti et al., 2001; Gattinoni et al., 2003). This tissue has a very long opening time constant, and thus it will take an extended period of time at any given pressure to recruit these surfactant deficient and edematous tissues. Once the collapsed alveoli are recruited, the opposite problem develops; the newly opened alveoli have a very brief collapse time constant (Neumann et al., 1998a,b, 2000). Thus, alveoli collapse quickly ( $\leq 0.5$  s) once a critical collapse airway pressure is reached (i.e., collapse is *time* and *pressure* dependent) (Kollisch-Singule et al., 2014a,b).

To effectively implement the OLA, the entire mechanical breath pattern (MBP), including all airway volumes, flows, pressure, rates, and the times during which they apply during

inspiration and expiration, must be analyzed (Kollisch-Singule et al., 2014a). The current OLA ventilation strategies do not consider the pathophysiological changes that occur in alveolar opening and collapse time constants. Attempting to recruit large volumes of collapsed lung with a single RM over a very brief period of time is often not physiologically possible depending on the degree of surfactant damage and edema. A more effective strategy may be a ventilation method that “nudges” the lung open over an extended period of time (6–24 h) using a high mean airway pressure held for most of each breath. Likewise, the very fast alveolar collapse time constants are not considered when setting PEEP with expiratory durations in the 2- to 3-s range. A more effective strategy may be to use a ventilator method with a very brief ( $\leq 0.5$  s) expiratory time while maintaining a level of time-controlled PEEP (TC-PEEP). Greatly limiting the expiratory duration ( $\leq 0.5$  s) keeps the lung from emptying completely, maintaining a TC-PEEP that is related to expiratory duration and the collapse time constant of the lung. Thus, for any given collapse time constant, the shorter the expiratory time, the higher the TC-PEEP and vice versa. In addition, since alveolar collapse is viscoelastic in nature (**Figure 9**), the very short expiratory duration would work synergistically with TC-PEEP to prevent alveolar collapse – alveoli simply would not have sufficient time to derecruit (Nieman et al., 2019). Analysis of the change in alveolar opening and collapse time constants with acute lung injury suggests that the time component of the

MB<sub>p</sub> (Kollisch-Singule et al., 2014a) can be used to improve the ability to recruit and stabilize acutely injured lung tissue, which is necessary to successfully implement the OLA.

In addition to the time component of MB<sub>p</sub>, the dynamic physiology of alveolar R/D must also be understood to design a mechanical breath for the OLA. Alveoli and alveolar ducts inflate and deflate as a viscoelastic system (Denny and Schroter, 2000; Escolar and Escolar, 2004; Farias et al., 2005; Carvalho and Zin, 2011; Suki and Bates, 2011; Nieman et al., 2017b). The model most used to analyze viscoelastic behavior is the spring and dashpot (**Figure 9**). The most important thing to know about a viscoelastic system, in relation to lung opening and collapse, is that there is a time lag from when the force (inspiratory pressure) is applied until alveoli begins to open and a lag between when force is removed (expiratory pressure) and when alveoli begin to collapse. Thus, the longer the inspiratory time, the more lung tissue that will be recruited, and the shorter the expiratory time, the less lung tissue that will be allowed to recollapse (**Figure 9**). A collapsed airway inflates after the opening threshold pressure is reached, and the pressure then propagates down the airway, inflating more airways and alveoli. This process progresses in an avalanche manner with power-law distributions of both the size of and intervals between avalanches (Suki et al., 1994; Alencar et al., 2002). It has been postulated that as the lung opens, the increase in parenchymal tethering of airways (Broche et al., 2017) and alveolar interdependence improves lung function as a power-law function (Nieman et al., 2019). These new perspectives inform the quest for novel protective ventilation strategies. Indeed, our work in translational animal models and a meta-analysis of data on surgical intensive care unit (SICU) patients has shown that our time-controlled adaptive ventilation (TCAV) method, using airway pressure release ventilation (APRV) mode, is highly effective at keeping the lung open and stable, significantly reducing morbidity in translational animal models and reducing the ARDS incidence and mortality rates of SICU patients at high risk of developing ARDS (Roy et al., 2012; Andrews et al., 2013; Emr et al., 2013; Roy S.K. et al., 2013; Kollisch-Singule et al., 2014a,b, 2015a,b, 2017; Nieman et al., 2015, 2017a,b, 2018; Smith et al., 2015; Jain et al., 2016, 2017; Satalin et al., 2018; Silva et al., 2018; Mahajan et al., 2019).

Others have shown the importance of ventilation time on lung mechanics. Saddy et al. (2013) calculated a pressure-time product (PTP)/breath as the integral of the change in esophageal pressure over time. They found that, when using biphasic positive airway pressure, PTP significantly increased when the rate of time-cycled control breaths was at 50 breaths/min as compared to when it was 100 or 75 breaths/min. The energetics of ventilation also contain components of ventilator time. Power is defined as work per unit time and is thus equal to pressure  $\times$  (volume/time) (Marini, 2018). Most of the energy applied to the lung during inflation is accounted for in elastic storage and airway resistance. It is postulated that the damage due to power is caused by the energy that is dissipated and unrecovered during exhalation. In addition, it is not just the power but also the changes in the microenvironment that result in tissue damage. Regional alveolar instability can develop during ARDS and can greatly

amplify energy dissipation locally. Regional instability acts as a stress-focus, and once a microstrain threshold is reached, the unrecovered energy will cause a rapid progression of lung tissue injury in a power-law fashion (Hamlington et al., 2018).

## ELIMINATING CONSTRAINTS OF VENTILATING THE ACUTELY INJURED LUNG

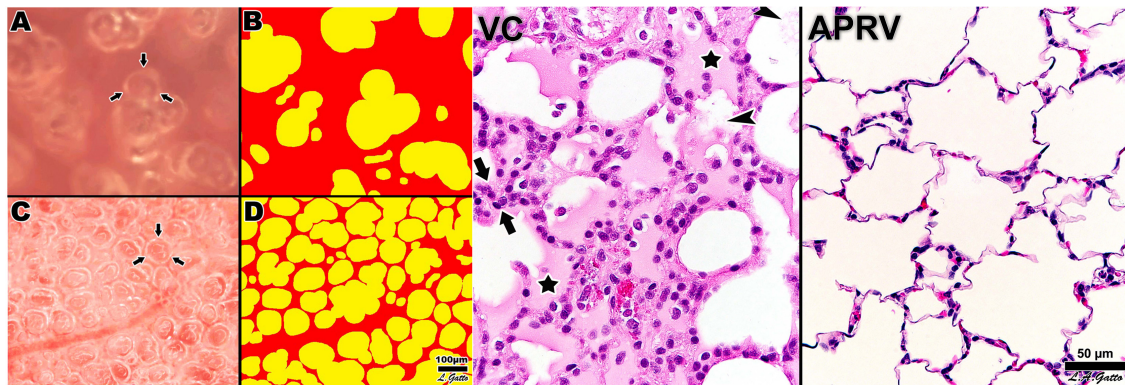
It was recently shown in ARDS patients that low V<sub>t</sub> and P<sub>plat</sub> do not correlate well with reduced patient mortality, whereas low  $\Delta P$  correlated strongly with improved survival (Amato et al., 2015). The critical lesson is that it is not the settings dialed into the ventilator (i.e., V<sub>t</sub>, P<sub>plat</sub>, and so on) that are key to improved survival, but rather the impact of these settings on lung physiology measured as a change in  $\Delta P$  (Kollisch-Singule et al., 2014a,b, 2015b).

Using the ARDSnet method, the V<sub>t</sub> was set at 6 cc/kg, the P<sub>plat</sub> was set at < 30 cm H<sub>2</sub>O, and PEEP was set on a sliding oxygenation scale; the mechanism of improved mortality was assumed to be due to these parameters. The Amato study clearly demonstrated that the mechanism of increased survival was not these desired setting values, because none correlated with outcome (Amato et al., 2015). Lower  $\Delta P$ , on the other hand, strongly correlated with reduced mortality. Respiratory system compliance (C<sub>RS</sub>) was used to calculate driving pressure ( $\Delta P = V_t/C_{RS}$ ), which was shown to decrease in patients who survived, reflecting a desirable change in lung physiology caused by recruitment.

The ARDSnet method assumes that the constraints of ventilating a heterogeneously collapsed lung are unavoidable, in which case the P<sub>tp</sub> is high due to the high E<sub>spec</sub> value and low baby lung (FRC) volume. However, if the entire lung could be fully recruited, these constraints would be eliminated, E<sub>spec</sub> reduced, and FRC increased, resulting in a significant reduction in the applied stress (i.e., P<sub>tp</sub>) for any given V<sub>t</sub>. Rahaman used a stress equation similar to Eq. 1 to analyze the mathematics of VILI (Rahaman, 2017). He concluded that stress increases for any given V<sub>t</sub> and PEEP with an increase in respiratory rate (RR). This conclusion assumes that the clinician is constrained in ventilating a heterogeneously collapsed lung such that neither FRC (i.e., the size of the baby lung) nor E<sub>spec</sub> can be changed. When these conditions are true, the conclusion that V<sub>t</sub>, PEEP, and RR must be kept low to reduce stress is correct. Conversely, our perspective is the better strategy is to treat the lung by reinflating the collapsed tissue, increase FRC (eliminating the baby lung), and decreasing E<sub>spec</sub>. This combination will reduce lung stress (P<sub>tp</sub>) during ventilation even at higher V<sub>t</sub>, PEEP, and RR (Eq. 1).

Of course the strategy of “casting” the broken lung open until it heals would be clinically effective only with a ventilation strategy that could perform such a feat (Nieman et al., 2018). Unfortunately, the current OLA strategies have not been shown effective at opening and stabilizing the lung (Bhattacharjee et al., 2018; Cui et al., 2019; Hodgson et al., 2019; Kang et al., 2019; Zheng et al., 2019), and the recent ART trial showed an increase in





**FIGURE 10 |** Left – Subpleural alveoli seen using *in vivo* microscopy in a rat hemorrhagic shock-induced ARDS model ventilated with volume cycled ventilation (VC; **A,B**) or airway pressure release ventilation (APRV) using the time controlled adaptive ventilation (TCAV) method (APRV; **C,D**). Individual alveoli are shown by arrows. Inflated alveoli were color coded yellow, and alveolar number, size, and surface area were measured by computer image analysis in each group. TCAV significantly improved alveolar patency and stability as compared with the VC group. Right – The APRV group delivered using the TCAV method stabilized alveoli that was associated with a significant reduction in lung histopathology as evidenced by open alveoli and reduced intra-alveolar edema (purple areas) as compared with the collapsed and edema-filled alveoli (stars), fibrinous deposits in the air compartment (arrowheads), and white cell infiltration (between arrows) in the VC group (Roy S.K. et al., 2013). Permissions obtained from Wolters Kluwer Health, Inc. License 4699411295724.

mortality using the OLA (Brower et al., 2004; Meade et al., 2008; Mercat et al., 2008; Cavalcanti et al., 2017).

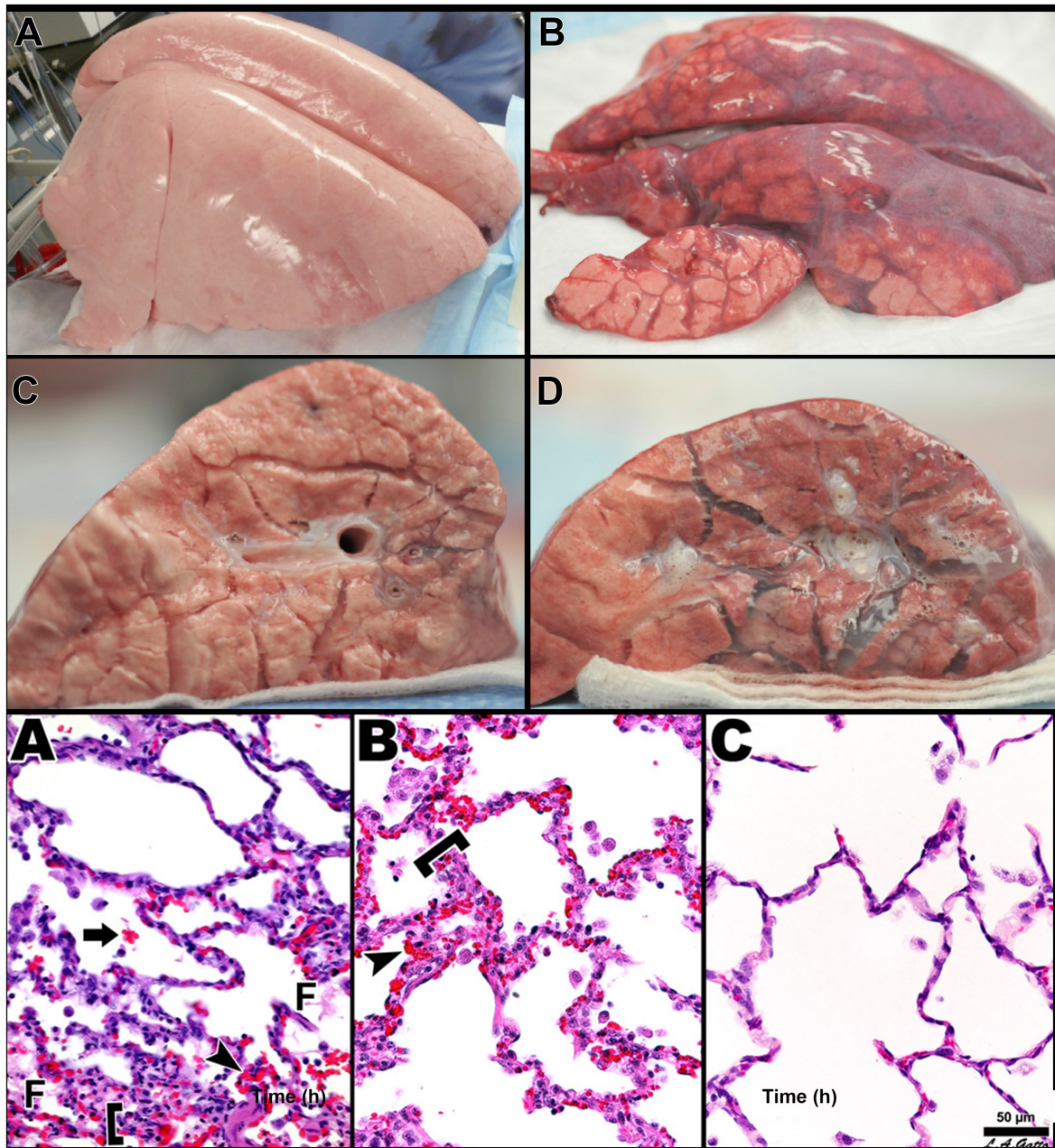
## THE TCAV METHOD TO OPEN AND STABILIZE THE ACUTELY INJURED LUNG

Our TCAV method using the APRV mode has been discussed in detail elsewhere (Habashi, 2005; Jain et al., 2016; Nieman et al., 2018, 2019; Kollisch-Singule et al., 2019). Briefly, TCAV consists of an extended (4–5 s) open valve continuous positive airway pressure (CPAP) phase with a very short ( $\leq 0.5$  s) release phase. The inspiratory:expiratory ratio is  $\sim 10:1$ . The open valve allows the patient to spontaneously breathe (inspiration or expiration) with little resistance. Tidal volume ( $V_t$ ) is not set but rather is a product of the CPAP level and lung compliance. A heterogeneously collapsed lung will have a very low  $V_t$  because the compliance will be low, but as the lung gradually recruits over time, the compliance will increase and so will the  $V_t$ . Since the  $V_t$  is set based on lung compliance, a high  $V_t$  will never be delivered to a non-compliant collapsed lung using the TCAV method. Thus, the  $V_t$  size is personalized and adaptive as the patient's lung gets better or worse, directed by changes in lung compliance. The extended CPAP time will gradually nudge viscoelastic alveoli open over several hours until the lung is fully inflated. The newly recruited alveoli will be prevented from recollapse through the use of a very short expiratory duration (release phase). Expiratory time is very short ( $\leq 0.5$  s), and thus the lung is reinflated (CPAP phase) before it has time to completely empty, maintaining a TC-PEEP. The very short expiratory time is not sufficient for viscoelastic alveoli to collapse and when combined with the TC-PEEP is highly effective at preventing alveolar derecruitment.

Our group has investigated the physiological impact of the TCAV method in both mechanistic and efficacy animal studies

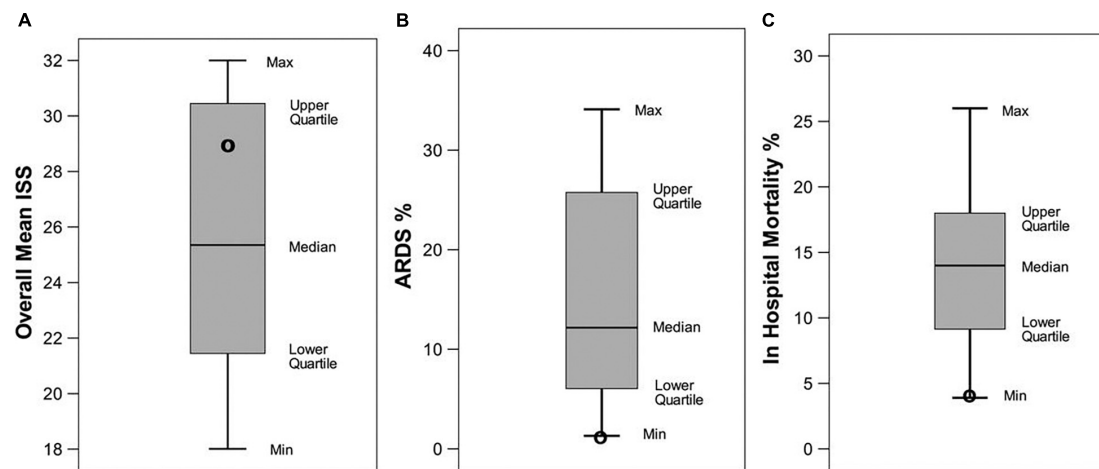
(Roy et al., 2012; Emr et al., 2013; Roy S.K. et al., 2013; Roy S. et al., 2013; Kollisch-Singule et al., 2014a,b, 2015a,b, 2017; Smith et al., 2015; Silva et al., 2018) and in a meta-analysis of data on SICU patients (Andrews et al., 2013). In addition, the TCAV method is the primary ventilator strategy used at the R Adam Cowley Shock Trauma Center in Baltimore, with well over 1,000,000 h of ventilator time. Below, we discuss the results from our animal data and our clinical statistical analysis as evidence for the TCAV method's mechanisms and efficacy.

In rat VILI and hemorrhagic shock models, it was shown that ventilation for 6 h using the TCAV method was superior to volume-controlled ventilation (VCV;  $V_t$  10 ml/kg, PEEP 0.5 cm  $H_2O$ ) at preventing the development of ARDS and that lung protection was associated with stabilization of alveoli (**Figure 10**) (Emr et al., 2013; Roy S.K. et al., 2013). The TCAV method was also shown to be lung protective in a preterm piglet model of infant respiratory distress syndrome (Kollisch-Singule et al., 2017). These data were supported by mechanistic studies showing the ability of the TCAV method to normalize alveolar and alveolar duct microanatomy (Kollisch-Singule et al., 2014b) (**Figure 7**) and to reduce dynamic alveolar strain (Kollisch-Singule et al., 2014a, 2015b; Smith et al., 2015). We developed a 48-hr clinically applicable, high-fidelity, porcine peritoneal sepsis (PS) plus gut ischemia/reperfusion (I/R), multiple organ dysfunction syndrome (MODS) and ARDS model. In three studies using this clinically applicable model, we demonstrated that the TCAV method was superior to VC or the ARDSnet method at blocking progressive acute lung injury and preventing ARDS development (**Figure 11**) (Roy et al., 2012; Roy S. et al., 2013; Kollisch-Singule et al., 2015a). In addition, we have shown that surfactant proteins A and B are both better preserved with the TCAV as compared with the ARDSnet method, suggesting that there is sufficient lung volume change with TCAV to preserve stretch-induced surfactant release (Roy et al., 2012; Emr et al., 2013; Roy S.K. et al., 2013; Roy S. et al., 2013; Kollisch-Singule et al., 2015a). Lastly, in a



**FIGURE 11 |** Three groups of pigs were ventilated for 48 h with a clinically applicable, high-fidelity porcine peritoneal sepsis (PS) and gut ischemia/reperfusion (I/R) acute respiratory distress syndrome (ARDS) model: (1) *Control* group without PS + I/R injury ventilated with a tidal volume ( $V_t$ ) of 10 cc/kg and a positive end-expiratory pressure (PEEP) of 5 cm  $H_2O$ . (2) *ARDSnet* group using a low- $V_t$  ventilation method, applied following PS + I/R injury at the time point at which the animal reached the oxygen saturation limit listed in the ARDSnet protocol, with PEEP and  $FiO_2$  adjusted by oxygenation (Acute Respiratory Distress Syndrome Network, 2000). (3) Time-controlled adaptive ventilation (*TCAV*) method using the airway pressure release ventilation (APRV) mode applied immediately after PS + I/R injury (Habashi, 2005; Jain et al., 2016). **Upper** – Gross lung photographs after 48 h of ventilation following PS + I/R injury at necropsy (*Control* not shown). In the *TCAV* group (**A,B**), lungs inflated fully to near total lung capacity at 25 cm  $H_2O$  without any gross atelectasis. The cut surface of the diaphragmatic lobe also showed no interstitial or airway edema and no atelectasis. Lungs in the *ARDSnet* group (**C,D**) also inflated to 25 cm  $H_2O$  showed low lung volume with heterogeneous collapse and atelectasis and were wet and “boggy.” The cut surface showed both interstitial and airway edema. **Lower** – Photomicrographs of representative lung sections of specimens from the *Control* (**A**), *ARDSnet* (**B**), and *TCAV* (**C**) groups each at 40 $\times$  magnification. F, fibrinous deposit in the air compartment; arrow, blood in alveolus; arrowhead, congested alveolar capillary; bracket, thickened alveolar wall. (**A**) *Control*: animals received 48 h of mechanical ventilation without PS + I/R injury. Specimen shows typical early acute lung injury pathology including fibrinous deposits, blood in alveolus, congested capillaries, and thickened alveolar walls. (**B**) *ARDSnet*: animals received PS + I/R injury, and  $LV_t$  ventilation was applied after the onset of acute lung injury (i.e.,  $PaO_2/FiO_2$  ratio <300). Specimen shows typical advanced acute lung injury pathology including fibrinous deposits, blood in alveolus, congested capillaries, leukocyte infiltration, and thickened alveolar walls. (**C**) *TCAV*: specimen shows normal pulmonary architecture, alveoli are well-expanded and thin walled, and there are no exudates (Roy S. et al., 2013). Permissions obtained from Wolters Kluwer Health, Inc. License 4699411460832.





**FIGURE 12 |** A systematic review of data from trauma patients who were ventilated with either conventional mechanical ventilation (CMV) or the time-controlled adaptive ventilation (TCAV) method using the airway pressure release ventilation (APRV) mode. Boxplots are mean and standard error for **(A)** Injury Severity Score (ISS), **(B)** percentage of patients who developed ARDS (ARDS%), and **(C)** in-hospital mortality (%) from 16 published papers using standard of care CMV. Black circles indicate the results in each category using the TCAV method at the *R Adam Cowley Shock Trauma Center* in Maryland. Although patients in the high-ISS range, they had the lowest levels of both ARDS incidence (ARDS%) and in-hospital mortality (%) as compared with patients ventilated using CMV (Andrews et al., 2013). Permissions obtained from Wolters Kluwer Health, Inc. License 4699420119915.

statistical analysis of data from SICU patients, the TCAV method was associated with a significant reduction in ARDS incidence and mortality as compared to standard of care ventilation in 15 SICUs (Figure 12) (Andrews et al., 2013).

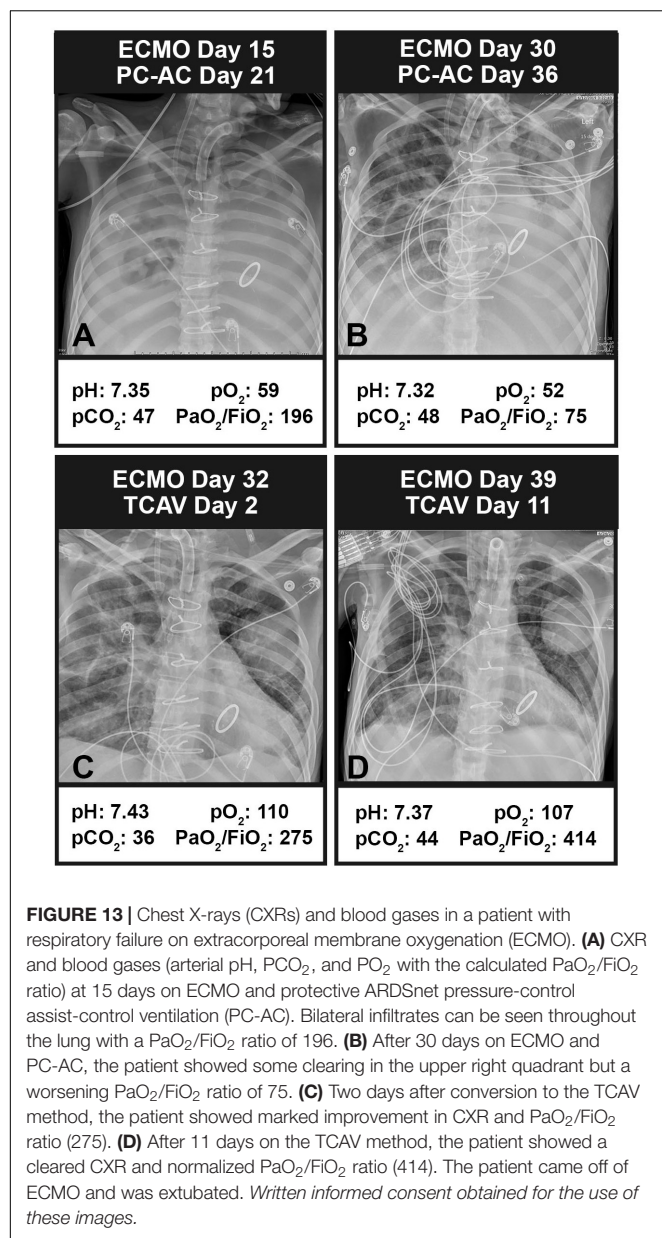
It is important to remember that if the acutely injured lung can be fully recruited, it will remain *time* and *pressure* dependent (i.e., will collapse quickly at atmospheric pressure) for a period of hours to days (Takahashi et al., 2015). Once the acutely injured lung is opened, the ventilator pressure/time support necessary to keep it open cannot be reduced until the lung “heals.” Gradually pulmonary edema will be reabsorbed and surfactant function restored (Vazquez de Anda et al., 2000). As more and more lung tissue is recruited, reestablishing alveolar interdependence (Figure 6) (Mead et al., 1970; Makiyama et al., 2014) and parenchymal tethering (Perun and Gaver, 1995), the lung will once again become stable at atmospheric airway pressure, and the weaning process can begin (Mead et al., 1970; Perun and Gaver, 1995; Makiyama et al., 2014).

Recent RCTs have shown mixed results in ARDS patients using APRV (but not utilizing the TCAV method). Zhou et al. (2017) randomized patients with a  $\text{PaO}_2/\text{FiO}_2$  (P/F) ratio < 200 to either ARDSnet LVt or APRV with TCAV-like settings. The APRV group demonstrated significant decreases in length of ICU stay, tracheostomy requirement, ventilator days, and mortality. The APRV group also had significant reductions in the need for prone positioning, sedation, and neuromuscular blockade.

Lalgudi Ganesan et al. (2018) conducted an RCT in children with ARDS, who were randomized to receive either standard LVt strategy or APRV. The APRV group was shown not to be lung protective, and the trial was terminated early. We postulate the failure was due to fundamental misconceptions as to the MBP necessary to protect the lung. A key objective in our TCAV method is to gradually nudge the lung open. In the Ganesan

study, the CPAP pressure was reduced to generate a low  $V_t$ , and thus the CPAP level was likely not above the lung critical opening pressure, meaning the lung was not inflated. In the TCAV method,  $V_t$  is not set (see TCAV description above), so an increase in release volume (analogous to  $V_t$ ) during the release phase and an increase in  $C_{RS}$  are positive signs and indicative of lung recruitment (Roy et al., 2012; Roy S. et al., 2013; Kollisch-Singule et al., 2015a). If the ventilation strategy used does not actually open the lung, the VILI mechanisms associated with heterogeneous ventilation will not be prevented (Figure 4). We postulate that this is also the reason for the failed RCTs using an RM and titrated PEEP (Brower et al., 2004; Meade et al., 2008; Mercat et al., 2008; Cavalcanti et al., 2017).

Hirshberg et al. (2018) conducted an RCT in adults, and similarly to the Ganesan study, targeted a  $V_t$  at  $\sim 6$  mL/kg. The study was stopped early, in part because the  $V_t$  often exceeded 12 mL/kg, even though there were no significant differences between groups in pneumothorax, sedation, vasoactive medications, P/F ratio, or outcome (Hirshberg et al., 2018). As stated above, when the TCAV method is used, an increase in  $V_t$  is indicative of lung recruitment and is a positive effect. Thus, one of the critical protective mechanisms of the TCAV method, the ability to fully open the lung, was not incorporated into the APRV setting in either the Hirshberg or Ganesan study. The conclusion from these clinical studies should not be that “APRV is not lung protective” but rather that the Zhou (Zhou et al., 2017) and TCAV methods (Andrews et al., 2013) are superior to the Ganesan (Lalgudi Ganesan et al., 2018) and Hirshberg (Hirshberg et al., 2018) methods for lung protection. Two recent statistical reviews and meta-analyses of RCTs have shown the APRV mode is associated with a mortality benefit, improved oxygenation, and a greater number of ventilator-free days when compared with conventional ventilation strategies,



without any negative hemodynamic impact or higher risk of barotrauma (Carsetti et al., 2019; Lim and Litton, 2019).

An example of the TCAV method's effectiveness when applied to a patient on extracorporeal membrane oxygenation (ECMO) with respiratory failure is seen in **Figure 13**. A 35-year-old man with a history of systemic lupus erythematosus, with catastrophic antiphospholipid syndrome, underwent a coronary artery bypass graft with mitral valve repair and was placed on protective pressure-control assist-control ventilation (PC-AC) with protective settings using the ARDSnet method. Chest X-rays (CXRs) on PC-AC for 21 days, 15 of those days on ECMO, showed widespread infiltrates (**Figure 13A**). Another 15 days on ECMO (30 days on ECMO total) and PC-AC showed minimal change in CXRs and worsening lung function assessed by P/F

ratio (A: 196, B: 75) (**Figure 13B**). Conversion to the TCAV method for 2 days resulted in a marked improvement in CXRs and P/F ratio (275) (**Figure 13C**). After 11 days on TCAV, the patient had a clear CXR and normal P/F ratio (414) (**Figure 13D**). **Figure 13D** was 6 h prior to decannulation and liberation from ECMO. After 39 days on PC-AC with worsening lung function, it took only 2 days on the TCAV method to reopen and stabilize the patient's lung, and after 11 days the patient was disconnected from ECMO, extubated, and removed from mechanical ventilation.

## CONCLUSION

Current protective ventilation strategies have not significantly reduced ARDS-related mortality in the 20 years since the ARMA study, possibly because strategies are constrained to ventilating the heterogeneously collapsed and unstable lung. In addition, current protective ventilation strategies have not considered all of the physiological parameters necessary to protect the acutely injured lung. Alveoli and alveolar ducts open and collapse as a viscoelastic system such that there is a time lag between when the airway pressure is applied and alveoli open, and between when the airway pressure is removed and alveoli collapse. Loss of pulmonary surfactant function, a key ARDS pathology, amplifies these viscoelastic properties, rendering the lung *time* and *pressure* dependent, such that it takes an extended time at the higher pressure for lung tissue to open and a very brief time, even with an elevated airway pressure, for the lung to recollapse.

This knowledge suggests that to eliminate VILI the ventilation strategy must open and stabilize the lung. Current ventilation strategies attempting this OLA have not reduced mortality in clinical trials. Since alveolar volume change is viscoelastic in nature, the *time* at both inspiration and expiration would be critical to accomplishing the OLA goals. We have developed a time-controlled adaptive ventilation TCAV method using the APRV mode and have shown that it is highly effective at opening and stabilizing the lung, which significantly reduces VILI-induced lung damage in animal ARDS models. We have also shown that preemptive application of the TCAV method in trauma patients significantly reduces ARDS incidence and mortality. Recent RCTs using the APRV mode but not adjusted with the TCAV method have shown mixed results, suggesting that properly adjusted APRV is critical to clinical success.

## AUTHOR CONTRIBUTIONS

GN drafted the manuscript. HA-K, MK-S, JS, SB, GT, PA, MM, LG, and NH critically revised the manuscript. All authors read and approved the final manuscript.

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**Conflict of Interest:** GN, HA-K, MK-S, JS, LG, PA, MM, and NH have lectured for Intensive Care On-line Network, Inc. (ICON). NH is the founder of ICON, of which PA and MM are employees. The authors maintain that industry had no role in the design and conduct of the study; the collection, management, analysis, or interpretation of the data; nor the preparation, review, or approval of the manuscript.

The remaining authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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# Mechanical Ventilation Lessons Learned From Alveolar Micromechanics

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Morbidity and mortality associated with lung injury remains disappointingly unchanged over the last two decades, in part due to the current reliance on lung macro-parameters set on the ventilator instead of considering the micro-environment and the response of the alveoli and alveolar ducts to ventilator adjustments. The response of alveoli and alveolar ducts to mechanical ventilation modes cannot be predicted with current bedside methods of assessment including lung compliance, oxygenation, and pressure-volume curves. Alveolar tidal volumes ( $V_t$ ) are less determined by the  $V_t$  set on the mechanical ventilator and more dependent on the number of recruited alveoli available to accommodate that  $V_t$  and their heterogeneous mechanical properties, such that high lung  $V_t$  can lead to a low alveolar  $V_t$  and low  $V_t$  can lead to high alveolar  $V_t$ . The degree of alveolar heterogeneity that exists cannot be predicted based on lung calculations that average the individual alveolar  $V_t$  and compliance. Finally, the importance of time in promoting alveolar stability, specifically the inspiratory and expiratory times set on the ventilator, are currently under-appreciated. In order to improve outcomes related to lung injury, the respiratory physiology of the individual patient, specifically at the level of the alveolus, must be targeted. With experimental data, this review highlights some of the known mechanical ventilation adjustments that are helpful or harmful at the level of the alveolus.

**Keywords:** alveolar stability, alveolar heterogeneity, lung injury, *in vivo* microscopy, micromechanics

## INTRODUCTION

Acute lung injury is caused by a pathologic tetrad of alveolar instability, endothelial leakage, alveolar edema, and surfactant dysfunction (Nieman et al., 2018). Atelectrauma and associated repetitive opening and collapse of the injured alveoli results in alveolar instability (Schiller et al., 2001). An increase in pulmonary capillary permeability (Matthay et al., 2012) combined with damage to the alveolar-capillary barrier leads to alveolar edema (Budinger and Sznajder, 2006). This edema and repetitive opening and collapse of unstable alveoli alters surfactant function and abundance, resulting in increased surface tension (Greene et al., 1999; Warriner et al., 2002), and promotion of alveolar epithelial injury (Ruhl et al., 2019). Finally, tissue injury activates

pro-inflammatory signaling, leading to biotrauma (Tremblay et al., 1997). Although mechanical ventilation can be necessary to support the injured lung in order to promote gas exchange, it can itself be injurious by exacerbating atelectrauma and recruitment/derecruitment ultimately leading to the acute respiratory distress syndrome (ARDS) (Gajic et al., 2004; Albert, 2012).

Despite decades of research into protective mechanical ventilation strategies, mortality rates associated with ARDS have remained disappointing with mortality rates ranging from 34.9 to 46.1% (Bellani et al., 2016) despite the use of protective non-injurious ventilation (Villar et al., 2011). When a patient is placed on the mechanical ventilator, the ventilator settings are modified to accommodate the physiology of the lung [tidal volumes ( $V_t$ ), compliance, pressure-volume curves, oxygen saturation, etc. . .], while taking into account the patient's underlying volume status and cardiac physiology (Vieillard-Baron et al., 2016). Regional microscale responses [in the alveoli, conducting airway, and interstitium] are not predictable from the macroscale inputs of the mechanical ventilator (Kollisch-Singule et al., 2014a). Therefore, the universal application of generic mechanical ventilator settings to all patients without considering patient-specific differences in the underlying micromechanics may not benefit the lung and even cause further injury. Personalizing mechanical ventilation in order to link the macro-parameters set on the mechanical ventilator to the dynamic changes that occur at the level of the alveolus will be important to attenuate the pathophysiology of lung injury: alveolar instability, endothelial leakage, alveolar edema, and surfactant dysfunction (Kollisch-Singule et al., 2018; Nieman et al., 2018). Herein, we review the current literature investigating the response of the lung micro-anatomy: the alveoli and alveolar ducts, to varying mechanical ventilation settings.

## ALVEOLAR RECRUITMENT

The majority of what is known about alveolar micromechanics is based on *in vivo* and *in vitro* models (Tschumperlin et al., 2000; Perlman and Bhattacharya, 2007; Mertens et al., 2009) incorporating methods of histology, electron microscopy, *in vivo* microscopy, optical coherence tomography, computed tomography, synchrotron imaging, electrical impedance tomography, inhaled polarized gases, and computer-based theoretical models (Broche et al., 2017; Grune et al., 2019), but there are no direct methods of assessing alveolar micromechanics, particularly the response to mechanical ventilation strategies (Roan and Waters, 2011).

At the level of the lung, it is well-recognized that even relatively high pressures are not harmful to the lung when applied tonically (as static strain) but becomes harmful when applied dynamically (as dynamic strain or with large driving pressures) (Protti et al., 2013; Amato et al., 2015; Jain et al., 2017). This does correlate with alveoli in that cyclic stretching and higher amplitude deformation of alveolar epithelial cells leads to greater cell damage whereas static or lower amplitude deformations do not (Tschumperlin et al., 2000). An individual alveolus requires

a certain pressure to re-open (critical opening pressure) and also have a pressure where it will collapse (critical closing pressure) (Albert et al., 2009) which is less than the opening pressure. This suggests that, in order for a recruited alveolus to remain open, the system must have a certain minimum airway pressure that is greater than the alveolar closing pressure, but does not need to be as high as the opening pressure (Bates and Irvin, 2002). Therefore, the application of positive end expiratory pressure (PEEP) at or above the alveolar closing pressure offers a static level of pressure to prevent alveolar derecruitment (Bates and Irvin, 2002).

*In vivo* microscopy has been used to directly monitor the alveolar recruitment patterns in response to lung injury and varying levels of PEEP (Kollisch-Singule et al., 2014a, 2016). Such studies have demonstrated that higher levels of PEEP lead to increased alveolar recruitment and surface area with particular benefit derived from mechanical ventilation strategies that offer a higher mean airway pressure ( $P_{aw}$ ) (Kollisch-Singule et al., 2014a), which allows for improved intratidal recruitment without causing alveolar overdistension (Smith et al., 2015). The distension that occurs at the level of the alveolus and alveolar duct in response to the stress of the mechanical ventilator is the micro-strain and has been calculated as:

$$\text{microstrain} = \Delta L_P / L_{Pe}$$

where  $\Delta L_P$  is the change in perimeter length between inspiration and expiration and  $L_{Pe}$  is the original perimeter length at expiration (Kollisch-Singule et al., 2014a). Using this calculation, it was shown that alveoli and alveolar ducts are both exposed to less micro-strain with higher levels of PEEP and  $P_{aw}$  (Kollisch-Singule et al., 2014a,b).

Although PEEP is critical to stabilizing both the alveoli and alveolar ducts (Kollisch-Singule et al., 2014a,b), it may cause impaired minute ventilation and subsequent hypercapnia (Acute Respiratory Distress Syndrome Network et al., 2000), and also may lead to a point when PEEP increases do not lead to any additional stability. This is the so-called 'best PEEP' however there is no consensus over what 'best' PEEP is. The 'best PEEP' should be dependent on the underlying alveolar compliance, alveolar closing pressures, and time (Bates and Irvin, 2002; Albert et al., 2009), but the majority of PEEP titration strategies do not provide a micromechanical basis (Chiumello et al., 2014; Pintado et al., 2017; Writing Group for the Alveolar Recruitment for Acute Respiratory Distress Syndrome Trial Investigators et al., 2017; Beitler et al., 2019). Alveolar stabilization may occur at varying levels of PEEP depending on the degree and type of underlying injury (Carvalho et al., 2008). In one murine model of direct lung injury, the 'best PEEP' leading to alveolar stability was found to be 9 cmH<sub>2</sub>O (Andrews et al., 2015), whereas in another it was at 16 cmH<sub>2</sub>O (Kollisch-Singule et al., 2014a). In a rabbit model of lung injury utilizing synchrotron imaging to estimate the response of the terminal airway to varying levels of PEEP, Broche et al. (2017) found that increasing PEEP led to improved lung aeration and that terminal airway derecruitment increased markedly for PEEP less than 6 cmH<sub>2</sub>O. The study also revealed that, although recruitment/derecruitment was attenuated with

increasing PEEP, it was still present at PEEP levels as high as 12 cmH<sub>2</sub>O (Broche et al., 2017). Although creative methods have been used to determine the best PEEP of the lung using bedside measurements, these strategies do not account for the variability or physiology of the alveoli and alveolar ducts (Chiumello et al., 2014; Pintado et al., 2017; Writing Group for the Alveolar Recruitment for Acute Respiratory Distress Syndrome Trial Investigators et al., 2017; Beitler et al., 2019). For instance, using *in vivo* microscopy, alveolar recruitment and derecruitment were compared against the inflection points of the pressure-volume curves and overall found to have a poor correlation, with the exception of the deflation limb upper inflection point, which was found to be related to the derecruitment pressure (Dirocco et al., 2007).

In a porcine model of acute lung injury, a recruitment maneuver was performed followed by stepwise decreases in PEEP with CT scans at end-inspiration and end-expiration, as well as calculation of respiratory system elastance, stress index, and percentage of volume-dependent elastance (Carvalho et al., 2008). The method of injury (pulmonary injury by lavage versus extrapulmonary lung injury with systemically administered oleic acid) changed the pulmonary mechanics such that the extrapulmonary lung injury revealed greater stability at higher PEEP (Carvalho et al., 2008), consistent with prior studies comparing the etiology of lung injury to PEEP-responsiveness (Gattinoni et al., 1998). The stress index and percentage of volume-dependent elastance were meant to be used as surrogates for alveolar hyperinflation but were found to be useful only in the non-injured lungs, as there was no significant change to either when PEEP was reduced in the injured lungs (Carvalho et al., 2008). In the injured lung, recruitment and overdistension were found to occur simultaneously, with higher PEEP leading to recruitment of dependent lung regions but hyperinflation of non-dependent regions (Carvalho et al., 2008). The study determined that the PEEP that generated the lowest respiratory system elastance provided the best balance between lung recruitment and hyperinflation (Carvalho et al., 2008). But the study also served to demonstrate that strict reliance on pressure-volume curves may fail in the injured lung when there is co-existence of hyperinflation and collapse (Carvalho et al., 2008).

Oxygenation has also been found to be a poor marker of alveolar stability (Cereda et al., 2016b). In a murine model of direct lung injury and ventilator induced lung injury, strain (but not oxygenation) was found to predict propagation of lung injury (Cereda et al., 2016b). In a murine model of lung injury, alveolar stability was achieved at 9 cmH<sub>2</sub>O with further increases in PEEP not leading to an increase in microscopic stability despite an improvement in oxygenation (Andrews et al., 2015). In another *in vivo* study, increases in PEEP from 5 to 10 cmH<sub>2</sub>O led to only a transient increase in oxygenation despite a marked improvement in stability with increasing PEEP (Halter et al., 2003). This has been demonstrated in other studies in which repeated recruitment maneuvers are necessary to maintain oxygen saturation (Fujino et al., 2001) with higher PEEP at the conclusion of the recruitment maneuver being crucial to maintaining open alveoli and sustained improvements in oxygenation (Rimensberger et al., 1999).

## ALVEOLAR TIDAL VOLUME

The low tidal volume (LVt) ventilation strategy has been embraced as a standard method of minimizing lung injury in patients with ARDS (Acute Respiratory Distress Syndrome Network et al., 2000), yet LVt has not demonstrated a persistent reduction in ARDS-associated mortality (Meade et al., 2008; Villar et al., 2011). This is likely because this strategy does not account for variability in patient disease, individual pulmonary mechanics, nor the alveolar micro-environment (Kollisch-Singule et al., 2018). A subsequent retrospective analysis of the LVt data (Acute Respiratory Distress Syndrome Network et al., 2000) revealed that the change in mortality was due to differences in driving pressure, or the pressure differential between inspiration and expiration (Amato et al., 2015). This study therefore demonstrated that when ventilator settings are adjusted to the lung compliance, an individual patient measurement, lung injury as measured by mortality may be attenuated (Amato et al., 2015). Even LVt can generate altered stress distribution in diseased state conditions such as emphysema (De Ryk et al., 2007) whereby stress concentrates in the injured alveoli, both at the perimeter of the weakened regions as well as the septal junction points (De Ryk et al., 2007).

LVt ventilation strategies in and of themselves do not lead to alveolar stabilization where alveolar stability is assessed by low alveolar volume change (Schiller et al., 2001; Kollisch-Singule et al., 2014a). The number of open and homogenous alveoli upon which a Vt is distributed is a greater determinant of alveolar stability and resulting alveolar Vt than the Vt set at the level of the mechanical ventilator (Kollisch-Singule et al., 2014a, 2016). Thus, factors that increase the number and openness of alveoli, such as increased P<sub>aw</sub>, lead to alveolar stabilization (Halter et al., 2003).

In a murine model of direct lung injury, LVt (6 mL·kg<sup>-1</sup>) was set at the level of the mechanical ventilator but the alveolar Vt (dynamic change in alveolar cross-sectional area between inspiration and expiration) varied considerably (Kollisch-Singule et al., 2014a). The alveolar Vt was less dependent on the set Vt on the ventilator but more on the P<sub>aw</sub> (Kollisch-Singule et al., 2014a). High alveolar Vt was observed when P<sub>aw</sub> was low, even though the lung Vt was held constant at 6 mL·kg<sup>-1</sup> (Kollisch-Singule et al., 2014a). Alveolar Vt and micro-strain decreased only once PEEP was set at 10 cmH<sub>2</sub>O or greater, as the associated alveolar recruitment allowed for additional surface area for the same Vt to be distributed across evenly (Kollisch-Singule et al., 2014a). This study demonstrated that even the LVt strategy may be deleterious when not applied to an open lung, but also revealed that higher Vt of up to 11 mL·kg<sup>-1</sup> set on the ventilator can be associated with low alveolar Vt and micro-strain when combined with higher P<sub>aw</sub> and a concomitant increase in alveolar recruitment (Kollisch-Singule et al., 2014a).

These findings are supported by a confocal study by Namati et al. (2008) in which alveolar size was found to increase as airway pressure increases, with a stabilization in alveolar number at ~25 cmH<sub>2</sub>O. Following this, subsequent increases in pressure above 30 cmH<sub>2</sub>O led not to additional alveolar strain, but to alveolar recruitment, with an increase in alveolar



number but a decrease in alveolar size as measured by chord length (Namati et al., 2008). One hypothesis for this is that a separate population of daughter alveoli are recruited during times of increased pressure in order to re-distribute stress amongst the alveoli (Namati et al., 2008). In another alveolar study in which alveoli were exposed to inflation pressures as high as 40 cmH<sub>2</sub>O, the alveoli were not observed to overdistend but rather to increase in number (Dirocco et al., 2007). This data must be interpreted with caution as 40 cmH<sub>2</sub>O may be a supraphysiologic pressure for a mouse (Zosky et al., 2008), however, pressures in excess of 40 cmH<sub>2</sub>O have not demonstrated structural lung parenchymal damage (Soutiere and Mitzner, 2004), and the lung mechanics ultimately returned to baseline, even after being stressed to 40 cmH<sub>2</sub>O (Zosky et al., 2008). Zosky et al. (2008) found that mice have a standard sigmoid pressure-volume curve up to 20 cmH<sub>2</sub>O but that subsequent inflation to 40 cmH<sub>2</sub>O led to a significant elevation in the slope of the pressure-volume curve, and a double sigmoidal pattern. One possibility for this finding is that there is a second population of alveoli that are not recruited until a pressure above 20 cmH<sub>2</sub>O is reached (Soutiere and Mitzner, 2004) but begin to recruit at higher pressures, consistent with the findings of Dirocco et al. (2007) and Namati et al. (2008). This newly recruited second population of alveoli then inflate smoothly during subsequent inhalations, leading to an overall improvement in compliance and an increase in tidal volume (Zosky et al., 2008). The findings of these studies demonstrating more alveolar recruitment and less overdistension were corroborated by a large animal model in which the majority of lung volume change was secondary to recruitment/derecruitment, but not due to alveolar distension (Carney et al., 1999).

## ALVEOLAR RECRUITMENT OVER TIME

The other component to mechanical ventilation that is seldom discussed but remains of critical importance for alveolar micromechanics is that of time. Alveolar opening and closing pressures are in part determined by both time and lung volume history (Bates and Irvin, 2002), as well as the open/closed status of the neighboring alveoli (Broche et al., 2017). In an *in vivo* study, alveolar recruitment was monitored over a 40 s recruitment maneuver (Albert et al., 2009). Despite keeping the recruitment pressure static, alveoli continued to recruit over the 40 s duration, suggesting that not only pressure but the time over which the pressure is held is vital to both alveolar recruitment and stability (Albert et al., 2009). Recruitment maneuvers, or pressure spurts over a short of time, in the absence of a sufficient PEEP allows for potential collapse of the alveoli that had just been recruited (Halter et al., 2003). In another *in vivo* study of alveolar responses to mechanical ventilation, brief increases in pressure with V<sub>t</sub> failed to induce sustained alveolar recruitment, supporting the importance of the inspiratory time on alveolar opening (Kollisch-Singule et al., 2014a). Although medium to high PEEP attenuates some degree of alveolar collapse at end expiration, extended expiratory times led to alveolar derecruitment (Kollisch-Singule et al., 2014a). Taken together, the inspiratory to expiratory ratio

plays an important role in alveolar stability with brief inspiratory times and extended expiratory times leading to increased alveolar micro-strain with wide amplitude swings between inspiration and expiration (Kollisch-Singule et al., 2014a).

The development of alveolar instability is not immediate and is dependent on the time alveoli are exposed to injurious mechanical ventilation settings (Pavone L.A. et al., 2007). In a murine model, alveoli that are initially exposed to injurious mechanical ventilation settings in the form of low PEEP with a high driving pressure did not immediately reveal instability (Pavone L.A. et al., 2007). Progressive injury, measured in the form of recruitment/derecruitment, took up to 30 min to manifest, with progressive injury demonstrated over time (Pavone L.A. et al., 2007).

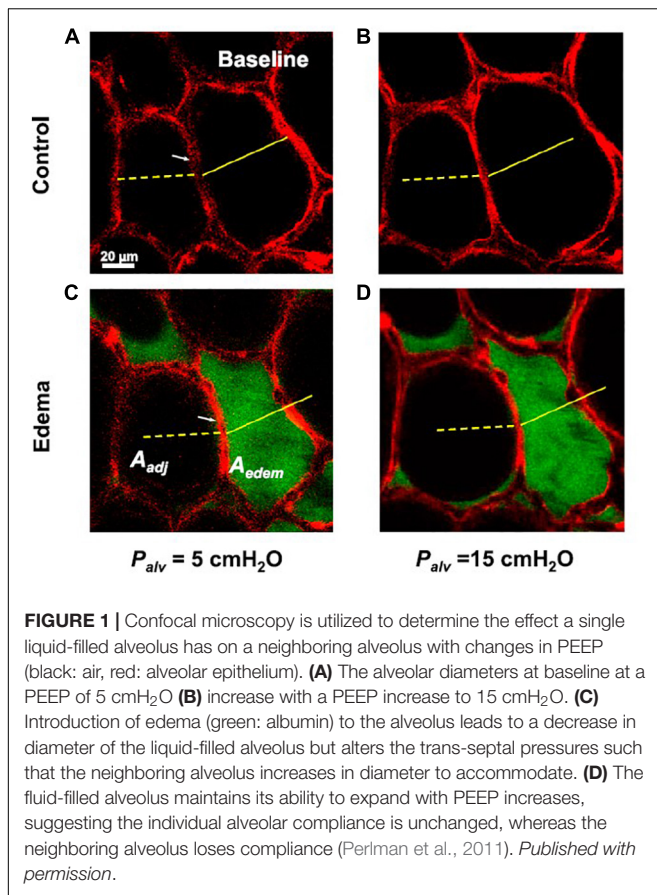
The importance of time is not limited to the alveoli. The alveolar ducts in the setting of low PEEP with an extended expiratory time and brief inspiratory time can be injuriously distended with increased micro-strain (Kollisch-Singule et al., 2014b). Alveolar collapse in proximity to an airway can lead to heterogeneous parenchymal tethering which can impact airway stability and peribronchial stress (Ryans et al., 2019). This parenchymal heterogeneity can drive further injury, however, higher mean airway pressures, a function of both pressure and time, also have a stabilizing effect on the parenchyma (Roy et al., 2013; Ryans et al., 2019).

Yamaguchi et al. (2017) demonstrated in an *in vitro* model of non-uniform bifurcating airways that flow will divert to the airways of lower resistance. Variation in airway width affects both hydraulic and capillary pressures and therefore has a greater divergence pattern as compared with variations in airway length, which affects hydraulic resistance alone (Yamaguchi et al., 2017). The study demonstrated that a 15% change in width between two airways can lead to a 100-fold change in relative velocity through the airways when combined with high surface tension, but that lower surface tension has a protective effect on asymmetric reopening (Yamaguchi et al., 2017).

In a mathematical model of a heterogeneous airway network, Stewart and Jensen (2015) found that the air finger, which mimics the pressure delivered by the mechanical ventilator, halts its progression through the airway network at specific points. These points of stagnation occur where the ductal opening pressure is greater than the delivery pressure, and the airway network will not open until either the airway pressure or the time of this applied pressure is increased, which triggers further recruitment (Stewart and Jensen, 2015). Full recruitment of the airway network was found to be dependent on the airway pressure, the time a given pressure was applied, and airway heterogeneity (Stewart and Jensen, 2015).

## ALVEOLAR EDEMA

One of the primary physiologic factors leading to ARDS is the accumulation of alveolar edema, which impairs gas exchange, deactivates surfactant, and leads to heterogeneous mechanical ventilation and ultimately a higher mortality (Greene et al., 1999; Warriner et al., 2002). Stress is concentrated between healthy



and edematous alveoli (Wu et al., 2017). This stress level is proportional to the surface tension and can be exacerbated by mechanical ventilation (Wu et al., 2017).

In a study by Perlman et al. (2011) confocal microscopy was utilized to determine the effect of a single liquid-filled alveolus on neighboring alveoli when exposed to varying pressures. In that study, the edematous alveolus decreased in size at a PEEP of 5 cmH<sub>2</sub>O but maintained its ability to increase in size in response to rising pressure, suggesting the individual alveolar compliance is unchanged (Perlman et al., 2011). But the presence of edema changed the *trans*-septal pressures such that the septum bowed toward the fluid-filled alveolus, mandating that the neighboring alveoli increased in size to accommodate, with a concomitant loss in compliance by approximately 24% (**Figure 1**) (Perlman et al., 2011). This phenomenon is well-supported by simulation models of injured and healthy alveoli which reveal that the recruitment maneuvers and pressures necessary to stabilize injured alveoli may lead to overdistension of the neighboring alveoli (Schirrmann et al., 2010).

Alveolar edema is also heterogeneous with alveolar flooding of the dependent regions of the lung and less flooding of the non-dependent regions (Wu et al., 2014). In an isolated perfused lung model with induced alveolar flooding, the permeability of the alveolar-capillary barrier increased over the study duration (Wu et al., 2014). Ventilation in all forms was found to be injurious, particularly with higher tidal volume, PEEP, and surface tension

(Wu et al., 2014). This study therefore highlights the importance of protecting the alveoli and alveolar ducts from edema with protective mechanical ventilation before the injury has a chance to occur (Nieman et al., 2018).

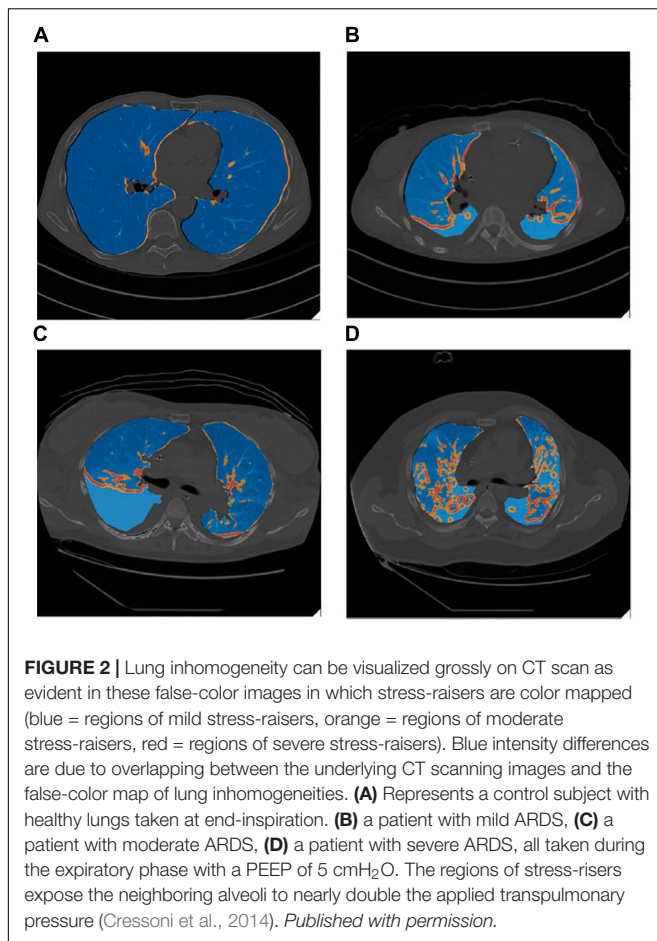
In another isolated perfusion lung model of both local and global alveolar edema, the impact of surface tension and accelerated deflation on alveolar edema clearance was studied (Wu et al., 2017). In lungs with local edema alone, and thus a relatively normal surface tension, accelerated deflation led to release of fluid from flooded alveoli, allowing for redistribution of the fluid, and a decrease in flooding heterogeneity (Wu et al., 2017). In lungs with global edema, accelerated deflation also led to release of fluid from flooded alveoli, but the fluid redistributed to neighboring alveoli due to the higher surface tension, with no improvement in flooding heterogeneity (Wu et al., 2017). The importance of accelerated deflation on mucous clearance has similarly been described in a porcine lung model and represents a ventilator setting that may alter the lung micro-environment (Mahajan et al., 2019).

## ALVEOLAR HETEROGENEITY

An injured lung induces heterogeneity at the level of the terminal airways which concentrates regional stress secondary to atelectasis, edema, and alterations in alveolar surface tension (Greene et al., 1999; Mertens et al., 2009; Schirrmann et al., 2010). This regional stress can concentrate alveolar strain to up to quadruple that of global strain (Rausch et al., 2011), propagating additional alveolar injury, apoptosis (Tschumperlin and Margulies, 1998), inflammation (Albaiceta and Blanch, 2011), and even membrane rupture (Vlahakis and Hubmayr, 2005). Given the degree of heterogeneity that manifests both at the regional and at the microscopic level in the injured lung, a given V<sub>t</sub> will not distribute evenly but will rather preferentially distribute to the regions of increased alveolar compliance (Cressoni et al., 2014; Zhao et al., 2014).

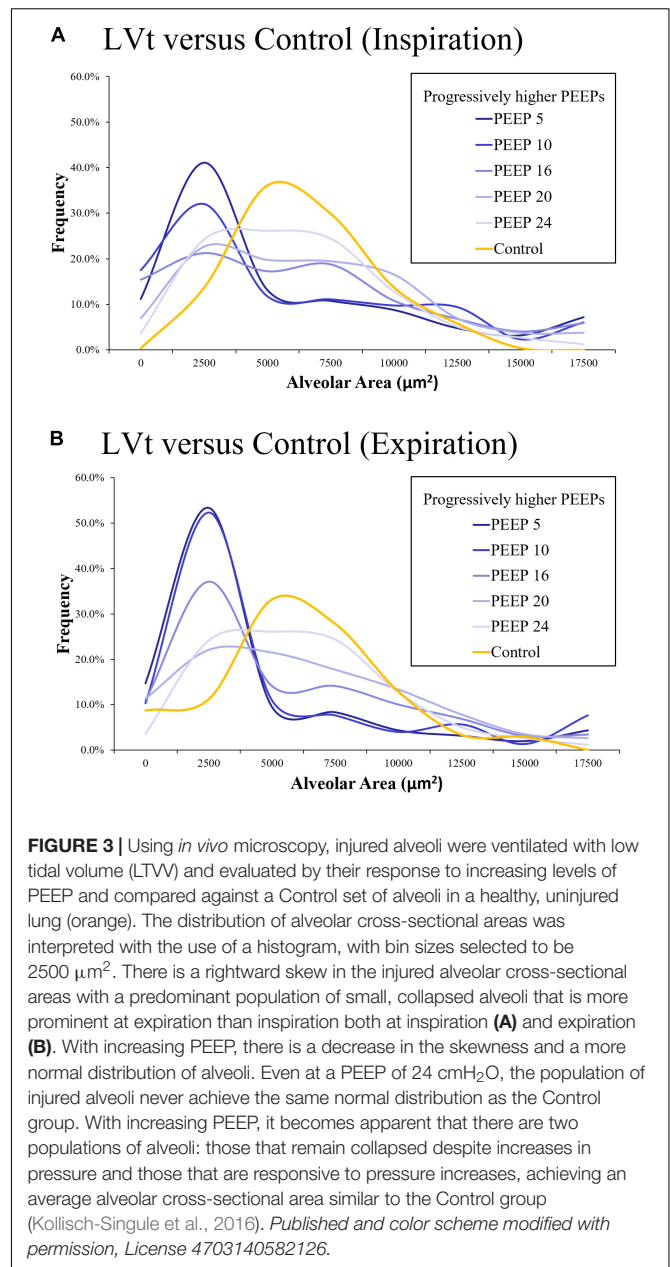
Lung inhomogeneity is correlated with not only the severity of ARDS but also with patient mortality (Cressoni et al., 2014). The degree of lung inhomogeneity in a patient with ARDS can be quantified using computerized tomography scans and determining regions of stress-risers where there is an inferred regional amplification of forces (**Figure 2**) (Cressoni et al., 2014). Theoretically, when lungs are healthy and homogeneously inflated, a delivered pressure will distribute across an open set of alveoli and the load-bearing elements will be exposed to the same degree of stress, such that the stretch elements will uniformly expand (Roan and Waters, 2011). In reality, stress is concentrated in regions of inhomogeneity where an open alveolus is adjacent to a collapsed or fluid-filled alveolus (Mead et al., 1970). Cressoni et al. (2014) calculated this stress multiplication factor to be an average of 1.9, concluding that these regions of increased stress are exposed to nearly double the applied transpulmonary pressure (**Figure 2**).

For the majority of patients, lung inhomogeneity decreases with increasing airway pressures but this is not true in all patients in which PEEP, lung inhomogeneity, and lung recruitability



were not related (Cressoni et al., 2014). This is consistent with other studies which have demonstrated that the best PEEP is not always the highest PEEP (Kollisch-Singule et al., 2014a), particularly when patients are stratified according to whether the ARDS is pulmonary or extrapulmonary in origin (Gattinoni et al., 1998), and has prompted searches for an algorithm to calculate the best PEEP for an individual patient (Chiumello et al., 2014). These scaled PEEP maneuvers, however, do not consider the heterogeneity within the subunits of the lung where regional specific tissue elastance, edema, and atelectasis will have different responses to the macro-parameter changes that are set on the ventilator (Chiumello et al., 2014; Pintado et al., 2017; Writing Group for the Alveolar Recruitment for Acute Respiratory Distress Syndrome Trial Investigators et al., 2017; Beitler et al., 2019).

On a microscopic level using *in vivo* microscopy, injured alveoli were evaluated by their response to increasing levels of PEEP (Kollisch-Singule et al., 2016). Increases in alveolar homogeneity were observed with higher set PEEP and  $P_{aw}$ , and particularly in the setting of an inverted inspiratory to expiratory ratio (**Figure 3**) (Kollisch-Singule et al., 2016). Re-establishing alveolar homogeneity becomes more difficult as alveoli become more injured (Kollisch-Singule et al., 2016). Even with PEEP levels set as high as 24 cmH<sub>2</sub>O, the population of



injured alveoli never achieved the same normal distribution of alveolar sizes as compared with a Control group of healthy alveoli (Kollisch-Singule et al., 2016). With increasing PEEP, it became apparent that there were two distinct populations of alveoli: those that were responsive to PEEP with a mean cross-sectional area similar to that of the Control group and a group of non-responders with an average cross-sectional area markedly less than that of the Control group (**Figure 3**) (Kollisch-Singule et al., 2016). This may be one reason why trials that set an arbitrarily higher PEEP do not routinely demonstrate a lower mortality than those patients set with lower PEEP, as the setting adjustments did not target the underlying alveolar pathophysiology (Mercat et al., 2008).



High-frequency oscillatory ventilation (HFOV) is a ventilation mode that should be considered lung-protective with increased mean airway pressures and small tidal volumes promoting recruitment while minimizing lung injury and ventilation-to-perfusion mismatching (Kaczka et al., 2015; Herrmann et al., 2020), but it is generally applied with a single frequency, and has failed to demonstrate improved outcomes over conventional modes (Ferguson et al., 2013; Young et al., 2013). HFOV, like all ventilator modes, relies on inference to predict how changes in pressure, frequency, and flow lead to changes in the alveoli and alveolar ducts (Herrmann et al., 2020). Using a computational model of the human lung, Herrmann et al. (2020) demonstrated that HFOV applied to all lung sizes, but especially larger lung sizes, resulted in regional heterogeneity, and that increasing frequency led to increasing flow heterogeneity. This study therefore demonstrated that increasing frequency in order to lower tidal volume may propagate lung injury by promoting ventilation heterogeneity (Herrmann et al., 2020). Furthermore, these results highlight the importance of considering the individual patient pathology, with each set of lungs benefiting from a different frequency and change in pressure (Herrmann et al., 2020).

One ventilation strategy that has been developed to account for underlying heterogeneity is that of multi-frequency oscillatory ventilation (MFOV) (Kaczka et al., 2015). Herrmann et al. (2018) demonstrated that the use of two frequencies led to reduced acinar strain heterogeneity as compared with the use of either isolated frequency. Kaczka et al. (2015) elevated this idea by proposing MFOV as a method of applying several frequencies simultaneously, thereby taking into account the regional heterogeneity that exists in the premature and injured lung, and minimizing underventilation of one region and overventilation of another. Using a preterm lamb model, MFOV resulted in a more uniform distribution of gas flow to the alveoli with a lower distending pressure, improved oxygenation index, and reduced respiratory system elastance, as compared with traditional single frequency oscillatory ventilation (Kaczka et al., 2015).

In a murine model of lung injury induced by surfactant wash-out and moderate tidal volumes ( $V_t$  12 mL·kg<sup>-1</sup>, PEEP 3 cmH<sub>2</sub>O), the lung parenchyma was analyzed with CT (Cereda et al., 2016b). This study demonstrated that ventilator induced lung injury propagated from the induced regions of lung injury concentrically outward (Cereda et al., 2016b). This suggests the alveoli neighboring the injured tissue are subjected to increased strain and subsequent injury from recruitment/derecruitment (Mertens et al., 2009; Cereda et al., 2016b). In a parallel group of rats that received no lung injury but injurious mechanical ventilation by way of large tidal volumes and ZEEP ( $V_t$  30 mL·kg<sup>-1</sup>, PEEP 0 cmH<sub>2</sub>O), the ventilator induced lung injury was found to begin in the periphery and spread centrally (Cereda et al., 2016b). This heterogeneous injury pattern is likely due to dependent alveoli/alveolar ducts undergoing recruitment/derecruitment (Cereda et al., 2016b).

In a murine model of surfactant depletion, atelectasis was found to occur primarily in dependent regions of the lung but demonstrated that ventilator induced injury occurred in the

non-dependent/non-atelectatic regions (Tsuchida et al., 2006), likely because tidal volumes were distributed to the regions of increased compliance (Gattinoni and Pesenti, 2005). Another murine study of healthy lungs mechanically ventilated with  $V_t$  10 mL·kg<sup>-1</sup> and ZEEP plus recruitment maneuvers used CT and MRI imaging to determine regional lung variations in response to mechanical ventilation (Cereda et al., 2016a). Ventilation with ZEEP led to heterogeneity of and an increase in regional fractional ventilation as measured by MRI, yet did not demonstrate macroscopic atelectasis on CT scan (Cereda et al., 2016a). This study demonstrated both the heterogeneous effect mechanical ventilation may have on the lung and also that subtle alterations in the micro-environment may not manifest on a macro-scale (Cereda et al., 2016a).

## SUMMARY AND CONCLUSION

Investigating the response of alveoli to parameters set on the mechanical ventilator may help to determine protective mechanical ventilation strategies that are also broadly protective at the microscopic level and take the physiology of the various underlying micro-environments into account. The mechanical ventilation modes and settings that appreciate alveolar stability will ultimately be the ones that minimize ventilator induced lung injury and limit the mortality of ARDS. When considering alveolar micromechanics in the acutely injured lung, alveolar instability may be directly related to alveolar heterogeneity and high alveolar  $V_t$ .

Alveolar  $V_t$  are not determined by the  $V_t$  set on the mechanical ventilator but by the number of recruited alveoli available to accommodate that  $V_t$  and their heterogeneous mechanical properties. Thus,  $LV_t$  set on the ventilator can lead to high alveolar  $V_t$  when imposed on a partially collapsed lung, but a high  $V_t$  set on the ventilator can lead to low alveolar  $V_t$  when expressed over a recruited lung with open, homogenous alveoli. In parallel, the pressure that alveoli are exposed to may not be as important as the duration of time those alveoli are exposed to a given pressure. A higher pressure when applied in only brief spurts may not improve long-term alveolar recruitment but may conversely cause harm with large amplitude pressure swings leading to increased strain. But a low pressure exposed over an extended period of time may be insufficient to open alveoli with high opening pressures (Albert et al., 2009). Thus, medium to higher pressures over an extended duration of time may be crucial to achieving alveolar stability. Finally, heterogeneity may be present on several size scales within the lungs, regions of the lung, alveolar subunits, and even the individual alveolar constituents.

CT scans can show regional atelectasis, edema and changes in tissue density to suggest unstable inflation (Cereda et al., 2016a, 2017; Xin et al., 2018) but is not specific enough to detect the immediate response of the alveoli and alveolar ducts to changes in mechanical ventilation (Cereda et al., 2016a, 2019). Electrical impedance tomography has demonstrated usefulness as a potential bedside tool to demonstrate changes in regional ventilation but may not be sensitive enough to detect subtle changes (Kaczka et al., 2015). Oxygenation has



been demonstrated to be a poor marker of alveolar instability (Halter et al., 2003; Andrews et al., 2015). Pressure-volume curves have also been shown to be a suboptimal indicator of alveolar recruitment and derecruitment (Dirocco et al., 2007). The ventilator calculates the respiratory system compliance [ $V_t/(P_{\text{plat}} - \text{PEEP})$ ] but does not partition out lung and chest wall compliance (Hess, 2014) where the lung compliance is impacted by alveolar stability (Pavone L. et al., 2007; Knudsen et al., 2018). The lung compliance as a single value may not account for the regional and alveolar heterogeneity associated with the injured lung (Kollisch-Singule et al., 2016), with discordant alveolar compliance even in adjacent alveoli (Perlman et al., 2011; Broche et al., 2017).

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- Thus, many of the bedside maneuvers clinicians have available to guide mechanical ventilation alterations are poor mirrors of alveolar health and stability. With experimental data, this review highlights some of the known mechanical ventilation adjustments that are helpful or harmful at the level of the alveolus.
- ## AUTHOR CONTRIBUTIONS
- MK-S drafted the manuscript. JS, SB, PA, LG, GN, and NH critically revised the manuscript. All authors read and approved the final manuscript.
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# Ventilation and Perfusion at the Alveolar Level: Insights From Lung Intravital Microscopy

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Intravital microscopy (IVM) offers unique possibilities for the observation of biological processes and disease related mechanisms *in vivo*. Especially for anatomically complex and dynamic organs such as the lung and its main functional unit, the alveolus, IVM provides exclusive advantages in terms of spatial and temporal resolution. By the use of lung windows, which have advanced and improved over time, direct access to the lung surface is provided. In this review we will discuss two main topics, namely alveolar dynamics and perfusion from the perspective of IVM-based studies. Of special interest are unanswered questions regarding alveolar dynamics such as: What are physiologic alveolar dynamics? How do these dynamics change under pathologic conditions and how do those changes contribute to ventilator-induced lung injury? How can alveolar dynamics be targeted in a beneficial way? With respect to alveolar perfusion IVM has propelled our understanding of the pulmonary microcirculation and its perfusion, as well as pulmonary vasoreactivity, permeability and immunological aspects. Whereas the general mechanism behind these processes are understood, we still lack a proper understanding of the complex, multidimensional interplay between alveolar ventilation and microvascular perfusion, capillary recruitment, or vascular immune responses under physiologic and pathologic conditions. These are only part of the unanswered questions and problems, which we still have to overcome. IVM as the tool of choice might allow us to answer part of these questions within the next years or decades. As every method, IVM has advantages as well as limitations, which have to be taken into account for data analysis and interpretation, which will be addressed in this review.

**Keywords:** intravital microscopy, alveolar dynamics, alveolar perfusion, pulmonary microcirculation, acute lung injury, lung video microscopy

## INTRODUCTION

Intravital microscopy (IVM) is a two-dimensional imaging technique that allows for visualization of biological processes *in vivo*. It is highly versatile as it can be adjusted to various tissues and can be combined with high quality state-of-the-art microscopy enabling high resolution of tissue and single cells in the natural and complex environment of a multicellular organism (**Figure 1**). Some tissues in experimental animals are easily accessible, such as the vessels of the ear or can

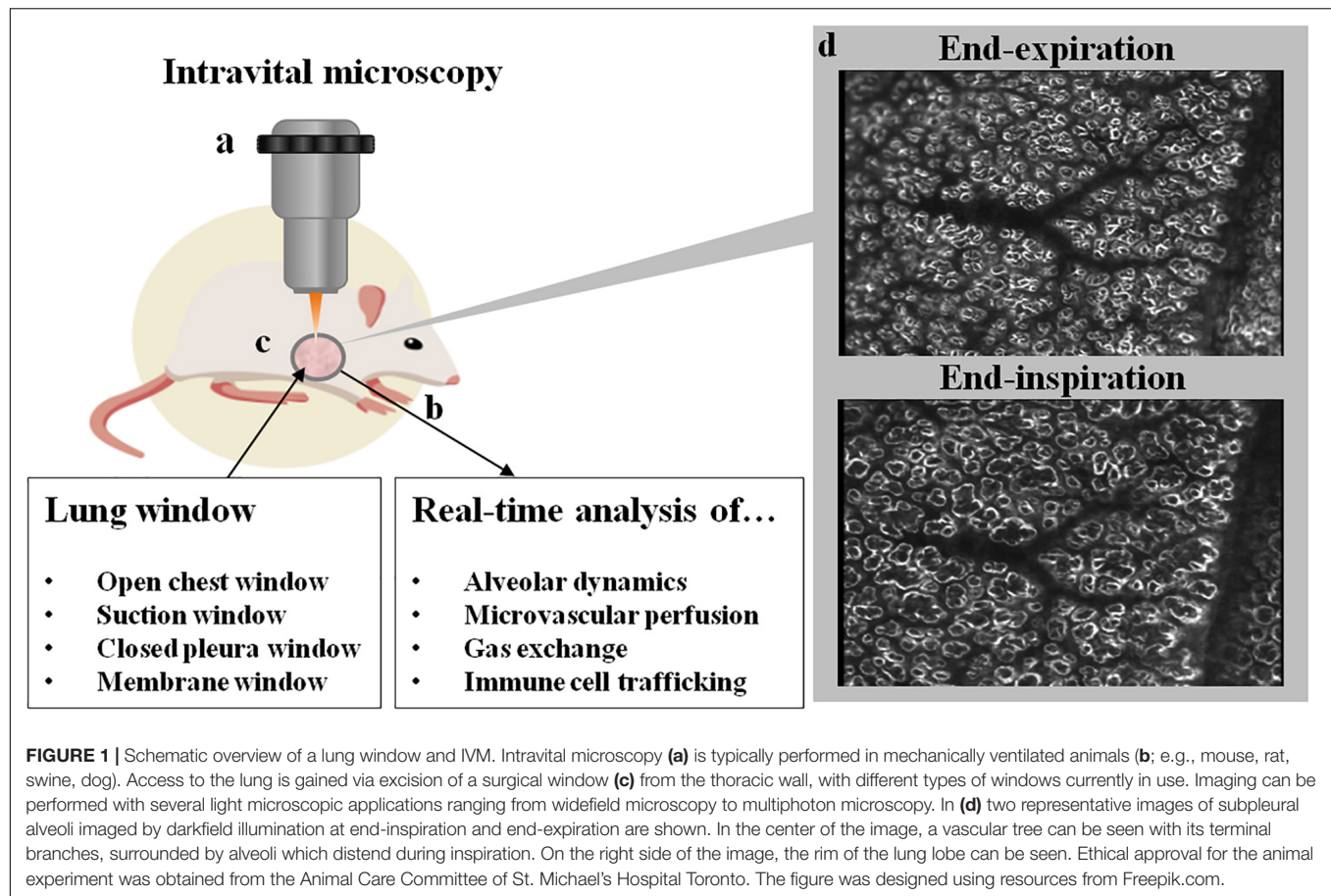


be easily exteriorized in mice for vascular IVM studies such as the mesentery or the cremaster muscle. For internal organs and/or chronic observation, the implantation of imaging windows is typically required, and widely used as abdominal, cranial and thoracic windows, as well as dorsal skin fold chambers. Depending on the desired penetration depth, the spatial resolution and the temporal resolution, different microscopic methods can be applied, ranging from widefield, laser scanning confocal, spinning disk, multi-photon microscopy or others. The use of fluorescent dyes and transgenic animals expressing fluorescent markers opens seemingly endless possibilities for the visualization of *in vivo* biological processes down to the subcellular level.

Albeit generations of excellent scientists have advanced our understanding of respiratory physiology to the current stage (Rahn et al., 1946; Suki and Bates, 2011), one of the most basic physiological principles, i.e., alveolar dynamics, is still surprisingly poorly understood. Our insight into the dynamic processes has been hampered by the limited accessibility of alveoli for dynamic studies at the microscale *in vivo* (Grune et al., 2019). Due to the lung's complex structure, direct visualization by IVM is only possible for structures close to the lungs surface, such as subpleural alveoli. *In vitro*, as well as *ex vivo* or *in situ* models can only partially reflect the complex physiologic situation at the level of the alveolus and its surrounding capillary network in health and disease. Standard clinical and experimental imaging approaches including X-ray, computer tomography (CT), magnet resonance imaging (MRI), positron emission tomography (PET) and single photon emission computed tomography (SPECT) are able to image the whole lung and thus, provide important insight into disease state and general mechanisms, but are unsuitable to detect structures and processes at the microscale alveolar level. At the moment no non-invasive imaging technique is available that would enable the imaging of the alveolar or capillary microarchitecture *in vivo* at single-cell or subcellular resolution. The same applies to dynamic phenomena, such as alveolar dynamics, defined here as changes in alveolar size and morphology over the time course of the respiratory cycle in consideration of the underlying biophysical forces, or capillary microhemodynamics, i.e., microvascular flow characteristics and their determining factors in alveolar capillaries. Due to its anatomical complexity (Schneider et al., 2019) and dynamic behavior both at the level of ventilation and perfusion, direct imaging can provide unique insights into our understanding of lung physiology, perfusion and immunology, especially at the alveolar level. Yet, IVM of the lung simultaneously poses a series of unique problems, such as the restricted accessibility of the organ within an anatomical cavity at physiologically subatmospheric pressures. The three-dimensional structure of the alveolo-capillary unit comprises abundant air-liquid interfaces which prevent exploitation of e.g., multiphoton imaging for deep tissue penetration. The dynamic behavior of the lung tissue poses unique problems in terms of motion control. And finally its immunoprivileged status predilects the lung for immune reactions in response to surgical trauma or mechanical ventilation. Although IVM has been successfully used to study pulmonary microvascular responses as well as alveolar

mechanics in real-time, the emerging understanding of alveolar physiology and pathophysiology are both still far from complete. Importantly, these limitations in our understanding are only in part attributable to a relatively small number of studies due to the complexity of such analyses. Adding to such limitations are controversial interpretations of the observations obtained from IVM. Such differences in interpretation relate in part to the above-mentioned methodological limitations of IVM, but also to the question how alveolar dynamics should be described, and what constitutes normal vs. pathological behavior, as will be discussed later in this review.

The key function of the pulmonary system is gas exchange, which is predominantly localized in the highly specialized respiratory zone, the alveoli. Interestingly, alveolarization and maturation of the microvasculature are the only developmental processes of the lung that continue after birth, up to 21 years (Schittny, 2017), emphasizing the importance and intricacy of the alveolar system. Alveoli are the dead-end of the respiratory tree and enable the uptake of oxygen and the removal of carbon dioxide at the alveolar membrane. To this end, the total alveolo-capillary membrane, comprised of the alveolar epithelial wall facing the gas side, the endothelial wall at the blood side, and a single fused basement membrane between the two, is extremely thin (at some places <100 nm thick). Almost 90% of the lung acts as a functional respiratory zone (parenchyma) with 300 million alveoli and an incredible surface area of 143 m<sup>2</sup> (Gehr et al., 1978). The quality of gas exchange of the lung is directly dependent on the number of functional alveoli, the thickness of the alveolo-capillary membrane, alveolar vascularization and perfusion. In various lung diseases, this delicate alveolar design can be compromised leading to injured and dysfunctional alveoli and impaired gas exchange which in some cases will require supplemental oxygen or even mechanical ventilation. A prime example for such an acute scenario is the acute respiratory distress syndrome (ARDS), an acute failure of the respiratory system with an in-hospital death rate of approximately 30% (Petrucchi and Iacovelli, 2007). ARDS is a multifactorial disease with various underlying causes, but is usually characterized by a rapid onset, an extensive inflammation of the lungs, and clinical characteristics such as failure of the alveolo-capillary barrier resulting in severely impaired gas exchange and abnormal low blood oxygenation (hypoxemia). In the absence of effective pharmacological treatments, mechanical ventilation is presently the mainstay of therapy to warrant oxygenation in ARDS. Yet, mechanical ventilation is a double-edged sword and has to be used with caution. On the one hand mechanical ventilation is essential for the patients' survival, but on the other hand it can inflict permanent damage to the lung referred to as ventilator-induced lung injury (VILI) or ventilator-associated lung injury (VALI) (Amato et al., 1998), which negatively impacts both survival and post-survival life-quality. In already injured alveoli mechanical ventilation can impose further damage to the alveolar wall by physical and biological stresses, such as volutrauma, biotrauma or ergotrauma (which will be discussed in greater detail in the section: intravital microscopy for analysis of alveolar dynamics), although there is no consensus with respect to the main mechanism of injury.



Although – as will be discussed later – important limitations exist, IVM is currently the gold standard for visualization of alveoli *in vivo* and offers a broad potential to provide new insight into alveolar dynamics. In this review we will draw attention to the opportunities but also to the challenges and limitations of IVM in this context. We will discuss the use of IVM in different fields of lung research and provide a perspective for future areas of research. First, we will begin with a brief background on the development of IVM in lung research.

## INTRAVITAL MICROSCOPY OF THE LUNG – FROM EARLY BEGINNINGS TO CURRENT STATE-OF-THE-ART

Although IVM of the lung will be considered by many as a very modern or recent technique, it was in fact applied as early as in 1661 by Marcello Malpighi. Malpighi observed the pulmonary microvasculature of the frog lung with a microscope and described for the first time alveoli and the surrounding alveolar capillaries (Young, 1929). More than 250 years later in 1925, Harry Hall visualized the pulmonary microcirculation in cats and rabbits by transilluminating the lung lobes outside of the chest (Hall and Chapman, 1925). Taking into account the importance of the natural physiologic environment of the

lung, Hall's approach to open up the chest and remove the lung for examination was successively replaced by a more elegant method, the thoracic window technique. The first attempt to create a thoracic window was accomplished by the removal of muscle from the rib cage with the parietal pleura being left intact (Wearn et al., 1934). The lung of the paralyzed animals was then transilluminated with a beam of light entering from a second window in the diaphragm. With this technique, Wearn et al. (1934) were able to describe the basis of capillary recruitment in the lung. The analysis of subpleural alveoli under closed thorax/chest condition was established in 1935 by Terry by implantation of a hollow metal cylinder centered by a cover glass (Terry, 1939). This revealed, however, a new problem of intravital imaging, namely the cyclic respiratory movements of the lung leading to motion artifacts. Wagner (1969) solved this problem in a canine model by a suction device which fixed the lung surface to a coverglass via negative pressure that was applied through a series of bore holes. This suction manifold was able to markedly reduce respiratory motion within the window of observation. Almost 50 years later, an improved lung window for stabilized imaging in mice was established by Looney et al. (2011) enabling live-imaging and in particular single cell tracking by two-photon imaging in an area of observation that is immobilized by a suction device. Vacuum suction stabilized lung windows are now widely used to analyze the pulmonary immune system (Looney et al.,

2011). This includes neutrophil margination (Kuebler et al., 1994, 1997; Park et al., 2019) or immune cell – tumor cell interactions (Hanna et al., 2016), as well as infections of the lung (Sewald, 2018; Ueki et al., 2018).

Yet, although suction devices can effectively reduce or even eliminate motion artifacts in IVM, mechanical stabilization of the lung surface generates a non-physiological situation that prevents adequate assessment of alveolar dynamics and the effects of ventilation on microvascular perfusion. In addition, suction of the lung surface to a glass window for observation may potentially injure the sensible lung surface and stimulate inflammatory responses. To overcome these limitations, Tabuchi et al. (2008) developed a thoracic window without suction in which the lung is allowed to move freely within a closed chest cavity, thus mimicking physiological situations at the expense of image stabilization. In this approach, a thoracic window of 7 mm in diameter is generated by removal of chest muscles and ribs, and a transparent membrane is glued to the thoracic wall to re-create a closed-chest situation. With the help of a transdiaphragmal catheter the pleural air is removed and negative pleural pressure re-established, lifting the lung surface to the membrane-sealed lung window for microscopic observation. Although movements from respiratory and cardiac cycles persist in this model, identical areas will return into the microscopic focus plane during the inspiratory or expiratory plateau phase, allowing for ventilation-triggered imaging acquisition during these periods. By use of this approach Tabuchi and colleagues studied blood oxygenation (Tabuchi et al., 2013) and alveolar dynamics in healthy and diseased lungs (Mertens et al., 2009; Nickles et al., 2014; Tabuchi et al., 2016).

Similar to the “pleural window” by Wearn et al. (1934), Mazzuca et al. (2014) created an “intact pleural window” (size 0.5 cm<sup>2</sup>) by removing tissue down to the transparent parietal pleura allowing for direct visualization under closed-chest conditions without the implantation of a “artificial” lung window. This technique combines the advantages of the “physiological” free-moving lung in the Tabuchi model with a reduced surgical trauma at the expense of a smaller area of observation (i.e., one intercostal space). Other researchers adjusted their lung window by placing it in a small chamber at 37°C to exclude temperature-related adverse effects on the tissue directly located under the window surface (Kreisel et al., 2010).

All of the abovementioned lung windows are typically used for short-time imaging that does not exceed several hours. Only a few lung windows have been reported that may allow for long-term observations in dogs, rabbits (De Alva and Rainer, 1963), rats (Fingar et al., 1994) or mice (Kimura et al., 2010), albeit without stabilization and at low spatial resolution. Recently, however, Entenberg and colleagues developed an impressive model of a permanently implanted lung window in mice, which is minimally invasive, allowing the mouse to awake from the surgical intervention and breathe independently. For this approach the authors used an inert and corrosion-resistant steel window for high-resolution imaging of the lung (WHIRL) that allows for long

term observation of the different stages of lung metastasis (Entenberg et al., 2018). According to this initial report, the window offers similar high-quality images as classic suction-fixed lung windows, with the possibility to visualize the same lung area repeatedly over several weeks by use of an established technique for microcartography (Entenberg et al., 2018). If this approach should be replicable in other labs and allow for longitudinal observations, it would open multiple new opportunities to monitor the progression of lung diseases. This would include changes in alveolar dynamics, microhemodynamics, microvascular tone regulation, and immune cell trafficking in animal models of different lung diseases including but not limited to ARDS/acute lung injury, lung fibrosis, COPD, pulmonary hypertension, and other parenchymal and vascular lung diseases.

Beside their “classic” use for intravital imaging, lung windows have also been effectively used to measure alveolar pressures in a closed-chest model in dogs (Bates et al., 1989), illustrating the versatility of the lung window approach. To this end, a small incision was made into the parietal pleura, and visceral and parietal pleura were glued together in this area. Next, a small plastic capsule was glued to the surface of the lung with a piezoresistive pressure transducer puncturing the visceral pleura for alveolar pressure measurement.

Despite the successful application of lung windows over several decades, some key limitations have to be taken into consideration for the study of alveolar dynamics. These restrictions relate in particular to four points, which will be discussed in greater detail in the chapter “Limitations of IVM”: First, IVM limitation to two-dimensional imaging, preventing three-dimensional analysis of alveolar dynamics. Second, IVM is presently restricted to structures at or close to the organ surface such as subpleural alveoli, while deeper lung compartments cannot be accessed. Third, IVM can only image and analyze a small percentage of the total number of alveoli. Fourth, the specific location at which IVM is performed may impact the findings, e.g., due to its position within the hydrostatic gradient of the lung (pulmonary bases vs. apex).

## INTRAVITAL MICROSCOPY FOR ANALYSIS OF ALVEOLAR DYNAMICS

Breathing is a complex process, in which air flows into the lung via the airways along a pressure gradient created by the contraction of the diaphragm and the external intercostal muscles. When external intercostal muscles and the diaphragm relax, lung elastic fibers and alveolar surface tension will cause a decrease in lung volume and thus, exhalation of carbon dioxide rich gas. Although the anatomical and physiological changes during the respiratory cycle at the level of the whole lung are well understood, there is presently no consensus on the corresponding tissue dynamics at the alveolar levels. Rather, different and in part mutually exclusive concepts and theories have been proposed how alveoli may behave during the physiological respiratory



cycle, and in particular in diseased lungs, which will be described in more detail in the following paragraphs.

## Alveolar Dynamics in Healthy Lungs

In 1929 the physiologist Charles Clifford Macklin was one of the first to study the mechanics of the distal airspaces during the respiratory cycle. He assumed that the main volume change in the respiratory area during breathing occurs in the alveolar ducts and not the alveoli itself. This concept was based on the notion that alveoli experience almost no stretch, except for the border area between alveolar duct and alveoli. Rather, ventilation would be controlled by a continuous muscle system running from the larynx to the alveoli (Macklin, 1929). Approximately 40 years later this theory was questioned by experiments in feline (Storey and Staub, 1962) and guinea pig lungs (Forrest, 1970) where a rapid-freeze method was applied to analyze lungs at different volumes of inflation. Morphometric methods were applied to quantify the impact of lung volume change on alveolar and alveolar duct dimensions. These studies revealed an increase in alveolar volume (2×) and surface area (70%) when lung volume increased from functional residual capacity to 75–80% of total lung capacity (Storey and Staub, 1962) suggesting isotropic “balloon-like” distension of the alveoli. Subsequent studies by Gil and Weibel using electron microscopy of fixed rabbit lungs similarly suggested a change of alveolar volume as a function of total lung volume and explained it with an unfolding of alveolar septal pleats and folds and uncrumpling of the alveolar surface (Gil and Weibel, 1972; Gil et al., 1979). Notably, the notion of septal unfolding and uncrumpling – albeit providing an intuitive concept for the extraordinary capacity of the lung to accommodate considerable volume changes within the normal breathing range with relatively minor pressure increase – has at large been neglected over the past decade in the discussion of alveolar dynamics. While generations of scientists have studied the effects of mechanical stretch on alveolar epithelial cells using various commercially available or custom-designed stretch devices it is important to note that alveolar epithelial stretch – at least within the confines of normal tidal volumes – may be minimal if alveolar distension and contraction are primarily the result of surface folding/crumpling and unfolding/uncrumpling. Beside unfolding of alveolar septa and isotropic “balloon-like” changes of alveolar size, two other mechanism have been proposed as theoretically possible causes for the change of lung volume during inflation, namely a sequential recruitment of previously collapsed alveolar units or simultaneous changes in alveolar shape and size (i.e., non-isotropic distension) (Gil et al., 1979).

Importantly, the above reported findings were unanimously derived from morphological examinations and stereological analyses of excised and fixed lungs, prevented the analysis of the effects of different inflation levels within the same lung. More importantly, *post mortem* findings can only reflect static conditions yet not the dynamic behavior of alveoli over the respiratory cycle. Just as static and dynamic lung compliance diverge considerably; extrapolations from static end-point measurements of alveolar mechanics may lead to potentially erroneous interpretations regarding the dynamic behavior of

alveoli in the intact lung. Important insights on such dynamic relationships was initially derived from theoretical models, notably the landmark paper by Jere Mead, who demonstrated the role lung distension and its relevance for the uniform expansion of air spaces (Mead et al., 1970). Other important topics addressed by theoretical models were stress-strain relationships (Fung, 1975), the dynamics of single vs. multiple alveoli (Schirrmann et al., 2010), as well as more complex alveolar regions (Tsuda et al., 2008; Sznitman et al., 2009).

Moreci and Norman (1973) performed the first *in vivo* observations of alveolar dynamics in a rat open chest preparation using incident light photomicrography. In this study, the authors observed a marked change in the size of the alveolar duct, whereas the alveolar volume only showed minor changes over the respiratory cycle. These findings were confirmed in a subsequent study from the same group (Daly et al., 1975) and would suggest the alveolar duct rather than the individual alveolus as the main site for airspace volume change. The group of Gary Nieman and colleagues, however, who performed an extensive series of IVM studies on alveolar dynamics in healthy and diseased lungs came to very different conclusions. At the end of the 1990s they proposed the concept of alveolar recruitment and derecruitment (R/D) in healthy dog lungs as the main mechanism for lung volume increase (Carney et al., 1999). Specifically, they proposed the recruitment (opening) of new (previously collapsed) alveoli when lung volume was increased from functional residual capacity (FRC) to 80% of total lung capacity (TLC). By IVM of dog lungs in an open chest approach via a glass coverslip that was carefully lowered onto the lung surface, the authors observed a small extent of isotropic alveolar distention during lung inflation, yet only up to 20% of TLC, with no detectable change in alveolar volume with further increases in lung volume. From these data and the observation that the number of alveoli per area of observation increased with higher lung volume, the authors concluded that changes in alveolar number due to recruitment rather than isotropic distension of alveoli (or alveolar ducts) must constitute the primary mechanism of physiological lung volume changes (Carney et al., 1999). In support of this notion, Hajari et al. (2012) calculated a linear increase in the number of alveoli with increasing total gas volume based on measurements by hyperpolarized  $^3\text{He}$  diffusion and MRI in healthy human subjects.

The concept of R/D as primary mechanism of lung volume change during the physiological respiratory cycle contrasts, however, with previous findings of alveolar distension and contraction as the predominant mechanism of volume change in healthy lungs (Storey and Staub, 1962; Forrest, 1970). Analogous to these latter reports, IVM studies of the mechanically unimpaired lung by use of the thoracic window technique developed by Tabuchi et al. (2008) identified alveolar clusters to expand gradually with increasing inspiratory pressure in ventilated mice. The resulting pressure-volume relationship for the individual alveolus followed a sigmoid curve (Mertens et al., 2009) that is largely reminiscent of the classic pressure-volume curve for the entire lung (Rahn et al., 1946). In contrast, the total number of alveoli per area of interest remained unchanged, indicating alveolar distension and contraction rather than R/D



as the main mechanism of lung volume change in this study (Mertens et al., 2009). As IVM is always hampered by the extrapolation of two-dimensional observations to the three-dimensional stage, the latter study was further validated by parallel optical coherence tomography (OCT) which confirmed alveolar distension and contraction at the three-dimensional level (Gaertner et al., 2012).

While IVM in intact, live animals – ideally under minimally invasive, closed chest conditions or even under spontaneous ventilation – is the gold standard for the visualization of alveolar dynamics, a common alternative – albeit less physiological – model used to analyze alveolar dynamics that allows for optimal control of ventilation and perfusion are excised, mechanically ventilated and constantly perfused lungs. By this approach, Namati et al. (2008) observed alveolar distension during lung inflation, yet at the end of inspiration the number of alveoli increased while alveolar volume decreased. The authors interpreted this finding as evidence for R/D and developed the concept of secondary daughter alveoli that get recruited by the primary (mother) alveoli via the pores of Kohn, i.e., hole-like interfaces between neighboring alveoli, rather than the conducting airways (Namati et al., 2008). In subsequent studies the same group switched from isolated lungs to *in vivo* optical frequency domain imaging (OFDI) in swine. Remarkably, in these studies alveolar dynamics were best fitted by uniform alveolar distension, although a heterogeneous component of airspace distension was observed as well (Namati et al., 2013), yet no R/D. These two studies from the same group highlight exemplarily the impact of the chosen experimental model on the results generated. Accordingly, one crucial factor for discordant results in the field of alveolar dynamics might be based on the use of different experimental models and methods, which are further complicated by species differences.

Although in the past 50 years several different groups tried to shed light on alveolar dynamics with different models and methods, no overall consent has been developed and as such, the topic remains controversial. A recent editorial by Nieman (2012) discussing Hajari et al.'s (2012) analysis of alveolar dynamics by MRI-based  $^3\text{He}$  lung morphometry *in vivo* ensued a subsequent debate (Mitzner and Smaldone, 2012; Smaldone and Mitzner, 2012; Weibel et al., 2012) which summed up the different viewpoints and potential problems. As mentioned before Hajari et al. (2012) suggested that alveoli are regularly recruited and derecruited during inflation and expiration with no change of the inner surface area. Smaldone and Mitzner pointed out that these results, albeit showing parallels to their own work, critically depend on adjusting the parameters of a model to a single alveolar duct, thereby simplifying physiologic conditions (Smaldone and Mitzner, 2012). In the same discussion, Weibel highlighted that alveoli are often regarded as a unique structure itself, but that this is a misjudgment and the surrounding tissue and its interactions such as fiber tension and surface forces “make” alveoli. Schittny proposed that alveolar folding can be a proper explanation for recruitment in adult lungs and that R/D may be based on surfactant and surface tensions (Weibel et al., 2012). These different opinions highlight the current state of uncertainty with respect to alveolar dynamics, as – in the words of Smaldone

and Mitzner – “what happens to lung acinar structure with lung inflation in a pathologic or even in a normal healthy lung remains unresolved” (Smaldone and Mitzner, 2012).

## Alveolar Dynamics in Diseased Lungs

The present lack of a consensus regarding normal alveolar dynamics constitutes one of the major obstacles for our understanding of pathological alveolar dynamics in various lung diseases. This is particularly relevant as an appropriate understanding of alveolar dynamics in the diseased lung is likely crucial for the development of optimized or personalized ventilation regimes and for the development of novel therapeutic strategies. The only current consensus on alveolar dynamics in diseased lungs is that they differ from normal alveolar dynamics and that this differential behavior will likely contribute to or aggravate VILI. The situation under pathologic conditions is further complicated by the expected heterogeneity of pathological alveolar dynamics. Alveolar mechanics under physiological conditions can be expected to be essentially uniform over time and even between species. In contrast, alveolar dynamics in injured lungs can be expected to be more heterogeneous at the regional or even local level (i.e., between neighboring alveoli), and may further differ depending on the etiology of ARDS (e.g., direct vs. indirect lung injury), its severity and time course, as well as the presence or absence of additional disease-related comorbidities.

The most popular concept for alveolar dynamics in the acutely injured lung postulates that alveoli become unstable, leading to collapse and reopening during spontaneous respiration and – in particular – mechanical ventilation. Several groups using a diverse set of methods have provided evidence in support of this concept. Taskar and colleagues ventilated rabbits with either healthy lungs (Taskar et al., 1995) or with lungs in which surfactant function had been impaired by inhalation of dioctyl sodium sulfosuccinate (DOSS) (Taskar et al., 1997) in an open chest setting. In both scenarios, ventilation with negative end-expiratory pressure (NEEP) caused R/D. In healthy lungs R/D as a consequence of NEEP ventilation caused a transient yet reversible decrease in arterial oxygenation and lung compliance, but no overt direct injury of the lung tissue on histological examination (Taskar et al., 1995). In contrast, in lungs with impaired surfactant function simulating an acutely injured lung, NEEP caused persistent severe tissue damage with impaired lung mechanics and gas exchange (Taskar et al., 1997). These effects were prevented by ventilation with positive end-expiratory airway pressure, suggesting that R/D may aggravate VILI in pre-injured but not necessarily in healthy lung. In line with these findings, Seah et al. (2011) showed in that a combination of high tidal volume and zero end-expiratory pressure (ZEEP) causes VILI due to R/D in a murine model, which was not the case when mice were ventilated with either high tidal volume or ZEEP. Based on these findings the authors postulated a “map” of “safe” and “unsafe” ventilation settings, highlighting that the “unsafe” area can dramatically widen in injured lungs. A time- and pressure-dependent effect on R/D was observed in saline-lavaged rat lungs following recruitment maneuvers (Albert et al., 2009). While rapid inflation occurred within 1–2 s, recruitment was notably delayed in that it was absent for the first seconds

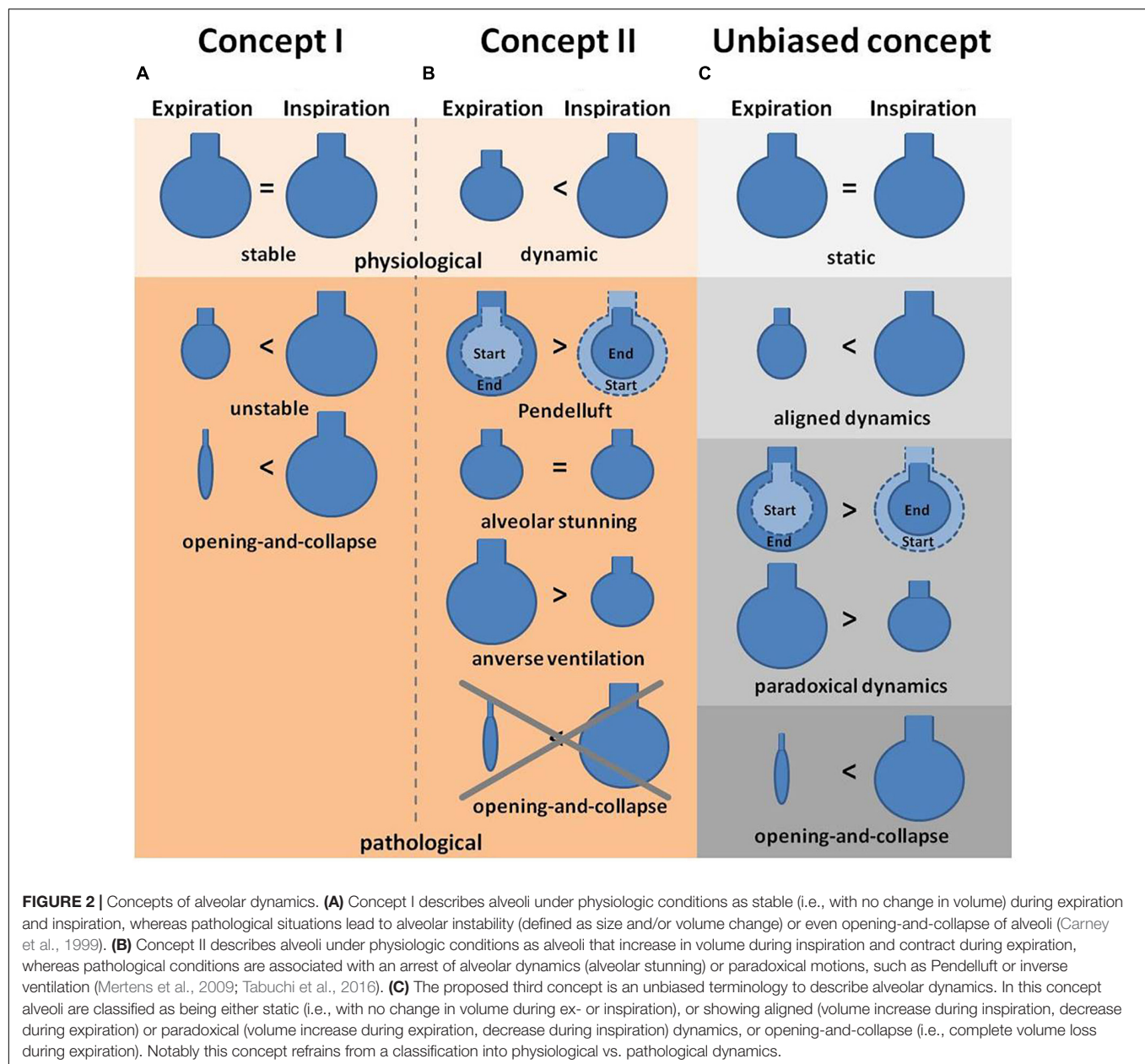
and then continued to progress over the entire measured time-frame of 40 s. This delayed recruitment response may be clinically relevant, as inspiratory time in the clinical setting is commonly in the range of 0.5–1.5 s, thus potentially preventing R/D in the clinical context.

In a different study, Neumann et al. (1998) tested three different injury models for their impact on alveolar dynamics as assessed by CT. After induction of lung injury by oleic acid, endotoxin, or lung lavage in six ventilated pigs, the authors measured lung density and observed a quick onset of R/D in all experimental models. The notion that R/D is a frequent form of impaired alveolar dynamics in injured lungs was further supported by a substantial number of IVM studies from the group of Gary Nieman. In one of their initial studies Nieman et al. (1981) demonstrated the importance of the surfactant stabilizing effect on alveoli in a canine model of surfactant deactivation by pulmonary lavage with Tween 20 or saline (as control), respectively. Surfactant deactivation by Tween lead to distinct changes in alveolar size, with total collapse at end-expiration, later defined as R/D. Within the 4 h of the experimental protocol, alveolar stability was restored. In subsequent studies with Tween-mediated surfactant deactivation in pigs the authors observed heterogeneous lung injury (Schiller et al., 2001) and progressive alveolar instability – notably defined as change in alveolar shape and size, see below – when tidal volume was increased from 6 to 12 and 15 mL/kg bw (Steinberg et al., 2002). A positive end-expiratory-pressure (PEEP) level of 10 cmH<sub>2</sub>O was able to stabilize alveoli, while lower PEEP levels resulted in R/D (Halter et al., 2003). In rats over-ventilated with an inspiratory peak pressure (IPP) of 45 cm H<sub>2</sub>O the authors observed alveolar instability or R/D after 45 min, which persisted for 90 min until the end of the study, yet contrary to what could be expected, gross damage to the alveolar epithelium was not observed. As such, the latter findings argue against a decisive role for R/D in the pathogenesis of VILI (Pavone et al., 2007). This notion is also supported by a series of preclinical and clinical studies suggesting that VILI is less pronounced in areas of cyclic R/D or atelectasis as compared to areas of high stretch and overventilation (Tsuchida et al., 2006; Bellani et al., 2011; Wakabayashi et al., 2014).

In a model of surfactant depletion by Tween instillation Andrews et al. (2015) tested the possibility that R/D may be masked by a proper oxygenation rate, although alveolar dynamics are impaired. The group observed R/D, yet no decline in oxygenation, suggesting that the partial pressure of oxygen (PaO<sub>2</sub>) is not a parameter to identify impairment of alveolar dynamics, such as R/D. This important claim was subsequently validated by Allen et al. (2005) in a rat model of overinflation injury analyzed by pulmonary impedance measurements and *in vivo* imaging. They showed in their study that injurious mechanical ventilation leads to alveolar instability, but already before imbalances in the gas exchange are measurable. It is important to note, however, that the interpretation of these findings critically depends upon the underlying concept of what constitutes physiological vs. pathophysiological alveolar dynamics – and hence, upon a matter of considerable controversy (Figure 2). In the work by Andrews et al. (2015), R/D was defined as increase in alveolar size from expiration to

inspiration – a behavior that many other studies would consider as physiological alveolar dynamics. Specifically, whereas some define distension of alveoli as a pathologic phenomenon, others interpret the distension from expiration to inspiration as the normal physiologic situation and no change in size as a sign for abnormalities. Conversely, as in the studies by Nieman cited above, a lack of change in alveolar size or shape is considered by some as physiological scenario and accordingly termed “alveolar stability”, whereas “alveolar instability” is used in these instances to describe any change in alveolar size or volume during the respiratory cycle. In contrast, other studies interpret alveoli with no volume change as pathological, and alveoli which distend and contract over the respiratory cycle [and would hence be considered as “instable” by Nieman et al. (1981), or as R/D according to Andrews et al. (2015)] as “normal” (Tabuchi et al., 2016). It goes without saying that these critical differences in terminology and interpretation have greatly contributed to the present lack of consensus on alveolar dynamics, and instead have added a substantial degree of confusion to the field. To limit the resulting ambiguity, we suggest here an unbiased terminology which categorizes alveolar dynamics into either “static” (i.e., no volume change), “aligned” (i.e., volume change in accordance with the parallel transpulmonary pressure changes), “paradoxical” (i.e., volume change that is not in accordance with the parallel transpulmonary pressure changes), and “opening-and-collapse” (R/D) (Figure 2). Notably, we refrain from a classification of these terms into physiological vs. pathological dynamics due to the ongoing controversy in this field. We hope that such a unifying terminology may ease comparability between future studies with the aim to ultimately allow for the development of a consensual concept.

In part, but not solely as a result of these ambiguities in terminology, the concept of R/D as postulated by the previously described studies has been opposed by a series of IVM studies that failed to observe any R/D under both physiological and pathological conditions (Mertens et al., 2009; Tabuchi et al., 2016). In a murine model of acid-induced lung injury a reduction of alveolar compliance was observed by dark field IVM that was especially pronounced in small alveolar clusters, thus causing a shift of alveolar ventilation to larger alveoli. Such a mechanism would amplify the heterogeneity of alveolar ventilation and thereby, promote alveolar overdistension (Mertens et al., 2009). Additionally, although no R/D was observed, several other “dyskinesias” such as pendelluft, alveolar stunning or reversed ventilation of alveoli were reported in different models of lung injury (Figure 2) including hydrochloric acid aspiration, Tween instillation for surfactant depletion and antibody mediated transfusion-related lung injury (Tabuchi et al., 2016). In all three models, the inflicted lung injury resulted in asynchronous alveolar ventilation, manifesting as alveolar pendelluft, as well as impaired gas exchange that was detected as local impairment of blood oxygenation. Notably, individual sighs of 10 s length were identified as an effective measure to reconstitute physiologic alveolar dynamics in some (acid-induced lung injury) but not all (Tween-injury) models of lung injury.



As such, considerable controversy exists regarding the characteristics and relevance of impaired alveolar mechanics in injured lungs in general, and the role of R/D in particular. Part of this controversy is attributable to different opinions on what constitutes “normal” alveolar dynamics and resulting differences in terminologies, definitions and interpretations. Methodological differences between analytical techniques (IVM vs. static) as well as specifics and limitations of the IVM technique itself (observation confined to subpleural alveoli, differences between hypostatic and apical lung zones, effects of alveolar edema) may contribute to seemingly opposing findings, while differences between species or models of acute lung injury are probably less likely to underlie these divergent findings.

## INTRAVITAL MICROSCOPY FOR ANALYSIS OF ALVEOLAR PERFUSION, GAS EXCHANGE, AND IMMUNE CELL TRAFFICKING

Alveoli are the functional units of the lung with the overall task to warrant gas exchange, i.e., oxygen supply and carbon dioxide removal from the body. Besides alveolar ventilation, alveolar gas exchange is critically dependent on microvascular capillary network architecture and perfusion. Accordingly, capillary perfusion and its regulation have been a key interest for IVM studies in the past. In the late 1960s, Wagner (1969) developed a lung window with a suction device for dogs and applied it



to analyze the pulmonary capillary transit time in local lung regions (Wagner et al., 1982). This development was a major advance, as before it had only been possible to measure the transit time for the entire lung which does not adequately reflect transit times in individual capillary beds. The measurement of pulmonary capillary transit time in dog lungs was realized by the injection of fluorescein isothiocyanate (FITC) labeled dextran into the corresponding lobe artery and subsequent microscopic observation of its passage through the pulmonary microvasculature. Notably, the mean capillary transit time was much longer than expected, namely  $12.7 \pm 3.2$  (mean  $\pm$  standard error) seconds in comparison to the 0.75 s for the whole lung capillary transit as measured by indirect methods. Wagner et al. (1982) concluded that this difference likely reflects the hydrostatic pressure gradient in the lung causing a similar vertical gradient of transit times.

Using a similar approach as Wagner, Fingar et al. (1994) implanted a transparent window chamber over the right lung lobe of Sprague Dawley rats to observe vessel permeability and edema formation in arterioles, capillaries and postcapillary venules. Pulmonary edema was induced by either oleic acid or compound 48/80 and measured by FITC-albumin leakage from the vessels into the alveolar space. Vascular leak was progressive over the observed time interval of 90 min and peaked after 30 min, with no measurable leak in control animals. Capillary leak from lung capillaries was similarly visualized by IVM as increase in alveolar septal thickness in a rabbit model of lung injury following complement activation by cobra venom factor (Kuhnle et al., 1999). The development of edema is a characteristic finding in ARDS that contributes critically to the propagation of VILI by diluting and inhibiting alveolar protective surfactant (Kobayashi et al., 1991), by reducing the fraction of aerated lung tissue that will consequently receive higher tidal volumes (“baby lung concept”) (Gattinoni and Pesenti, 2005), and by the development of transient liquid bridges which exert excessive shear stress to airway epithelial cells (Bilek et al., 2003; Huh et al., 2007).

In addition to the detection of edema formation, IVM has also been used extensively to characterize the processes of capillary recruitment and derecruitment (not to be confused with alveolar R/D discussed above). IVM studies in mechanically ventilated rabbits or dogs or isolated rat lungs have demonstrated the considerable potential for capillary recruitment in the pulmonary vasculature at high perfusion rates or pressures (Wagner, 1988; Hanson et al., 1989; Kuhnle et al., 1995; Baumgartner et al., 2003), respectively. Importantly, this topic has recently gained considerable translational attention since several clinical studies of pulmonary hemodynamics at rest and during exercise in healthy resting supine subjects suggest that most of the pulmonary microvasculature is already recruited at baseline. Specifically, these studies show that even a three- to fourfold increase in pulmonary flow results only in a small decrease in pulmonary vascular resistance (Argiento et al., 2012; Kovacs et al., 2012; Wolsk et al., 2017). As a consequence, the evidence for capillary recruitment in healthy, spontaneously breathing subjects remains inconsistent, and comparative studies using IVM (or similar techniques) under conditions of both mechanical

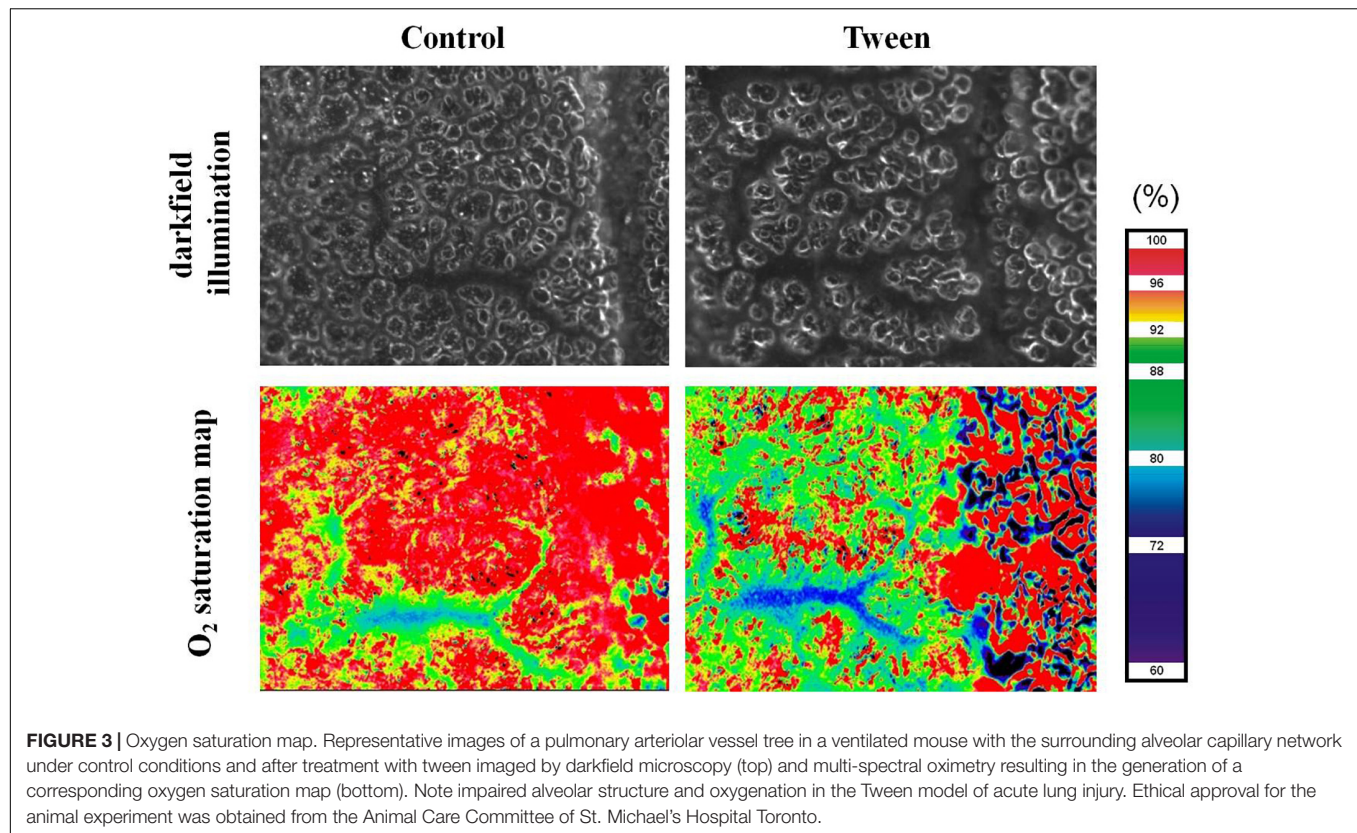
ventilation and spontaneous breathing would be important to clarify this hallmark of classic lung physiology.

In addition to changes in capillary density, pulmonary vasoreactivity has been a subject of lung IVM studies, in particular focusing on the site and mechanism of hypoxic pulmonary vasoconstriction. Although IVM is limited to the visualization of blood vessels close to the lung surface, such as smaller arterioles and venules, it offers a versatile tool for the analysis of pulmonary vasoreactivity with unmatched temporal and spatial resolution in an intact anatomical and morphological context (McCormack et al., 2000). By use of the murine lung window technique Tabuchi and colleagues were able to monitor and quantify the vasoreactive response of pulmonary arterioles and venules as small as 20–30  $\mu\text{m}$  in diameter to hypoxia (11%  $\text{O}_2$ ) or the thromboxane analog U-46619 in real-time (Tabuchi et al., 2008; Mertens et al., 2009). The typical vasoconstrictive response was predominantly located to arterioles with a diameter of 30–50  $\mu\text{m}$ , less prominent in arterioles smaller than 30  $\mu\text{m}$  and largely absent in venules. Hypoxic pulmonary vasoconstriction was similarly evident in pulmonary arterioles of the non-ventilated lung in rabbits undergoing one-lung ventilation (Groh et al., 1992).

In the early 2000's, the group of Axel Pries developed a novel IVM technique to directly visualize microvascular oxygen saturation in individual vessel segments *in vivo* (Styp-Rekowska et al., 2007). To this end they utilized multispectral oximetry, i.e., the recording of entire absorption spectra over the wavelength range from 480–630 nm from the surface of a vascular network, subsequent pixel-based matching of the recorded spectra to the known absorption spectra of oxy- and deoxyhemoglobin, and vascular segmentation to ultimately generate oxygenation maps of intact microvascular networks. In combination with Tabuchi's murine window technique, this approach allowed for the first direct visualization of the blood oxygenation process in the intact lung, an approach that surprisingly revealed that 50% of the total oxygen uptake at rest occurs in the precapillary arterioles before the blood enters the capillary network proper (Tabuchi et al., 2013). Combination of multispectral oximetry with IVM of alveolar dynamics and/or capillary perfusion as well as microhemodynamics yields a complex but versatile tool (Figure 3) that can provide unique insights into the process of alveolo-capillary gas exchange in the healthy and diseased lung (Tabuchi et al., 2016).

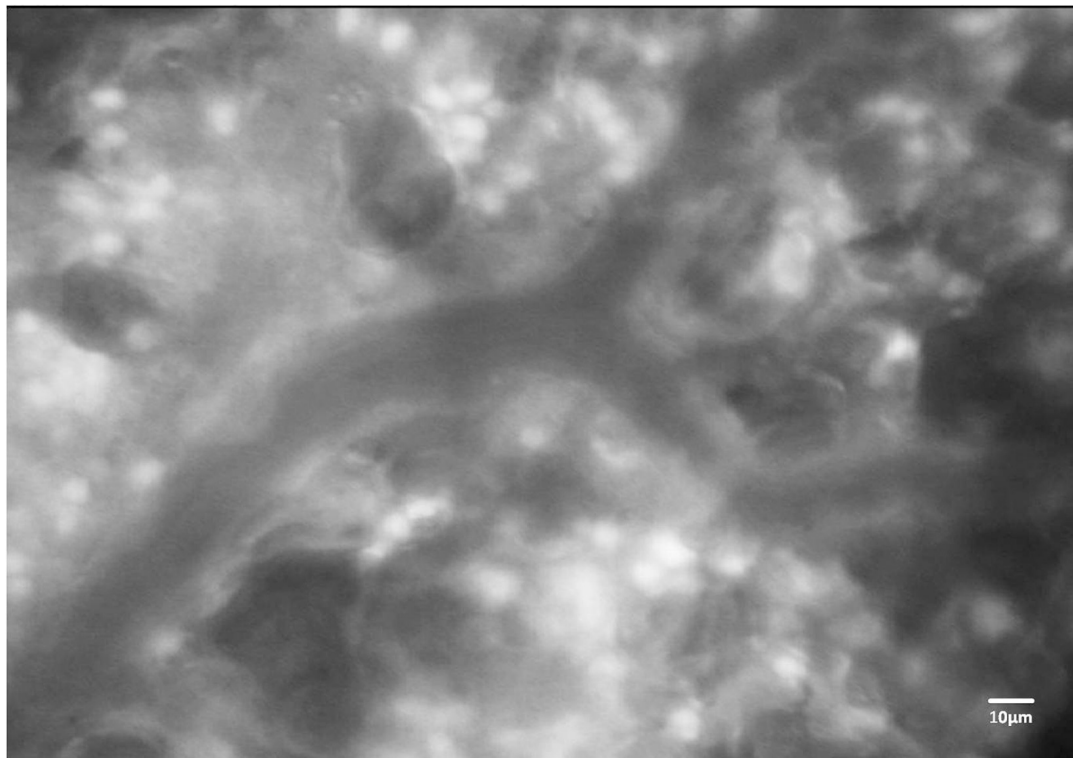
Leukocytes play key roles in inflammatory and immune responses of the lung. By use of IVM, the alveolar capillary bed has been identified as the main site of leukocyte retention during their passage through the lung (Lien et al., 1991; Kuebler et al., 1994), where they accumulate to form the so-called “marginated pool” (Kuebler and Goetz, 2002). This accumulation is attributable to the fact that the passing of leukocytes through the narrow capillary segments of the pulmonary microvasculature requires considerable neutrophil deformation, a process that has been termed neutrophil margination or sequestration (Doerschuk, 2001). Mechanical hindrance during the passage through the alveolar capillary network (Gebb et al., 1995; Kuebler et al., 1999) and the contribution of endothelial adhesion molecules and their interaction with





leukocytes (Kuebler et al., 1997) constitute the predominant mechanisms that determine leukocyte sequestration and – upon appropriate chemotactic gradients – emigration into the alveolar space. Lien et al. (1991) suggested that leukocytes accumulate as a result of a misbalance between neutrophil delivery to the lung and divergent transit times along the capillaries. Kuebler and Kuhnle used IVM in a series of studies to identify the site of leukocyte sequestration (Kuebler et al., 1994), the effects of microvascular blood flow on leukocyte trafficking (Kuhnle et al., 1995), and the role of selectins in leukocyte margination (Kuebler et al., 1997). In addition to the dyes used for leukocyte labeling *in vivo* or *ex vivo*, these analyses were frequently combined with the use of other fluorescent dyes for concomitant analysis of edema formation by the assessment of vascular permeability, or for visualization and quantification of blood flow with plasma markers or labeled red blood cells. E.g., studies by Kuebler et al. (1994, 1997) and Kuhnle et al. (1995) in rabbits used FITC-labeled erythrocytes which were injected intravenously (i.v.) for quantification of blood flow velocity, red cell flux, and microhematocrit and i.v. administered rhodamine6G (Figure 4) as a marker for leukocytes with subsequent detailed analysis by IVM. Early on, the role of neutrophils within the pool of margined and emigrating leukocytes has been of specific interest given their critical role in acute lung injury, pneumonia, and ARDS. Neutrophils not only play a critical role in the defense against pathogens, but also promote host tissue damage by the release of reactive oxygen species (ROS) (Simon et al., 1986; Smedly et al., 1986) thus aggravating edema formation

and worsening outcome in ARDS patients (Steinberg et al., 1994). However, in early IVM studies the lack of specific dyes precluded a differentiation between different leukocyte subsets (Kuebler et al., 1994, 2000). In recent years, this limitation has been overcome by e.g., combinations of fluorescent dyes and antibodies to differentiate leukocyte subsets. To address the role of neutrophils in a model of sepsis-induced lung injury, Park et al. (2019) labeled erythrocytes *ex vivo* with DiD and reinfused them via a catheter. Concomitantly, vessels were visualized with FITC and Tetramethylrhodamine (TMR) conjugated dextran and neutrophils were specifically labeled *in vivo* with an anti-Ly6G<sup>+</sup> monoclonal antibody tagged with a fluorophore. In this study, the authors confirmed the previously described retention of neutrophils within the pulmonary microvascular system (Doerschuk et al., 1987; Lien et al., 1987, 1991; Kuebler et al., 1994), but in addition could link it to an increase in dead space ventilation due to microvascular injury by ROS, ultimately causing impaired oxygenation and hypoxemia. Mark Looney and his group, which had revitalized the study of immune cells in the lung by their development of a stabilized murine lung window (Looney et al., 2011), performed a series of studies in which they addressed the kinetics of neutrophils in the lung. In a recent paper from 2018 they showed that the reduction of neutrophil extracellular trap (NET), a form of innate defense mechanism, by pharmacological or genetic tools resulted in less lung injury and improved outcome in a model of pneumonia induced by methicillin-resistant *staphylococcus aureus* (MRSA) infection. Conversely, in patients with ARDS high levels of NET



**FIGURE 4 |** Fluorescence imaging of immune cells in the mouse lung. Representative image of a pulmonary microvessel after i.v. injection of rhodamine 6G. Note the accumulation of stained leukocytes in the alveolar networks outside of the larger pulmonary microvessel in the image center. Ethical approval for the animal experiment was obtained from the Animal Care Committee of St. Michael's Hospital Toronto.

formation were associated with increased mortality (Lefrancais et al., 2018). Studies by Yipp et al. (2017) identified a defense niche for neutrophils during infection with *Escherichia coli*, in that neutrophils can respond almost instantaneously via TLR4-MyD88 and abl tyrosine kinase signaling to gram-negative pathogens and endotoxins. These findings highlight the potential of IVM to unravel novel mechanisms of lung immunosurveillance and the roles of innate and adaptive immune cells in lung health and disease.

## LIMITATIONS OF IVM

Intravital microscopy is a versatile tool that offers multiple possibilities to analyze biological processes in a realistic anatomical and physiological multicellular environment. IVM can be applied to a large variety of different organs, often in combination with other imaging modalities such as optical coherence tomography (Mertens et al., 2009; Gaertner et al., 2012). In case of internal organs or structures window techniques are commonly applied to provide visual access to the organ of interest such as the skeletal muscle. The lung, however, is an especially complex organ and difficult to image due to its inherent respiratory movements, the propagation of cardiac motion artifacts to the lung surface, as well as to the lung's vulnerability to mechanical stress. Accordingly, preparation of

lung windows without irritation of the lung surface and with maintenance of physiologic cardiovascular body functions (heart rate, arterial blood pressure, oxygenation, and cardiac output) throughout the experimental protocol with ongoing anesthesia and mechanical ventilation is challenging. Some lung windows are constructed to stabilize the lung surface for improved imaging with reduced motion artifacts. While this technique has proven highly efficient for tracking of immune cells, it will impair assessment of basic physiological phenomena, specifically alveolar dynamics and ventilation-dependent effects on lung perfusion due to the artificial removal of respiratory movements in the area of observation. In some studies IVM has been applied in open lung approaches by simply removing part of the thoracic wall and observation of the lung through this opening in the absence of a window. These approaches not only bear the risk of rapid drying of the area of observation and/or its exposure to artificial surfaces (such as cover slips) or environmental pathogens. It should also be considered that the mechanics of the thoracic wall and the interplay between intrapleural and transpulmonary pressures are fundamental factors of respiratory physiology. The disregard of these factors will have significant consequences on alveolar dynamics as well as microvascular perfusion and may contribute to the differential results obtained in studies of alveolar dynamics and the subsequent controversies.

In a pioneering study the group of Gary Nieman proposed that the volume change in healthy lungs is primarily based on the

opening (recruitment) and collapse (derecruitment) of individual alveoli rather than the distension and contraction of alveoli (Carney et al., 1999). In this study which used an open chest technique the authors refrained from suction stabilization of the lung surface. Instead, a coverslip connected to the microscope objective was lowered onto the lung surface to generate a horizontal optical plane. While care was taken not to impact the underlying tissue, it seems difficult to conceive that this procedure would not lead to compression of the underlying alveolar structures. Other studies which used closed chest models in mice without suction applied to the lung surface, thus allowing for free movement of the lung, did not observe any R/D under physiologic conditions (Mertens et al., 2009), but instead described alveolar distension as the predominant mechanism of lung volume change.

While these discordant findings highlight how seemingly minor differences in experimental models and approaches may result in rather opposing results and interpretations, some general limitations that apply to all IVM models should not go unmentioned.

First, in many IVM models the lung surface is exposed to varying temperatures or room temperature, which will affect temperature-sensitive processes. Such processes are e.g., the activation of ion channels critical for the regulation of endothelial barrier function and neutrophil activation in ARDS (Goldenberg et al., 2015; Ahl et al., 2019). This can be avoided by the use of warmed lung window chambers (Kreisel et al., 2010) or simply by use of water immersion microscopy and continuous superfusion of the window with a pre-warmed solution (Kuhnle et al., 1993; Kuebler et al., 1994). Second, IVM of the lung is currently limited to the observation of subpleural alveoli, due to the restricted penetration depth of conventional fluorescence (approximately 30–50  $\mu\text{m}$ ), confocal (approximately 50–60  $\mu\text{m}$ ), and even two-photon microscopy (approximately 100  $\mu\text{m}$ ), therefore excluding deeper structures from analysis (Looney et al., 2011). Second, traction forces exerted by surrounding alveoli will differ between subpleural alveoli and deeper lung regions. Subpleural alveoli are on one side attached to the visceral pleura whereas in deeper lung regions alveoli are surrounded on all sides by other alveoli. Next, it should be considered that different regions of the lung differ in terms of ventilation and perfusion due to the vertical gravitational gradient. Consequentially, IVM observations, which are always restricted to a specific location, may differ considerably between lung base and apex. Both considerations (i.e., the problem of subpleural alveoli and the problem of different lung regions) relate to a more general limitation of IVM, namely the fact that the number of visualized (and analyzed) alveoli is commonly only a small fraction of the total alveoli in the lung and thus, not necessarily representative. Third, the limitation of IVM in terms of longitudinal studies should be considered. The majority of lung windows is too invasive to allow for long-term studies. The recently developed permanent lung window by Entenberg et al. (2018) is a notable exception, and may present a promising tool for future long-term observations. Fourth, albeit still the gold standard in terms of temporal and spatial resolution, IVM is a two-dimensional imaging method, giving only limited information about three-dimensional alveolar

dynamics. While walls and outer diameter of the alveoli are commonly visible as bright reflections, it should be noted that these reflections can also result from capillaries or collagen in the pleura, making interpretations about the real alveolar dimension difficult. In healthy lungs air-filled alveoli appear as white ring structures in dark-field images; however, these rings are in fact the result of specific reflection processes, such as partial reflection and total internal reflection between neighboring alveoli. As a consequence, IVM dark-field images may result in an overestimation of actual alveolar size by a factor as big as  $\sim 1.6$  (Gaertner et al., 2015).

Optical coherence tomography, as a three-dimensional imaging modality albeit with a lesser temporal and spatial resolution as compared to IVM, avoids the above problem (Meissner et al., 2010) and further reveals another disadvantage of IVM, namely the inability to differentiate between collapsed or liquid filled alveoli (Gaertner et al., 2015). In ARDS the development of alveolar edema is a critical factor for impaired lung function and gas exchange, respectively, but its effect on alveolar dynamics is only partly understood. Edema fluid entering the alveolar space as a result of increased permeability of the alveolar wall accumulates in and ultimately floods entire alveoli. Alveolar flooding in turn impairs gas exchange and affects alveolar stability by diluting and inactivating surfactant, which functions as alveolar stabilizer by decreasing surface tension. In studies of alveolar micromechanics under pathologic conditions (such as instillation of the lung with liquid for mimicking edema, surfactant deactivation, or models of lung infection) cyclic disappearance and re-appearance of alveoli in IVM are commonly interpreted as R/D (Nieman et al., 1981; Schiller et al., 2001; Steinberg et al., 2002; Halter et al., 2003). In fact, however, this observation may similarly reflect fluid-filled alveoli becoming cyclically aerated and deaerated over the respiratory cycle. This was elegantly demonstrated by Gaertner et al. (2015) in a study directly comparing IVM and OCT imaging in fluid-filled lungs. Whereas in OCT the alveolar walls remained clearly visible (and showed open, yet fluid-filled alveoli), alveolar walls had seemingly disappeared in IVM images given the false impression of alveolar collapse.

## CONCLUSION

While IVM remains a key technology for the assessment of alveolar dynamics and perfusion, its inherent limitations necessitate validation by and combination with additional three- or even four-dimensional imaging techniques such as e.g., OCT. Only a combination of different imaging modalities, measurements of lung mechanics (e.g., by forced oscillations), and theoretical models can be expected to ultimately clarify the ongoing controversies in the field. Such a joint, interdisciplinary approach may not advance our understanding of respiratory physiology, but may promote the development of optimized and personalized ventilation modes based on a better understanding of alveolar dynamics and their impact on alveolar perfusion and gas exchange in healthy and diseased lungs.



## ETHICS STATEMENT

Ethical approval for conducted animal experiment was given by the Animal Care Committee of the St. Michaels Hospital Toronto.

## AUTHOR CONTRIBUTIONS

WK, JM and AT contributed to the conception and design of the manuscript and wrote the sections of the manuscript.

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# Alveolar Dynamics and Beyond – The Importance of Surfactant Protein C and Cholesterol in Lung Homeostasis and Fibrosis

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Surfactant protein C (SP-C) is an important player in enhancing the interfacial adsorption of lung surfactant lipid films to the alveolar air-liquid interface. Doing so, surface tension drops down enough to stabilize alveoli and the lung, reducing the work of breathing. In addition, it has been shown that SP-C counteracts the deleterious effect of high amounts of cholesterol in the surfactant lipid films. On its side, cholesterol is a well-known modulator of the biophysical properties of biological membranes and it has been proven that it activates the inflammasome pathways in the lung. Even though the molecular mechanism is not known, there are evidences suggesting that these two molecules may interplay with each other in order to keep the proper function of the lung. This review focuses in the role of SP-C and cholesterol in the development of lung fibrosis and the potential pathways in which impairment of both molecules leads to aberrant lung repair, and therefore impaired alveolar dynamics. From molecular to cellular mechanisms to evidences in animal models and human diseases. The evidences revised here highlight a potential SP-C/cholesterol axis as target for the treatment of lung fibrosis.

**Keywords:** surfactant protein C, pulmonary fibrosis, alveolar dynamics, lipid metabolism, alveolar macrophages, cholesterol, metaflammation

## WHY IS CHOLESTEROL PRESENT IN THE LUNG?

As recently reviewed by Zuniga-Hertz and Patel (2019), 2.32 billion years ago, the atmospheric oxygen raised (Bekker et al., 2004) leading to many changes in life. One of these changes may have been the appearance of sterols, around 2.7 billion years ago (Brocks et al., 1999; French et al., 2015) after the GOE (Great Oxygen Event) as suggested by fossil evidences. However, which is the connection between oxygen and sterols? It has been proposed that sterols emerged as an evolutionary strategy to reduce oxygen diffusion through cellular membranes, probably in a world where organisms were not ready to respond to oxidative stress yet. Interestingly, sterol biosynthesis is highly dependent on oxygen (DeBose-Boyd, 2008).

How can sterols, such as cholesterol, regulate oxygen diffusion through biological membranes? The molecular mechanism by which cholesterol can influence small solute permeation and

diffusion through lipid membranes is not well understood. However, it has been proposed that the interactions between cholesterol and the acyl carbon chains in phospholipids (stabilized by Van der Waals' forces) (Wennberg et al., 2012) create tightly packed arrangements that limits small molecule diffusion (Zocher et al., 2013). By decreasing trans-gauche rotation of the phospholipid acyl chains, membrane rigidity increases (Cassera et al., 2002; Molugu and Brown, 2019) leading to less free volume and free pockets which may accommodate oxygen, therefore reducing its flux (its partition and diffusion) through membranes (Zuniga-Hertz and Patel, 2019).

Mammals developed sophisticated organs to optimize the uptake of oxygen during the life essential breathing cycle. From conducting airways to the second biggest surface exposed to the environment, the alveolar human surface (Ochs et al., 2004). In addition, the first membrane that oxygen encounters in the mammalian lungs is a complex mixture of lipids (mainly phosphatidylcholines (PC), such as dipalmitoylphosphatidylcholine (DPPC), up to a 90%) and proteins (10%) with a 5–10% of cholesterol (14–20% mol) (Zuo et al., 2008; Bernhard, 2016), called lung surfactant (surface active agent). Interestingly two surfaces in the human body present with abnormally higher cholesterol molar ratio, and both of them are in contact with the environment tightly regulating the uptake of oxygen. On the one hand, as previously explained, lung surfactant presents around a 14–20% mol cholesterol in its composition. On the other hand the eye lens surface contains up to 35% mol of cholesterol (Raguz et al., 2008; Mainali et al., 2013), compared to a normal cell plasma membrane with a 0.5 phospholipid to cholesterol molar ratio (van Meer et al., 2008; Widomska et al., 2017). Although the main function of lung

surfactant has not been related to oxygen flux control, it has been described to accelerate oxygen diffusion through a water layer (Olmeda et al., 2010), reflecting the importance of lung surfactant as potential oxygen flux regulator. The main function of lung surfactant is to reduce surface tension in order to prevent alveolar collapse during expiration and therefore stabilizing open alveoli allowing oxygen to diffuse through the lung tissue to the blood (Knudsen et al., 2017; Bates and Smith, 2018; Knudsen and Ochs, 2018). Alveolar parenchyma is thin enough to allow oxygen diffusion and is composed of a minimum of three components: (1) alveolar epithelium, where alveolar epithelial type I cells (AE1C) cover 60% of the surface with a small cytoplasm but in a long and thin disposition, whereas alveolar type II cells (AE2C) are in charge of synthesizing, secreting and regulating surfactant composition; (2) both cells sit on a very thin basal membrane; (3) to which a thin endothelium is attached on the opposite side, creating a thin but extensive air-blood barrier. The last step oxygen encounters in its way to the rest of the organs is the erythrocyte membrane. Red blood cells present a rather high cholesterol content, which comprises a 1:1 phospholipid to cholesterol ratio (Zuniga-Hertz and Patel, 2019). In addition, it has been described that oxygen diffusion through red blood cell membranes is decreased in the presence of increased cholesterol content (Buchwald et al., 2000). And therefore, reduction of cholesterol content in those membranes (such as after the use of Simvastatin for 12 weeks) improves oxygen diffusion rate (Menchaca et al., 1998).

In the long way of oxygen through the human body this review focuses on the first barrier, lung surfactant and how its components may impact the normal function of the lung. There is a particular interest in the relevance of the role of cholesterol, and more specifically, in the long described potential relation between surfactant protein C (SP-C) and cholesterol content in lung surfactant. Here, we described the state of the art at the molecular level, contrasting with data from animal models and human patients, where lung mechanics and alveolar dynamics is affected during SP-C deficiency related disease.

## IS THERE A RELATIONSHIP BETWEEN SP-C AND CHOLESTEROL?

### Known Functions of SP-C

SP-C is the smallest (4.2 kDa) and most hydrophobic protein in lung surfactant. It accounts for ~1% of lung surfactant mass, becoming the most abundant protein in molar terms. SP-C appeared relatively late in evolution and its sequence has remained highly conserved among species (Potter et al., 2007). The lack of any known homologous protein and its confined expression (Korfhausen et al., 1990), makes it a specific marker associated with the differentiation of lung tissue, and particularly of AE2C. SP-C exists as a 35 amino acid transmembrane protein expressed as a larger precursor (21 kDa) in AE2C cells. Structurally, it adopts a metastable  $\alpha$ -helical structure, although its high proportion of branched residues makes it prone to adopt  $\beta$ -sheet structures and fibrillogenic amyloid-like aggregates (Johansson, 2001; Johansson et al., 2004;

**Abbreviations:**  $\alpha$ -SMA, alpha smooth muscle actin; aaAMs, alternatively activated alveolar macrophages; ABCA1, ATP binding cassette transporter A1; ABCG1, ATP binding cassette transporter G1; ADA, adenosine-deaminase; ADP, adenosine diphosphate; AEC, alveolar epithelial cell; AE1C, alveolar epithelial type 1 cell; AE2C, alveolar epithelial type 2 cell; ALI, acute lung injury; AM, alveolar macrophages; AMP, adenosine monophosphate; ApoA1, apolipoprotein A1; ApoE, apolipoprotein E; ARDS, acute respiratory distress syndrome; Arg-1, arginase 1; ASC, apoptosis speck-like protein; ATP, adenosine triphosphate; BALF, bronchoalveolar lavage fluid;  $\text{Ca}^{2+}$ , calcium; caAMs, classically activated alveolar macrophages; CARD, caspase recruitment domain; chILD, Children Interstitial Lung Disease; DAMPs, damage associated molecular patterns;  $\text{D}_{\text{LCO}}$ , diffusion capacity for carbon monoxide; DPPC, dipalmitoylphosphatidylcholine; EC, extracellular; ECM, extracellular matrix; EMT, epithelial to mesenchymal transition; ER, endoplasmic reticulum; FEV1, forced expiratory pressure in 1 second; FRC, forced residual capacity; GOE, great oxygen event; HCl, chloride acid; HPS, Hermansky-Pudlak syndrome; HRCT, high resolution computed tomography; ILD, interstitial lung disease; IPF, idiopathic pulmonary fibrosis; LA, large aggregate; LAP-1, latency associated peptide 1; LDL, low-density lipoprotein; LPS, lipopolysaccharide; LTP-1, latency TGF- $\beta$ 1 binding protein-1; mRNA, messenger ribonucleic acid; MMP-9, matrix-metalloprotease 9; MMP-13, matrix-metalloprotease 13; MyD88, myeloid differentiation primary response 88; NF $\kappa$ B, necrosis factor-kappa-beta; NLRP3 NOD-, LRR- and pyrin domain-containing protein 3; NOS-2, inducible nitric oxide synthase; NRDS, neonatal respiratory distress syndrome; PAP, pulmonary alveolar proteinosis; PC, phosphatidylcholine; PEEP, positive end-expiratory pressure; P2XR7, P2X purinoreceptor 7; P2  $\times$  4R, P2X purinoreceptor 4; P2Y2R, P2Y purinoreceptor 2; Relm- $\alpha$ , resistin-like alpha; ROS, reactive oxygen species; RSV, respiratory syncytial virus; SA, small aggregate; SHH, sonic hedgehog; SP-B, surfactant protein B; SP-C, surfactant protein C; SFTPC, surfactant protein C gene; TGF- $\beta$ 1, transforming growth factor beta 1; TIMP1, tissue-metalloprotease inhibitor 1; TLC, total lung capacity; TLR-4, Toll-like receptor 4; TNF- $\alpha$ , tumor necrosis factor alpha; UIP, unusual interstitial pneumonia; VILI, ventilation induced lung injury; YM1, chitinase-like protein 1.



Chou and Fasman, 2006), a common feature in several interstitial lung diseases such as pulmonary fibrosis. SP-C greatly alters lipid packing in membranes influencing lipid motion and lateral distribution (Morrow et al., 1993; Dico et al., 1997). As described before, this may also influence the availability of free volume and free pockets, which may accommodate oxygen. However, a direct study of SP-C content and oxygen diffusion through surfactant membranes has not been assessed so far. SP-C also increases membrane permeability (Plasencia et al., 2004; Parra et al., 2011, 2013) and promotes interfacial lipid adsorption and lipid transfer among different lipid structures (Creuwels et al., 1993; Possmayer et al., 2001; Wang et al., 2005). SP-C is responsible for the reversible formation of multilayered stacks connected to the interfacial monolayer (Amrein et al., 1997; Wang et al., 2005). Doing so, it allows the capture of surfactant material presumably squeezed out during exhalation (area compression) and surfactant re-spreading upon inhalation (area expansion). In this process, protein palmitoylation seems to be relevant to sustain protein association to the highly compressed interfacial films reached during exhalation (Plasencia et al., 2001; Lukovic et al., 2012).

SP-C-associated functions overlap in many cases with surfactant protein B (SP-B) activity, at least when assayed in different *in vitro* models. This includes facilitating lipid adsorption (Creuwels et al., 1993; Possmayer et al., 2001; Wang et al., 2005) into the air-liquid interface or generating 3D structures that serve as a surfactant reservoir (Amrein et al., 1997; Wang et al., 2005), which store newly secreted surfactant complexes and surfactant molecules squeezed out from the interface upon compression. In this context, SP-C could be figured as a supporting molecule for SP-B function rather than an element competent by itself to assist specific features of the complex and dynamic surfactant functionality. Nevertheless, considering the extensive processing of SP-C to its mature form, its extremely conserved sequence and tissue-specific localization, and the difficulties that a cell must overcome to produce and store such a hydrophobic molecule, it is unlikely that this peptide appeared evolutionarily just as an alternative strategy to assist SP-B activities.

## SP-C and Cholesterol Relationships in the Lung Surfactant Context

Surfactant cholesterol represents a paradox regarding its origin (Orgeig and Daniels, 2001; Lopez-Rodriguez et al., 2017). Some works have suggested that it is supplied by the low and high-density lipoproteins present in blood circulation (Olmeda et al., 2017). However, other studies have failed to prove that circulating cholesterol ends up forming part of surfactant complexes (Orgeig and Daniels, 2001; Milos et al., 2016), suggesting that other possible sources must be taken into account. It is remarkable that cholesterol levels in surfactant are tightly regulated to ensure a proper breathing function, and they are able to increase and decrease extremely fast in response to changes in temperature or breathing rate (Doyle et al., 1994; Orgeig et al., 2011). This seems to imply that a cholesterol reservoir might exist in order to provide cholesterol at fast rates when an increase is required.

A specific cell type, the lipofibroblast, has been suggested as a reservoir of cholesterol (Besnard et al., 2009; Torday and Rehan, 2011), although further validation is required to confirm its presence through different organisms and whether it constitutes a surfactant cholesterol storage. AE2C cells are able of producing cholesterol in peroxisomes (Batenburg and Haagsman, 1998), but alveolar macrophages (AMs) also exhibit enzymes involved in cholesterol synthesis (Baker et al., 2010b). Elucidating how cholesterol levels are regulated in the context of surfactant physiology is key to understand responses associated with several respiratory pathologies, especially those characterized by the incorporation in surfactant of abnormal cholesterol amounts such as the acute respiratory distress syndrome (ARDS) (Vockeroth et al., 2009) or pulmonary alveolar proteinosis (PAP).

The presence of cholesterol induces a marked segregation of fluid phases in surfactant (Bernardino de la Serna et al., 2004; Keating et al., 2007), and variations in cholesterol levels are known to adapt surfactant structures extremely fast to defined physiological situations (Doyle et al., 1994; Orgeig and Daniels, 2001). This evidence highlights cholesterol as a structural modulator of surfactant membranes and films. Besides, mechanisms involved in cholesterol sensing and mobilization may be evolutionary conserved to regulate cholesterol levels in surfactant. On the other hand, some studies suggest that SP-C might be involved in cholesterol regulation (Gómez-Gil et al., 2009a,b; Baumgart et al., 2010; Roldan et al., 2016, 2017), which could also be linked to the role of SP-C in lung homeostasis. Therefore, the role of SP-C in cholesterol mobilization and dynamics could be tracked back to a combined effect of protein- and cholesterol-induced alterations on membrane structure. In fact, an increase in cholesterol motion was described upon incorporation of SP-C into lung surfactant-derived vesicles (Roldan et al., 2016), an effect potentially associated to SP-C-promoted membrane-fragmenting effect (Parra et al., 2011, 2013; Roldan et al., 2016). Besides, SP-C and cholesterol have been also related to modulating membrane architecture responding in a coordinate manner to temperature changes (Roldan et al., 2017), suggesting that SP-C is involved in cholesterol mobilization by altering membrane structure (Roldan et al., 2016). In addition, taking into account that SP-C supplementation restores the functionality of cholesterol-containing films in a dynamic context (Gómez-Gil et al., 2009b; Baumgart et al., 2010), we could hypothesize that SP-C could be related to the compositional refinement of lung surfactant films from less surface-active molecules, involving cholesterol and other unsaturated phospholipids. Interestingly, observations made by Leonenko et al. (2007) could support this hypothesis. The incorporation of increasing amounts of cholesterol in a surfactant clinical preparation resulted in structurally and functionally different interfacial films (Gunasekara et al., 2005; Leonenko et al., 2007). Compression-expansion isotherms allowed the determination of lipid loss from the interfacial film upon compression, which were considerably low for physiological cholesterol amounts, permitting the re-establishment of a functional interfacial film (Gunasekara et al., 2005; Leonenko et al., 2007). Shifting that to SP-C function, lipid loss occurring for physiological cholesterol levels could be associated with a

SP-C-dependent cholesterol refinement, in which SP-C-induced lipid reorganizations could be involved. However, lipid loss increased substantially for cholesterol concentrations beyond physiological levels, showing a markedly different film structure and impaired functionality (Gunasekara et al., 2005; Leonenko et al., 2007). For these supra-physiological cholesterol levels, the SP-C amount present in a clinical surfactant preparation like the one tested in this study (~1 wt%), could be likely insufficient to overcome cholesterol impairing effects and the irreversible film collapse. Supplementation of these films with different SP-C amounts would provide valuable information to confirm SP-C effects on cholesterol mobilization.

SP-C/cholesterol relationships might be involved in surfactant refinement with a homeostatic purpose in the lung. Both, cholesterol-loaded vesicles, as well as their combination with SP-C, led to a higher lipid engulfment by AMs (Ruwich et al., 2020). Increased cholesterol content, however, seemed to increase lipid uptake by AMs regardless of the presence of SP-C. Vesicle size and membrane fluidity can affect lipid uptake by AMs (Justice et al., 2014), and thus, the combined effect of cholesterol and SP-C on membrane structure and fluidity (Roldan et al., 2016, 2017) is a factor that must be taken into account. The study of the transcriptional response of MH-S cells to lipid administration revealed that genes associated to lipid metabolism and cholesterol transport were altered upon lipid uptake. Changes in gene expression appear to depend on lipid composition, including the presence or absence of SP-C and/or cholesterol. However, specific effects of cholesterol and SP-C require a thorough and extensive analysis, which also warrant a deeper exploration of the poorly studied pathways for cholesterol synthesis, degradation and mobilization in AMs.

SP-C could then be considered as a pivotal molecule linking cholesterol and lipid homeostasis, lung immunity, lung surfactant biophysical activity and potentially oxygen diffusion regulation, which would explain its particular features, lung tissue specific localization and sequence conservation along evolution. Several questions remain to be answered, including how SP-C effects are coordinated with SP-B function to modulate surfactant activity; which are the molecular mechanisms and SP-C structural determinants involved in membrane reorganizations and how cholesterol levels in surfactant are sensed and regulated regarding SP-C function by both AE2C and AMs. Future research assessing these questions would constitute an essential piece to understand the molecular mechanisms ruling lung surfactant behavior and its implication in respiratory pathologies, generating valuable information useful to improve the current clinical preparations applied for surfactant replacement therapy.

## SP-C, CHOLESTEROL AND ALVEOLAR MICROMECHANICS

### SP-C Deficiency Predisposes to Alveolar Instability

According to LaPlace law, the intra-alveolar pressure of and idealized isotropic alveolus is inversely proportional to its radius.

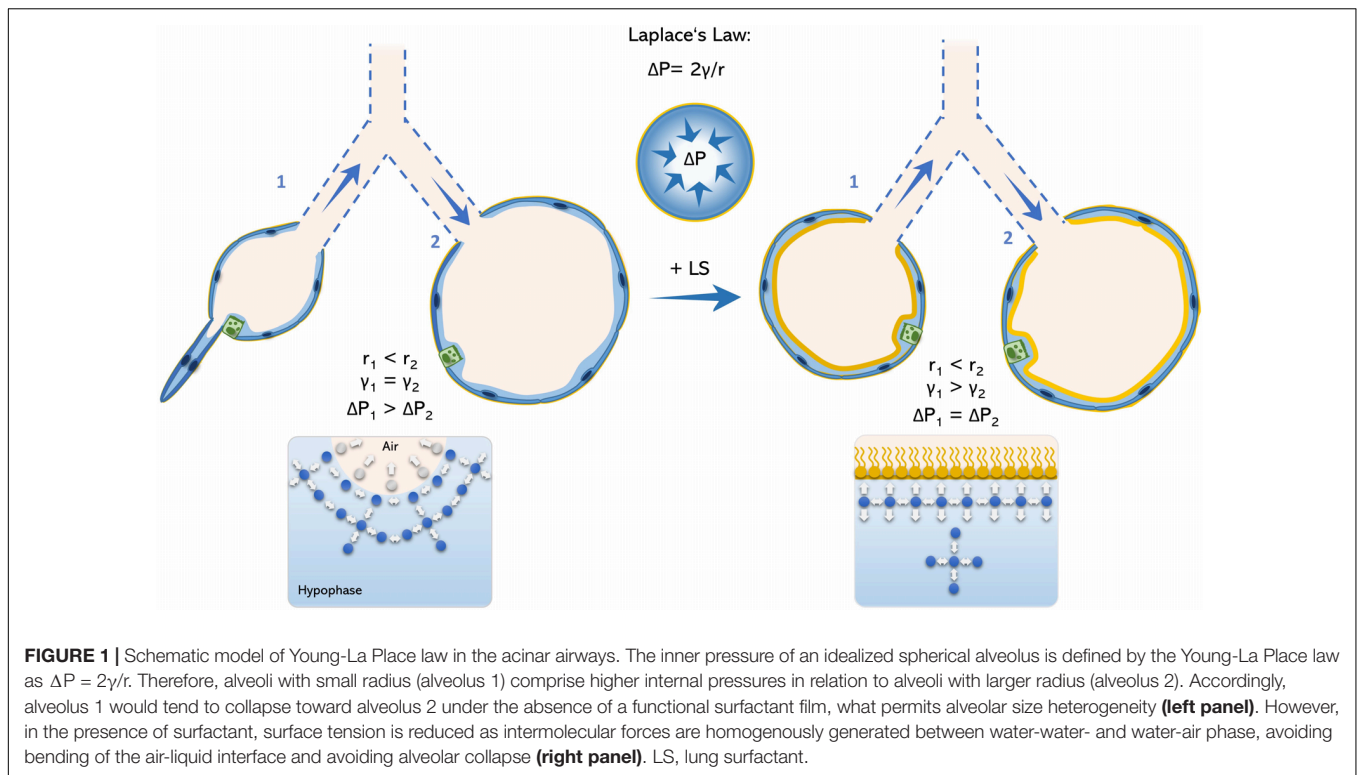
Therefore, at end-expiration, the breathing stage in which the intra-alveolar volume reaches its minimum (ignoring rare occurring phenomena like Pendelluft; Tabuchi et al., 2016), the intra-alveolar pressure reaches its maximum. Under physiologic conditions, end-expiratory pressure is homogeneously distributed among the alveoli and surface tension is low enough preventing alveolar collapse. To maintain alveolar pressure throughout the lung constant, surface tension also changes accordingly to alveolar radius (**Figure 1**).

However, during expiration the surfactant film collapses and thus, end-expiratory surface tension may drastically increase and lead to higher intra-alveolar pressures as well as a rather heterogeneous inter-alveolar pressure distribution. As the intra-alveolar pressure is *per se* higher in small-radius alveoli (relative to its larger neighbors) by its anatomy, this may increase the likelihood of alveolar collapse. Hence, it has been described that the result of surfactant dysfunction in a murine model of AE2C apoptosis is ductal airspace over distention together with alveolar collapse (Mouded et al., 2009). On the one hand, this may explain the increased vulnerability of small subpleural alveoli to surfactant dysfunction. On the other hand, points toward an essential role of alveolar collapse in fibrotic remodeling, as collapsing alveoli was proposed to be the initiating hotspot in pulmonary fibrogenesis (Mai et al., 2016; Knudsen et al., 2017; Petroulia et al., 2018).

### Alveolar Collapse – The Springboard for Lung Mechanic Impairment

The central role of alveolar collapse in the development of diseases such as lung fibrosis is not a novel finding and was already stated by Myers and Katzenstein (1988). Moreover, alveolar collapse induced by surfactant dysfunction has also been well described in the field of ARDS and acute lung injury (ALI) (Bates and Smith, 2018; Nieman G.F. et al., 2018). Although the increase in surface tension and alveolar instability is much more pronounced in ARDS (Smith et al., 2017; Autilio and Pérez-Gil, 2018) than under SP-C deficiency, leading to a rather acute than chronic respiratory pathology, ARDS as well as rather chronic lung fibrosis may be associated with a similar underlying disease mechanism. This is highlighted by the fact that alveolar collapse, respiratory distress and concomitant ventilation inhomogeneities have been demonstrated to be present in patients from both diseases (Todd et al., 2015; Al-Saiedy et al., 2018; Autilio and Pérez-Gil, 2018; Petroulia et al., 2018). Moreover, pulmonary fibrosis is also seen in later disease stage of ARDS patients, resembling an aberrant pulmonary repair mechanism in response to lung injury (Hasan et al., 2017), which has also been stated to be the major mechanism of disease in idiopathic pulmonary fibrosis (IPF) patients (Snijder et al., 2019).

Atelectrauma and volutrauma are two mechanism contributing to tissue injury in ARDS (**Figure 2**). In the injured lung, repetitive alveolar collapse (atelectrauma) is caused by increased surface tension (induced by various agents). During the inspiration phase, the transpulmonary pressure gradient increases until the alveolar pressure of the closed (de-recruited) alveolus is exceeded and is re-opened (recruited). If the maximal



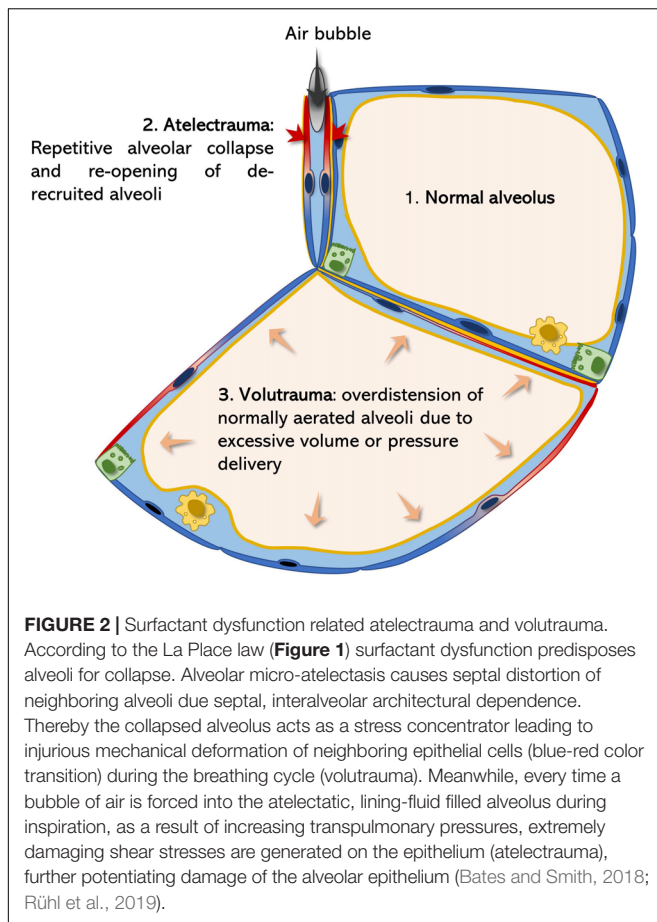
**FIGURE 1 |** Schematic model of Young-La Place law in the acinar airways. The inner pressure of an idealized spherical alveolus is defined by the Young-La Place law as  $\Delta P = 2\gamma/r$ . Therefore, alveoli with small radius (alveolus 1) comprise higher internal pressures in relation to alveoli with larger radius (alveolus 2). Accordingly, alveolus 1 would tend to collapse toward alveolus 2 under the absence of a functional surfactant film, what permits alveolar size heterogeneity (left panel). However, in the presence of surfactant, surface tension is reduced as intermolecular forces are homogeneously generated between water-water- and water-air phase, avoiding bending of the air-liquid interface and avoiding alveolar collapse (right panel). LS, lung surfactant.

generated transpulmonary pressure fails to exceed the intra-alveolar pressure, the alveolus remains collapsed and its alveolar walls stay adjacent to each other. This model is supported by findings of Bachofen and Schürch, who described alveolar wall stretching and ductal airspace over distension on electron microscopic images resulting from surfactant inactivation-induced alveolar collapse (Bachofen and Schürch, 2001). Considering the mechanism of atelectrauma, the alveolar lining fluid should not be neglected. Weibel and Gil first described the alveolar lining lavage as an interfacial film and sub-interfacial liquid reservoir defined as the hypophase (Weibel and Gil, 1968). As the alveolus deflates during expiration, its defining septa start to fold. The folding septal branches are continuously filled with this alveolar lining fluid during expiration (Rühl et al., 2019). Under increased surface tensions the alveolus is further de-recruited leading to more pronounced septal folding and enhanced inter-septal liquid accumulation. During inspiration, an increasing transpulmonary pressure is generated by the respiratory muscles (Mead et al., 1970; Gattinoni et al., 2017). As soon as this pressure exceeds the end-expiratory intra-alveolar pressure, a bubble of air is forced through the lining fluid between the septal folds in order to increase alveolar volume by forcing septal de-folding. During this process mechanical axial shear stresses are generated with the air-bubble moving toward the lining fluid, leading to injurious deformation of AEC2 (Bilek et al., 2003). Of note, the cell damaging force vectors strongly increase with rising surface tension at the interface of the lining fluid, as the speed of the bubble is highly reduced (Cassidy et al., 1999; Ghadiali and Gaver, 2008). Meanwhile, AEC2 injury impairs the epithelial functional integrity resulting in

accumulation of alveolar edema and reduced rates of surfactant production. Thus, starting a vicious cycle leading to continuously increasing surface tension and epithelial injury, resulting in AEC2 hyperplasia and fibrosis (Fehrenbach, 2001; Mouded et al., 2009; Sisson et al., 2010) (Figure 2).

In the healthy parenchymal lung architecture, tissue stress and stretch occurring during breathing are homogeneously distributed. However, if certain alveolar regions become atelectatic, homogenous ventilation is significantly impaired. Alveolar collapse leads to microscale air redistribution, resulting in an inhomogeneous alveolar size distribution before inspiration (Mead et al., 1970). According to alveolar anatomy, single septal walls usually build the parenchymal border of two neighboring alveoli, also known as alveolar interdependence (Knudsen and Ochs, 2018). If one of these alveoli collapses, septal distortion of the adjacent alveoli leads to rising mechanical stresses (Mead et al., 1970). Hence, atelectatic alveoli act as stress concentrators and amplify the applied stresses and strains of their neighbors (Bates and Smith, 2018). During inspiration and increasing lung volumes, this phenomenon becomes even more relevant: transpulmonary pressures generated during inspiration will initially rather lead to over inflation of the already enlarged, distorted alveoli than reopening the atelectatic ones. This causes further alveolar over distension during inspiration. During over distension, an alveolus is first fully de-folded before its wall is stretched. Therefore, the effective septal deformation (= strain) strongly depends on the inspired/applied tidal volume and the alveolar “baseline” shape during resting expiratory position. Usually mechanical stretch primarily occurs under rather high pressures reaching over the upper inflection





point of the pulmonary pressure-volume curve (Knudsen and Ochs, 2018). However, when inflating a healthy lung beyond total lung capacity (TLC) of 80% the extracellular matrix components of the alveolar septa, collagen and elastin, become the major stress bearing components, thus mechanical forces start acting on the septal interstitium (Bachofen et al., 1987; Knudsen and Ochs, 2018). Moreover, single vulnerable alveoli in proximity to stress concentrators, may already get stretched at physiologic low tidal volumes (Mead et al., 1970). In line with this, Kollisch-Singule et al. (2015) found pulmonary injury in surfactant depleted pig lungs already at physiologic tidal volumes (6 ml/kg bodyweight), while pigs with maintained surfactant function, required a drastically higher degree of volutrauma to induce relevant lung injury (30 ml/kg bodyweight). In the ARDS lung atelectrauma and volutrauma act synergistically to induce vascular leakage. Smith et al. (2013, 2017) elegantly demonstrated that initial epithelial injury by atelectrauma predisposes septal walls for volutrauma, leading to significant leakage of the gas-blood barrier. Ventilated mice lungs only developed high concentrations of BALF protein levels, an indicator for gas-blood barrier integrity, when ventilated at PEEP (positive end-expiratory pressure) of 0cmH<sub>2</sub>O (atelectrauma) in combination with mid or high tidal volumes (volutrauma) (see **Figure 2**). Meanwhile, neither atelectrauma nor volutrauma alone were sufficient to induce pulmonary edema (Smith

et al., 2017). As alveolar epithelial cell (AEC) damage has been demonstrated to precede edema formation (Rühl et al., 2019), the absence of alveolar edema in the SP-C deficient lung (Ruwisch et al., 2020), does not rule out the relevance of this protein in preventing alveolar collapse and alveolar over distension, which commonly lead to microscale tissue injuries. Interestingly, hyperplastic AEC2 are present in a global SP-C knock out (KO) mouse model, which may resemble a reaction to chronic mechanical stress (Glasser et al., 2003; Ruwisch et al., 2020). Moreover, surfactant dysfunction in a chronic murine model of AEC injury impressively demonstrated the long-term effects of chronic airway instability to cause microarchitectural air redistribution resulting in an emphysema-like phenotype, which is characterized by collapsed alveoli and enlarged alveolar ducts (Mouded et al., 2009). Furthermore, repetitive insults during dynamic strain have been related to more harmful properties on AEC integrity than constant high static strains (Nieman G. et al., 2018). This may further emphasize the relevance of airway instabilities, in the absence of volutrauma, in a rather chronic setting, as occurs in IPF patients, where recruitment/de-recruitment cycles take place over a long period of time. In line with this, “velcro-crackles” have been often described to precede computer tomographic changes in IPF lungs. Indeed, they are considered the auditory correlate of damaging energy-rich alveolar re-openings during inspiration, supporting the clinical relevance of impaired alveolar micromechanics in fibrosing lung diseases (Vyshedskiy et al., 2009).

At the lung mechanical macroscale level, alveolar collapse and surfactant dysfunction exhibit notable influence on the lung's viscoelastic properties. Collapsed airways require high amounts of energy to be reopened, while dysfunctional surfactant increases the hysteresis effect in inflating lungs by rising surface tension. This effect results in parenchymal stiffening, increasing levels of pulmonary tissue elastance (Smith et al., 2013; Birkelbach et al., 2015). During inspiration, the energy applied is rather dissipated creating injurious axial force vectors on the airway epithelium than being stored in the septal elastic fiber network. Therefore, pulmonary tissue damping rises accordingly. In line with this, data from our group demonstrated a significant increase in tissue damping and tissue elastance in 10 weeks old SP-C deficient mice in contrast to age-matched control mice, supporting the concept of alveolar collapse as an initial trigger (Ruwisch et al., 2020). During aging, redistribution of air as well as ECM (Extracellular Matrix) remodeling may alter lung mechanics consistent with findings of Glasser et al. (2001, 2003). Indeed, this work emphasized aberrant tissue hysteresivity (the quotient of energy dissipative forces and lung elastance) at low PEEP, a condition where alveoli are prone to collapse. At those low lung volumes, surfactant becomes the major defining factor of pulmonary breathing mechanics (Bachofen et al., 1987). Moreover, pressure-volume loops demonstrated an increased pulmonary hysteresis, which also reflects increased energy dissipation during inflation of the lung. Gattinoni et al. (2017) already suggested this energy to be potentially harmful for the pulmonary tissue, as it is not reused for elastic recoil properties. Persistent septal micro injury may be, in turn, a relevant factor for altered AEC2 biology, aberrant



wound repair, pulmonary inflammation and interstitial fibrotic remodeling. Phenomena described in a number of children suffering interstitial lung disease (chILD), who showed reduced or absent levels of mature SP-C (Cong et al., 2017), as described in the next sections.

## Establishing Injurious Mechanical Stress as a Driving Factor for Fibrogenesis

Under healthy conditions and homogeneously distributed lung stress, plasma membrane injury of AEC is normally seen. Indeed, AEC are highly capable of  $\text{Ca}^{2+}$  and lysosome dependent repair mechanisms as well as membrane folds for preventing cellular damage (Cong et al., 2017). However, lysosomal stress as seen in Hermansky-Pudlak Syndrome (HPS) patients may impair cellular repair, favoring profibrotic wound repair and the development of unusual interstitial pneumonia (UIP) (Ozyilmaz et al., 2013; Kook et al., 2016). Moreover, if high parenchymal stress leads to plasma membrane defects of more than 1  $\mu\text{m}$ , aberrant AEC wound repair cascades are induced (Cong et al., 2017). Very high strains induced by pressure above 40cmH<sub>2</sub>O have been shown to be sufficient to cause membrane blebbing and cellular apoptosis (Dreyfuss et al., 1999).

Typically, AEC injury response includes signaling of several mechano-transduction pathways including the transforming growth factor  $\beta$ 1 (TGF- $\beta$ 1), Wnt  $\beta$ -catenin, sonic hedgehog (Shh), and the Notch-midkine signaling pathways as well as induction of endoplasmic reticulum (ER) stress. Interestingly, all these pathways have been interlinked with the induction of profibrotic genes, epithelial-to-mesenchymal transition (EMT) or increased ECM deposition. Moreover, ER stress is known to compromise the secretory capacity of AEC2, impairing surfactant metabolism, which initiates a vicious cycle of alveolar instability and stress-mediated AEC injury (Cong et al., 2017). In a murine model of chloride acid (HCl) induced surfactant depletion, impaired lung mechanics was characterized by increased tissue elastance. This was followed by an increased expression of various mesenchymal markers, such as  $\alpha$ -smooth muscle actin ( $\alpha$ -SMA) and vimentin in AEC2, whereas the expression of epithelial cell markers, including pro-SP-B, were reduced (Cabrera-Benítez et al., 2012; Mao et al., 2017). Consequently, EMT may be a potent second hit even further compromising: (1) surfactant function and; (2) the regenerative capacity of the pulmonary epithelium further directing the damage response toward fibrosis. TGF- $\beta$ 1 is expressed by both AECs as well as resident inflammatory cells like AM (Saito et al., 2018). In addition, a large pool of latent-inactive TGF- $\beta$ 1 is located as a complex with latency associated peptide 1 (LAP-1) and latency TGF- $\beta$ 1 binding protein-1 (LTBP-1) in the ECM (Hinz and Suki, 2016; Saito et al., 2018). In the healthy lung, during inspiration, ECM fiber stretching is not sufficient to release active TGF- $\beta$ 1 from its inhibitory binding complex. However, as soon as pulmonary tissue stiffening occurs, interstitial fibroblasts are primed toward myofibroblast differentiation by expressing contractile actin-myosin elements (Zhou et al., 2013). This drastically increases the likelihood of TGF- $\beta$ 1 release upon parenchymal strain, as myofibroblast are able to bind LAP-1 via  $\alpha$ V-integrins (Hinz, 2012; Hinz and Suki, 2016). Interestingly, increased

epithelial injury resulted in increased expression of epithelial  $\alpha$ V $\beta$ 6-integrins, further potentiating the release of TGF- $\beta$ 1 by mechano-transduction (Sheppard, 2015). In line with this, Froese et al. (2016) showed increased expression and release of TGF- $\beta$ 1 in fibrotic IPF lungs, which are characterized by parenchymal stiffening. Importantly the pressures generated by Froese and his team rather reflected gradients comparable to pressure induced by spontaneous breathing than high unphysiological gradients, emphasizing the role of spontaneous breathing as a relevant source of mechanical stress-released active TGF- $\beta$ 1 (Hinz and Suki, 2016). Nevertheless, the role of non-fibrotic but rather collapse-induced parenchymal stiffening in the context of extracellular (EC) TGF- $\beta$ 1 release to date has not been clarified. Finally, TGF- $\beta$ 1 overexpressing mice have been shown to develop surfactant dysfunction and high surface tension (Lopez-Rodriguez et al., 2016) including down-regulation of SP-C expression, by interfering with its transcription factor activity. In this context, considering the afore mentioned section, it becomes clear that an EC TGF- $\beta$ 1 pool bears the potential of an additional devastating loop by further compromising lung mechanics, potentiating epithelial injury.

## Inflammatory Response Under Impaired Lung Mechanics – Where Sterols Come Into Play

The role of inflammation and inflammatory cells in fibrogenesis has been controversial over the last decades. Although anti-inflammatory medications have produced devastating clinical results in a IPF clinical trials (Raghu et al., 2006; Idiopathic Pulmonary Fibrosis Clinical Research Network et al., 2012), the role of immune cells, like AMs, in lung fibrogenesis and pulmonary tissue repair has been repetitively underscored (Wynn and Barron, 2010; Wynn et al., 2013; Romero et al., 2014; Jin et al., 2018; Smigiel and Parks, 2018; Puttur et al., 2019). A promising link between mechanical stretch and inflammatory response may be the release of adenosine triphosphate (ATP) (Cong et al., 2017; Hasan et al., 2017). Physiologically, mechanical stretch of AEC1 transmits the release of ATP via P2XR7, functioning as a stretch sensor (Patel et al., 2005; Mishra et al., 2011). However, under prolonged alveolar injury concentrations of ATP and its related nucleotides sharply rise, finally overwhelming the degradative enzymatic machinery. Hence, levels of ATP continuously stay high in the early exudative stage of ARDS until the expression of its degrading ecto-enzyme catches up (Hasan et al., 2017). Under these circumstances, ATP and its metabolites act as damage associated molecular patterns (DAMPs). This results in pro-inflammatory signaling on the one hand, but interestingly also in the induction of various profibrotic pathways on the other hand. In fact, high levels of EC ATP enhanced TGF- $\beta$ 1 expression and deposition of collagen 1 and fibronectin in fibroblasts via P2XR7 signaling *in vitro* (Wang et al., 2003; Qu et al., 2009). Meanwhile, ATP signaling via the same receptor enhanced the release of profibrotic tissue-metalloprotease inhibitor 1 (TIMP1), which attenuates the function of ECM-degrading enzymes, resulting in increased interstitial amounts of ECM, a hallmark of lung fibrosis (Gu and Wiley, 2006). Interestingly, elevated levels

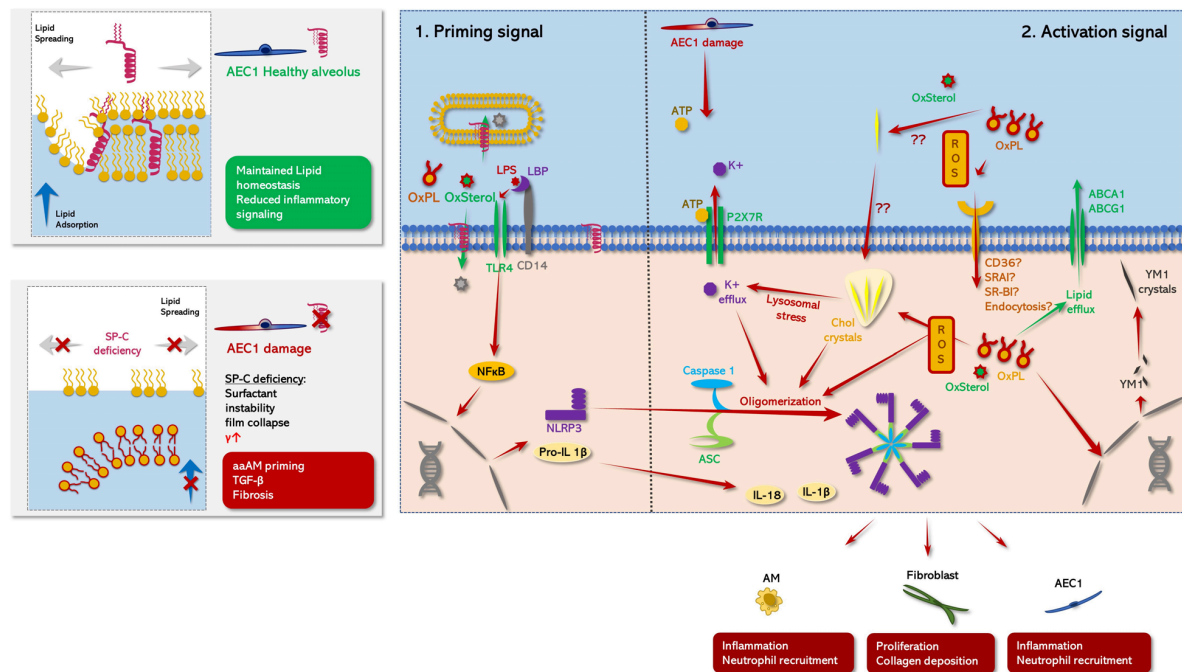
of TIMP1 have also been observed in bronchoalveolar lavage fluid (BALF) of IPF patients, whereas expression of Timp1 was induced in 10 weeks old SP-C deficient mice (Beeh et al., 2003). In addition, both  $\text{Ca}^{2+}$  and ATP are well-known stimulating agents of surfactant secretion (Voyno-Yasenetskaya et al., 1991; Dico et al., 1997; Patel et al., 2005; Dietl et al., 2012). This may reflect a counteracting response, where surfactant secretion may be enhanced during high release of ATP and  $\text{Ca}^{2+}$ , during injury.

Alternatively activated alveolar macrophages (aaAMs) are mainly characterized by expression of resistin-like alpha (Relm- $\alpha$ ), chitinase-like proteins (YM1), inducible nitric oxide synthase (NOS-2) or arginase 1 (Arg-1) (Wynn and Barron, 2010). Their profibrotic potential derives primarily through expression of TGF- $\beta$ 1 and the activation of latent TGF- $\beta$ 1 via matrix-metalloproteases (e.g., MMP-9) (Xing et al., 1997; Schmid-Kotsas et al., 1999; Cameron et al., 2001; Karlmark et al., 2009; Lin et al., 2009). Moreover, aaAMs have been shown in topographic proximity to myofibroblasts, being highly capable of collagen secretion (Ramm et al., 1998; Leicester et al., 2004; Thompson et al., 2008). Finally, aaAMs prime the alveolar micromilieu toward fibrosis by secreting various pro-fibrotic cytokines including IL-4, IL-10, IL-13 and the rather pro-inflammatory cytokine IL-1 $\beta$ . Of note, induced expression of YM1, a chitinase-like protein 1 (Bargagli et al., 2007; Terèlj et al., 2009; Wynn and Barron, 2010), but also in SP-C deficient mice (Glasser et al., 2003). Increased accumulation of macrophages with induced TGF- $\beta$ 1 expression was seen in bleomycin-challenged SP-C deficient mice in areas with significant parenchymal distortion. This further emphasizes the link between mechanical stress and macrophage regulation (Lawson et al., 2005). Interestingly, this misbalance between classical and alternative differentiation was not solely dependent on SP-C deficiency, but also specific to the genetic 129/Sv6 background. The 129/Sv6 strain is characterized by an increased dietary cholesterol accumulation and has been described to develop foamy, lipid-laden macrophages with highly induced YM1 expression with age (Jolley et al., 1999; Hoenerhoff et al., 2006). Curiously, SP-C deficient mice as well as patients suffering mutant SP-C derived interstitial lung diseases (ILDs) related to mutations of SP-C, showed similar foamy macrophages in BALF and tissue as well as abundant cholesterol clefts (Glasser et al., 2003; Hamvas et al., 2004; Abou Taam et al., 2009; Ruwisch et al., 2020). Taken together, this suggests a SP-C deficiency and cholesterol induced axis resulting in dysregulated macrophage metabolism and in misbalanced alternative differentiation (**Figure 3**). Cholesterol clefts are present in aging 129/Sv4 mice (Hoenerhoff et al., 2006), SP-C deficient mice (Glasser et al., 2003; Ruwisch et al., 2020) or aaAMs in human herpes virus (HHV)-induced lung fibrosis (Mora et al., 2006). Hence, this may be a potential morphological biomarker of dysregulated alternative activation and an indicator for lung fibrosis. However, the exact interplay between cholesterol and SP-C and macrophage regulation has not been yet elucidated. Nevertheless, studies from our group, suggested SP-C to be necessary for maintaining cholesterol homeostasis in an AM cell line (MHS cells) (Ruwisch et al., 2020). In line with this, Romero and colleagues recently proposed the profibrotic potential of a lipid related paracrine axis between macrophages and epithelial

cells (Romero et al., 2014). Interestingly, their team demonstrated the presence of foamy, lipid-laden macrophages overexpressing YM1 and TGF- $\beta$ 1 in bleomycin induced lung injury, which has been already associated with reduced expression of the *Sftpc* and *Sftpb* gene (Schmidt et al., 2004; Lutz et al., 2015). Romero's team further showed oxidized phospholipids to be another crucial inductor of foam cell formation and alternative differentiation. The role of oxidized lipid species to induce foam cell formation in macrophages has been extensively studied in the field of atherosclerosis (Ertunc and Hotamisligil, 2016). Circulatory macrophages located in atherosclerotic plaques are frequently challenged with oxidized low-density lipoprotein (LDL), oxysterols or cholesterol. These lipids are endocytosed via various receptors, including CD36 and scavenger receptors. Accumulation of toxic lipid species decompensates the metabolic capacity of those macrophages, leading to cholesterol cleft formation and induction of necrotic factor kappa beta (NF $\kappa$ B) related cellular stress pathways. One central element in the so called "metaflammatory" process. This is the formation of the NOD-, LRR- and pyrin domain-containing protein 3 (NLRP3) inflammasome, resulting in the production of pro-inflammatory cytokines including IL-1 $\beta$  and IL-18 (Düewell et al., 2010; Ramji and Davies, 2015). Importantly, macrophage derived IL-1 $\beta$  and inflammasome activation have been referred to as key features in various forms of lung fibrosis including IPF (Zhang et al., 1993; Kolb et al., 2001; Gasse et al., 2007; Wynn and Barron, 2010; Eldridge et al., 2017).

In addition, cholesterol-induced "metaflammation" in macrophages may also be not only important in development of atherosclerosis but seems to be also highly relevant in the lung. For example, AMs are central elements in surfactant catabolism (comprehensively reviewed in Lopez-Rodriguez et al., 2017), and are continuously challenged with various phospho- and neutral lipids. Therefore, knocking down cholesterol transporters, such as ATP binding cassette transporter A1 (ABCA1) and G1 (ABCG1) leads to impaired cellular cholesterol efflux and cholesterol accumulation. In addition, those animal models showed respiratory distress, impaired surfactant metabolism and cholesterol cleft containing, lipid-laden AMs (Thomassen et al., 2007; Baker et al., 2010a; Chai et al., 2017; Fessler, 2017). Moreover, impaired reverse cholesterol transport in apolipoprotein E (ApoE) and apolipoprotein A1 (ApoA1) deficient mice was also linked to increased pulmonary oxidative stress and inflammation (in ApoE KO mice) as well as to foam cell formation and lung fibrogenesis (in ApoA1 KO mice) (Yao et al., 2016). Interestingly, surfactant function as well as metabolic integrity of AM was restored after application of cyclodextrin, a cholesterol sequestering-drug, underlining the injurious potential of cholesterol for surfactant function and pulmonary lipid homeostasis (Gunasekara et al., 2010). The finding of cholesterol clefts and lipid laden macrophages in patients with SP-C mutations suggests impaired cholesterol homeostasis to be of relevance for development of lung disease in these patients (Hamvas et al., 2004; Abou Taam et al., 2009; Mechri et al., 2010; Cottin and Cordier, 2011; Litao et al., 2017).

Cholesterol overloaded macrophages exhibited an increased Toll-like receptor 4 (TLR-4) signaling mediated immune



**FIGURE 3 |** Schematic role of SP-C in pulmonary metaflammation. (**Left panel**) comparison between the status of AEC1C in the presence (healthy alveolus, top panel) or absence (damaged alveolus, bottom panel) of SP-C. (**Right panel: 1**) **Priming signal:** TLR4 signaling is abrogated under the presence of mature SP-C. On the one hand, SP-C interferes with the complex formation of LBP and CD14 potentially attenuating TLR4 mediated NLRP3 priming in response DAMP/PAMP stimuli. This anti-inflammatory effect may be further potentiated by the N-terminal segment of SP-C transferring TLR4 activators either into neighboring phospholipid microsomes or directly to the cytoplasmic compartment of the macrophage (Chaby et al., 2005; Garcia-Verdugo et al., 2009). Moreover, maintained surfactant homeostasis/surfactant catabolism counteracts the accumulation/formation of oxidized lipid species and cholesterol clefts on the one hand, and minimizes atelect-and volutrauma on the other hand (Ruwisch et al., 2020), likely diminishing the release of DAMPS like ATP on the other hand. Together this prevents the buildup of inflammasome oligomerizing stimuli, what may at least partly explain the aberrant inflammatory response of SP-C KO mice to various inflammatory stimuli in contrast to WT mice (Glasser et al., 2008, 2013a). (**Right panel: 2**) **Activating signal:** NLRP3 inflammasome comprises an initial  $\text{NF}\kappa\text{B}$  related priming phase, preceding a secondary activation signal (Swanson et al., 2019): In the first step various proinflammatory DAMPS (oxysterols, oxidized PL species) or PAMPs (LPS) activate macrophages via TLR-4 signaling via an either LPS binding protein (LBP)/CD14 dependent or independent way (Chaby et al., 2005; Garcia-Verdugo et al., 2009). Thereby, LBP facilitates the binding of e.g., LPS to CD14, what accelerates LPS related TLR4 signaling. TLR4 signaling in turn drives  $\text{NF}\kappa\text{B}$ -mediated expression of NLRP3, pro-IL- $\beta$  and pro-IL-18 (Priming phase) (Gasse et al., 2007; Swanson et al., 2019). In the second step, multiple potential hits including PAMPs like extracellular ATP (Mariathasan et al., 2006; Swanson et al., 2019), intracellular cholesterol clefts (Ertunc and Hotamisligil, 2016), oxysterols and oxidized phospholipid derived mitochondrial oxidative stress (Fessler, 2017; Manon et al., 2018) induce previously synthesized NLRP3 to form oligomers with caspase 1 and ASC leading to mature inflammasome formation. Thereby, increased level of extracellular ATP may be derived from mechanically stressed AEC1 (Hasan et al., 2017), leading to an inflammasome activating  $\text{K}^+$  efflux via P2X7R. Meanwhile, SP-C deficiency related dysfunctional surfactant catabolism and surfactant dysfunction may favor the generation of oxidized PL species and the formation of cholesterol clefts (Fessler and Summer, 2016; Ruwisch et al., 2020). Likewise, these cholesterol crystals cause lysosomal stress, which in turn resembles another potent driving factor of inflammasome formation via induction of a  $\text{K}^+$  efflux. Finally, the active NLRP3 inflammasome converts inactive pro-IL- $\beta$  and pro-IL-18 into their active form IL- $\beta$  and IL-18. IL-1 $\beta$  promotes fibrotic remodeling (Gasse et al., 2007; Cassel et al., 2008; Wree et al., 2014; Lv et al., 2018). Meanwhile, another effect of accumulation of injurious lipid species inside the macrophages may also prime their hosts toward a profibrotic aaAM-phenotype (Romero et al., 2014) via induction of several aaAM related genes including, chitinase-like-3 (YM1), which has also been described to form electron dense crystals in various alternative activation of macrophages-disease models (Hoenerhoff et al., 2006; Mora et al., 2006), what may result in a profibrotic feed-forward loop (Smigiel and Parks, 2018).

response as well as elevated expression levels of IL-1 $\beta$ , emphasizing a potential role of NLRP3 inflammasome activation in pulmonary macrophages (Fessler, 2017). The NLRP3-inflammasome consists of three elements including the NLRP3, procaspase 1 and the apoptosis speck-like protein (ASC) containing a caspase recruitment domain (CARD), which links NLRP3 with procaspase 1 (Robert et al., 2016). In order to generate full activation of the inflammasome complex usually two independent signals are needed (**Figure 3**): (1) a  $\text{NF}\kappa\text{B}$  priming signal TLR-4 signaling [enhanced by lipopolysaccharide (LPS) or oxidized phospholipid species] or the presence of cholesterol

crystals (Bauernfeind et al., 2009; Ertunc and Hotamisligil, 2016; Fessler and Summer, 2016; Nakayama, 2018; Saito et al., 2019) and; (2) purinergic signaling as may result from mechanical stress induced AEC1 injury (Hasan et al., 2017). Elevated levels of ATP have been found in BALF of patients with lung fibrosis, further supporting the idea of EC ATP as a potential inflammasome co-activator (Riteau et al., 2010). Hence, the NLRP3 inflammasome may resemble a crucial link between impaired lung mechanics and aberrant lipid metabolism in fibrosing lung diseases. Interestingly, IPF patients have been described to have elevated levels of unsaturated PC, a PC variant which highly susceptible



for oxidative stress (Fessler and Summer, 2016). In combination with the fact, that IPF occurs predominantly in the elderly and has been interlinked with cigarette smoking, mitochondrial stress and cellular senescence, factors driving the generation of reactive oxygen species (ROS). Thus, the IPF lung appears as a hotspot for lipid oxidation (Lederer and Martinez, 2018). Elevated levels of ROS and increased levels of cholesterol in surfactant are also present in bleomycin-induced lung fibrosis (Allawzi et al., 2019), highlighting the relevance of ROS, surfactant oxidation and foam cell formation in fibrogenesis. This is further supported by the presence foamy, Oil-Red-O positive cells in BALF of patients not only with *Sftpc* mutations, but also in patients with sporadic interstitial fibrosis (Basset-Léobon et al., 2010).

Nevertheless, SP-C deficiency may play a distinct role in foam cell formation. Not only is SP-C crucial for stabilizing cholesterol-containing surfactant films (Gómez-Gil et al., 2009a,b) and maintaining physiologic mechanical lung properties but also it seems to interfere with TLR-4 signaling. *In vitro* studies demonstrated that SP-C attenuates LPS induced cytokine production via TLR-4 signaling in a macrophage cell line, suggesting SP-C to play a role in innate immunity (Augusto et al., 2003). Thereby, SP-C seems to compromise the affinity of TLR-4 to LPS via a complex interplay with CD14 (Chaby et al., 2005). However, Garcia-Verdugo et al. (2009) also proposed a CD14 independent mechanism, by which the transfer of LPS into liposomes mediated by the N-terminal SP-C segment would prevent LPS binding to TLR4. This results in a reduced cytokine production upon LPS stimulation (Garcia-Verdugo et al., 2009). In line with these findings, SP-C KO mice exhibited an increased inflammatory response upon LPS challenge characterized by increased macrophage accumulation and higher expression levels of IL-1 $\beta$ , IL-6 and tumor necrosis factor alpha (TNF- $\alpha$ ) (Glasser et al., 2013a). Interestingly, SP-C containing phospholipid vesicles reduced TLR-4 signaling in these mice. Noteworthy, this immunomodulatory role of SP-C seems to not to be restricted to LPS and bacteria-induced inflammation, as SP-C also demonstrated an anti-inflammatory role under pathogen-free conditions (Jin et al., 2018). Taken all together, this suggest that SP-C may not only orchestrate the activation of TLR-4 in an infectious setting, but it also has an impact on TLR-4 signaling in macrophages induced by oxidized surfactant lipids, a question that, to date, remains unclear.

Assuming this hypothesis (Figure 3), SP-C deficiency could predispose to TLR-4 activation by various oxidized cholesterol and PL species as well as their uptake. This results in proinflammatory signaling and NLRP3 inflammasome activation in macrophages (Ertunc and Hotamisligil, 2016). Impaired lung mechanics induced by SP-C deficiency may further promote inflammasome activation by ATP release and at the same time, lead to accelerated surfactant aggregate conversion (Veldhuizen et al., 1996, 1997; Vazquez De Anda et al., 2000; Maitra et al., 2002). Reduced amounts of surface-tension lowering large aggregates (LA) of surfactant, resulting from pronounced aggregate conversion to inactive small aggregates (SA), were accompanied by larger amounts of ROS susceptible phospholipid species (Fessler and Summer, 2016). Increased uptake of SA by AMs in combination with SP-C disrupted cholesterol

metabolism, which may partly explain the presence of foamy macrophages in the SP-C deficient lung and lung diseases related to SP-C mutated forms (Glasser et al., 2003; Hamvas et al., 2004; Lawson et al., 2004; Stevens et al., 2005; Henderson et al., 2013; Liptzin et al., 2015; Salerno et al., 2016).

The relevance of inflammasome activation and IL-1 $\beta$  signaling in fibrotic parenchyma remodeling has been shown for silica induced-ILDs (Cassel et al., 2008), bleomycin-induced lung fibrosis (Gasse et al., 2007) and various other organ systems (Vilaysane et al., 2010; Wree et al., 2014; Lv et al., 2018). NLRP3 associated IL-1 $\beta$  release mediates NF $\kappa$ B activation via IL-1R1/myeloid differentiation primary response 88 (MyD88) related signal transduction in fibroblasts. This results in a misbalance between TIMP-1 and matrix-metalloprotease 9 (MMP-9) and 13 (MMP-13) promoting interstitial collagen deposition and fibrosis (So et al., 2007; Ertunc and Hotamisligil, 2016). Furthermore, genetic deletion of NLRP3-inflammasome associated genes in a ventilated-induced fibrosis model resulted in decreased rates of stretch-induced EMT, which was accompanied by ameliorated fibrotic lung remodeling (Lv et al., 2018).

## SP-C, CHOLESTEROL AND LUNG MECHANICS. EVIDENCES FROM ANIMAL MODELS AND HUMAN PATIENTS

All the molecular and cellular mechanisms explained in the previous sections impact the health and mechanical properties of the lungs. We described in this section the results of deleting the expression or mutating SP-C in animal models (Table 1). In addition, we present here evidences from ILD patients, described to have different mutations in SP-C (Table 2).

### SP-C Modifications in Animal Models

Glasser et al. (2001, 2003) reported the generation of SP-C null mutant mice deficient in the expression of *Sftpc* in a Swiss black background. SP-C deficient mice were viable at birth and did grow and reproduce normally with only mild alterations in lung mechanics. In addition, *in vitro* studies of the SP-C deficient derived surfactant proved reduced stability of small bubbles but normal activity at normal bubble size using a captive bubble surfactometer (Glasser et al., 2001, 2003). In contrast, in 129/Sv background, SP-C deficient mice presented with severe morphological changes including enlargement of alveoli, AE2C hyperplasia and interstitial thickening together with a peribronchiolar and perivascular monocyte infiltration in some animals. Although areas of thickened alveolar septa stained positive for alpha-smooth muscle actin and blue in trichrome staining, septa were thinner in regions of airspace enlargement and total lung hydroxyproline remained unaffected (Glasser et al., 2003; Ruwisch et al., 2020). Importantly, lung structure was normal at birth, but emphysema and remodeling developed upon aging suggesting a process of ongoing injury and repair. Investigation of pulmonary mechanics exhibited increased lung volumes at higher pressures as well as increased hysteresivity



**TABLE 1** | SP-C related mouse models.

Mouse model		General results	Lung morphology	BALF	Lung mechanics
<b>SP-C null mutants</b>					
Glasser et al., 2001	Generation of SP-C null mutant mice, Swiss black background	Viable, normal growth and reproducibility Reduced stability of small bubbles but normal activity at standard bubble size	Indistinguishable from controls		Reduced hysteresivity at each end-expiratory pressure
Glasser et al., 2003	SP-C null mutant mice, 129/Sv background	Reduced health and fecundity	From 2 months: enlargement of alveoli, irregular alveolar septation, multifocal cellular infiltrates. From 6 month: type 2 cell hyperplasia, interstitial thickening, peribronchiolar and perivascular monocytic infiltration Intracellular lipid inclusions in macrophages and AE2C, cytoplasmic crystals in macrophages	Increased macrophage number	Increased lung volumes at higher pressures, increased hysteresivity, increased airway resistance and tissue damping
<b>2nd hit models</b>					
Lawson et al., 2005	Intratracheal bleomycin application, Swiss black background	Higher mortality and weight loss, more pronounced fibrosis and delayed resolution	Increased number of inflammatory cells, fibrotic foci (collagen, fibroblasts, destroyed septa), enhanced collagen deposition; delayed resolution of fibrosis	Increased neutrophil counts	
Madala et al., 2011	Bleomycin and rapamycin, S129S6 background	Preventive and therapeutic treatment with rapamycin failed to reduce bleomycin induced tissue inflammation and collagen deposition			
Glasser et al., 2008	Instillation of <i>Pseudomonas aeruginosa</i> , 129S6 and FVB/N strain	Reduced survival of 2-week-old mice, increased bacterial colony counts in 2-week-old 129S6 but not in FVB/N mice	Increased inflammation, tissue and airway infiltrates (neutrophils and enlarged macrophages with cytoplasmic inclusions)	Increased total cell counts: neutrophils; large foamy macrophages	
Glasser et al., 2009	Respiratory syncytial virus infection, 129S6 and FVB/N	Higher susceptibility to RSV and delayed resolution of induced changes in lung morphology in both strains	More extensive interstitial thickening, air space consolidation, goblet cell hyperplasia.	Increased total cell counts: polymorphonuclear leucocytes, lymphocytes, enlarged foamy mononuclear cells	
Glasser et al., 2013b	RSV infection, expression of SP-C inducible by doxycycline (on 129S6; 55.3/ <i>Sttpc</i> <sup>-/-</sup> )	SP-C expression reduced RSV-induced tissue inflammation and inflammatory cell counts and increased viral clearance	Diffuse alveolar and interstitial infiltrates in doxycycline untreated mice, reduced inflammation in doxycycline treated mice	Reduced total cell counts and percentage of neutrophil counts in doxycycline -treated mice	
Glasser et al., 2013a	LPS challenge, 129S6 background	More intense airway and airspace inflammation, delayed resolution of tissue inflammation	More intense cellular infiltration, perivascular edema, fragmentation of alveolar septa; residual inflammation 30 days post LPS exposure	Increased total cell counts without LPS challenge (reduced by application of Surventa)	
<b>Models with incomplete proSP-C processing</b>					
Conkright et al., 2002	Expression of SP-C <sub>24–57</sub> HA, FVB/N	Delayed/arrested lung development and lethal neonatal respiratory distress syndrome			

(Continued)

**TABLE 1 |** Continued

Mouse model		General results	Lung morphology	BALF	Lung mechanics
Bridges et al., 2003	Deletion of exon 4	Not viable	Fetal lung tissue: disrupted lung organogenesis, branching morphogenesis, dose-dependent cell cytotoxicity		
Lawson et al., 2011	Conditional expression of L188Q upon doxycycline; intratracheal bleomycin	No spontaneous pulmonary fibrosis; more extensive fibrosis in response to bleomycin	Increased apoptosis, total lung collagen, higher number of myofibroblasts after bleomycin	Cell numbers unaltered in bleomycin treated WT and mutant mice	More reduced static lung compliance in bleomycin treated L188Q mice than challenged controls
Nureki et al., 2018	Conditional mouse mutant, constitutive and inducible I73T expression (by Tamoxifen), C57BL/6J	Increased early mortality, spontaneous acute alveolitis, parenchymal injury, fibrotic remodeling	Constitutive I73T expression: diffuse parenchymal lung remodeling; disrupted embryonic lung architecture Induced expression: acute, diffuse lung injury after tamoxifen, partial recovery but development of fibrotic phenotype	Constitutive expression: age-dependent increases in BALF cellularity Induced expression: increased total cell counts, early macrophage accumulation, followed by polymorphonuclear cells and eosinophilia, milder increase in total lymphocytes	Induced expression: restrictive pattern (PV loops), decreased static compliance
Venosa et al., 2019	Conditional mouse mutant, I73T expression induced by Tamoxifen; Local and i.v application of clodronate	Multiphasic and multicellular alveolitis; local clodronate application reduced survival, i.v. clodronate improved survival and reduced eosinophilia		Early reduction of macrophages, followed by accumulation of immature macrophages, neutrophils and eosinophils	
Katzen et al., 2019	Constitutive and conditional C121G mutant inducible by tamoxifen, C57BL/6J	Constitutive expression: lethal postnatal respiratory failure Conditional expression in adult mice: dose-dependent morbidity and mortality, multiphasic polycellular alveolitis with increased BALF cell counts	Constitutive: distorted architecture, enlarged airspaces, interstitial widening, inflammatory infiltrates, proteinaceous fluid conditional expression: acute diffuse lung injury, partial recovery but spontaneous fibrotic lung remodeling	Conditional expression: polycellular alveolitis, increased total cell counts, early macrophage increase, followed by neutrophils and eosinophils, milder increase in lymphocytes	Restrictive pattern: decline in static lung compliance
Jin et al., 2018	Sterile injury model (surfactant protein C-thymidine kinase) induced by ganciclovir in presence (SPC-TK) and absence (SPC-TK/SPC-KO) of SP-C expression	Increased injury and higher mortality in absence than in presence of SP-C expression	Diffuse alveolar damage qualitatively similar but more pronounced in SPC-TK/SPC-KO	Total cell counts unaltered in SPC-TK/SPC-KO and SPC-TK, higher neutrophils and lymphocyte cell counts in SPC-TK/SPC-KO	

in SP-C deficient mice. Abnormal intracellular lipid inclusions and crystals were observed in macrophages and AE2C (Glasser et al., 2001, 2003). While phospholipid content was normal in SP-C deficient lungs on the swiss black background, it was 2-fold elevated in 129/Sv background. In addition, lung mechanics showed increased lung volume at high pressure, tissue damping and hysteresivity in 129Sv background. Together, both studies show strain specific influences on the severity of the pulmonary phenotype (Glasser et al., 2001, 2003). Interestingly, as mentioned before, the 129Sv strain demonstrates an increased absorption

of dietary cholesterol (Jolley et al., 1999) which might also contribute to the strain specific phenotype in *Sftpc* null mice.

Further investigations included additional hits aggravating the effects of SP-C deficiency (Lawson et al., 2005; Glasser et al., 2008, 2009, 2013a,b). Intratracheal application of bleomycin led to higher mortality, more pronounced weight loss, increased neutrophil counts and enhanced collagen deposition in SP-C deficient mice compared to controls. Increased fibrosis as additionally indicated by morphological parameters went along with a delayed resolution of bleomycin-induced fibrosis

**TABLE 2 |** Lung mechanics and BALF cells data from patients.

Variant	BALF cells	Lung mechanics	Reference
L188Q		TLC 52%, DLCo 51% (male patient, onset 20 years); FVC 21% (female patient, onset 17 years)	Thomas et al., 2002
I73T	85% M, 12% L, 3% N		Tredano et al., 2004
R167Q	84% M, 11% L, 5% N		
I73T	92% M, 7% N, 1% L, 0% E	FRC: 69% (8 months), 77% (13 years) DLCo: 25% (8 months), 51% (13 years)	Abou Taam et al., 2009
I73T	30% M, 60% N, 10% L, 0% E (Moraxella catarrhalis)	FRC: 138% (36 months), DLCo: 111% (33 months), 128% (36 months), 156% (42 months)	
I73T	82% M, 13% N, 3% L, 2% E	FRC: 120% (26 months), 128% (35 months), 73% (39 months) DLCo: 98% (26 months), 89% (35 months), 164% (39 months)	
I73T	84% M, 5% N, 11% L, 0% E		
I73T	93% M, 1% N, 6% L, 0% E	FRC 112% (26 months), DLCo: 87% (26 months)	
15x I73T, 1x V39A, c.325-1G > A, c.424delC, c.435G > C (Q145H), L188P, C189Y, L194P	70 ± 5% M, 8 ± 2% L, 18 ± 4% N, total: 379 ± 56 × 10 <sup>3</sup>	82% patients with SpO <sub>2</sub> testing <95%	Thouvenin et al., 2010
I73T	40% M, 57% N, 3% L (mother 32 years)	FVC 62%, TLC 77%, FEV1 83%, RV 108%, DLCo 33%, PaO <sub>2</sub> room air 11.3 kPa, PaO <sub>2</sub> after 10 min exercise (35W): 7.3 kPa	Cottin et al., 2011
G100S	74% M, 20% N, 4% L, 2% E (child, 3 months) BAL cell count (100.000 cells/ml): 2.4, 90% M, 7.5% L, 2.5% N, 0% E, CD4/CD8 ratio: 1.7 BAL cell count (100.000 cells/ml): 2, 86% M, 12% L, 1% N, 1% E, CD4/CD8 ratio: 1.6 BAL cell count (100.000 cells/ml): 1.4, 91% M, 5.8% L, 2.4% N, 0.8% E, CD4/CD8 ratio: 1.5 BAL cell count (100.000 cells/ml): 1.21, 54.2% M, 10.1% L, 34.5% N, 1.2% E, CD4/CD8 ratio: 0.25 BAL cell count (100.000 cells/ml): 3.85, 80% M, 17.3% L, 1.1% N, 1.6% E, CD4/CD8 ratio: 0.6 (time diagnosis)	VC 72.2%, FEV1 84.1% DLCo: 69.3% VC 85%, FEV1 90.3% DLCo: not available VC 96.6%, FEV1 85% DLCo: 65.2% VC 42.5%, FEV1 92.9% DLCo: 38.5% VC 65.3%, FEV1 83.3% DLCo: not available (at time diagnosis)	Ono et al., 2011
Y104H	91% M, 8% L, 1% N	FVC 85%, DLCo 89%, oxygen saturation 97% to 95% (with exercise)	Kuse et al., 2013
I73T		16 years: 90% FVC, 86% TLC, 96% DLCo, 96% VO <sub>2</sub> max; 37 years: FVC 65%, TLC 91%, DLCo 42%, VO <sub>2</sub> max: 5	Avital et al., 2014
I38F		14 years: FVC 77%, TLC 90%, DLCo 108%, VO <sub>2</sub> max 78%; 32 years: FVC 94%, TLC 96%, DLCo 82%, VO <sub>2</sub> max 69%, high breathing reserve: 115 l/min, saturation 100% at peak exercise	
I73T		7 years: FVC 59%, TLC 95% DLCo not available, VO <sub>2</sub> max 80%, 28 years: FVC 46%, TLC 48%, DLCo 58%, VO <sub>2</sub> max 79%	
I73T		8 years: FVC 69%, TLC 100%, DLCo 107%, VO <sub>2</sub> max 83%, 29 years: FVC 102%, TLC 106%, DLCo 95%, VO <sub>2</sub> max 83%	
V39L		16 years: FVC 88%, TLC 95%, DLCo 109%, VO <sub>2</sub> max 93%; 37 years: 94% FVC, 96% TLC, 82% DLCo, 91% VO <sub>2</sub> max	
C121F	Infiltration of granulocytes and alveolar macrophages		van Hoorn et al., 2014
I73T		4 months: 88% oxygen saturation, respiratory rate 85, V <sub>T</sub> 6.0 ml/kg, V <sub>E</sub> 507 ml/min/kg, Crs 2.96 ml/cmH <sub>2</sub> O, Crs/kg 0.76/kg, VC 92 ml(52%), TLC 196 ml(74%), FRC 128 ml(110%), RV 104 ml(99%), V <sub>max</sub> FRC 416 ml/s (263%), FEF <sub>75</sub> 410 ml/s (207%), FEF <sub>85</sub> 295 ml/s (258%)	Hevroni et al., 2015

(Continued)

TABLE 2 | Continued

Variant	BALF cells	Lung mechanics	Reference
I38F		3.3 months: 91% oxygen saturation, respiratory rate 77, $V_T$ 6.3 ml/kg, $V_E$ 484 ml/min/kg, Crs 2.26 ml/cmH <sub>2</sub> O, Crs/kg 0.59/kg, VC 28 ml(69%), TLC 211 ml(94%), FRC 138 ml(125%), RV 108 ml(109%), $V_{max}$ FRC 343 ml/s (245%), FEF <sub>75</sub> 579 ml/s (334%), FEF <sub>85</sub> 477 ml/s (476%)	
I73T	Normal cytology and lipid index lipid-laden alveolar macrophages		Salerno et al., 2016
L188E		Normal lung volumes, diffusion capacity 18% of predicted	Chibbar et al., 2004
E66K	Increased cellularity with foamy mononuclear cell		Stevens et al., 2005

Summary of data from patients suffering fibrosis related to a SP-C mutation. Changes in BALF cells and lung mechanics are summarized for the available data. Crs, respiratory system compliance; PaO<sub>2</sub>, partial pressure of oxygen; RV, residual volume; VC, vital capacity;  $V_E$ , minute ventilation;  $V_T$ , tidal volume; VO<sub>2</sub> max, maximal oxygen uptake; FEF<sub>75</sub>, Forced expiratory flow at 75% of forced vital capacity; FEF<sub>85</sub>, Forced expiratory flow at 85% of forced vital capacity. M, macrophage; N, neutrophil; L, lymphocyte; E, eosinophil.

(Lawson et al., 2005). Preventive and therapeutic treatment with rapamycin failed to reduce bleomycin induced tissue inflammation and collagen deposition in SP-C deficiency (Madala et al., 2011). Instillation of *Pseudomonas aeruginosa* increased pulmonary injury and bacterial colony counts in SP-C deficient mice compared to control mice. As for unchallenged SP-C deficient mice, sensitivity to *Pseudomonas* challenge seemed to be strain specific since bacterial cell counts were enhanced in 129/Sv6 strain but unaltered in age-matched FVB/N mice. Further, neutrophils and enlarged macrophages with cytoplasmic inclusions were observed upon *Pseudomonas aeruginosa* challenge in absence of SP-C whereby the phagocytic index of macrophages in the SP-C deficient mouse model was reduced (Glasser et al., 2008). Similarly, SP-C deficient mice were more susceptible to respiratory syncytial virus (RSV) infection and resolution of RSV-induced alterations in lung morphology was delayed. Mice exhibited more extensive interstitial thickening, air space consolidation and goblet cell hyperplasia. Polymorphonuclear and macrophage cell counts were increased in BALF obtained from SP-C deficient mice as well as viral titers in lung homogenate (Glasser et al., 2008, 2009). In contrast to challenge with *Pseudomonas aeruginosa*, increased susceptibility of SP-C deficient mice to RSV was not restricted to 129/Sv6 strain but also observed in FVB/N background (Glasser et al., 2008, 2009). However, induction of SP-C expression in compound transgenic mice could reduce RSV-induced tissue inflammation and inflammatory cell counts (Glasser et al., 2013b). LPS-challenged mice develop more intense airway and airspace inflammation in the absence of SP-C. While control mice demonstrate a rapid resolution of LPS-induced cellular and tissue inflammation, inflammation persisted longer in SP-C deficient mice. Cell culture experiments further demonstrated increased LPS-induced cytokine expression of SP-C deficient AE2C compared to those from controls (Glasser et al., 2013b).

The model studied by Glasser et al. (2001, 2008) represents a null mutant mouse model without sufficient *Sftpc* expression leading to the absence of SP-C and proSP-C. Other models include mutations that cause aberrant accumulation of SP-C precursor proteins. Deletion of exon 4 (g.1728 G3A), a mutation

detected in human SFTPC, resulted in a truncated form of SP-C (SP-CΔexon4) and incomplete pro-protein processing. Affected mice exhibited disrupted lung organogenesis, branching morphogenesis and expression-dependent epithelial cell cytotoxicity (Bridges et al., 2003). Further, transgenic mice that express the mutant L188Q SP-C did not develop pulmonary fibrosis spontaneously, despite induction of ER stress, but developed a more extensive pulmonary fibrosis with reduced compliance and enhanced AEC apoptosis in response to bleomycin and authors suggested alveolar epithelial ER stress to play a crucial role in enhanced disease development (Lawson et al., 2011). Recently, Nureki et al. (2018) developed a conditional mouse mutant in which the expression of I73T, the most common SFTPC mutation found in human patients, is regulated by tamoxifen. In their study, expression of the human mutation induced a spontaneous acute alveolitis, followed by parenchymal injury and fibrotic remodeling in mice (Nureki et al., 2018). Tamoxifen controlled expression of isoleucin to threonine substitution at codon 73 in *Sftpc* (I73T) results in misprocessed proSP-C and leads to increased mortality at day 7 to 14 and acute diffuse parenchymal lung injury with polycellular alveolitis. An early influx of polymorphonuclear cells and macrophages was followed by eosinophilia. Partial recovery from acute injury was followed by aberrant remodeling, collagen deposition and AE2C cell hyperplasia and mechanical abnormalities. Pressure-volume curves displayed a restrictive pattern at 4 to 6 weeks post-tamoxifen and static compliance was reduced at week 4 but rose with resolution of inflammation. However, the fibrotic phenotype was preceded by TGF-β1 (Nureki et al., 2018). A detailed analysis of the same model showed an early reduction of macrophages, followed by an accumulation of immature macrophages and neutrophils before onset of eosinophilia at week 2 in combination with shift from proinflammatory to anti-inflammatory/profibrotic activation state in mRNA BALF cell analysis (Venosa et al., 2019). Total inspiratory capacity and static compliance were reduced in transgenic mice following the induction of the mutant protein whereas tissue damping was elevated, all together suggesting an enhanced tissue stiffness. While local clodronate application



diminishing resident macrophages led to reduced survival, intravenous application of clodronate decreased accumulation of immature macrophages, improved survival and reduced eosinophilia (Venosa et al., 2019). Expression of another mutant protein, C121G, resulted in postnatal respiratory failure due to disrupted lung morphogenesis with enlargement of airspaces and interstitial widening in mice constitutively expressing C121G whereas a tamoxifen-mediated expression in adult mice induced acute parenchymal lung injury and a multiphasic polycellular alveolitis with increased BALF cell counts. Similar to the I73T model, an early increase of macrophages and neutrophils was followed by a later influx of eosinophils. Overall, lung mechanics showed a restrictive impairment indicated by a decline in static lung compliance (Katzen et al., 2019).

## SP-C Mutations in Human Patients

Since Noguee et al. (2001) described the first case of a *Sftpc* mutation in an infant girl and her mother diagnosed with ILD (Noguee et al., 2001), several studies have been conducted to provide a link between variants in *SFTPC* and the manifestation of ILDs in adults or children. Since previous groups have already performed systematic reviews describing detected mutations, clinical parameters and radiographic as well as histological findings (Ono et al., 2011; Litao et al., 2017), we decided to focus on the work that reported either BALF cell counting or data on lung mechanics in their study (Table 2). In general, lung mechanics display a restrictive pattern (Thomas et al., 2002; Ono et al., 2011; Kuse et al., 2013; Avital et al., 2014; Hevroni et al., 2015). In particular, vital capacity, forced vital capacity were markedly reduced in some patients (Ono et al., 2011; Kuse et al., 2013; Avital et al., 2014; Hevroni et al., 2015) whereas mild reductions in forced expiratory pressure in 1 s (FEV1) (Cottin et al., 2011; Ono et al., 2011) were attributable to a generally reduced lung volume and not indicative of an obstruction. However, the reported residual volumes were high to normal (Cottin et al., 2011; Hevroni et al., 2015). Changes in functional residual capacity (FRC) were unspecific. While some patients demonstrated a reduced FRC, other studies reported elevated or normal values. Gas exchange as indicated by diffusing capacity for carbon monoxide exhibited distinct impairment in most (Thomas et al., 2002; Abou Taam et al., 2009; Cottin et al., 2011; Ono et al., 2011; Avital et al., 2014) resulting in a generally reduced oxygen (Thouvenin et al., 2010; Hevroni et al., 2015). However, Abou Taam and coworkers reported normal and increased diffusion capacity for carbon monoxide ( $D_{LCO}$ ) in two patients (Abou Taam et al., 2009) and oxygenation was sufficient in another patient reported by Avital et al. (2014). Hence, heterogeneity of the disease is also reflected in lung function. While the majority of studies linked *SFTPC* mutations to the familial form of pulmonary fibrosis, genetic mutations in *SFTPC* were also detected in a subset of patients suffering from sporadic IPF (Lawson et al., 2004). Interestingly, sporadic patients also demonstrate with mixed pattern as reported by Cottin et al. (2011). Indeed, they reported a case of combined pulmonary fibrosis and emphysema in a patient with the most common I73T mutation.

As explained before, pulmonary fibrosis and especially IPF was linked to an AE2C dysfunction and increased ER stress response due to aberrant protein accumulation. Hyperplastic AE2C in histological examination are a common finding (Noguee et al., 2001; Chibbar et al., 2004; Hamvas et al., 2004; Cameron et al., 2005; Stevens et al., 2005; Soraisham et al., 2006; Mechri et al., 2010; Thouvenin et al., 2010; Citti et al., 2013; Litao et al., 2017; Park et al., 2018) and enhanced ER stress is a widely acknowledged pathomechanism in IPF (Korfei et al., 2008). However, reduced transcription of *SFTPC* due to promotor variant were associated with neonatal respiratory distress syndrome in late preterm infants (Wambach et al., 2010) and SP-C was absent in BALF samples of a family with chronic ILDs, together with reduced pro-SP-C staining, though no mutation was identified (Amin et al., 2001). While the majority of mutations leads to the onset of ILDs already in childhood (Chibbar et al., 2004; Hamvas et al., 2004; Tredano et al., 2004; Rosen and Waltz, 2005; Stevens et al., 2005; Bullard and Noguee, 2007; Guillot et al., 2009; Mechri et al., 2010; Cottin et al., 2011; Citti et al., 2013; Henderson et al., 2013; Hepping et al., 2013; Turcu et al., 2013; Akimoto et al., 2014; Avital et al., 2014; van Hoorn et al., 2014; Kroner et al., 2015; Liptzin et al., 2015; Peca et al., 2015; Griesse et al., 2016; Liu et al., 2016; Hayasaka et al., 2018) a subset of variants results in a manifestation in later childhood or adulthood (Lawson et al., 2004; Setoguchi et al., 2006; Markart et al., 2007; van Moorsel et al., 2010; Cottin et al., 2011; Ono et al., 2011; Kuse et al., 2013) suggesting a chronic process.

Besides to AE2C hyperplasia, cholesterol clefts are frequently detected on lung biopsy in context of an *SFTPC* mutations (Hamvas et al., 2004; Abou Taam et al., 2009; Mechri et al., 2010; Cottin et al., 2011; Litao et al., 2017) or on lung specimen from ILD patients lacking SP-C (Amin et al., 2001). Macrophages were often described as foamy (Lawson et al., 2004; Stevens et al., 2005; Henderson et al., 2013) or lipid-laden (Liptzin et al., 2015; Salerno et al., 2016). When analyzing BALF cells, the majority of cells usually consists of macrophages (Abou Taam et al., 2009; Thouvenin et al., 2010; Ono et al., 2011). However, some samples showed a marked increase in neutrophil (Thouvenin et al., 2010; Cottin et al., 2011) or lymphocyte (Ono et al., 2011) cell counting in the absence of an infection. Whether immune cell infiltration occurs in reaction to abnormal histological findings or rather causes alterations remains unclear in view of single time point studies in human patients. In addition, a detailed characterization of macrophages was not provided by the majority of studies, but different activation could have distinct effects on fibrogenesis.

## LUNG FIBROSIS AND CHOLESTEROL

Recently, we have described the accumulation of cholesterol crystals in AMs of SP-C deficient animals (Ruwisch et al., 2020). We also showed similar crystals accumulated in the lung of an IPF patient. Looking through the literature this feature is commonly described (Glasser et al., 2003; Hoenerhoff et al., 2006; Mora et al., 2006) but no further investigated. Therefore, the role of cholesterol or accumulation of cholesterol in the form of crystals in cells is yet not well understood

and often overlooked. As explained before, cholesterol is also involved in many processes apart from regulating membrane biophysical properties. Not many experimental data are available in the context of the influence of cholesterol in lung diseases. However, in the clinic settings, it is not surprising that certain patients are suffering from comorbidities that should be treated such as hypercholesterolemia. In fact, it is known that IPF increases the risk of heart diseases. Thus, it is common for IPF patients to receive medications aimed at reducing cardiovascular risk, including statins, which lower cholesterol levels (Kreuter et al., 2018). Data in this regard is still quite controversial. While, 3-hydroxy-3-methylglutaryl-coenzyme A reductase inhibitors (statins) aggravated pulmonary fibrosis in mice by increased production of mitochondrial ROS and NLRP3 inflammasome activation in macrophages. Statins, as potent inhibitors of the endogenous cholesterol synthesis have been associated with a lower decline in FVC in a cohort of untreated IPF patients (Kreuter et al., 2018). In line with this, diet induced systemic hyperlipidemia resulted in altered surfactant phospholipid composition leading to increased alveolar collapsibility, providing evidence that pulmonary lipid homeostasis is strongly related to the blood circulation (Baritussio et al., 1980). As approximately 83% of surfactant cholesterol has been stated to be derived from blood plasma (Turley et al., 1981), statins could contribute in preventing deleterious high levels of cholesterol in surfactant films, providing surfactant film stability and avoiding alveolar collapse. In addition, evaluation of lung function showed that patients receiving statin therapy and Ofev had less decline in pulmonary capacity, compared with a placebo (Kreuter et al., 2018). The yardstick that researchers used was patients' annual rate of decline in forced vital capacity (FVC). The results suggested that statins do not diminish Ofev's effectiveness (Kreuter et al., 2018).

Statins may also have an anti-inflammatory effect in the lung (Liao and Laufs, 2004; Jain and Ridker, 2005), thus a multifactorial mechanism may play an important role in their use. In conclusion, more experimental evidence is needed to support the use of cholesterol lowering drugs for the treatment of

lung diseases such as fibrosis. In addition, the role of cholesterol and SP-C has to be further described and understood in order to develop new therapies. However, there is already promising data in this regard, opening a new pathway to target.

## CONCLUSION

Summing up there are various potential either direct or indirect mechanisms how SP-C is able to interfere and modulate fibrogenesis in the lung. While SP-C deficiency mediated surfactant dysfunction and impaired lung mechanics are likely contributors in the generation of local mechanical stresses and strains, its biophysical interplay with cholesterol on the one hand, and its modulation of TLR-4 signaling on the other hand, highlights SP-C as a key element in a complex profibrotic network. Thereby SP-C deficiency comes into play not only in animal models, but also in patients with familial and non-familial forms of lung fibrosis such as IPF. Further research is needed in order to determine the potential of cholesterol lowering drugs as treatment or combined with anti-fibrotic drugs to find a better therapy for IPF patients.

## AUTHOR CONTRIBUTIONS

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**Conflict of Interest:** NR was employed by the company AlveoliX AG.

The remaining authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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# The Contribution of Surface Tension-Dependent Alveolar Septal Stress Concentrations to Ventilation-Induced Lung Injury in the Acute Respiratory Distress Syndrome

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In the acute respiratory distress syndrome (ARDS), surface tension,  $T$ , is likely elevated. And mechanical ventilation of ARDS patients causes ventilation-induced lung injury (VILI), which is believed to be proportional to  $T$ . However, the mechanisms through which elevated  $T$  may contribute to VILI have been under-studied. This conceptual analysis considers experimental and theoretical evidence for static and dynamic mechanical mechanisms, at the alveolar scale, through which elevated  $T$  exacerbates VILI; potential causes of elevated  $T$  in ARDS; and  $T$ -dependent means of reducing VILI. In the last section, possible means of reducing  $T$  and improving the efficacy of recruitment maneuvers during mechanical ventilation of ARDS patients are discussed.

**Keywords:** acute respiratory distress syndrome (ARDS), mechanical ventilation, ventilation-induced lung injury (VILI), surface tension, stress concentrations, recruitment maneuvers

## INTRODUCTION

In healthy lungs, the alveoli are lined by a thin, aqueous liquid lining layer with associated surface tension,  $T$  (Gil et al., 1979). Surface tension acts in parallel with lung tissue elasticity to tend to collapse the lungs. The impact of  $T$  is lessened by alveolar epithelial type II cell secretion of pulmonary surfactant, a complex mixture of phospholipids, neutral lipids, and hydrophobic and hydrophilic proteins (Haagsman and van Golde, 1991). Surfactant reduces  $T$  at the alveolar interface, yet  $T$  varies cyclically as lung inflation decreases interfacial surfactant concentration and increases  $T$  (Kharge et al., 2014). Surfactant is first produced in the third trimester of gestation. In neonatal respiratory distress syndrome (NRDS), babies born severely prematurely have reduced levels of lung surfactant, thus high surface tension in their lungs, and are unable to breathe unassisted (Clements, 1997). This situation demonstrates the important contribution of  $T$  to lung mechanics.

In adults, a variety of pulmonary or systemic insults—e.g., pneumonia caused by a coronavirus, gastric aspiration, sepsis, or acute pancreatitis—can lead to acute respiratory distress syndrome (ARDS) (Ware, 2006; Wu et al., 2020). In ARDS, regardless of initial insult, pulmonary inflammation is present and causes an increase in alveolar–capillary barrier permeability. Barrier permeability leads first to interstitial and then to alveolar edema. The edema liquid, which contains

plasma proteins, impairs gas exchange. Additionally, in ARDS, alveolar  $T$  is believed to be elevated (Günther et al., 1996; Holm et al., 1999).

Both NRDS and ARDS patients are treated by mechanical ventilation, which supports gas exchange but also causes an exacerbation of underlying lung injury—known as ventilation-induced lung injury (VILI)—and can prevent patient recovery (Jobe et al., 1983; Brower et al., 2000; Cereda et al., 2017). In NRDS, surfactant therapy, i.e., tracheal instillation of exogenous surfactant, is a successful intervention that supplements the low surfactant level of immature lungs and reduces or prevents VILI (Clements, 1997). Stemming from the success in NRDS, it is widely believed that surfactant therapy should likewise reduce VILI in ARDS. However, surfactant therapy has failed in clinical trials to reduce ARDS mortality (Brower and Fessler, 2011).

The failure of surfactant therapy for ARDS raises doubts about the connection between  $T$  and VILI, and the mechanical mechanism through which  $T$  may influence VILI is not fully understood. While there have been excellent studies of  $T$  effects on the mechanics of injured whole lungs (e.g., Bachofen et al., 1987; Gommers et al., 1993; Yamashita et al., 2008),  $T$  effects on alveolar septal micromechanics in the presence of injury or edema have been under-studied. Following below is a conceptual analysis of the influence of  $T$  on septal mechanics in injured regions, causes of elevated  $T$  in ARDS, and possible means of reducing VILI by reducing  $T$ -dependent septal stress concentrations in injured regions.

## MECHANICAL MECHANISMS OF VENTILATION-INDUCED LUNG INJURY AND THE EFFECTS OF SURFACE TENSION

If mechanical properties were homogenous throughout the parenchyma of injured lungs, then elevated  $T$  would uniformly restrain the lungs and be protective. As mechanical properties throughout injured lungs are heterogeneous, however, there are stress concentrations present that are proportional to  $T$  and can be exacerbated by elevated  $T$ .

### Injury Heterogeneity

Injury throughout ARDS lungs is heterogeneous in type and in spatial distribution. Types of parenchymal injury include, but are not limited to: (i) edematous alveoli flooded with proteinaceous blood plasma; (ii) hemorrhagic alveoli flooded with whole blood, including lysed red blood cells (RBCs); and (iii) collapsed alveoli (Staub et al., 1967; Henzler et al., 2011; Santos et al., 2012; de Prost et al., 2014). By microscopy of the injured lung surface, flooding and hemorrhage have been observed. By histology, all three forms of injury have been observed (Wu et al., 2017).

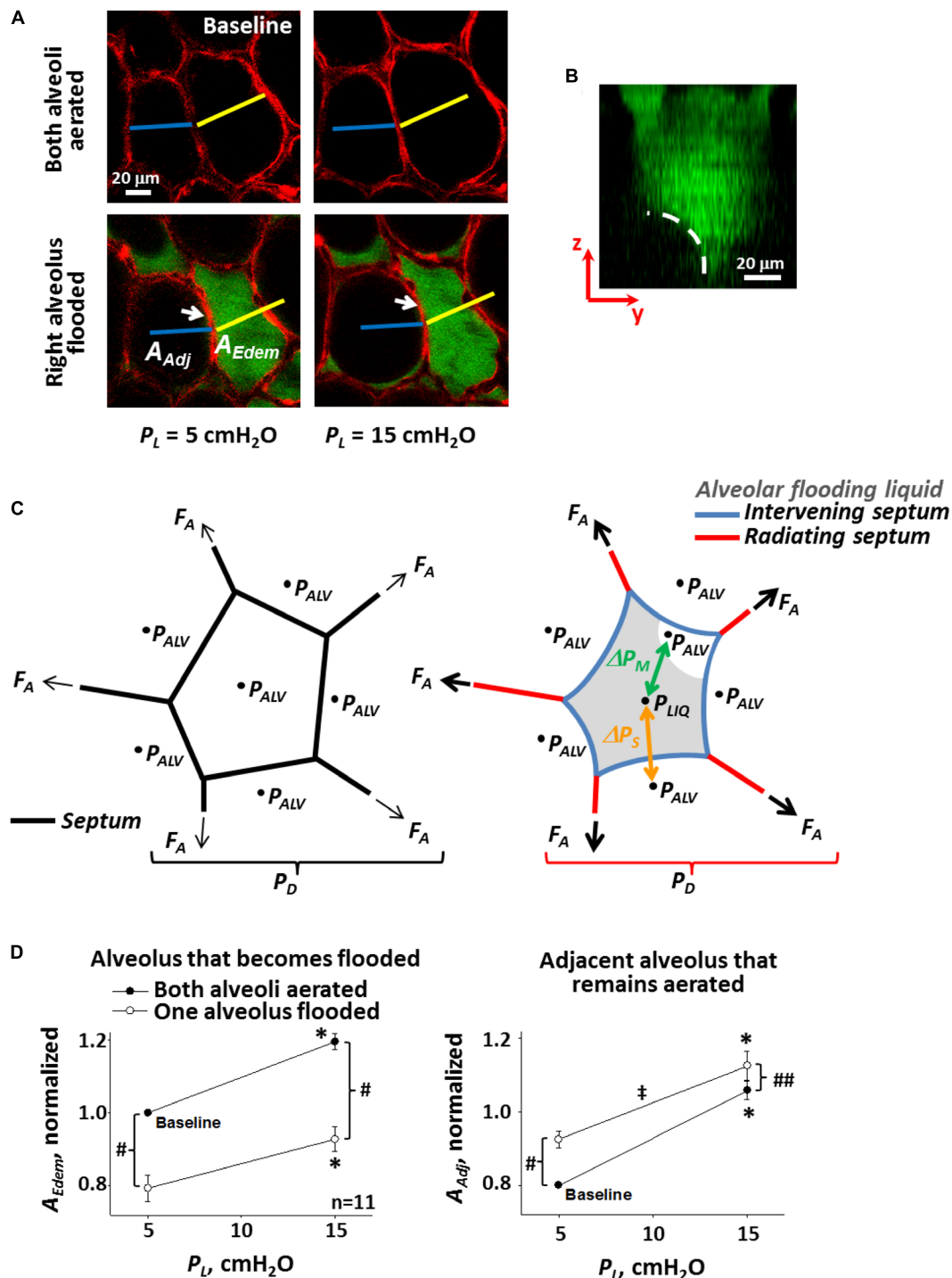
Spatial heterogeneity of injury is evident at scales from that of the alveolus to that of the whole lung. At the alveolar scale, histologic analysis shows that edema, hemorrhage, and collapse are all present in a heterogeneous fashion, interspersed

with aerated alveoli (Staub et al., 1967; Henzler et al., 2011; Santos et al., 2012; de Prost et al., 2014). At an intermediate scale, the surfaces of lungs excised after 5 min of ventilation with a high peak inspiratory pressure (PIP) of 45 cm H<sub>2</sub>O exhibit focal regions of injury surrounded by apparently healthy parenchyma (Dreyfuss and Saumon, 1998). And at the scale of the whole lung, computed tomography (CT) shows edema/collapse to be prevalent in the dependent lung (Gattinoni et al., 2001).

### Static, $T$ -Dependent Stress Concentrations Due to Injury Heterogeneity

At the alveolar scale, with the lungs held at constant volume, alveoli that are flooded are diminished in size (Figure 1A) (Staub et al., 1967; Perlman et al., 2011). The diminishment is attributable to the interface of the flooding liquid forming a meniscus at the alveolar mouth (Figure 1B) (Bachofen et al., 1993; Perlman et al., 2011; Rühl et al., 2019) and the fact that there is a pressure drop,  $\Delta P_M$ , across the meniscus. Consider an alveolus that is initially aerated and surrounded by aerated neighbors; air pressure in all alveoli is  $P_{ALV}$  (Figure 1C, left). As air pressure is the same across all septa, septa are planar. When the central alveolus becomes flooded, air pressure above the meniscus and in surrounding alveoli remains  $P_{ALV}$ . However, according to the Laplace relation,  $\Delta P_M = P_{ALV} - P_{LIQ} = 2T/R$ , where  $P_{LIQ}$  is liquid pressure below the meniscus, and  $R$  is meniscus radius of the curvature, such that  $P_{LIQ} < P_{ALV}$  (Figure 1C, right). As a result of the lower pressure within than around the flooded alveolus, the flooded alveolus decreases in size. In particular, the decrease is often due to bowing into the flooded alveolus of “intervening” septa (Figure 1A, arrows; Figure 1C, blue septa) (Staub et al., 1967; Perlman et al., 2011) separating the flooded alveolus from surrounding aerated alveoli. Intervening septal bowing is caused by pressure difference  $\Delta P_S$ , equal to higher  $P_{ALV}$  in the aerated alveolus to one side minus lower  $P_{LIQ}$  in the flooded alveolus to the other side. The bowing over-extends intervening septa beyond their length when they are planar in normal, aerated lungs, making intervening septa sites of stress concentration. Further,  $\Delta P_S = P_{ALV} - P_{LIQ} = \Delta P_M \sim T$ . Thus, intervening septa are over-extended to a degree  $\sim T$ .

Alveolar derecruitment and collapse have also been attributed to elevated  $T$  (Albert et al., 2019; Kiefmann et al., 2019; Rühl et al., 2019). And diminishment of an individual alveolus tends, by pulling inward, to over-extend “radiating” septa that splay outward through the surrounding aerated parenchyma (Figure 1C, red septa). Thus, as supported by modeling (Mead et al., 1970; Albert et al., 2019), radiating septa are likely another site of  $T$ -dependent stress concentration. At the same time as a diminished alveolus pulls inward on radiating septa, each radiating septum transmits a higher-than-normal axial distending force,  $F_A$ , to the diminished alveolus. The ratio of the summed  $F_A$  around an alveolus to the surface area (or in a two-dimensional analog, perimeter length) of that alveolus applies an effective outward distending pressure,  $P_D$ , to the alveolus, and a

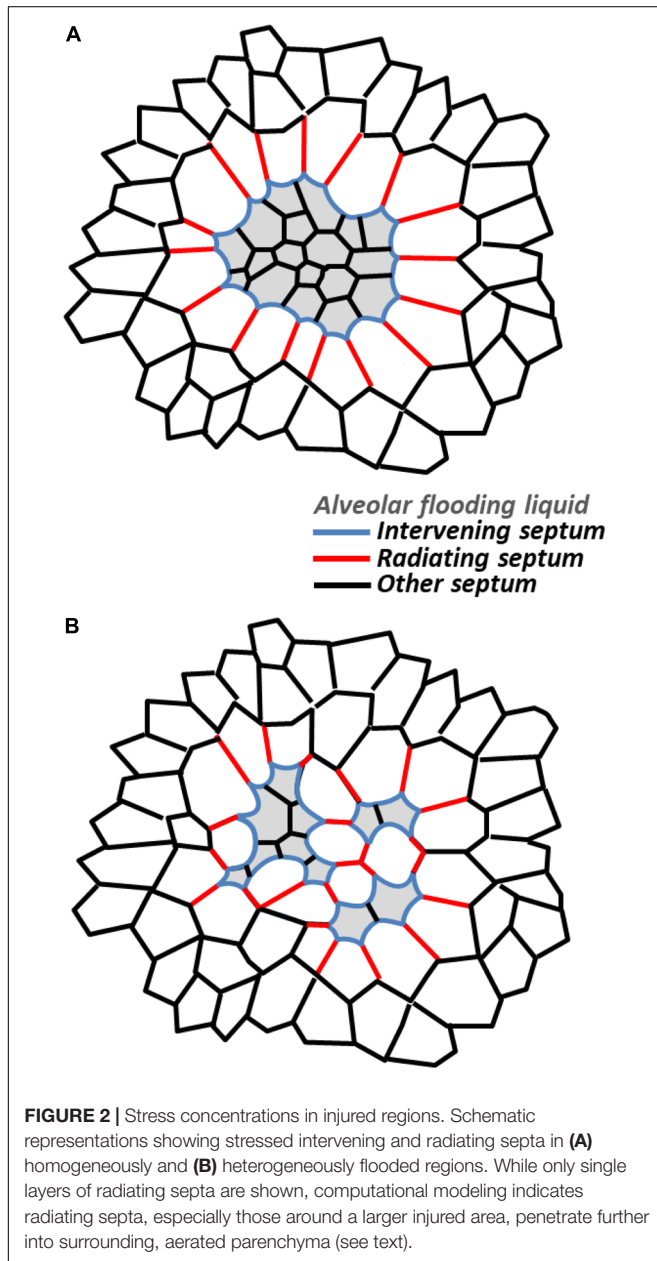


**FIGURE 1 |** Single alveolar edema model. **(A)** Inflation and flooding effects on alveolar geometry. Optical sections of two surface alveoli in isolated, perfused rat lungs. Epithelium labeled with calcein red-orange. Transpulmonary pressure,  $P_L$ , as indicated. In bottom images, right alveolus flooded with fluorescein-labeled 5% albumin solution. Air appears black. Sections are 2- $\mu\text{m}$  thick and at 20- $\mu\text{m}$  sub-pleural depth. Flooding right alveolus causes bowing of central “intervening” septum that separates aerated and flooded alveoli (arrows). Scale bars from baseline image are superimposed on all other images. Right alveolus that becomes flooded and left alveolus that remains aerated have areas  $A_{Edem}$  and  $A_{Adj}$ , respectively. **(B)** Meniscus in flooded alveolus. Image is  $y$ - $z$  section, constructed from confocal  $z$ -stack, of an alveolus flooded with fluorescein-labeled 5% albumin solution. Pleural surface is at top of image. Epithelium is unlabeled and, along with air, appears black. Dashed line shows meniscus at mouth of flooded alveolus. **(C)** Schematics of alveolus before (left) and after (right) liquid flooding. Intervening septa separate aerated from flooded alveoli. Radiating septa are directed outward from flooded alveolus and have aerated alveoli to each side.  $P_{ALV}$  is alveolar air pressure.  $P_{LIQ}$  is flooding liquid pressure. Air-liquid interface in flooded alveolus forms a meniscus.  $\Delta P_M = P_{ALV} - P_{LIQ}$  is pressure drop across meniscus.  $\Delta P_S = P_{ALV} - P_{LIQ}$  is pressure

(Continued)

**FIGURE 1 | Continued**

drop across intervening septa. Axial distending force  $F_A$  acts at ends of sectioned septa and is greater in radiating septa around flooded alveolus on the right than in normally-stressed septa around aerated alveolus on the left. Ratio of summed  $F_A$  over alveolar surface is an effective distending pressure  $P_D$  applied to central alveolus. **(D)** Alveolar compliance. Alveolar areas plotted vs.  $P_L$  for pairs of adjacent alveoli, one of which becomes flooded as in **(A)**. Slope of lines is a two-dimensional analog of compliance. Statistics: \*Area greater at  $P_L$  of 15 than 5 cm H<sub>2</sub>O ( $p < 0.01$ ), for state before or after one alveolus is flooded. #Area different after than before one alveolus is flooded, at constant  $P_L$  ( $p < 0.01$ ). ##Same as “#” but  $p < 0.02$ . \*Slope less after than before one alveolus is flooded ( $p < 0.01$ ). **(A,B,D)** Modified, with permission, from Perlman et al. (2011).



diminished alveolus is subject to a greater  $P_D$  than a normal-sized alveolus (Mead et al., 1970; Albert et al., 2019).

At the intermediate scale, a region of homogeneously flooded or collapsed alveoli should have the effect of a giant, individual flooded or collapsed alveolus (**Figure 2A**). In the case of flooding,

with menisci present at the mouths of all regional alveoli, or in common ducts, the region as a whole should be diminished below its normal, aerated size. Septa within the region should be shorter than when the regions is aerated and normal-sized and, with equal  $P_{LIQ}$  to each side, subject to  $\Delta P_S = 0$  cm H<sub>2</sub>O and planar. The septa should be subject to reduced stress. Septa composing the perimeter of the flooded region will be intervening septa. If the region as a whole is not too diminished in size, the septa may be sites of stress concentration. (Significant regional diminishment may move the septal endpoints close enough that even bowing does not cause over-distension). And radiating septa splaying outward from the injured region should be sites of stress concentration. Computational modeling indicates that radiating septal stress concentrations are greater and penetrate further into surrounding aerated parenchyma for a multi-alveolar injured region than for a single injured alveolus (Albert et al., 2019). Mead et al.'s (1970) classic model suggests that  $P_D$  around a multi-alveolar injured region exceeds the recoil pressure of the lungs. Further, two injured regions in relatively close proximity would be expected to amplify stress concentrations in radiating septa bridging through healthy tissue between the regions. How injured-region size and distance between injured regions affect stress in radiating septa between the regions has yet to be characterized.

For a region with heterogeneous flooding or collapse (**Figure 2B**), stress concentrations within the region should be higher than normal and higher than within a homogeneously flooded region. That is, there will be stressed intervening septa and stressed radiating septa (bridging between two flooded/collapsed alveoli) within a heterogeneously injured region. With the heterogeneously injured region containing injured/diminished and aerated/over-expanded alveoli, the region as a whole should be less diminished in size than if homogeneously injured. Thus, intervening septa on the perimeter may well be a site of stress concentration. And radiating septa should be less stressed than those around a homogeneously injured region, though they may still be a site of stress concentration.

At the whole-lung scale, the dependent lung is often a gross region of extensive flooding or collapse (Gattinoni et al., 2001). (Both the flooded dependent lung and aerated non-dependent lung likely comprise, to greater or lesser degrees, sub-regions of homogeneously flooded or collapsed alveoli, heterogeneously flooded or collapsed alveoli, and aerated alveoli). Stress might be expected to be concentrated at the border between the dependent and non-dependent regions. However, CT data show the border region to exhibit an intermediate density between that of the dependent and non-dependent regions (Terragni et al., 2007). Thus, with the caveat that there could be a few layers of stressed,



over-distended alveoli or septa in the border region that are not detectable by CT, there is no evidence for stress concentration at the border. There is, however, evidence that diminishment of the flooded dependent lung is marked enough to cause ventilation-induced over-distension injury throughout the non-dependent lung. In a saline lavage-induced high  $T$  injury model in rats, high tidal volume,  $V_T$ /low positive end-expiratory pressure (PEEP) ventilation caused atelectasis in the dependent lung and greater alveolar injury in the non-dependent than in the dependent lung (Tsuchida et al., 2006). The larger the injured area, it appears, the further acting the effect of interdependence.

## Alveolar Compliance and Septal Stress

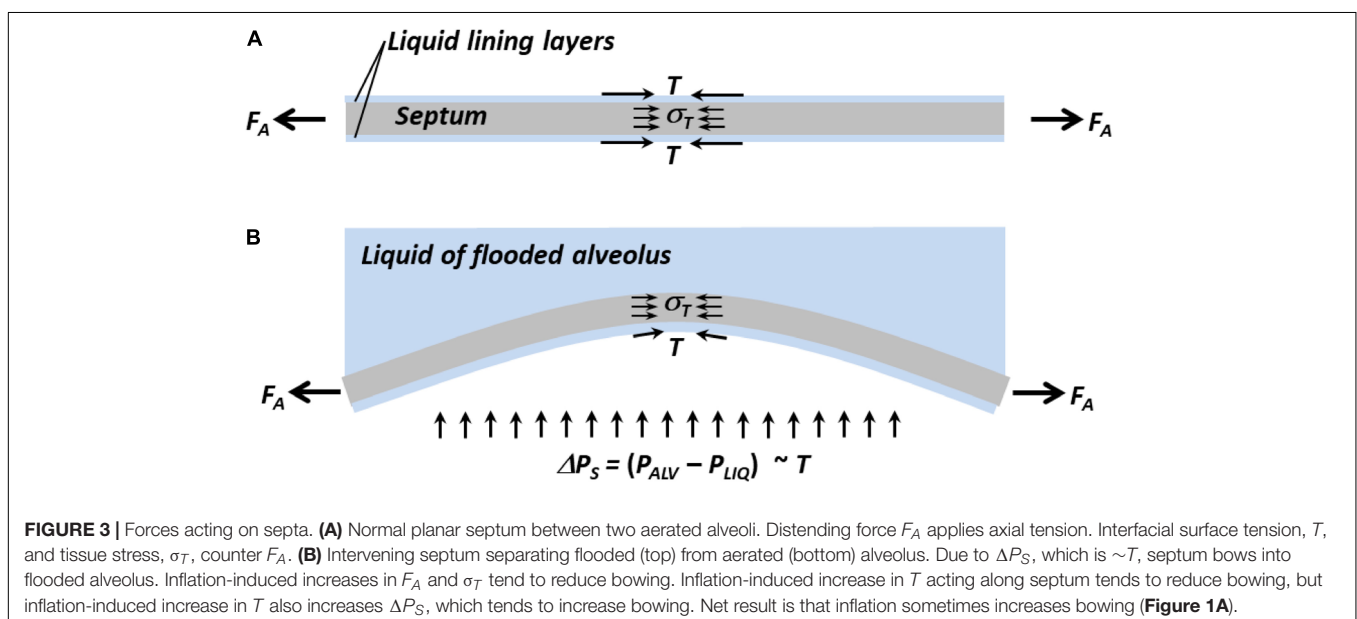
Consideration of alveolar compliance yields additional insight into the stresses applied to intervening and radiating septa. The injured lung exhibits reduced compliance. Contrary to expectation, however, flooding alone does not alter alveolar compliance. When a single alveolus in a healthy lung is flooded and  $T$  remains normal, the alveolus becomes diminished in size but maintains normal compliance (Figure 1D) (Perlman et al., 2011). Adjacent aerated alveoli, due to interdependence, become enlarged and, due to the non-linear stress-strain relation of septal tissue (Perlman and Wu, 2014), exhibit reduced compliance.

Lung inflation increases  $F_A$  and extends septa. In planar septa, the increase in  $F_A$  is balanced by increases in  $T$  and tissue stress,  $\sigma_T$  (Figure 3A). In intervening septa (Figure 3B), the increase in  $F_A$  tends to pull apart the septal endpoints and reduce bowing, and the increase in  $\sigma_T$ , which still counters  $F_A$ , likewise tends to reduce bowing. However, the inflation-induced increase in  $T$  has two opposing effects. Acting along the septum, like  $\sigma_T$ , elevated  $T$  tends to reduce bowing. Elevated  $T$  also increases  $\Delta P_S$ , which tends to increase bowing. Thus, lung inflation sometimes increases bowing of intervening septa (Figure 1A).

Inflation-induced increase in intervening septal bowing into a flooded alveolus/out of an adjacent aerated alveolus should tend to decrease compliance of the flooded alveolus and increase compliance of the adjacent aerated alveolus. The perimeter of a single flooded alveolus is formed entirely by intervening septa. For a single flooded alveolus to exhibit the same compliance as in its prior aerated state (Figure 1D, left) requires that inflation, at the same time as increasing inward bowing of some intervening septa, cause the septal junctions at the alveolar corners to move outward. If inflation moves apart the endpoints of an intervening septum while simultaneously increasing bowing of the septum, then inflation increases stress in the septum. The perimeter of an adjacent aerated alveolus includes one intervening septum and two radiating septa. For an adjacent aerated alveolus to exhibit reduced compliance compared with its state prior to flooding of its neighbor (Figure 1D, right) requires that inflation, at the same time as increasing outward bowing of the intervening septum, cause less distension of the radiating septa than prior to flooding of the neighbor. That is, the radiating septa must be stiffer than prior to flooding of the neighbor. Thus, the observation of flooding-induced decrease in compliance in adjacent aerated alveoli supports the prediction from modeling (Mead et al., 1970; Albert et al., 2019) that stress is concentrated in radiating septa.

## Dynamic, $T$ -Dependent Stress Concentrations

Oftentimes, there is a threshold opening pressure,  $P_O$ , required at the airway entrance to open flooded, collapsed, or injured lung regions, and  $P_O \sim T$ . For air to enter and cause initial inflation of fluid-filled fetal lungs requires a  $P_O$  that is proportional to  $T$  (Enhörning and Robertson, 1972). Similarly, for air to enter a fluid-filled region of an injured lung or peel apart apposed septa separated by a thin liquid layer in a collapsed alveolus should require a  $P_O$  that is proportional to  $T$  (Gaver et al.,



1990; Rühl et al., 2019). When  $PEEP < P_O < PIP$ , intervening and radiating septa around a flooded or collapsed region will be subject to maximal stress, in each ventilation cycle, just before the airway entrance pressure,  $P_{AW}$ , exceeds  $P_O$ . Thus, maximal stress in the septa surrounding an injured region that cyclically reopens should be proportional to  $T$ .

Interestingly, increasing  $P_{AW}$  above  $P_O$  could be a moving goal post. Once inflation commences, newly opened interfacial area may increase  $T$  and thus the  $P_O$  required for continued inflation. This scenario is one of negative feedback that may underlie incomplete opening of flooded or injured lung regions, particularly in cases of high  $T$  (Enhörning and Robertson, 1972).

## Experimental Evidence That Heterogeneous Flooding Causes Injurious Stress Concentrations

To determine whether stress concentrations in regions of heterogeneous flooding are injurious, my group performed experiments in isolated rat lungs.

We developed a local VILI assay in heterogeneously flooded regions of healthy lungs, in which alveolar-capillary barrier permeability was initially normal, and used increase in permeability as an indicator of injurious stress level (Figure 4A) (Wu et al., 2014). In isolated perfused rat lungs, we labeled the perfusate with fluorescein. By micropuncture of a surface alveolus, we infused a non-fluorescent solution of 3% albumin in normal saline into a local region of the parenchymal airspace. The infusion resulted in heterogeneous alveolar flooding. In control regions, we omitted the micropuncture and infusion such that all alveoli remained aerated. Following this preparation, we held the lungs at a constant transpulmonary pressure,  $P_L$ , of 5 cm H<sub>2</sub>O and imaged a flooded or control region at two baseline time points; provided five ventilation breaths with a PEEP of 0–20 cm H<sub>2</sub>O (airway pressure adjusted to account for isolated lung with pleural pressure of zero) and a  $V_T$  of 6 or 12 ml/kg; and returned the lungs to a constant  $P_L$  of 5 cm H<sub>2</sub>O for 10 min of post-ventilation imaging. In control regions without alveolar flooding, thus without septal stress concentrations, fluorescein concentration in the alveolar liquid lining layer remained constant at the baseline level, regardless of ventilation settings, over the 10-min post-ventilation period. In flooded regions with stress concentrations, just five breaths with the gentlest ventilation settings caused fluorescein to leak into the alveolar flooding liquid. Further, fluorescein concentration increased continuously over the 10-min post-ventilation period, indicating that transient ventilation caused a sustained increase in barrier permeability. Increasing PEEP or  $V_T$  increased the rate of fluorescein entrance into the alveolar liquid.

In a different, global VILI assay, we assessed ventilation-induced increase in  $T$  in the presence of heterogeneous flooding throughout the lungs (Figure 4B) (Wu et al., 2017). Our protocol was as follows. First, in isolated and perfused but unventilated rat lungs, we raised left atrial pressure to generate hydrostatic edema. We obtained heterogeneous alveolar flooding. Second, we arrested perfusion and determined  $T$  at the meniscus of a flooded surface alveolus according to our established method (Khargé

et al., 2014). Briefly, following two ventilation cycles between  $P_L$  of 5 and 15 cm H<sub>2</sub>O, we held the lungs at constant  $P_L$  of 15 cm H<sub>2</sub>O, determined  $P_{ALV}$  with a tracheal transducer, determined  $P_{LIQ}$  by servo-nulling pressure measurement, determined three-dimensional interfacial radius of curvature by confocal imaging, and calculated  $T$  according to the Laplace relation. We found that hydrostatic flooding did not alter  $T$  from normal. [We determined normal  $T$  in healthy lungs by applying the same method to the curved interface of the liquid lining layer in the corners of aerated alveoli (Khargé et al., 2014).] Finally, with perfusion still arrested, we gently ventilated the heterogeneously flooded lungs 50 times between  $P_L$  of 5 and 10 cm H<sub>2</sub>O and then again determined  $T$ . The ventilation increased  $T$  by 52%; we speculate that, as discussed below, debris from damaged cells caused the increase in  $T$ . Thus, again, ventilation exacerbated stress concentrations present due to heterogeneous alveolar flooding and led to lung injury.

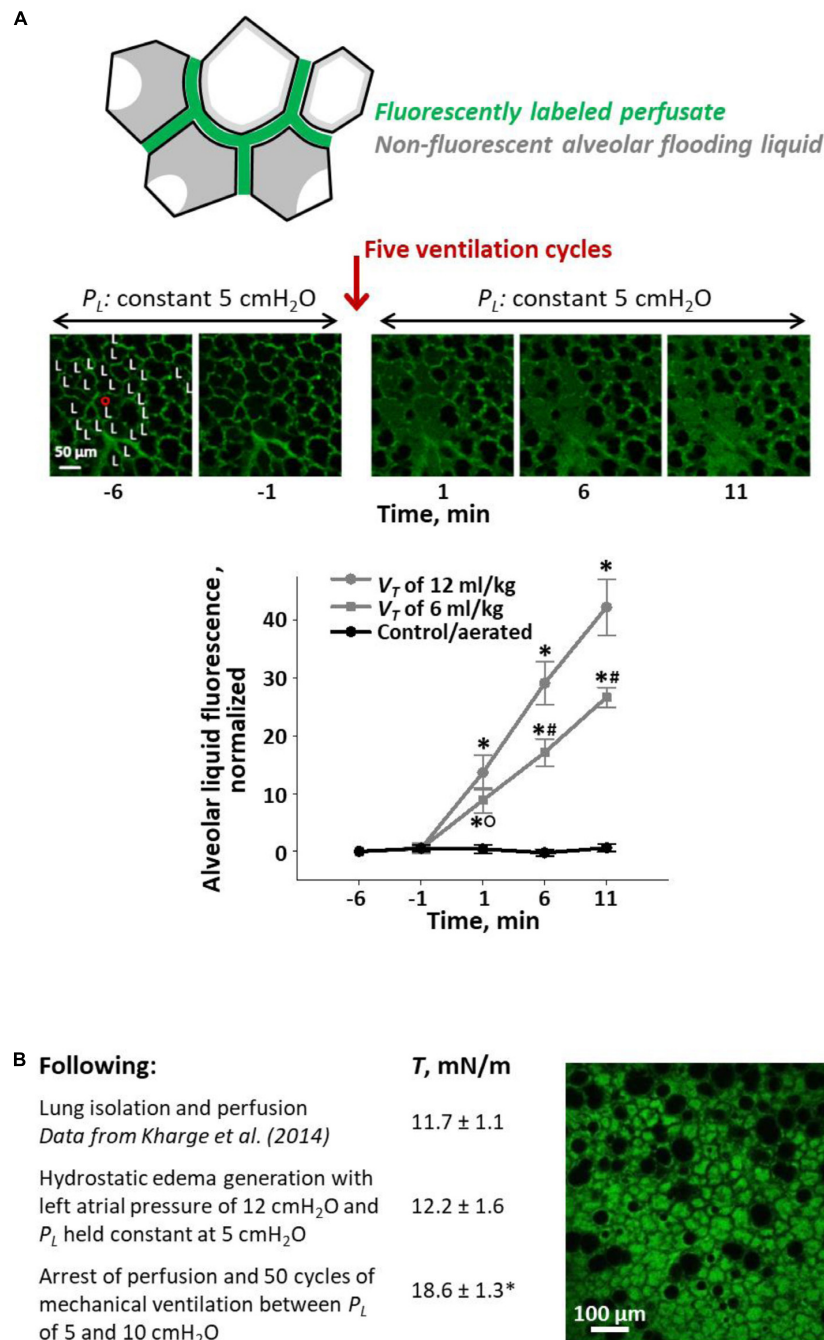
We have not, to date, been able to distinguish between injury to intervening vs. radiating septa. However, our studies demonstrate that stress concentration levels are injurious in at least one of the two types of septa.

## Spatial Propagation of Injury

Computed tomography analysis, in an acid-induced ARDS animal model and clinical ARDS, showed that ventilation causes injured areas to grow larger over time (Cereda et al., 2017). That over-stressed intervening and radiating septa are located at the perimeters of injured regions suggests that injured areas might grow larger through over-expansion of initially normal alveoli at the borders of injured regions. In this first scenario, high maximum  $T$  might be especially problematic. Alternatively, ventilation-induced exacerbation of the condition in an injured region—for example, by transiently high-pressure gradients imposed when  $P_{AW} > P_O$  re-expands an injured region (Bilek et al., 2003)—might exacerbate already-elevated barrier permeability and lead to additional extravasation of liquid. The new liquid might extend, and thus generate stress concentrations, beyond the originally-injured area, thus leading to outward expansion of the injured area. In this second scenario, as  $P_O \sim T$ , high minimum  $T$  might be especially problematic. The mechanism of spatial injury propagation remains to be determined.

## SURFACE TENSION IN ARDS

Bronchoalveolar lavage fluid (BALF) from ARDS patients exhibits increased adsorption time and elevated minimum surface tension,  $T_{MIN}$ , when tested *in vitro* in Langmuir–Wilhelmy troughs and pulsating bubble surfactometers (PBSs) (Hallman et al., 1982; Gregory et al., 1991). These results have overwhelmingly been attributed to the presence of plasma proteins in edema liquid. My group (Khargé et al., 2014) and Holm et al. (1988, 1999) have suggested, as detailed below, that the results are attributable co-adsorption of surfactant and plasma proteins in *in vitro* tests and shown that when an intact surfactant monolayer is present before plasma proteins enter the



**FIGURE 4 |** Ventilation-induced lung injury (VILI) assays. **(A)** Local VILI assay of ventilation-induced injury to alveolar–capillary barrier in the presence of heterogeneous alveolar flooding. Top schematic: Isolated lung is perfused with fluorescein-labeled blood/5% albumin mixture. A glass micropipette is used to puncture a surface alveolus and infuse non-fluorescent 3% albumin solution, which causes heterogeneous alveolar flooding in a local region. Menisci are present in flooded alveoli. Middle images: With  $P_L$  held at 5 cm H<sub>2</sub>O, the region is imaged by confocal microscopy over 5-min baseline period. “L” labels alveoli flooded with non-fluorescent liquid. Then, five ventilation cycles are administered with an end-expiratory  $P_L$  equivalent to an *in vivo* positive end-expiratory pressure (PEEP) of 10 cm H<sub>2</sub>O and a tidal volume,  $V_T$ , of 12 ml/kg. Following ventilation,  $P_L$  is returned to 5 cm H<sub>2</sub>O, and the region is imaged for 10 additional minutes. Bottom graph: plot of increase above baseline of normalized fluorescence in alveolar liquid vs. time. Gray: experimental, heterogeneously flooded regions in lungs subjected to five ventilation breaths with 10 cm H<sub>2</sub>O PEEP and  $V_T$  as specified (fluorescein intensity quantified in alveolar flooding liquid). Black: control, aerated regions in lungs subjected to five ventilation breaths with 10 cm H<sub>2</sub>O PEEP and 6 or 12 ml/kg  $V_T$  (data for two  $V_T$  groups combined; fluorescein intensity quantified in liquid lining layer). Statistics: \* $p$  < 0.01 vs. baseline; # $p$  < 0.01 vs. both other groups at the same time point; \* $p$  < 0.01 vs. control group at the same time point. Figure modified, with permission, from Wu et al. (2014). **(B)** Global VILI assay of ventilation-induced increase in  $T$  in the presence of heterogeneous alveolar flooding. Table: summary of experimental protocol and  $T$ -values, all determined at  $P_L$  of 15 cm H<sub>2</sub>O, at different time points. Statistics: \* $p$  < 0.05 vs.  $T$ -values at two earlier time points. Image: representative view of alveolar flooding pattern on surface of lungs at final time point after induction of VILI and elevation of  $T$ . Alveolar edema liquid labeled by fluorescein administered to the perfusate. Figure modified, with permission, from Wu et al. (2017).

subphase, as occurs in the lungs, plasma proteins do not alter  $T$ . Other causes of elevated  $T$  in ARDS have been proposed, and indeed, Günther et al. (1996) showed that ARDS BALF from which proteins were removed still exhibited elevated  $T$ . However, other purported  $T$ -raising substances have also generally been tested under co-adsorption conditions. And even if a monolayer is formed first, another consideration is that, in the absence of transformation by rapid compression, *in vitro* monolayers lack the metastability exhibited by surfactant in the lungs (Horie and Hildebrandt, 1971; Smith et al., 2004). The ability of other substances to raise  $T$  of an intact and metastable monolayer requires testing.

## Plasma Components

Proteins are the plasma component in alveolar edema liquid most widely cited as raising  $T$ . However, plasma proteins have only been shown to raise  $T$  by competitive adsorption and may not have the opportunity to adsorb in the lungs. With an initially clean interface in a trough with constant interfacial area or a PBS with constant bubble volume, plasma proteins that co-adsorb with surfactant raise  $T$  (Holm et al., 1988, 1999; Seeger et al., 1993). Proteins that co-adsorb with surfactant in a PBS also raise the  $T_{MIN}$  achieved by subsequent bubble pulsation (Seeger et al., 1993; Holm et al., 1999). With an initially-intact interfacial surfactant monolayer in a Langmuir–Wilhelmy trough, plasma proteins injected into the subphase raise  $T_{MIN}$  during subsequent 80% cyclic surface area compression (Holm et al., 1999; Warriner et al., 2002). In the Langmuir–Wilhelmy trough, plasma proteins should have the opportunity to co-adsorb after the monolayer is ruptured by compression to 20% of initial area or to adsorb at peak surface area when regions of clean interface are exposed by monolayer expansion into the two-dimensional gaseous phase (Warriner et al., 2002; Wüstneck et al., 2005). However, with an intact surfactant monolayer, plasma proteins lack access to the interface and fail to raise  $T$ . Holm et al. (1988) showed that albumin injection below a static, intact surfactant monolayer fails to raise  $T$ . Holm et al. (1999) also generated an intact monolayer in a PBS and then added albumin to the subphase by subphase exchange. Even with subsequent 50% cyclic surface area compression, albumin below the intact monolayer failed to raise  $T_{MIN}$ . While 50% is just about the compression that begins to collapse the monolayer (Schürch et al., 1992; Holm et al., 1999), we estimate compression in the lungs to be, at most, ~40% (Khargé et al., 2014). Further, the monolayer in the lungs is always in the liquid-condensed phase (Wüstneck et al., 2005; Khargé et al., 2014; Nguyen and Perlman, 2018) such that even maximal lung inflation should not expose clean interface. Accordingly, in isolated healthy rat lungs held above functional residual capacity (FRC), alveolar injection of 5% albumin solution or blood plasma does not raise  $T$ . That plasma fails to raise  $T$  in the lungs indicates that, as discussed previously (Khargé et al., 2014), no plasma protein is likely at physiologic concentration to raise alveolar  $T$  with an intact surfactant monolayer.

In injured lung regions, it is possible that the surfactant monolayer might collapse, and allow plasma protein adsorption,

at the end of expiration. In rat lungs at FRC,  $P_L$  is in the range of 3.5–4.5 cm H<sub>2</sub>O (Schürch et al., 1976). With albumin present in alveolar flooding liquid, ventilating between  $P_L$  of 3 and 30 cm H<sub>2</sub>O failed to increase  $T$ ; ventilating between  $P_L$  of 1 and 30 cm H<sub>2</sub>O caused a transient increase in  $T$  that was subsequently completely reversed by additional surfactant spreading (Khargé et al., 2014). In injured regions, local volume is certain to be below normal at FRC. Whether that volume is sufficiently low to enable plasma proteins to raise  $T$ , and whether any increase in  $T$  would be sustained, remains to be determined.

Another plasma component in alveolar edema liquid suspected of raising  $T$  is cholesterol. Native surfactant includes 5–10% cholesterol. Additional cholesterol has been mixed with surfactant by organic phase combination or, with cyclodextrin-facilitated solubilization, aqueous phase combination (Gunasekara et al., 2005; Lugones et al., 2018). Cholesterol-induced  $T$  elevation has been shown, following co-adsorption, to depend on concentration, requiring a nominal cholesterol fraction of  $\geq 20\%$ , and surfactant composition. However, cholesterol in blood plasma did not raise  $T$  of an intact surfactant monolayer in the lungs (Khargé et al., 2014).

## Debris From Damaged Cells

With elevated barrier permeability and occasional hemorrhagic regions in ARDS, cells including epithelial cells and RBCs are damaged, and their contents should be present in edema liquid (Henzler et al., 2011; Santos et al., 2012). Cellular components including hemoglobin (Hb) from RBCs and phospholipids—particularly unsaturated phospholipids and lysophospholipids—and cholesterol from cell membranes may interfere with surfactant function and raise  $T$  (Holm and Notter, 1987; Holm et al., 1991, 1999; Hite et al., 2005; van Meer et al., 2008). The ability of Hb and RBC membrane lipids to increase  $T$  depends on the quantities of these inhibitory factors relative to the quantity of surfactant present (Holm and Notter, 1987; Holm et al., 1991, 1999; Hite et al., 2005). In ARDS edema liquid, my group estimated phospholipid concentration to be 2 mg/ml  $\approx 2.7$   $\mu\text{mol/ml}$ , based on the molecular weight of dipalmitoylphosphatidylcholine (Khargé et al., 2014). At a comparable 2  $\mu\text{mol/ml}$  of lipids in whole lung surfactant, Holm and Notter (1987) found membrane lipids more inhibitory than Hb and  $>1$   $\mu\text{mol/ml}$  membrane lipids necessary to raise  $T_{MIN}$ . Holm et al. (1999) also found lysophosphatidylcholine capable of raising  $T$  of an already-established intact surfactant monolayer. The high cholesterol content of cell membranes might also behave differently than plasma cholesterol and contribute to surfactant dysfunction (Gunasekara et al., 2005; van Meer et al., 2008; Lugones et al., 2018). Thus, cell debris may contribute to the elevated  $T$  of alveolar edema liquid.

## Surfactant Degradation

Surfactant lipids and proteins may be degraded by enzymes or reactive oxygen species (ROS). Inflammatory cells release secretory phospholipase A<sub>2</sub> and certain bacteria, including *Pseudomonas*, release phospholipase C (Holm et al., 1991;



Kitsioulis et al., 2009). Accordingly, in BALF from ARDS patients, elevated phospholipase levels and activity have been observed (Hallman et al., 1982; Seeds et al., 2012). Phospholipases could elevate  $T$  directly, by reducing the availability of  $T$ -lowering surfactant phospholipids. Additionally, the products of phospholipase activity, lysophospholipids and fatty acids, raise  $T_{MIN}$  in a PBS, perhaps by intercalating into and increasing fluidity of the monolayer (Holm et al., 1991, 1999; Hite et al., 2005). As mentioned, lysophosphatidylcholine, in particular, has been shown to raise  $T$  of an already-established intact surfactant monolayer (Holm et al., 1999). Thus, phospholipases in alveolar edema liquid may increase  $T$  in the lungs.

In ARDS, ROS from activated leukocytes and macrophages can attack the surfactant monolayer from below. Oxidation of phospholipids first transforms unsaturated hydrocarbon tails and then causes cleavage, resulting in lysophospholipids and fatty acids (Rodríguez-Capote et al., 2006). Oxidized phospholipids cause only a marginally greater increase in  $T$  than their unoxidized counterparts and, thus, might not increase  $T$  much more than any alteration in phospholipid composition due to contamination by lipids of degraded cell membranes. However, ROS-induced generation of lysophospholipids, which increase  $T$  of an intact surfactant monolayer, has the potential to raise  $T$ . Oxidation also alters the form and function of surfactant proteins B and C (SP-B and -C) (Rodríguez-Capote et al., 2006). For example, oxidation causes depalmitoylation of SP-C, which is known to inactivate SP-C (Gustafsson et al., 2000). Nonetheless, it is almost entirely oxidation of SP-B that results in elevated  $T$  (Rodríguez-Capote et al., 2006). The effect of ROS on surfactant proteins has been tested with co-adsorption of reconstituted surfactant components including already-oxidized proteins but not with ROS application below an intact surfactant monolayer.

Surfactant protein alteration might also contribute to the acceleration, in ARDS, of normal surfactant recycling. Surfactant isolated from BALF by centrifugation partitions into surface-active large aggregates and surface-inactive small aggregates. In ARDS, the ratio of large-to-small aggregates decreases (Günther et al., 2002). In addition, conversion of large-to-small aggregates has been shown to be facilitated by serine-active carboxyl esterases (Ruppert et al., 2003). However, whether one of the surfactant proteins might be a substrate of the esterases is not known.

## Gastric Liquid Aspiration

Aspiration of acidic gastric contents is a common cause of ARDS. In this situation, low pH gastric contents pass through the airways and mix with airway liquid, *en route* to the alveoli.

Low pH does not appear directly to alter surfactant function. In a PBS, pH as low as 2 did not alter  $T_{MIN}$  of the hydrophobic fraction of calf lung surfactant (Haddad et al., 1994). In addition, when we administered pH 1.9 HCl solution by direct micropuncture to surface alveoli of isolated rat lungs, the solution raised alveolar  $T$  over a period of  $\sim 30$  min (Nguyen and Perlman, 2018). The time delay in the lungs suggests that low pH might raise  $T$  indirectly, perhaps by damaging the alveolar epithelium

and releasing cell components that subsequently interfere with surfactant function.

Administration of pH 1.9 hydrochloric acid (HCl) solution via the trachea also raised alveolar  $T$  in isolated rat lungs. Surprisingly, however, this effect was not pH dependent. Tracheal instillation of pH 5.0 normal saline caused the same increase in alveolar  $T$  (Nguyen and Perlman, 2018). The  $T$ -raising effect of HCl or saline instillation was not due to surfactant dilution as direct alveolar injection of saline, which should cause greater dilution, did not alter  $T$  from normal. Further, even tracheal instillation of the surfactant Infasurf raised alveolar  $T$ . Thus, we suspected the involvement of airway mucins and, indeed, injection into surface alveoli of tracheal lavage liquid raised alveolar  $T$ . Addition to the tracheal lavage liquid of HCl or calcium, both of which aggregate mucins, reduced or eliminated the effect of tracheal lavage liquid on alveolar  $T$ . And, following tracheal saline administration, alveolar liquid sampled directly by vacuum suction through a glass micropipette contained mucin 5B. Thus, we demonstrated that tracheal liquid instillation raises alveolar  $T$  by washing  $T$ -raising airway mucins to the alveolus.

In gastric aspiration, the effects of pH and mucins should tend to balance one another. If gastric contents mix significantly with airway liquid, then they should be partially buffered but also collect mucins (Kim et al., 2014; Nguyen and Perlman, 2018). The higher pH might not be injurious, but the mucins might elevate  $T$  (Nguyen and Perlman, 2018). Alternatively, if there is relatively little mixing with airway liquid, there will be relatively little buffering, and pH will remain low. The low pH will tend to aggregate mucins such that the mucins might not contribute to elevated  $T$  (Hong et al., 2005; Nguyen and Perlman, 2018). The low pH, itself, should lead to elevated  $T$ , albeit perhaps indirectly via debris from damaged epithelial or other cells. Regardless of the degree of mixing between gastric contents and airway liquid, gastric aspiration is likely to raise alveolar  $T$ .

## MEANS OF REDUCING $T$ -DEPENDENT VILI

Surface tension is believed to be elevated in ARDS and is further increased by lung inflation during ventilation. And the static and dynamic stress concentrations described above, which likely contribute to VILI, are proportional to  $T$ . Thus, lowering  $T$  should reduce the VILI.

### Means of Reducing $T$

Surfactant therapy has been tested for ARDS but, in six randomized controlled clinical trials, failed to reduce mortality (Brower and Fessler, 2011). Certainly, surfactant could lower  $T$  and yet fail to reduce mortality. However, surfactant therapy only improved oxygenation significantly in one of the six trials and marginally in one other and did not improve compliance in either of the two trials in which compliance was assessed (Weg et al., 1994; Anzueto et al., 1996; Gregory et al., 1997; Spragg et al., 2004, 2011; Kesecioglu et al., 2009), suggesting

that it is a challenge for exogenous surfactant to lower alveolar  $T$ . Problematic surfactant dosage, administration technique, and formulation have been discussed as possible causes of the failure of surfactant therapy in ARDS (Spragg et al., 2011; Kazemi et al., 2019). My group has identified two new potential causes for the failure of surfactant therapy. First, surfactant delivery appears to be problematic. As detailed above, tracheal instillation of any liquid washes  $T$ -raising mucins to the alveolus. Thus, tracheal instillation of surfactant, contrary to expectation, *raises* alveolar  $T$  (Nguyen and Perlman, 2018). [Lower mucin production and more airspace liquid to dilute mucins may enable surfactant therapy efficacy in NRDS (Buisine et al., 1999)]. Second, when  $T$  is elevated in ARDS, adding more surfactant may fail to reduce  $T$ . In isolated rat lungs, we modeled acid-aspiration ARDS by administering pH 1.9 HCl solution to the alveolus by direct micropuncture or indirect tracheal instillation (Nguyen and Perlman, 2018). Both administration methods raised alveolar  $T$ . In both cases, however, subsequent alveolar delivery of mucin-free Infasurf by micropuncture failed to reduce  $T$ . Whether surfactant, if it could be delivered mucin-free in a clinical setting, would be effective in other forms of ARDS remains to be determined.

With our  $T$ -determination method, we identified a potential alternative means of reducing  $T$  in ARDS. We found that the non-toxic dye sulforhodamine B (SRB) acts in conjunction with albumin present in edema liquid to improve the efficacy of native lung surfactant and lower  $T$  27% below normal in healthy lungs (Kharge et al., 2015). Thus, albumin, generally believed to be detrimental, might beneficially help lower  $T$ . Further, SRB, which has a molecular weight of 577 and is water soluble, might be administered intravenously. In this case, SRB would be expected to reach the alveolar liquid, along with albumin, specifically in injured regions where barrier permeability is elevated. Whether SRB will work in the presence of the various factors responsible for elevating  $T$  in ARDS remains to be determined.

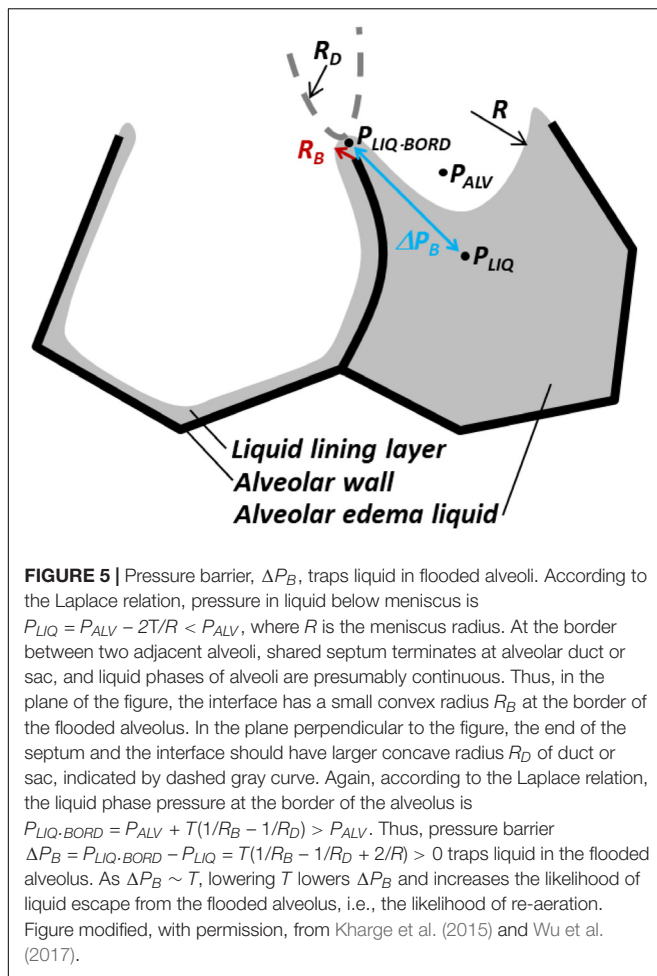
## Effects of Reducing $T$

Reducing  $T$  should help reduce VILI via various mechanisms. Direct effects of lowering  $T$  are as follows. Lowering  $T$  should increase  $P_{LIQ}$  in flooded alveoli, thus reduce bowing of and stress concentrations in intervening septa. Lowering  $T$  should reduce the diminishment of flooded alveoli and may prevent or reverse alveolar collapse, thus should reduce stress concentrations in radiating septa. And reducing stress concentrations in intervening or radiating septa should reduce VILI. Indeed, with our local VILI assay (Figure 4A), we demonstrated that lowering  $T$ , including by administration of SRB, reduced ventilation-induced barrier injury (Wu et al., 2014; Kharge et al., 2015).

Lowering  $T$  should also indirectly reduce stress concentrations in radiating septa. That is, lowering  $T$  should reduce the  $P_O$  required for air to enter a flooded region or to peel open the apposed septa of a collapsed region (Enhörning and Robertson, 1972; Gaver et al., 1990). Thus lowering  $T$ , by lowering  $P_O$ , should reduce the peak cyclic stress applied, just before reopening, to radiating septa around the injured region.

Further, lowering  $T$  may reduce VILI by promoting re-aeration of previously flooded or collapsed alveoli. Low  $T$ -induced re-aeration of a flooded alveolus is a rapid process in which liquid that has been sequestered in the alveolus redistributes, more equitably, across regional alveoli. In regions of heterogeneous alveolar flooding or collapse (Figures 2B, 4), re-aeration should reduce the degree of heterogeneity, thus, the number of intra-regional stress concentrations. For example, in regions of heterogeneous alveolar flooding, considering that bowed intervening septa are likely more stressed than planar septa separating two aerated or two flooded alveoli, we quantified heterogeneity as the percentage of all septa that were intervening septa (Wu et al., 2017). (In this basic analysis, we did not account for the presence of stressed radiating septa within injured regions). We found that heterogeneity peaked when ~50% of alveoli were flooded. Thus with heterogeneous flooding, reducing the number of flooded alveoli should reduce the number of intervening septa in which stress is concentrated and, in turn, VILI. (If >50% of alveoli are initially flooded, reducing the number of flooded alveoli should first exacerbate and then, once alveolar flooding decreases below 50%, relieve VILI). In regions with homogeneous alveolar flooding or collapse, re-aeration is most likely to occur on the periphery of the region (see below). As intervening and radiating septa around the perimeter of a homogeneously injured region are the sites of greatest stress concentration, re-aeration should, by reducing injured region perimeter length, reduce the number of septa in which stress is concentrated and reduce VILI.

Experimental evidence supports the possibility that lowering  $T$  may promote rapid re-aeration that could be beneficial in the time period before re-absorption causes the permanent re-aeration of ARDS resolution. Though the mechanism of rapid re-aeration has yet to be fully elucidated, my group has made observations that inform an understanding of the process (Kharge et al., 2015; Wu et al., 2017). (i) Flooded alveoli generally remain flooded and, at normal  $T$ , lung inflation does not generally cause re-aeration. However, occasionally, a flooded alveolus will spontaneously re-aerate. (ii) When  $T$  is reduced by SRB administration and the lungs are gently ventilated, the frequency of re-aeration increases. The direct effect of lowering  $T$  might be amplified by reduced  $T$  causing greater tissue stretch and thus contributing to enhanced surfactant secretion. (iii) It is also possible to promote re-aeration by accelerating deflation to increase momentum transfer to the flooding liquid and, essentially, catapult liquid out of alveoli. Accelerated deflation successfully reduces the number of flooded alveoli, and thus flooding heterogeneity, only when  $T$  is normal (below-normal  $T$  should be even better), and PIP is moderate, such that  $T$  at peak inflation is not too high. (iv) When  $T$  is elevated ~50% above normal in our model of Figure 4B, accelerated deflation still propels liquid out of flooded alveoli, but the high  $T$  keeps the liquid aggregated. The liquid transfers *en mass* to a neighboring alveolus that was previously aerated and the number of flooded alveoli remains unchanged. (Consistent with the hydrostatic origin of flooding in this model, the observation



of liquid transfer between alveoli indicates that alveoli are truly flooded, not collapsed. That is, flooding liquid volume is greater than the aggregated liquid lining layer volume that would be found in the center of a collapsed alveolus. (v) Finally, whether spontaneous or prompted by reduced  $T$  or accelerated deflation, we do not observe re-aeration of flooded alveoli surrounded entirely by other flooded alveoli but, rather, always of flooded alveoli that were in contact with one or more aerated alveoli. We interpret that flooded alveoli that are adjacent to at least one aerated alveolus are in a state of  $T$ -dependent unstable equilibrium.

The unstable equilibrium of flooded alveoli with aerated neighbors may be attributable to the antagonism across each intervening septum of outward-acting  $P_D$ , applied by radiating septa (Figure 1C, right), vs. inward-acting  $\Delta P_S$  (Figure 3B). We have not identified the circumstances in which outward  $P_D$  sometimes prevails over inward  $\Delta P_S$ , but note that a greater number of aerated neighbors make this occurrence more likely. Nevertheless, flooded alveoli typically remain flooded. This general stability is assisted by liquid pressure being greater at the border than in the center of flooded alveoli. That is, there is a pressure barrier,  $\Delta P_B$ , that opposes liquid flow out of flooded alveoli and that is proportional to  $T$  (Figure 5). By

trapping liquid in flooded alveoli,  $\Delta P_B$  tends to maintain the low  $P_{LIQ}$  in flooded alveoli and thus maintain the diminished size of flooded alveoli. However, lowering  $T$  reduces  $\Delta P_B$  and increases the likelihood of re-aeration (Kharge et al., 2015). For this reason, accelerated deflation most effectively clears alveoli when PIP is moderate, such that high elastic recoil for momentum transfer is balanced with low peak  $T$  for maintaining a low  $\Delta P_B$ , and SRB administration increases the frequency of re-aeration during gentle ventilation (Kharge et al., 2015; Wu et al., 2017).

The existence of a pressure barrier is also supported by—and helps to explain—the difference in efficacy between two alternative recruitment maneuvers for initial inflation of immature fetal lungs. In a preterm lamb model, Tingay et al. (2019) showed that a gradual recruitment maneuver increases lung compliance more than an abrupt maneuver. This result might be explained by greater alveolar aeration at moderate  $P_L$  values—due to a moderate  $T$  and consequently moderate  $\Delta P_B$ —in the course of the gradual maneuver. Although Tingay et al.'s (2019) direct comparison appears to be unique, other studies suggest that gradual recruitment may also result in greater re-aeration in ARDS. First, ARDS lung volume increased more in response to inflation from  $P_L$  of 19 to 28 cm H<sub>2</sub>O than from 28 to 40 cm H<sub>2</sub>O (Cressoni et al., 2017). Second, in an ARDS recruitment maneuver comprising a 7-s ramp up to a sustained 40 cm H<sub>2</sub>O, essentially all of the effected volume increase occurred within the first 10 s after the ramp up period (Arnal et al., 2011). Finally, the response, in ARDS patients, to an abrupt 40 cm H<sub>2</sub>O recruitment maneuver was inversely proportional to extravascular lung water index (Smetkin et al., 2012)—suggesting that high pressure may not effectively clear fluid from edematous alveoli, perhaps due to a high  $\Delta P_B$ . A gradual recruitment maneuver might be more effective than an abrupt maneuver.

Re-aeration, by distributing liquid equitably between alveoli and thereby reducing the prevalence of stress concentrations, should reduce VILI. The balance between entering air (promoted by a high  $P_{AW} > P_O$ ) and escaping liquid (promoted by a low  $P_L$  that maintains a low  $T$  and low  $\Delta P_B$ ) that causes re-aeration of a flooded alveolus remains to be determined. Such an understanding of the mechanism of flooded alveolar re-aeration might lead to new ventilation and recruitment maneuver protocols for maintaining an open lung.

## DISCUSSION AND CONCLUSION

The above analysis stems from observations of  $T$  effects on flooded alveolar mechanics and speculates about consequences not yet investigated experimentally. The speculation, however, has limitations. First, the experimental observations were made in alveoli that were generally flooded with proteinaceous model edema liquid but that were otherwise, at least prior to ventilation, normal. The influence of pre-existing injury on flooded alveolar mechanics is not known. For example, whether flooded injured alveoli maintain normal compliance is not known. Second,

discussion of  $T$  effects in regions of alveolar collapse is speculative. Alveolar collapse in a lung injury model has not, to date, been identified by microscopy on the surface of isolated lungs. Thus, collapse has not been studied, like flooding, with high resolution and tracking across varied inflation pressures. Third, the mechanism of flooded alveolar re-aeration, which should reduce the prevalence of stress concentrations, remains to be elucidated. And the feasibility of permanently re-aerating injured alveoli in ARDS is not known. Nonetheless, evidence suggests that lowering  $T$  should reduce alveolar septal stress concentrations and that lowering  $T$  in conjunction with application of gradual recruitment maneuvers may improve lung re-aeration. And both interventions should reduce VILI. Treatment with SRB appears a promising avenue of investigation for lowering  $T$  and VILI in ARDS.

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## ETHICS STATEMENT

Ethical review and approval was not required for the animal experiments because this manuscript presents animal data from prior studies, for which IACUC approval was previously obtained, but not any new animal data.

## AUTHOR CONTRIBUTIONS

CP conceived of the subject matter for and wrote this manuscript.

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# Three Alveolar Phenotypes Govern Lung Function in Murine Ventilator-Induced Lung Injury

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Mechanical ventilation is an essential lifesaving therapy in acute respiratory distress syndrome (ARDS) that may cause ventilator-induced lung injury (VILI) through a positive feedback between altered alveolar mechanics, edema, surfactant inactivation, and injury. Although the biophysical forces that cause VILI are well documented, a knowledge gap remains in the quantitative link between altered parenchymal structure (namely alveolar derecruitment and flooding), pulmonary function, and VILI. This information is essential to developing diagnostic criteria and ventilation strategies to reduce VILI and improve ARDS survival. To address this unmet need, we mechanically ventilated mice to cause VILI. Lung structure was measured at three air inflation pressures using design-based stereology, and the mechanical function of the pulmonary system was measured with the forced oscillation technique. Assessment of the pulmonary surfactant included total surfactant, distribution of phospholipid aggregates, and surface tension lowering activity. VILI-induced changes in the surfactant included reduced surface tension lowering activity in the typically functional fraction of large phospholipid aggregates and a significant increase in the pool of surface-inactive small phospholipid aggregates. The dominant alterations in lung structure at low airway pressures were alveolar collapse and flooding. At higher airway pressures, alveolar collapse was mitigated and the flooded alveoli remained filled with proteinaceous edema. The loss of ventilated alveoli resulted in decreased alveolar gas volume and gas-exchange surface area. These data characterize three alveolar phenotypes in murine VILI: flooded and non-recruitable alveoli, unstable alveoli that derecruit at airway pressures below 5 cmH<sub>2</sub>O, and alveoli with relatively normal structure and function. The fraction of alveoli with each phenotype is reflected in the proportional changes in pulmonary system elastance at positive end expiratory pressures of 0, 3, and 6 cmH<sub>2</sub>O.

**Keywords:** ventilator-induced lung injury, stereology, pulmonary surfactant, lung function, alveolar mechanics

## INTRODUCTION

Mechanical ventilation is required for major surgery and resuscitation and in critical emergencies such as acute respiratory distress syndrome (ARDS) (Force et al., 2012), but this lifesaving therapy carries the risk of ventilator-induced lung injury (VILI). The mechanisms of VILI are well documented and include direct tissue injury from overdistension (volutrauma) (Webb and Tierney, 1974; Hernandez et al., 1989) and the cyclic collapse and reopening of small airways and alveoli (atelectrauma) (Muscedere et al., 1994). These injurious forces act at the microscale to damage the epithelial and endothelial cells that comprise the blood-gas barrier (Dreyfuss and Saumon, 1998; Hamlington et al., 2018b), allowing the ingress of proteinaceous edema into the distal airspace that is associated with changes in lung mechanics (Hamlington et al., 2016a).

Changes in the lung structure–function relationship during VILI are currently understood through the lens of organ-scale imaging techniques such as CT (Yen et al., 2019). However, the positive feedback mechanism between leak, surfactant function, altered mechanics, and injury occurs at the alveolar and acinar scales (Knudsen et al., 2018). As such, measurements of morphometry are necessary to bridge studies of cellular injury and alveolocapillary barrier disruption (Hamlington et al., 2018a) to organ-scale measurements of structure and function. Understanding how these mechanisms are associated across length scales is critical for developing approaches to mitigating them. Structure–function correlations may also improve clinical practice by defining the mechanistic basis for diagnostic parameters such as the driving pressure (Aoyama et al., 2018; Pereira Romano et al., 2020) and subject-specific computational models (Hamlington et al., 2016b; Mellenthin et al., 2019; Morton et al., 2019) that seek to optimize ventilation based on patient-specific alveolar mechanics.

To address this knowledge gap, we used design-based stereology to measure parenchymal structure over a range of air inflation pressures in a mouse model of VILI. The state of the pulmonary surfactant system was assessed by measuring minimum surface tension and surfactant composition. Organ-scale mechanical function was determined with the forced oscillation technique (FOT) to quantify stiffness, airway resistance, and tissue damping at different levels of lung inflation. Together, these data define the structure–function relationship in murine VILI.

## MATERIALS AND METHODS

### Animal Procedures

Eight to ten week old female BALB/c mice (Jackson Laboratories, Bar Harbor, ME, United States) weighing 17.1–22.3 g were studied under Institutional Animal Care and Use Committee (IACUC)-approved protocols. Mice were anesthetized with an intraperitoneal (IP) injection of 100 mg/kg ketamine and 16 mg/kg xylazine, tracheostomized with a 18 ga metal cannula, and ventilated using a flexiVent small animal ventilator (SCIREQ, Montreal, QC, Canada). Respiratory drive was suppressed *via*

0.8 mg/kg pancuronium bromide administered at the onset of mechanical ventilation. Alternating doses of 50 mg/kg ketamine and 50 mg/kg ketamine with 8 mg/kg xylazine were administered at 30-min intervals with 150  $\mu$ L IP 5% dextrose lactated Ringer's solution. Fluid volume from the anesthetic was 10  $\mu$ L/g. The electrocardiogram was monitored to assure that the rodents maintained a deep plane of anesthesia during paralysis.

Mechanical ventilation experiments to generate tissue for structural analysis were conducted at the University of Vermont and approved by the University of Vermont Institutional Animal Care and Use Committee (IACUC #14-056). Bronchoalveolar lavage fluid for surfactant analysis was collected under identical ventilation conditions by the same investigator at the University of Colorado Denver in experiments approved by the University of Colorado Denver Anschutz Medical Campus, IACUC (#00230).

### Ventilation Protocol

All animals were ventilated for a 10-min stabilization period with a delivered tidal volume ( $V_t$ ) = 10 ml/kg at a respiratory rate (RR) = 200 breaths/min and a positive end expiratory pressure (PEEP) = 3 cmH<sub>2</sub>O (baseline ventilation). Recruitment maneuvers (RM) consisting of a 3 sec ramp to 30 cmH<sub>2</sub>O followed by a 3 sec breath hold were applied to reopen regions that may have collapsed during the surgical procedure. Following the stabilization period, lung function was assessed. Testing consisted of an RM and a dynamic pressure–volume (PV) loop that ramped airway pressure ( $P_{aw}$ ) from 0 to 37.5 cmH<sub>2</sub>O, held pressure for 3 sec, and ramped pressure back to zero over 3 sec. Derecruitability tests were then performed at PEEP = 6, 3, and 0 cmH<sub>2</sub>O, denoted by  $D_{rec}^{PEEP6}$ ,  $D_{rec}^{PEEP3}$ , and  $D_{rec}^{PEEP0}$ . Each test consisted of an RM and then  $V_t$  = 10 ml/kg and RR = 200 breaths/min at the specified PEEP. Nine multi-frequency FOT impedance measurements were recorded at 18 s intervals and fit to the constant phase model (Hantos et al., 1992) to determine respiratory system elastance (H), tissue damping (G), and Newtonian resistance (Rn). The total duration of the lung function assessment was 13 min. Lungs from the control group were then harvested for morphometric analysis. In a separate sub-group of animals, bronchoalveolar lavage fluid (BALF) was collected for surfactant analysis.

The VILI group was then subjected to repeated blocks of ventilation consisting of 4 min 45 s of injurious ventilation with a plateau pressure ( $P_{plat}$ ) = 37.5 cmH<sub>2</sub>O, RR = 50 breaths/min, inspiratory:expiratory ratio of 1:2, and PEEP = 0 cmH<sub>2</sub>O. This  $P_{plat}$  was selected to generate severe VILI in an experimentally tractable timeframe without causing any pneumothoraces. At the end of each block a PV loop was recorded followed by two FOT measurements separated by 10 s of baseline ventilation. These 5-min ventilation blocks were applied until  $H$  doubled, at which point the lung function assessment was repeated prior to harvest for either morphometry or surfactant analysis. The mean duration of injurious mechanical ventilation was 87.3 min with a standard deviation of 17.5 min. Including with the 10 min stabilization period and two 13 min lung function assessments, the mean duration of ventilation for the VILI group was 123.3 min.



## Surfactant Analysis

Bronchoalveolar lavage fluid was collected by instilling and suctioning back 1 ml warm normal saline three times and then centrifuging at 700 *g* at 4°C for 5 min. A total of 100  $\mu$ l of the cell-free supernatant for each animal was separated, and the remainder of the BALF from three mice in the same treatment group was combined and centrifuged at 40,000 *g*. The ultracentrifuged supernatant containing the surfactant small aggregate (SA) was stored at –80°C for later analysis. The surfactant pellet, containing the large aggregate (LA) fraction, was washed twice by resuspending the pellet in 1 ml saline and centrifuging at 40,000 *g*. Finally, the LA pellet was resuspended in 100  $\mu$ l saline and stored at –80°C for later analysis.

Quantitation of the surfactant recovered from the BAL was completed by measuring lipid phosphorous content in the LA and SA fractions as previously described (Rouser et al., 1970). Total surfactant recovery represents the combined amount of both fractions. Total BAL protein was quantified with a BCA assay (ThermoShandon-Pierce). Surfactant surface lowering activity was assessed by measuring minimal surface tension of the LA fraction *ex vivo* using a pulsating bubble surfactometer (General Transco) as described (Enhörning and Holm, 1993; Hite et al., 2005). Surfactant was preheated to 37°C at 2 mg (PL from LA)/ml in 150 mM NaCl, 5 mM CaCl<sub>2</sub>, 5 mM Tris solution, and the samples were pulsed at 20 pulses/min for 20 min.

## Lung Tissue Preparation

Lung structure was analyzed in a separate subgroup of mice that were not subjected to a bronchoalveolar lavage. The lungs were fixed through the vasculature while the air inflation pressure was held at a prescribed level (described below) to maintain surface tension effects and allow comparison to the lung function data (Gil et al., 1979; Bachofen et al., 1982). The fixation process was initiated during baseline ventilation by performing a bilateral thoracotomy and flushing the pulmonary circulation with 5 ml 100 U/ml heparinized saline with 3% 100 kDa dextran at a pressure of 25 cmH<sub>2</sub>O. Three RMs were applied and then Paw increased to 30 cmH<sub>2</sub>O over 3 s, held for 3 s, decreased to either 2, 5, or 10 cmH<sub>2</sub>O, and the trachea was ligated. These pressures were selected based on our previous morphometric analysis of bleomycin-injured rats (Knudsen et al., 2018) where nearly all recruitable alveoli were open at Paw = 10 cmH<sub>2</sub>O and approximately half the recruitable alveoli were closed at Paw = 5 cmH<sub>2</sub>O. The lower limit of Paw = 2 cmH<sub>2</sub>O was selected since PEEPs < 2 cmH<sub>2</sub>O are not typically applied in lung-protective ventilation. Five animals were prepared at each airway pressure for the control and VILI groups. The lungs were then perfused with 1.5% glutaraldehyde, 1.5% paraformaldehyde in 0.15 M HEPES buffer for approximately 5 min before immersion fixation for at least 24 h.

Tissue processing and sampling was conducted using standardized protocols (Mühlfeld et al., 2013; Knudsen et al., 2018). Briefly, non-pulmonary tissue was removed, and the total lung volume determined using Archimedes principle. The first step of systematic uniform random sampling was conducted by cutting the lungs into 1.5 mm transverse sections and retaining

either even or odd numbered slabs. The slabs were post-fixed with 1% OsO<sub>4</sub> in 0.1 M cacodylate buffer for 2 h and then overnight in half saturated aqueous uranyl acetate, dehydrated in a graded acetone series, and embedded in glycol methacrylate (Technovit 7100, Heraeus Kulzer, Wehrheim, Germany) to avoid tissue shrinkage (Schneider and Ochs, 2014). The first and fourth 1.5  $\mu$ m sections from a consecutive series were mounted and stained with orcein and then used with the physical disector stereology probe to estimate alveolar number. Another 1.5  $\mu$ m section was stained with toluidine blue to estimate volumes and surface areas.

## Design-Based Stereology

The stereological analysis was conducted according to standards for lung structure quantification (Hsia et al., 2010). A majority of the systematic uniform random sampling and image acquisition was conducted using a Zeiss Axioscope II with a Zeiss Axiocam AR camera (Zeiss, Thornwood, NY, United States) controlled with the Stereo Investigator software package (MBF Bioscience, Williston, VT, United States). Approximately 10% of the images (distributed randomly across groups and subjects) were recorded using an Olympus BX53 with a DP73 camera (Olympus, Waltham, MA, United States) controlled with the NewCast stereology software (Visiopharm, Hørsholm, Denmark). Stereological quantification of all images was performed using a custom MATLAB (Mathworks, Natick, MA, United States) graphical user interface.

A cascade sampling design was used starting with the volume fraction of parenchyma in the whole lung [ $V_v(\text{par/lung})$ ] that we define as areas contributing to gas exchange and excluding airways, vessels outside the septal walls, and peribronchiolar tissue. This, and all volume fractions, were measured using point counting. The percentage of the tissue section analyzed (the sampling fraction,  $S_F$ ) for  $V_v(\text{par/lung})$  was 100% at 5 $\times$  magnification. The parenchyma was then subdivided into volume fractions of alveolar airspace [ $V_v(\text{alvair/par})$ ], alveolar duct airspace [ $V_v(\text{ductair/par})$ ], and non-air material [ $V_v(\text{non-air/par})$ ] that include tissue and airspace edema fluid. This assessment was performed at 20 $\times$  magnification and  $S_F = 11\%$ . Fields of view were selected for analysis using systematic uniform random sampling whereby the morphometry software selected a random starting location and images were then automatically sampled on a 1,200  $\times$  1,200  $\mu$ m grid over the entire tissue section. This approach blinds the investigator to the selection of the images used for analysis, thus removing the potential for bias. The non-air material in the parenchyma [ $V_v(\text{non-air/par})$ ] was then analyzed at 40 $\times$  magnification ( $S_F = 2.8\%$ , 1,200  $\mu$ m grid spacing) to determine the volume fractions of septal tissue of patent alveoli [ $V_v(\text{sep,air/par})$ ], total septal tissue [ $V_v(\text{sep,total/par})$ ], and airspace edema [ $V_v(\text{edema/par})$ ]. The volume of each compartment (demarcated with  $V$  in place of  $V_v$ ) was determined by multiplying the volume fractions by the volume of the reference space. The surface area per volume available for gas exchange [ $S_v(\text{alvair/par})$ ] was estimated at 40 $\times$  magnification ( $S_F = 2.8\%$ , 1,200  $\mu$ m grid spacing) by counting line intersections with aerated septal tissue that was not covered with alveolar edema. The gas exchange surface area

[S(alvair)] was determined by multiplying  $S_v(\text{alvair}/\text{par})$  by the parenchymal volume  $V(\text{par})$  and the mean septal thickness defined as  $\tau(\text{sep}) = 2 V(\text{sep}, \text{air})/S(\text{alvair})$ . The physical disector method (Ochs et al., 2004) was used to determine the number of patent  $N(\text{alv})$  and flooded  $N(\text{flood})$  alveoli that we define as alveoli with visible architecture and alveolar edema fully blocking the alveolar mouth using  $40\times$  magnification ( $S_F = 6.25\%$ ,  $800 \mu\text{m}$  grid spacing). The total number of alveoli is then  $N(\text{alv}, \text{total}) = N(\text{alv}) + N(\text{flood})$ , the number-weighted average alveolar volume  $V_n(\text{alv}) = V(\text{alvair})/N(\text{alv})$ , and the alveolar surface area to volume ratio  $S/V(\text{alv}) = S(\text{alvair})/V(\text{alvair})$ .

## Statistical Analysis

Data were curated in MATLAB and statistical analysis was performed in R (The R Foundation). A Shapiro–Wilk test was used to assess normality. If the data were not significantly different from the normal distribution ( $p > 0.05$ ) then an ANOVA was performed followed by pairwise comparisons using the lsmeans package (Lenth, 2016) and Tukey's adjustment for multiple comparisons. Data that failed the normality test was analyzed with a Kruskal–Wallis test followed by a rank-sum Conover–Iman test (PMCMR package) with the Holm correction for multiple comparisons.

The time series of lung function parameters  $H$ ,  $G$ , and  $R_n$  measured during the derecruitability tests were analyzed using a linear mixed effects model (LME) (NLME package in R) on the natural logarithm of the time and parameter values. This is equivalent to fitting the equation  $y = \alpha t^\beta$  to the time series of measurements as we have previously described (Smith et al., 2017). Fixed effects were derecruitability test PEEP ( $D_{\text{rec}}^{\text{PEEP}}$ ), the time within the derecruitability test ( $t$ ), and whether the measurement was recorded before or after VILI (Injury). The intercept for each animal was included as a random effect and the Akaike information criterion (AIC) was used to determine the most appropriate model. Temporal autocorrelation was accounted for with a first-order autocorrelation structure for the continuous time covariate grouped by animal, derecruitability test PEEP, and injury status (Pinheiro and Bates, 2000).

## RESULTS

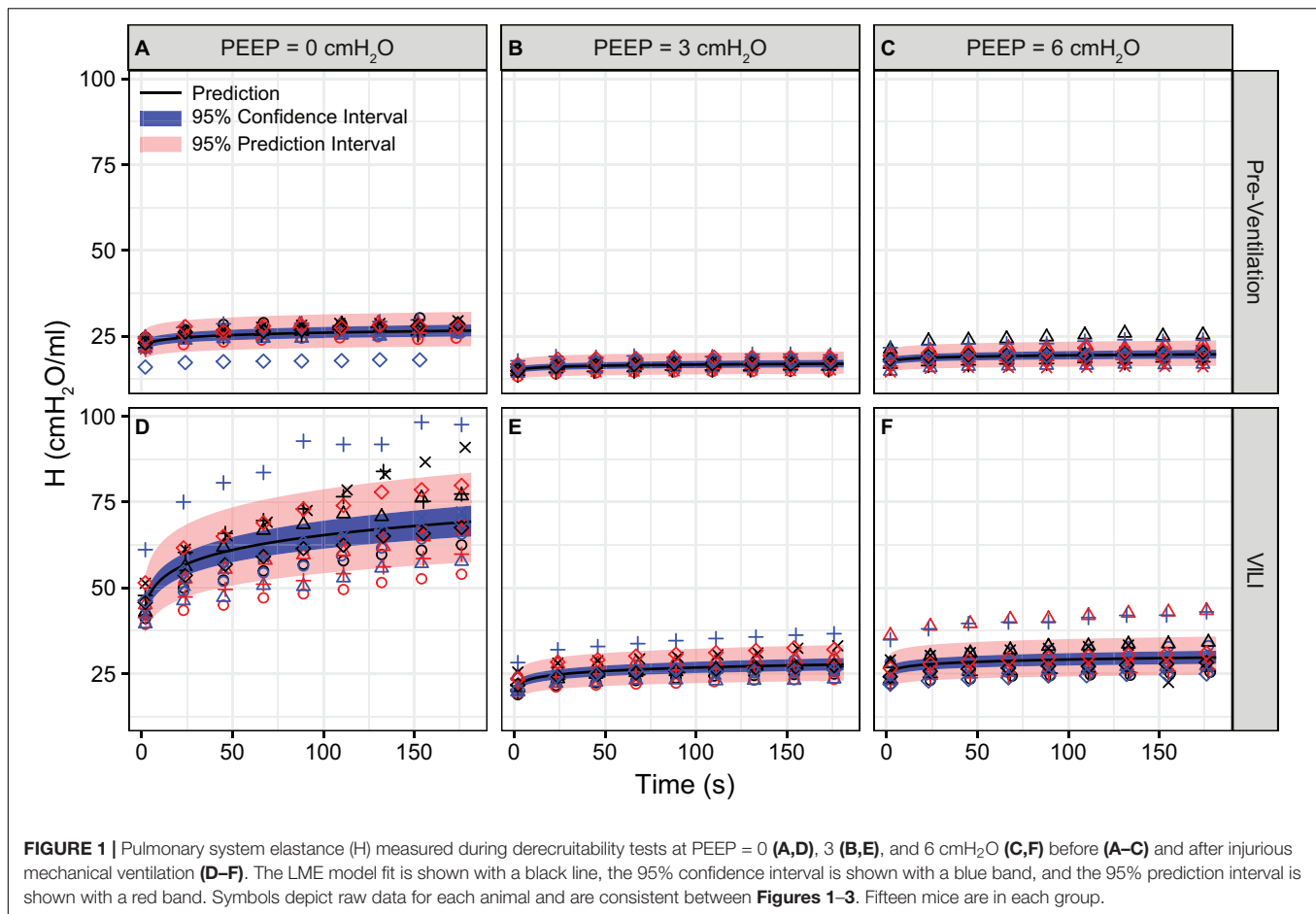
Pulmonary system elastance following an RM in the uninjured lungs (Figure 1, first row) was significantly different between the derecruitability tests at different PEEP levels, while the rate of change of  $H$  over time (the slope) remained consistent between PEEPs (Table 1). VILI (Figure 1, second row) increased the  $H$  intercept at all PEEPs with a proportionally greater increase occurring in  $D_{\text{rec}}^{\text{PEEP}0}$  where the elastance at the start of the derecruitability test was approximately doubled. The rate of elastance increase over time was also elevated in  $D_{\text{rec}}^{\text{PEEP}0}$  and, to a lesser extent, in  $D_{\text{rec}}^{\text{PEEP}3}$ . Tissue damping ( $G$ ) increased monotonically with PEEP prior to injury (Figure 2, first row) and was independent of  $t$  (Table 2). Following VILI,  $G$  demonstrated a marked increase in  $D_{\text{rec}}^{\text{PEEP}0}$  that was similar in magnitude to the change in  $H$ . Central airway resistance ( $R_n$ ) tended to decrease with

PEEP (Figure 3) in both healthy and injured lung. Following VILI,  $R_n$  was slightly increased in  $D_{\text{rec}}^{\text{PEEP}0}$  and decreased in  $D_{\text{rec}}^{\text{PEEP}6}$ . The temporal dependence of  $R_n$  was not affected by VILI (Table 2).

The changes in lung function are associated with structural alterations in the perfusion-fixed lung tissue. Alveoli in the Control lungs (Figure 4, first row) remained patent from  $P_{\text{aw}} = 10 \text{ cmH}_2\text{O}$  (right column) down to airway pressures of  $2 \text{ cmH}_2\text{O}$  (left column). Note that these airway pressures are applied in open-chested mice, and the contributions of the chest wall are discussed below. By contrast, the VILI lungs exhibited diffuse alveolar edema (second row, asterisks) and retraction of the alveolar septa (second row, arrows) at  $P_{\text{aw}} = 5$  and  $10 \text{ cmH}_2\text{O}$ . At  $P_{\text{aw}} = 2 \text{ cmH}_2\text{O}$ , the injured parenchyma tended to consolidate into patches of flooded and collapsed alveoli with air remaining in the ductal space. These injured regions were interspersed between areas of parenchyma that appeared normal.

Quantitative structural changes with VILI included a significant decrease in  $V(\text{alvair})$  (Figure 5A) in conjunction with reduced  $N(\text{alv})$  (Figure 6B). The average alveolar volume  $V_n(\text{alv})$  is defined as the ratio of these two quantities and indicates a modest stiffening of patent alveoli with injury (Figure 6E). By contrast,  $V(\text{ductair})$  did not demonstrate significant alterations in VILI (Figure 5B), leading to a fractional shift of ventilation volume from the alveoli to the alveolar ducts with VILI (Figure 5C) that was significant at all airway pressures. The surface area available for gas exchange (Figure 5D) was significantly reduced across all airway pressures in VILI. This reduction is primarily due to a loss of ventilated alveoli and not to reduced surface area to volume ratio in the remaining patent units as indicated by increased  $S/V(\text{alv})$  when comparing control and VILI at  $P_{\text{aw}} = 2 \text{ cmH}_2\text{O}$  (Figure 6F, lines). For comparison, Figure 6F shows the hypothetical surface area to volume ratios for perfectly spherical alveoli (symbols), and these values are less than those measured *in vivo* despite the reduction in area caused by the alveolar mouth. The increase in  $S/V(\text{alv})$  at low  $P_{\text{aw}}$  in VILI suggests that the alveolar geometry becomes more distorted in the injured lung. Injurious ventilation did not change  $V(\text{sep}, \text{total})$  (Figure 5E) or  $\tau(\text{sep})$ , and although septal thickness tended to increase with decreasing  $P_{\text{aw}}$  there were no significant alterations (Figure 6A). Little to no airspace edema was observed in the control animals (Figure 5F), and  $V(\text{edema})$  was constant across inflation pressures in VILI.

The number of ventilated alveoli  $N(\text{alv})$ , Figure 6B] remained constant across inflation pressures in the Control animals, indicating an absence of derecruitment even at  $P_{\text{aw}} = 2 \text{ cmH}_2\text{O}$ . The VILI mice demonstrated a constant  $N(\text{alv})$  at  $P_{\text{aw}} = 5$  and  $10 \text{ cmH}_2\text{O}$  that was significantly less than in the Controls. Reducing the inflation pressure to  $2 \text{ cmH}_2\text{O}$  in the VILI animals led to a significant reduction in aerated alveoli. Flooded alveoli  $N(\text{flood})$ , Figure 6C] were defined as having a liquid meniscus fully spanning the alveolar mouth.  $N(\text{flood})$  remained constant across inflation pressures in the VILI group, and no flooded alveoli were observed across the 15 control lungs analyzed (Table 3). Figure 6D shows that the total number of flooded and aerated alveoli  $N(\text{alv}, \text{total})$  is consistent across all



**TABLE 1** | Pairwise comparison of the LME model using log-transformed lung function parameters, which is equivalent to fitting the equation  $y = \alpha t^\beta$  to the raw data.

Pairwise comparison	Slope			Intercept		
	H	G	Rn	H	G	Rn
$D_{rec}^{PEEP0} (Pre) - D_{rec}^{PEEP3} (Pre)$	-0.012	0.002	-0.016	0.68	1.25	0.61
$D_{rec}^{PEEP0} (Pre) - D_{rec}^{PEEP6} (Pre)$	-0.013	0.001	-0.032	0.79	1.78	0.52
$D_{rec}^{PEEP3} (Pre) - D_{rec}^{PEEP6} (Pre)$	-0.001	-0.001	-0.016	1.17	1.42	0.85
$D_{rec}^{PEEP0} (Pre) - D_{rec}^{PEEP0} (Post)$	0.060	0.115	0.008	1.90	2.17	1.15
$D_{rec}^{PEEP3} (Pre) - D_{rec}^{PEEP3} (Post)$	0.029	0.022	0.009	1.40	1.06	0.97
$D_{rec}^{PEEP6} (Pre) - D_{rec}^{PEEP6} (Post)$	0.008	-0.018	-0.002	1.44	1.16	0.86
$D_{rec}^{PEEP0} (Post) - D_{rec}^{PEEP3} (Post)$	-0.042	-0.090	-0.013	0.50	0.61	0.51
$D_{rec}^{PEEP0} (Post) - D_{rec}^{PEEP6} (Post)$	-0.065	-0.090	-0.041	0.60	0.95	0.38
$D_{rec}^{PEEP3} (Post) - D_{rec}^{PEEP6} (Post)$	-0.022	-0.005	-0.028	1.21	1.55	0.75

The numeric values for slope indicate the change in  $\beta$  from the left-hand to the right-hand derecruitability test listed under "Pairwise Comparison." The numeric values provided for the intercepts indicate the fold change in the raw (not log transformed) intercept  $\alpha$ . Gray cells indicate  $p < 0.05$ . Fifteen mice are in each group.

groups except at  $Paw = 2$  cmH<sub>2</sub>O where there is a striking decrease with VILI.

Figure 7 shows the pairwise relationships between the last elastance measurement in  $D_{rec}^{PEEP0}$ ,  $D_{rec}^{PEEP3}$ , and  $D_{rec}^{PEEP6}$  and  $N(alv)$  at  $Paw = 2, 5$ , and  $10$  cmH<sub>2</sub>O. Note that the mean pressure of the derecruitability tests is approximately 2–3 cmH<sub>2</sub>O greater than the onset pressures so that the mechanics and structure are measured at roughly the same pressure. Elastance is strongly

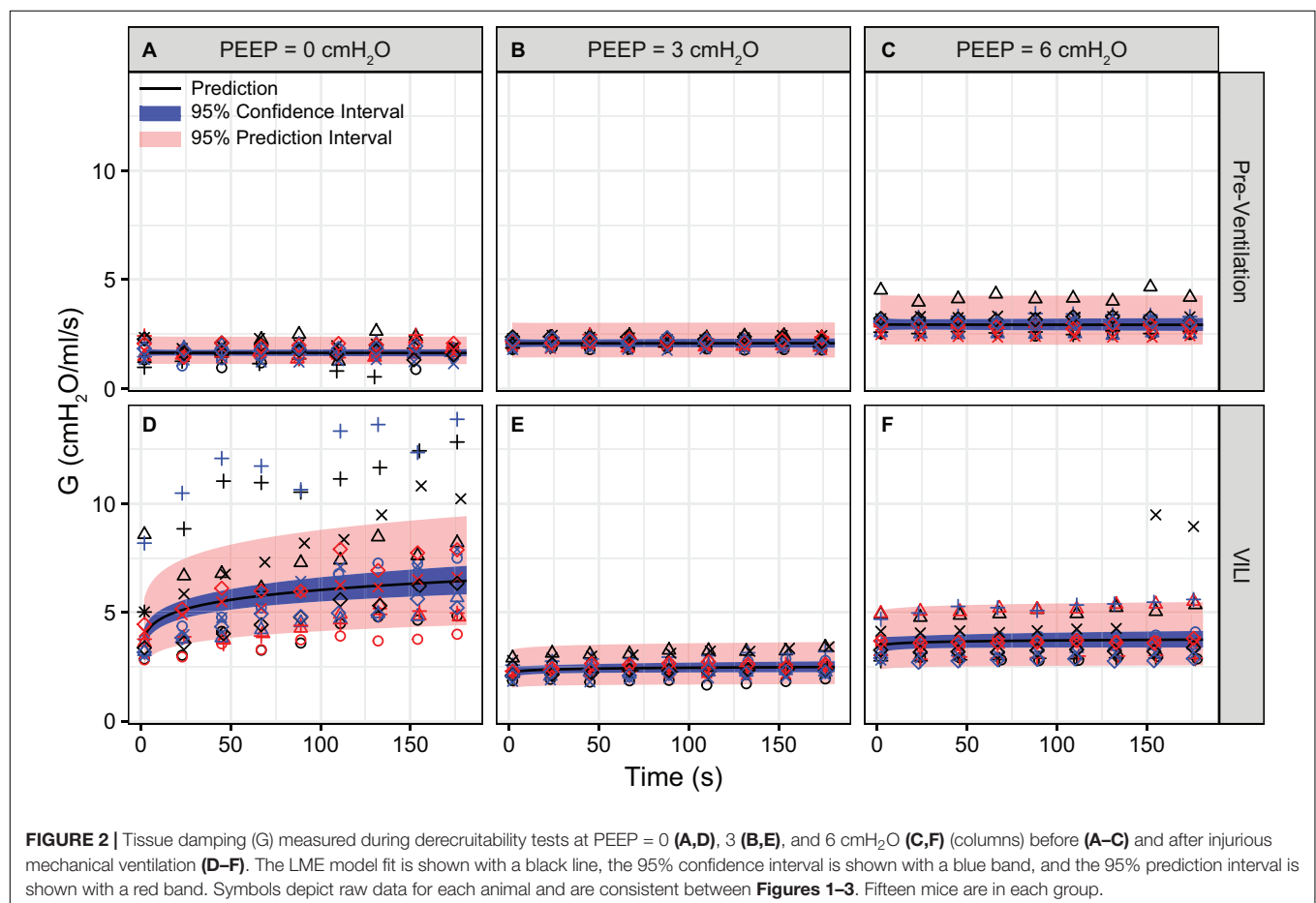
correlated with the number of patent alveoli ( $R^2 = 0.78$ ), and the form of the regression was selected based on our prior computational simulations where elastance increases with the inverse of the lung open fraction (Smith et al., 2013, 2015; Hamlington et al., 2016b; Mellenthin et al., 2019).

The changes in lung structure and function are accompanied by alterations in the pulmonary surfactant system. BALF total phospholipid (PL) content (Figure 8A) significantly increased

**TABLE 2 |** Results from regression analysis predicting log-transformed H, G, or Rn from derecruitability test PEEP ( $D_{rec}^{PEEP}$ ) with factors  $D_{rec}^{PEEP0}$ ,  $D_{rec}^{PEEP3}$ , and  $D_{rec}^{PEEP6}$ ; the log-transformed continuous time within the derecruitability test ( $t$ ); and an *Injury* factor describing if the measurements were recorded at the start of the experiment (pre-ventilation) or after ventilation to a doubling of pulmonary system elastance (VILI).

Predictor	H		G		Rn	
	Estimate (SE)	p-value	Estimate (SE)	p-value	Estimate (SE)	p-value
Intercept	3.083 (0.034)	<0.0001	0.500 (0.062)	<0.0001	-1.103 (0.057)	<0.0001
$t$	0.038 (0.006)	<0.0001	-0.002 (0.015)	0.8857	0.035 (0.009)	0.0002
$D_{rec}^{PEEP3}$	-0.386 (0.036)	<0.0001	0.228 (0.075)	0.0024	-0.499 (0.009)	<0.0001
$D_{rec}^{PEEP6}$	-0.229 (0.036)	<0.0001	0.580 (0.075)	<0.0001	-0.657 (0.047)	<0.0001
VILI	0.642 (0.036)	<0.0001	0.778 (0.075)	<0.0001	0.146 (0.047)	0.0021
$t \times D_{rec}^{PEEP3}$	-0.012 (0.008)	0.1529	0.002 (0.021)	0.8910	-0.016 (0.013)	0.2292
$t \times D_{rec}^{PEEP6}$	-0.014 (0.008)	0.1088	0.001 (0.021)	0.9627	-0.032 (0.013)	0.0138
$t \times VILI$	0.060 (0.008)	<0.0001	0.115 (0.021)	<0.0001	0.008 (0.013)	0.5550
$D_{rec}^{PEEP3} \times VILI$	-0.309 (0.051)	<0.0001	-0.710 (0.106)	<0.0001	-0.176 (0.067)	0.0089
$D_{rec}^{PEEP6} \times VILI$	-0.279 (0.051)	<0.0001	-0.623 (0.106)	<0.0001	-0.298 (0.067)	<0.0001
$t \times D_{rec}^{PEEP3} \times VILI$	-0.031 (0.012)	0.0100	-0.093 (0.030)	0.0015	0.002 (0.019)	0.9034
$t \times D_{rec}^{PEEP6} \times VILI$	-0.051 (0.012)	<0.0001	-0.097 (0.030)	0.0009	-0.009 (0.019)	0.6143

Fifteen mice are in each group.

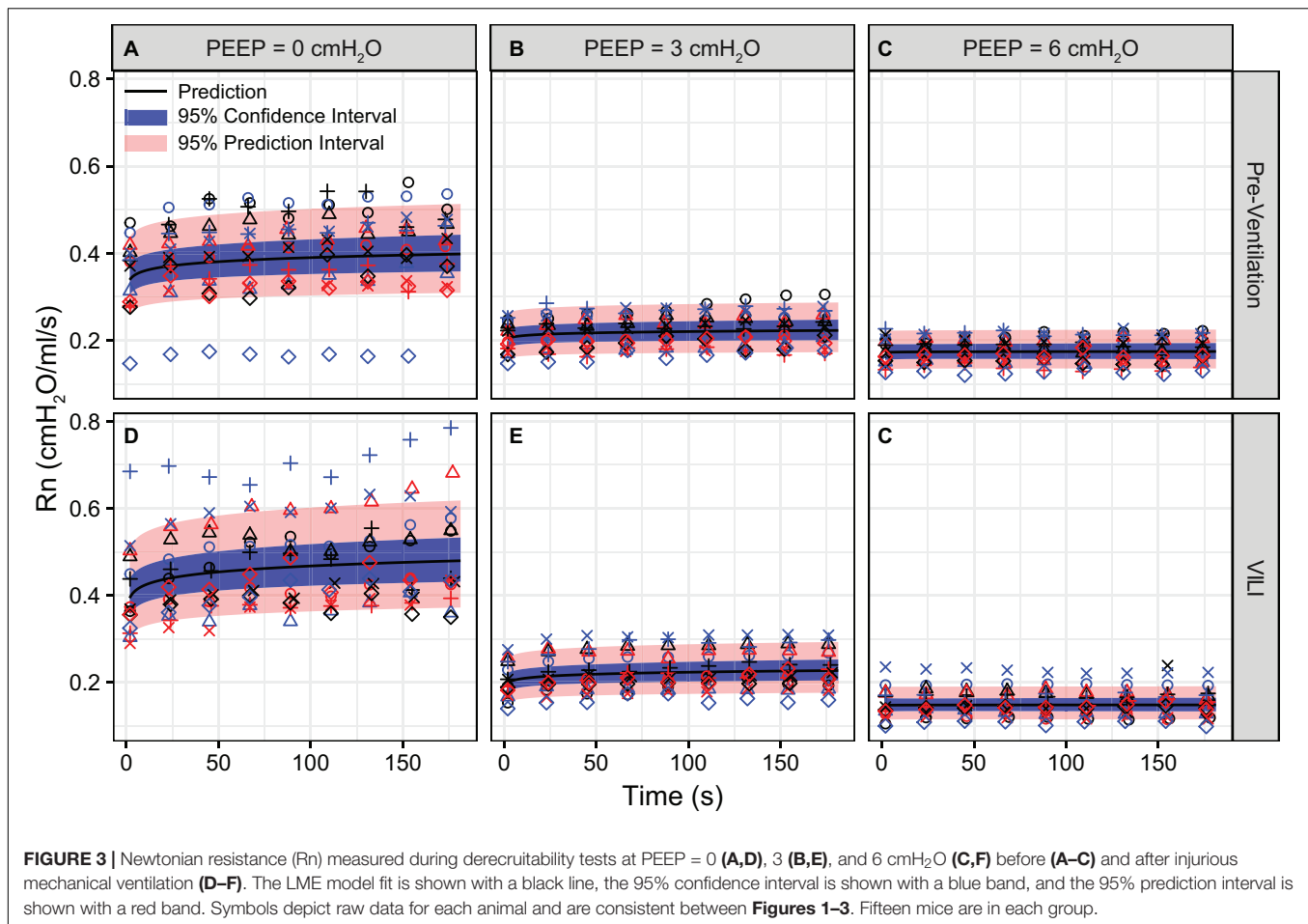


**FIGURE 2 |** Tissue damping (G) measured during derecruitability tests at PEEP = 0 (A,D), 3 (B,E), and 6 cmH<sub>2</sub>O (C,F) (columns) before (A–C) and after injurious mechanical ventilation (D–F). The LME model fit is shown with a black line, the 95% confidence interval is shown with a blue band, and the 95% prediction interval is shown with a red band. Symbols depict raw data for each animal and are consistent between **Figures 1–3**. Fifteen mice are in each group.

following high tidal volume ventilation due primarily to an increase in SA, which are less surface active. The increase in SA fraction also resulted in a striking and significant decrease in the LA/SA ratio (**Figure 8B**), a frequent marker of

surfactant degradation, turnover, and/or injury. The fraction of the most surface-active LA was unchanged after VILI, but the functional quality of the LA pellet was significantly disrupted as demonstrated by a marked increase in minimum surface tension





(**Figure 8D**), which translates *in vivo* to reduced surface tension lowering activity and reduced overall surfactant function. The airspace of the injured lung contained eightfold more protein (**Figure 8C**), which likely represents a combination of proteins released by the lung parenchyma and serum protein extravasation across a disrupted alveolocapillary barrier.

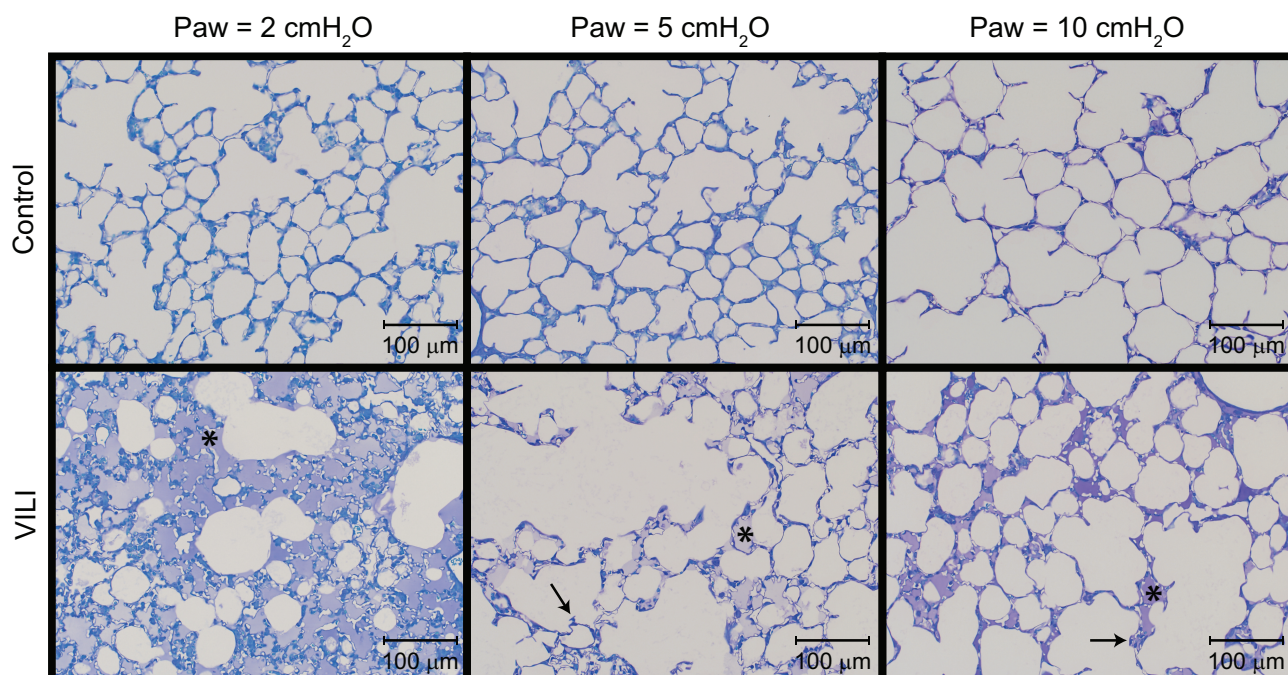
## DISCUSSION

The macroscale pressures and flows applied at the trachea during mechanical ventilation result in microscale parenchymal injury (Dreyfuss and Saumon, 1998). The resulting ingress of protein-rich edema into the parenchymal airspace causes changes in alveolar dynamics at the microscale that are then reflected in macroscale alterations in lung function (Hamlington et al., 2018b). Macro- to micro-scale interactions in VILI thus take place in both directions, which we investigated by correlating VILI-induced changes in mouse lung microstructure to changes in lung function. Understanding the link between structure and function at both micro and macro levels of scale is crucial for developing optimized mechanical ventilation strategies that interrupt the vicious cycle of surfactant degradation and inactivation (Agassandian and Mallampalli, 2013), mechanical

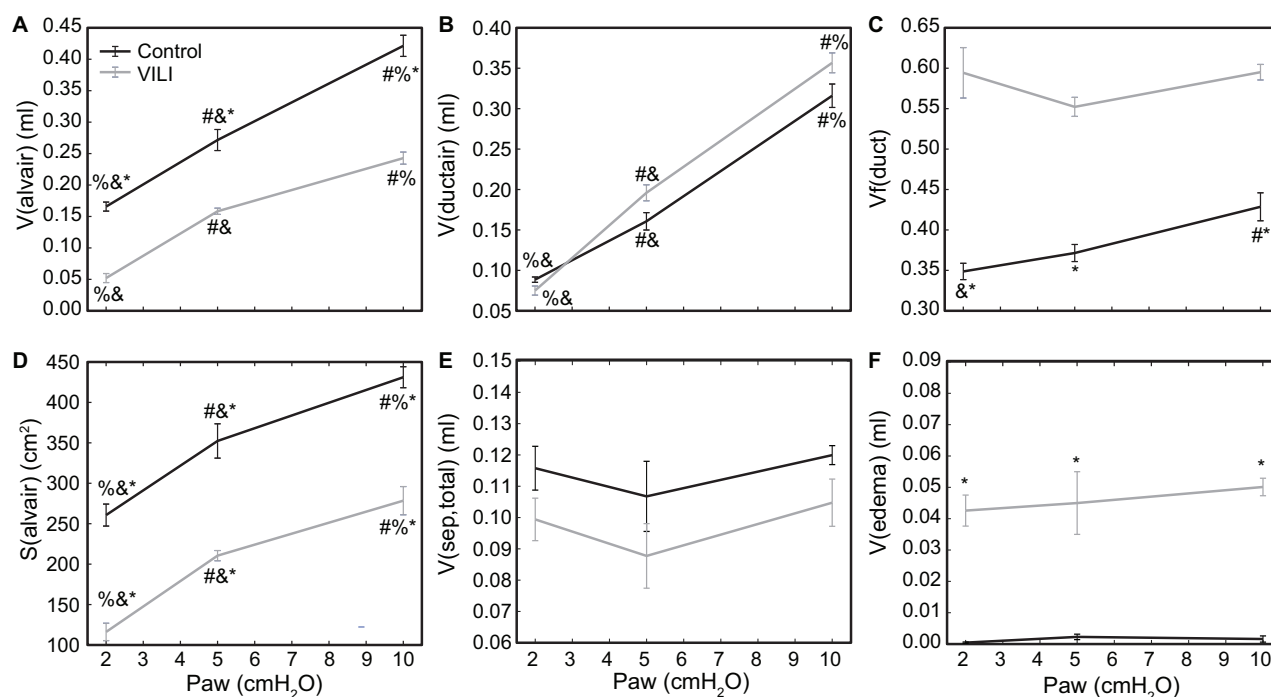
injury, inflammation, and altered lung function that drives VILI pathogenesis.

The most striking alterations in VILI-related organ-scale function are seen at low lung volumes (**Figure 1**, column 1), where we observe an approximately twofold increase in the first value of elastance measured at PEEP = 0 cmH<sub>2</sub>O immediately following an RM in VILI compared to controls (**Table 1**, intercept). This is attributable to the loss of roughly half the ventilated alveoli [ $N(\text{alv})$ , **Figure 6B**], due both to derecruitment that is reversible with an RM and the flooding of alveoli [ $N(\text{flood})$ , **Figure 6C**] that are not recruitable.  $H$  then continues to increase over the subsequent three minutes of  $D_{\text{rec}}^{\text{PEEP0}}$  at a rate that is greater in the injured lungs (**Table 1**, slope). Although we cannot assess time-dependent alveolar collapse in fixed tissue, our previous studies indicate that this increased rate of lung stiffening is a consequence of accelerated alveolar derecruitment (Smith et al., 2015) that we would ascribe, in the current study, to elevated minimum surface tension (**Figure 8D**).

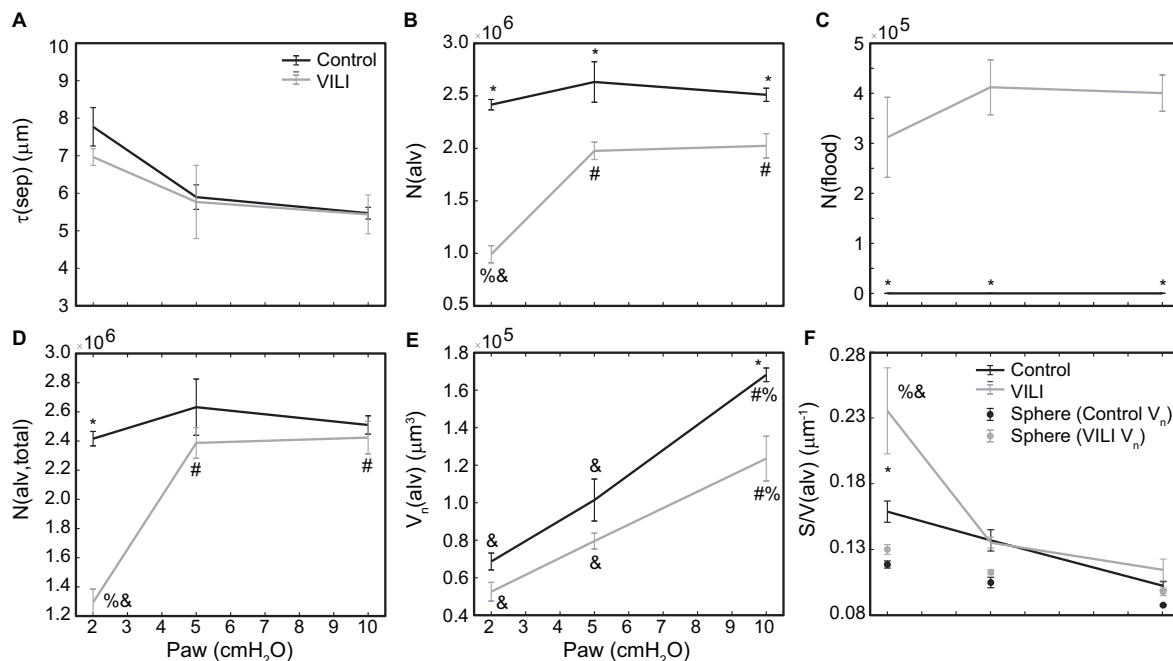
The PEEP = 3 and 6 cmH<sub>2</sub>O derecruitability tests also show progressive increases in  $H$ , although of substantially smaller magnitudes than at PEEP = 0 cmH<sub>2</sub>O (**Table 1**), no doubt because airway pressures remained above the derecruitment pressures of most of the unstable alveoli at the higher PEEP levels. This is borne out by our stereological analysis, which shows a decrease



**FIGURE 4 |** Representative micrographs for control (first row) and VILI (second row) mice that were perfusion fixed at an airway pressure  $Paw = 2$  cmH<sub>2</sub>O (first column),  $Paw = 5$  cmH<sub>2</sub>O (second column), and  $Paw = 10$  cmH<sub>2</sub>O (third column). Asterisk indicates alveolar edema and arrows denote retracted alveolar septa.



**FIGURE 5 |** Volume of air in the alveoli  $V(\text{alveir})$  (A), volume of air in the alveolar ducts  $V(\text{ductair})$  (B), volume fraction of parenchymal air in the alveolar ducts  $V_f(\text{duct})$  (C), gas-exchanging surface area  $S(\text{alveir})$  (D), total septal tissue volume  $V(\text{sep, total})$  (E), and alveolar edema volume  $V(\text{edema})$  (F) for the control (black lines) and VILI (gray lines) mice fixed at airway pressures  $Paw = 2, 5$ , and  $10$  cmH<sub>2</sub>O. Significant differences from  $Paw = 2$  cmH<sub>2</sub>O (#),  $Paw = 5$  cmH<sub>2</sub>O (%),  $Paw = 10$  cmH<sub>2</sub>O (&) in the same treatment group. Significant difference at the same airway pressure between treatment groups is shown with asterisks.  $n = 5$  for each point and the error bars show standard error.



**FIGURE 6 |** Average alveolar septal wall thickness (A), number of patent alveoli  $N(\text{alv})$  (B), number of flooded alveoli  $N(\text{flood})$  (C), total number of alveoli with discernable structure  $N(\text{alv,total}) = N(\text{alv}) + N(\text{flood})$  (D), and the number-weighted mean alveolar volume  $V_n(\text{alv})$  (E) for the control (black lines) and VILI (gray lines) mice fixed at airway pressures  $P_{aw} = 2, 5$ , and  $10$  cmH<sub>2</sub>O. Points plotted with the alveolar surface area to volume ratio  $S/V(\text{alv})$ , (F) depict the  $S/V$  for a sphere with volume  $V_n(\text{alv})$ . Significant differences from  $P_{aw} = 2$  cmH<sub>2</sub>O (#),  $P_{aw} = 5$  cmH<sub>2</sub>O (%),  $P_{aw} = 10$  cmH<sub>2</sub>O (&) in the same treatment group. Significant difference at the same airway pressure between treatment groups is shown with asterisks.  $n = 5$  for each point and the error bars show standard error.

in  $N(\text{alv})$  at the higher PEEP levels that is commensurate with the corresponding rates of increase in  $H$ . However, the total number of alveoli,  $N(\text{alv,total})$ , which includes both patent and flooded units, was unchanged in the VILI animals compared to controls at  $P_{aw} = 5$  and  $10$  cmH<sub>2</sub>O. This indicates that the increase in elastance in  $D_{rec}^{PEEP3}$  and  $D_{rec}^{PEEP6}$  is primarily due to the accumulation of flooded, non-recruitable alveoli rather than recruitment-resistant atelectasis or small airway closure. Figure 7 shows that the  $H$  values measured at the end of the derecruitability tests in all animals are inversely related to the fraction of patent alveoli (the “open fraction”), as we have previously postulated in our modeling studies of ventilator and acute lung injury in rodents (Smith et al., 2013, 2015; Hamlington et al., 2016b). This type of relationship was also observed during the acute phase of bleomycin injury in rats (Lutz et al., 2015; Knudsen et al., 2018) and lends strong support to the notion that the increases in lung stiffness seen in the acutely injured lung are largely reflective of loss of lung units through various derecruitment mechanisms. This has the important corollary that the dynamics of recruitment and derecruitment in the injured lung may be inferred directly from observed changes in  $H$ .

As expected, the loss of ventilated alveoli with VILI was accompanied by corresponding losses in  $V(\text{alvair})$  at all pressures (Figure 5A). Less expected was the reduction in  $V_n(\text{alv})$  (Figure 6E), because we previously observed mean alveolar volume to increase during the first 3 days of bleomycin injury in rats (Knudsen et al., 2018). Bleomycin-treated rats experience

similar changes in minimum surface tension (Lutz et al., 2015) to those we found in the present study, so the differences in alveolar volume behavior cannot be attributed to differences in surfactant function. On the other hand, there may have been differences in the way that alveoli became derecruited in the two models. Finite element simulations indicate that the degree of alveolar enlargement caused by tethering forces from adjacent derecruited regions of the lung is greater when the adjacent alveoli are collapsed as opposed to being merely flooded (Albert et al., 2019). The later stages of bleomycin injury are characterized by widespread alveolar collapse that is resistant to reopening even at high airway pressures (Knudsen et al., 2018), which may explain why the mean volume of open alveoli was increased in this model. In contrast, in the VILI model of the present study the collapsed alveoli could be reopened by an RM, and the alveoli remained patent down to  $P_{aw} = 5$  cmH<sub>2</sub>O, which would have reduced the tethering forces. Furthermore, at  $P_{aw} = 2$  cmH<sub>2</sub>O the VILI lungs were characterized by extensive areas of both flooded and collapsed alveoli interspersed with regions of normal-appearing alveoli, so that tethering-induced alveolar volume increases would be confined to the boundaries between the collapsed and open regions.

The surface area available for gas exchange (Figure 5D) followed the same trend as  $V(\text{alvair})$ , increasing with  $P_{aw}$  and decreasing with VILI. However, the mean surface area-to-volume ratio of an individual alveolus (Figure 6F) showed a striking increase with VILI at  $P_{aw} = 2$  cmH<sub>2</sub>O, indicating that the

TABLE 3 | Summarized stereological data from control and VILI lungs.

Paw cmH <sub>2</sub> O	V(alvair) ml	V(ductair) ml	V(edema) ml	V(sep,air) ml	V(sep,total) ml	S(alvair) cm <sup>2</sup>	τ (sep) μm	N(alv)	N(flood)	N(alv,total)	V <sub>n</sub> (alv) μm <sup>3</sup>
<b>Control</b>											
2	0.166% <sup>*,*</sup> (0.016)	0.089% <sup>*,*</sup> (0.007)	0.000* (0.000)	0.101* (0.019)	0.116 (0.016)	260.6% <sup>*,*</sup> (30.4)	7.8 (1.1)	2,416,000* (110,815)	0* (0)	2,416,000* (110,815)	68,660 <sup>Δ</sup> (10,074)
5	0.272% <sup>*,*</sup> (0.037)	0.161% <sup>*,*</sup> (0.024)	0.002* (0.002)	0.105* (0.025)	0.107 (0.025)	352.3% <sup>*,*</sup> (47.4)	5.9 (0.7)	2,632,000* (431,010)	0* (0)	2,632,000 (431,010)	101,420 <sup>Δ</sup> (25,039)
10	0.421% <sup>*,*</sup> (0.038)	0.316% <sup>*,*</sup> (0.032)	0.002* (0.002)	0.118* (0.008)	0.120 (0.007)	431.1% <sup>*,*</sup> (29.1)	5.5 (0.3)	2,510,000* (140,712)	0* (0)	2,510,000 (140,712)	168,200% <sup>*,*</sup> (8,106)
<b>VILI</b>											
2	0.052% <sup>*,*</sup> (0.016)	0.075% <sup>*,*</sup> (0.013)	0.043* (0.011)	0.040* (0.009)	0.099 (0.015)	116.1% <sup>*,*</sup> (24.0)	6.9 (0.5)	991,800% <sup>*,*</sup> (182,486)	312,020* (178,976)	1,294,000% <sup>*,*</sup> (202,745)	52,540 <sup>Δ</sup> (11,141)
5	0.158% <sup>*,*</sup> (0.011)	0.196% <sup>*,*</sup> (0.022)	0.045* (0.022)	0.062* (0.027)	0.088 (0.023)	210.5% <sup>*,*</sup> (14.1)	5.8 (2.2)	1,976,000% <sup>*,*</sup> (184,201)	412,200* (122,873)	2,386,800% <sup>*,*</sup> (235,812)	79,540 <sup>Δ</sup> (9,362)
10	0.243% <sup>*,*</sup> (0.022)	0.357% <sup>*,*</sup> (0.027)	0.050* (0.006)	0.075* (0.015)	0.105 (0.017)	278.4% <sup>*,*</sup> (39.0)	5.4 (1.2)	2,024,000% <sup>*,*</sup> (259,962)	400,400* (81,048)	2,423,400% <sup>*,*</sup> (247,958)	123,520% <sup>*,*</sup> (26,696)

Lungs were perfused at airway pressures Paw = 2, 5, and 10 cmH<sub>2</sub>O. Values are given as mean (standard deviation). Significant differences from Paw = 2 cmH<sub>2</sub>O (#), Paw = 5 cmH<sub>2</sub>O (%), Paw = 10 cmH<sub>2</sub>O (&) in the same treatment group. Significant difference at the same airway pressure between treatment groups is shown with asterisks. Each pressure in control and VILI includes n = 5 mice.

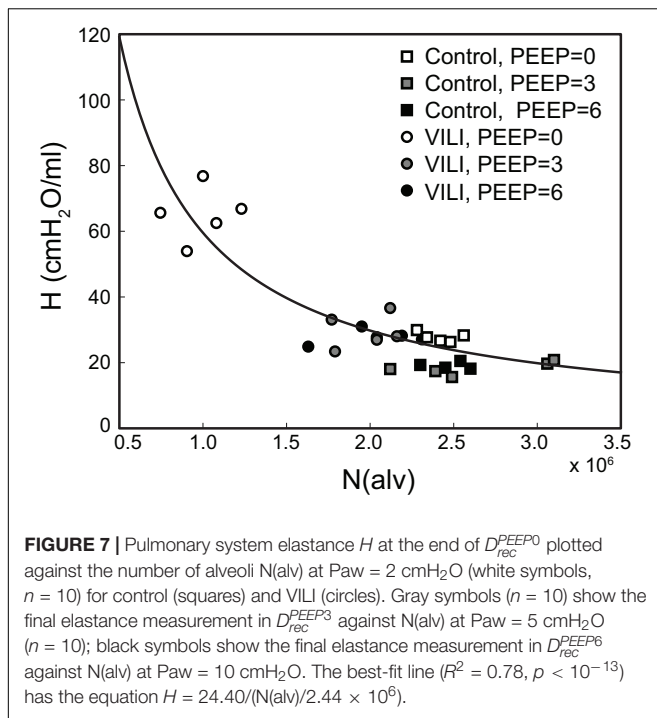
alveoli themselves had become less spherical and the alveolar septa possibly more convoluted. This is generally what one might expect in a deflating alveolus (Knudsen and Ochs, 2018), particularly if the alveolar walls become stiffer in VILI. Alveolar wall thickness was essentially unchanged by VILI (Figure 6A), however, so the stiffening was more likely due to increased surface tension.

The effect of alveolar stiffness on macro-scale mechanics was secondary to the loss of ventilated alveoli due to collapse and flooding (Figure 7). Our data indicate that the degradation of mechanical function with VILI follows the same path as in ARDS where different alveolar phenotypes have been postulated to define three distinct lung zones (Gattinoni et al., 1987): Zone D is comprised of damaged alveoli that cannot be recruited, corresponding to N(flood) in the current study. Zone R is comprised of unstable alveoli that are injured but recruitable, represented by the decrease in N(alv) between Paw = 5 and 2 cmH<sub>2</sub>O in VILI (Figure 6D). This represents an VILI-induced upward shift of the distribution of alveolar derecruitment pressures (i.e., alveolar instability) since there is no change in N(alv) between Paw = 5 and 2 cmH<sub>2</sub>O in the controls. Zone H comprises the remaining open alveoli (i.e., the “baby lung”) that remain aerated at low Paw. Our microscale analysis shows that the mechanics of these open alveoli are not entirely normal since V<sub>n</sub>(alv) and S/V(alv) are altered in VILI, but these alterations are secondary contributors to organ-scale mechanics when compared to the loss of ventilated alveoli. These three alveolar phenotypes have different dynamic behaviors that are reflected in the time- and pressure-dependence of H. It is important to note that while these three alveolar phenotypes are generally stable there may be variability between respiratory cycles. *In vivo* confocal microscopy shows that flooded alveoli are typically stable but may occasionally expel their edematous contents and become re-aerated (Wu et al., 2017). Likewise, nearby alveoli may alternately collapse on subsequent respiratory cycles (Broche et al., 2017) so that on subsequent breaths a single alveolus may either be collapsed or open.

The correlation between alveolar recruitment and elastance (Figure 7) may provide a mechanistic basis for identifying optimally lung-protective ventilation strategies. Figure 6 shows alveolar recruitment occurring between pressures of 2 and 5 cmH<sub>2</sub>O and, as such, H decreases as PEEP is increased from 0 to 3 cmH<sub>2</sub>O (Figure 1). By contrast, further increasing PEEP to 6 cmH<sub>2</sub>O causes a modest increase in elastance (and thus driving pressure) that is indicative of parenchymal overdistension. Taken together, these data suggest that the optimal PEEP based on lung elastance (or driving pressure) for these VILI mice lies between 3 and 6 cmH<sub>2</sub>O to recruit the recruitable alveoli (Zone R) without causing tissue overdistension by applying excessive PEEP in a futile attempt to recruit the Zone D alveoli that, in our VILI model, are flooded with edema.

Tissue damping is challenging to interpret through the lens of fixed tissue because it describes the viscous losses in the parenchyma that are, by definition, dynamic processes. The fractional changes in G during the derecruitability tests were, for the most part, rather similar to the corresponding fractional changes in H (Table 1), which is most readily interpreted as being



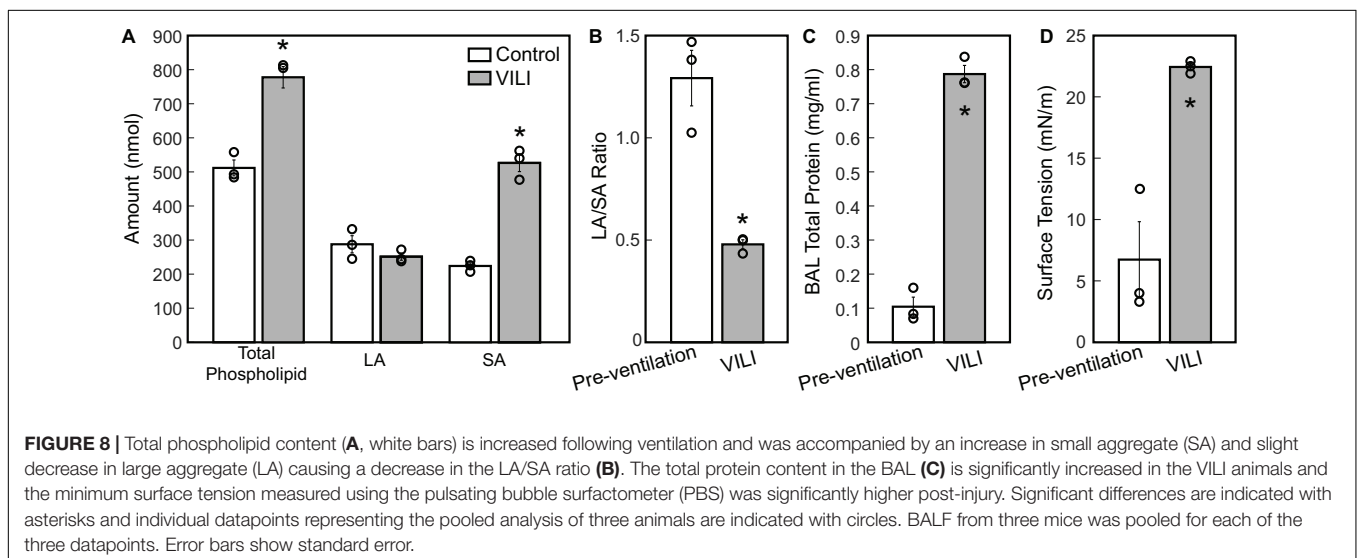


due simply to derecruitment of lung units, although it could also reflect an intrinsic coupling of the elastic and dissipative properties of lung parenchyma (Kaczka and Smallwood, 2012). Nevertheless, the largest alteration in  $G$  caused by VILI was an approximately twofold increase during  $D_{rec}^{PEEP0}$  (Figure 2D) that was slightly larger than the corresponding relative increase in  $H$  (Figure 1D). This may have been due to an increase in some form of dissipative process in the lung, such as intra-tidal recruitment (Kaczka et al., 2005, 2011), movement of fluid within and between partially flooded alveoli, or the folding and unfolding of septal pleats as suggested by an increased

$S/V(\text{alv})$ . In contrast, at  $PEEP = 3$  and  $6 \text{ cmH}_2\text{O}$  the VILI-induced changes in  $G$  were relatively less than those in  $H$ . This contrasts with findings in open-chest but otherwise healthy mice in which tissue hysteresivity =  $G/H$  remained constant with lung volume (Sly et al., 2003). Theoretical analysis, however, shows that reductions in hysteresivity can arise if ongoing recruitment and derecruitment of lung units occurs while lung impedance is being measured by the FOT (Bates and Allen, 2006), as might easily be the case in severely injured lungs.

The decrease in airway resistance with PEEP (Figure 3) is readily attributable to the increase in airway caliber caused by airway-parenchymal tethering forces. This mechanism may also explain the modest VILI-induced decrease in  $R_n$  during  $D_{rec}^{PEEP6}$ , since flooded alveoli near the airways would be unable to expand normally during lung inflation and thus would cause tethering-forces on the airway to be correspondingly increased. Similarly, reduced or compressive tethering forces in atelectatic regions might explain why  $R_n$  was increased after VILI during  $D_{rec}^{PEEP0}$ . However, these changes in  $R_n$  were relatively minor, and were even non-existent during  $D_{rec}^{PEEP3}$ , indicating that central airway structure was not substantially affected by injurious ventilation. Indeed, stereological analysis revealed only occasional edema in the airways, and we did not find any airways that were either partially buckled or fully collapsed.

The structural and functional changes detailed above are associated with changes to the alveolar fluid-mechanical microenvironment that oppose alveolar inflation and promote collapse. The increased volume of fluid (Figure 5F) in partially flooded alveoli decreases the interfacial radius of curvature, which increases the pressure differential across the air-liquid interface and causes the lining fluid to exert a greater inward force that facilitates collapse. Furthermore, the functionality of the surfactant system is compromised (Figure 8C) from an apparent increase in surfactant degradation (increased SA fraction and decreased LA/SA ratio) and inactivation of PLs in the LA aggregates. The degradation of surface-active LA (Yamada et al., 1990) into surface-inactive SA (Figure 8A) may be attributed to



large cyclic strains imposed by high-volume, PEEP = 0 cmH<sub>2</sub>O ventilation (Greenfield et al., 1964) that severely compresses the interfacial film so that it ruptures on re-expansion (Wyszogrodski et al., 1975). These mechanical effects can occur in the first 5 min of high tidal-volume ventilation (McClenahan and Urtnowski, 1967; Forrest, 1972). Therefore, in the present study, ventilation-induced surfactant degradation may have been the first step in the vicious cycle of altered alveolar dynamics, collapse, atelectrauma, and volutrauma that lead to eventually fatal VILI.

The mechanism for inactivation of the LA fraction is less clear and may very well be multifactorial. Airspace protein content is elevated (**Figure 8C**) due to alveolar surface damage (Dreyfuss et al., 1988; Hamlington et al., 2018b) and the resulting alveolocapillary leak (Hamlington et al., 2018a). Alveolar surface damage increases the BALF concentration of epithelial proteins such as E-cadherin while alveolocapillary leak accounts for the presence of serum proteins including albumin and immunoglobulin (IgG) in the BALF of mice ventilated under similar conditions (Smith et al., 2017). Our surface tension analysis includes the effects of BAL proteins that migrate with the PLs of the LA fraction during ultracentrifugation and inhibit surface lowering activity through disruption of phospholipid packing in the molecular films at the air-liquid interface. Furthermore, changes to the LA composition including phospholipids, surfactant-associate proteins or both may be present, and were not explored in these studies. Preliminary studies examining the presence of secretory phospholipases capable of targeting surfactant PLs revealed no significant changes in the BAL during this VILI model (data not shown) (Hite et al., 1998).

Our study has a number of limitations. First, the lungs were prepared for morphometric analysis with the chest wall retracted, which means that at high inflation pressures the lung volumes would have been greater than in closed-chest animals due to absence of constraint by the thorax. Conversely, at low inflation pressures the absence of the chest wall would have resulted in lower lung volumes due to the absence of the negative pleural pressure that opposes collapse. Based on lung volumes, airway pressures, and esophageal pressures measured in mice of equivalent age and weight to those used in the current study (Lai and Chou, 2000) we estimate that our morphometry data recorded at Paw = 2 cmH<sub>2</sub>O corresponds to Paw = 1.5 cmH<sub>2</sub>O in the intact mouse, an open-chested Paw = 10 cmH<sub>2</sub>O is equivalent to 12 cmH<sub>2</sub>O with the chest wall present, and at Paw = 5 cmH<sub>2</sub>O the contribution of the chest wall is approximately zero. In addition, our morphometry was conducted on fixed tissue sections and this limits the analysis to static conditions following a prolonged breath hold. As such, we are unable to offer any insights into the intra-breath alveolar and acinar dynamics, which could provide important insights into, for example, how the elastance of an individual alveolus is altered by VILI. Phase contrast synchrotron computed tomography offers a pathway to analyze alveolar dynamics in future studies (Chang et al., 2015; Morgan et al., 2020). Another limitation is that the high inspiratory pressures and zero PEEP used to generate VILI in the current study are far outside clinical guidelines for safe ventilation. Indeed, they were

specifically chosen to provide the volutrauma and atelectrauma necessary for VILI pathogenesis, while reducing the potential for deleterious metabolic effects occurring over long periods of ventilation (Wilson and Takata, 2019). Accordingly, our analysis is limited to the direct effects of VILI without the contribution of downstream inflammatory effects that take longer to manifest. Finally, the fact that our analysis was conducted in mice must be considered when applying our findings to ARDS and VILI in human subjects. Since the mouse lung is quite small, the effect of the gravitational gradient on lung structure and function is reduced in comparison to human subjects. Intrinsic structural differences are also present, including the pattern of branching which is monopodial (asymmetric) in mice and dichotomous (symmetric) in humans.

## CONCLUSION

Three alveolar phenotypes typically develop with VILI: (1) flooded alveoli that cannot be recruited at any pressure, (2) unstable alveoli that are open at high pressures but readily collapse as pressure is reduced, and (3) relatively normal alveoli that remain open at low pressures. The relative proportions of each phenotype can be estimated using derecruitability tests that quantify time-dependent alveolar derecruitment as a function of PEEP. These correlations between lung structure and function could provide insights into optimally lung-protective ventilation strategies.

## DATA AVAILABILITY STATEMENT

The datasets generated for this study are available on request to the corresponding author.

## ETHICS STATEMENT

The animal study was reviewed and approved by University of Vermont, Institutional Animal Care and Use Committee and the University of Colorado Denver Anschutz Medical Campus, Institutional Animal Care and Use Committee.

## AUTHOR CONTRIBUTIONS

BS, GR, KH, LK, MO, RH, and JB contributed to the conception and design of the study. BS, GR, AC, CM, KO, CC, and MN acquired the experimental data. BS, KH, RH, and JB analyzed and interpreted the data. BS drafted the manuscript. CM, KO, RH, and JB wrote sections of the manuscript. All authors contributed to the article and approved the submitted version.

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**Conflict of Interest:** The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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# Surfactant-Mediated Airway and Acinar Interactions in a Multi-Scale Model of a Healthy Lung

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We present a computational multi-scale model of an adult human lung that combines dynamic surfactant physicochemical interactions and parenchymal tethering between ~16 generations of airways and subtended acini. This model simulates the healthy lung by modeling nonlinear stress distributions from airway/alveolar interdependency. In concert with multi-component surfactant transport processes, this serves to stabilize highly compliant interacting structures. This computational model, with ~10 k degrees of freedom, demonstrates physiological processes in the normal lung such as multi-layer surfactant transport and pressure–volume hysteresis behavior. Furthermore, this model predicts non-equilibrium stress distributions due to compliance mismatches between airway and alveolar structures. This computational model provides a baseline for the exploration of multi-scale interactions of pathological conditions that can further our understanding of disease processes and guide the development of protective ventilation strategies for the treatment of acute respiratory distress syndrome (ARDS).

**Keywords:** biofluid mechanics, surfactant, multi-scale modeling, fluid–structure interactions, high-performance computing, acute respiratory distress syndrome

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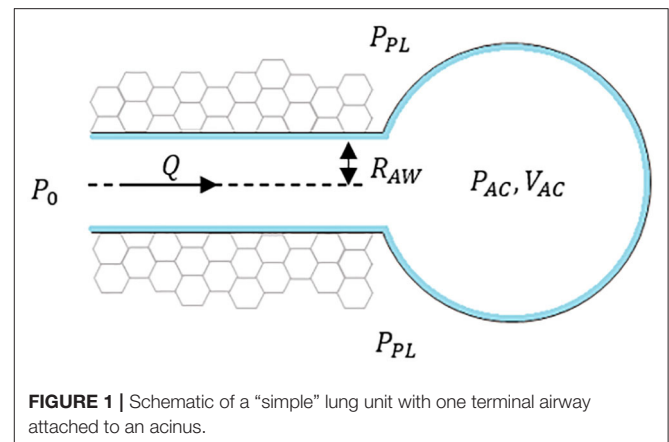
## INTRODUCTION

The lung is an extraordinary example of a physiological organ whose stability and function depends critically upon multiscale geometric interactions and processes that interlink tissue and biofluid mechanics. Airflow during inspiration and expiration changes the lung volume, causing the geometric change of highly compliant pulmonary tissues. During this volume change, tissue-level interactions like parenchymal tethering and molecular level interactions like surfactant re-distribution take place simultaneously in order to stabilize the lung. The lung's large surface area to volume ratio suggests the great importance of surfactant-mediated surface tension to lung stability. Meanwhile, the mechanical interdependency of lung units provides parenchymal tethering support for compliant airways that is instrumental to stabilizing the lung by maintaining adequate airflow to foam-like acinar structures that, in turn, support compliant airways. The large liquid-covered surface of the pulmonary tissue requires surfactant transport to dynamically modulate the surface tension during volume cycling in order to prevent fluid–structure instabilities, as it reduces the work of breathing (West, 1977, 2012; Notter, 2000). In this paper, we describe the development of a multi-scale model of a healthy lung from which future studies of pathophysiological systems can be explored.

The computational investigations of lung mechanics have been conducted on different scales. For example, at the organ level, our model is based upon an algorithm developed by Tawhai et al. who presented a computational method for generating the conducting airway network (Tawhai et al., 2000). At the tissue level, Lambert et al. (1982) and Fujioka et al. (2013) have developed computational models to describe the non-linear properties of the acinus and conductive airways, respectively. Micro-mechanical models of parenchyma support are based upon the recent work by Ryans et al. (2019), that is based on the foundational work of Wilson (1972), Lai-Fook et al. (1977, 1978), and Anafi and Wilson (2001). Surfactant transport properties are based on multilayer transport processes described by Krueger and Gaver (2000), which models surfactant behavior originally described by Clements (1957), Horn and Davis (1975), Smith and Stamenovic (1986), and Schurch (1995).

While these and many other studies have provided useful information and analysis about pulmonary mechanics on separate scales, the interactions between all of these interlinking processes have not been modeled directly. Ryans et al. demonstrated a reduced-dimension modeling approach for investigating the recruitment/de-recruitment of the airways without full fluid–structure interactions or surfactant transport processes (Ryans et al., 2016). Wall et al. (2010) developed a 3-D lung model with CT-based geometries up to a maximum of approximately seven generations, including not only airway wall deformability but also the influence of surrounding lung tissue. Filoche et al. (2015) presented a mathematical model of surfactant replacement therapy in a 3-D lung structure to investigate whether the instilled surfactant mixture actually reaches the adult alveoli/acinus in therapeutic amounts. Interlinking the multiscale processes is likely to introduce forcing and response characteristics that are not investigated in isolated models of isolated scales. For example, the multilayer surfactant behavior has heretofore been modeled in an oscillating bubble system with a pre-defined bubble radius. In contrast, in the pulmonary system the radius of airways and acini are driven by an oscillating pleural pressure on the surface of the lung. This, in turn, induces a heterogeneous distribution of mechanical stresses within the lung that dynamically modifies the lung sub-structure. In this process, the geometry of the airways and alveoli are modified, which induces surfactant transport that modulates the surface tension of the lining fluid on the internal structures of the airways and alveoli and, once again, modulates the tethering pressure and geometry of the system (Perun and Gaver, 1995). These feedback processes, when fully modeled, may elucidate pulmonary behavior that cannot be understood from the reductionist approach and may exhibit emergent behavior (Suki and Bates, 1985).

In this study, our goal is to build a computational model of an adult human lung that combines dynamic multi-scale interactions between ~16 generations of airways and subtended acini generated by a space filling algorithm, including airflow, multilayer surfactant transport and airway/alveolar interdependency. We explore this system under an oscillating pleural pressure that is applied to simulate the breathing of a healthy lung. Our goal is to develop this



model as a useful tool to understand the multi-scale lung mechanics and a critical baseline for the future study of the pathological conditions.

## MATERIALS AND METHODS

### Conceptual Formulation Framework

We have developed a rational engineering design approach for elucidating the surfactant physicochemical interactions and the mechanical interdependency within a healthy lung. It is assumed that under healthy conditions, the pleural pressure ( $P_{PL}$ ) is always negative and varies with time during the normal breathing cycle. The framework of this simulation approach is based upon three components:

- I. Tissue Components represent the series and parallel segments of airways and acini. The 3-D structure of airways and acini is determined using an anatomically based space-filling algorithm (Tawhai et al., 2000) in order to introduce inter-connections between airways and acini via parenchymal tethering, which is heterogeneously distributed.
- II. Air Components represent the volume of the air spaces, with temporal changes based upon the flow rate within each segment. Segmental flow rates are determined by regional pressure differences and the status of each of the compliant airways and acini as determined from the Tissue Component.
- III. Liquid Components represent the lining fluid and surfactant in the airways and acini, which dynamically modulate the surface tension. This, in turn, influences the Tissue Component stresses and thus affects flow rate.

### Interactions Among Components

To illustrate the concept of interactions among the three components, consider the presence of a terminal airway surrounded by parenchyma and connected to an acinus at one end as seen in **Figure 1**, where  $P_{PL}$  is the pleural pressure,  $P_{AC}$  is internal acinar pressure,  $R_{AW}$  is the radius of airway,  $Q$  is the

airflow toward the acinus. The pressure at the open end of the airway is considered a constant  $P_0$  to simplify this situation.

### I. Tissue Components

These are defined by airways and acini, shown in simplified form in **Figure 1**. The components are defined by

- Airways:** The dynamic radius of the airway is defined by the tube law (Lambert et al., 1982) as a function of the airway transmural pressure ( $P_{TM,AW}$ ), described conceptually as:

$$P_{TM,AW} = P_{int,AW} - P_{ext,AW}, \quad (1)$$

where  $P_{int,AW}$  represents the internal pressure from the internal air pressure and the Laplace pressure drop from surface tension, and thus is modulated by Air and Liquid Components.  $P_{ext,AW}$  represents the external stresses from the time-dependent pleural pressure ( $P_{PL}$ ) and is modulated by the parenchymal tethering using a shear modulus ( $G_{eff}$ ) representation of the acinar support as described in Ryans et al. (2019).

- Acinus:** Similarly, from Fujioka et al. (2013), the volume of acinus is a function of acinar transmural pressure

$$P_{TM,AC} = P_{int,AC} - P_{ext,AC}, \quad (2)$$

where  $P_{int,AC}$  represents the internal pressure from the acinus air pressure and the Laplace pressure drop from surface tension within alveoli that create the acinus, and  $P_{ext,AC} = P_{PL}$ .

In addition to structural coupling that exists through  $P_{int,AW}$  and tethering forces between the acini and the exterior of airways, internal coupling exists through internal pressures because  $P_{int,AC}$  is a function of the acinus volume. This sets  $P_{AC}$  as the end-condition of the Air Component system, which is necessary for determining the flow rates in the system, as described below.

### II. Air Components

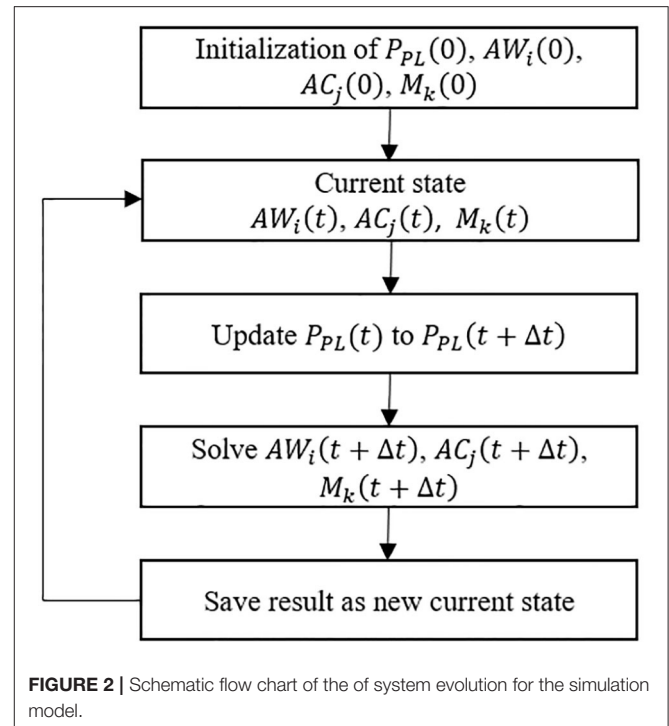
These are driven by airflow to and from airways and the subtending downstream acinus in the following manner:

- Airflow ( $Q$ ):** Determined by the pressure difference at the two ends of the airway ( $P_{AW}$ ), and the conductance ( $C$ ) of the airway,  $Q = CP_{AW}$ .
- Air Conductance ( $C$ ):** We simplify conductance as a function of the pressure-dependent airway radius, viscosity and length, following a Poiseuille relationship.
- Conservation of volume** dictates that the flow determines the change of volume of the downstream acinus ( $V_{AC}$ ).

As can be seen from the above descriptions, the Air Components create an internal coupling to the Tissue components through  $P_{int,AW}$  and  $P_{int,AC}$ .

### III. Liquid Components

These determine the distribution of fluid in the airways and alveoli. Two fundamental aspects are imposed:



**FIGURE 2** | Schematic flow chart of the of system evolution for the simulation model.

- Conservation of mass:** The volume of liquid is conserved within each airway and acinus. So, as an airway or acinus changes shape, the liquid film thickness changes accordingly.
- Surfactant physicochemical interactions:** Conservation of mass of surfactant is enforced. As the airway and alveolar surface areas change, this triggers multilayer surfactant transport (Krueger and Gaver, 2000). Through a surface tension equation of state, a dynamic surface tension exists and leads to a realistic full-lung pressure–volume loop.

As can be seen from these interactions, the liquid components directly influence  $P_{int,AW}$  and  $P_{int,AC}$  in Tissue Components.

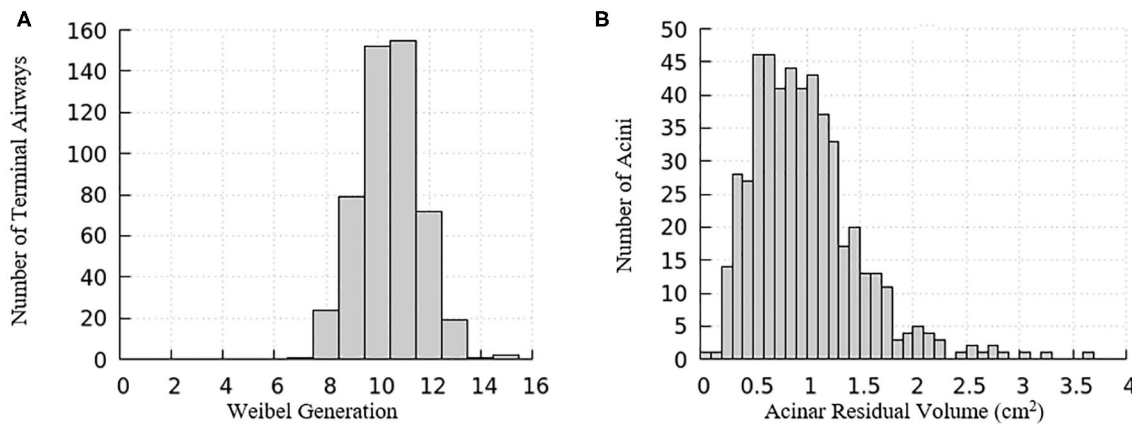
### System Evolution

The key to the modeling approach is the evolution of the system as each component interacts with each other. To evolve the system, the time-dependent pleural pressure  $P_{PL}(t)$  is prescribed and the rest of the system is updated with an adaptive time increment  $t$  from the current state. The new state after the time increment is solved by the method described in the Modeling Implementation section and the breathing cycle is tracked.

## Modeling Implementation

### Modeling Overview

To investigate surfactant-surface tension interactions and the mechanical interdependency within a healthy lung, the algorithm shown in **Figure 2** was used to simulate the whole lung respiration. Initially the time-dependent pleural pressure  $P_{PL}(t)$  is prescribed at the beginning of each time step. This provides the driving pressure for ventilation, as exists for normal respiration. We define the fundamental solution vectors for the airways, acini



**FIGURE 3 |** Distribution relationships for the computational model of a half-lung. **(A)** The Weibel generation of the terminal airways connecting to acinar regions, **(B)** the residual volume of the acini connecting to the terminal airways.

and surfactant as  $AW_i(t) = [P(t), R(t)]_i$ ,  $AC_j(t) = [P(t), V(t)]_j$ , and  $M_k(t) = [M_p(t), M_s(t), M_b(t)]_k$ , respectively, where  $P$  is airway/acinus pressure,  $R$  is airway radius,  $V$  is volume of acinus,  $M$  is a vector consists of the surfactant masses in each region of the multilayer structure, including  $M_p$  for the primary layer,  $M_s$  for the secondary layer,  $M_b$  for the bulk liquid. Each airway or acinus is represented by two solution vectors, one of which is  $AC_i(t)$  or  $AW_j(t)$  containing tissue component properties, and the other is  $M_k(t)$  containing liquid component properties.  $AC_i(t)$ ,  $AW_j(t)$  and  $M_k(t)$  are solved simultaneously based on the mechanical relationship described in Network Flow Dynamics using a differential-algebraic equation systems solver.

## Tissue Components

### I. Airway Morphology

The domain of one half of the lung is generated using an anatomically based space-filling algorithm from Tawhai et al. (2000). It consists of a network of airways that has up to an equivalent Horsfield 15th generation (bottom-up with terminal airway defined as generation 1) that terminate into acinar regions with mechanical properties described in the “Acinus Component” section (Fujioka et al., 2013). The equivalent Weibel generation (top-down from trachea as generation 0) of terminal airways and the residual volume of their attached acini are shown in **Figure 3**. We note that structural differences exist among airways and acini, which will appear as important contributors to the heterogeneity in surface tension and parenchymal tethering described in the “Results and Discussion” section.

Airways and acini are positioned in a 3-D space in order to build inter-connections between the airways and acini (Tawhai et al., 2000). The morphology of the pulmonary airways was based on Lambert et al. by providing the airway maximum radius ( $R_{AW,max}$ ) and normalized cross-sectional area  $\alpha$  at  $P_{TM,AW} = 0$ , i.e.,  $\alpha_0 = \frac{A_0}{A_{max}}$  (Lambert et al., 1982).

### II. Compliant Airway Components

We used the airway morphological data to construct a tube law that describes the radius of a compliant airway as a function of the airway transmural pressure. For a healthy lung, we assume

**TABLE 1 |** Generation-based constants used for the tube law used in Equation (3).

Generation ( $n$ )	$a$	$b$
1	0.0354	0.8486
2	0.0841	0.3504
3	0.0947	0.1004
4	0.0969	-0.0889
5	0.1115	-0.2347
6–15	0.1219	-0.3506

that the acinus is the most compliant region of the system, so that the parenchyma tethers the embedded airway open during inspiration, as described in the “Parenchymal Tethering” section, below. To do so, we defined a tube-law that follows a sigmoidal form that matches the airway-based morphological parameters. The general form of the tube-law is defined as

$$\frac{R_{AW}}{R_{AW,max}} = \sqrt{0.5 \times [1 + \operatorname{erf}(aP_{TM,AW} + b)]}, \quad (3)$$

where  $P_{TM,AW}$  is the transmural pressure defined in Equation (1),  $R_{AW,max}$  is the maximum radius of this airway. The parameters  $a$  and  $b$  are generation-based constants shown in **Table 1**. The tube law behavior through the Weibel 6th generation as well as experimental data for the first 3 generations are shown in **Figure 4** (Lambert et al., 1982).

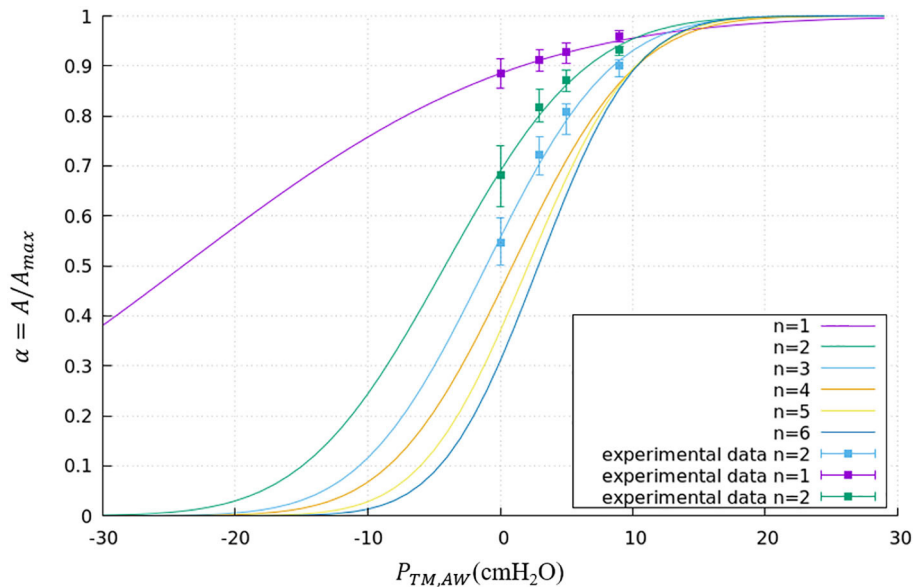
The internal airway pressure  $P_{int,AW}$  is subject to the airway pressure determined by the average of the upstream and downstream pressure as well as the Laplace pressure drop from the liquid lining of the airway. The Laplace pressure drop and airway pressure can be expressed respectively as

$$P_{int,AW} = P_{AW} - \frac{\gamma}{R_{in,AW}}, \text{ and} \quad (4)$$

$$P_{AW} = \frac{P_{DN} + P_{UP}}{2}, \quad (5)$$

where  $P_{AW}$  is the airway pressure,  $\gamma$  is the surface tension of the liquid lining,  $R_{in,AW}$  is the radius from the center line





**FIGURE 4 |** Tube law through the Weibel 6th generation. Airways smaller than the 6th generation are assumed to have the same tube law as the 6th generation. Experimental data is shown for the first 3 generations.

of the airway to the interior surface of the liquid lining,  $P_{DN}$  is the downstream pressure,  $P_{UP}$  is the upstream pressure. For the airway shape calculation, we assumed the pressure is uniform within an airway and determined the average pressure by Equation (5).

The external airway pressure  $P_{ext,AW}$  is subject to the pleural pressure and the parenchymal tethering from surrounding acini. We modeled tidal breathing by forcing the pleural pressure to be prescribed by a sinusoidally varying waveform with a 1:2 inspiration–expiration ratio that varies between  $-5$  cmH<sub>2</sub>O and  $-8.2$  cmH<sub>2</sub>O with a period of 5 s (Swan et al., 2012). The parenchymal tethering pressure is determined based on the work from Ryans et al. detailed in Parenchymal Tethering (Ryans et al., 2019). The peri airway pressure can be expressed as

$$P_{ext,AW} = P_{PL} + 2G_{eff} \left( \frac{\Delta R}{R} \right), \quad (6)$$

where  $P_{PL}$  is the pleural pressure,  $G_{eff}$  is the effective parenchyma shear modulus,  $\frac{\Delta R}{R}$  is the fractional radius change from the “hole” radius of parenchyma as described below in Equation (12). From Equations (4) to (6), Equation (1) can be rewritten as

$$P_{TM,AW}(t) = P_{AW} - 2G_{eff} \left( \frac{\Delta R}{R} \right) - P_{PL}(t) - \frac{\gamma}{R_{in,AW}(t)}, \quad (7)$$

where the transmural pressure varies with time due to the change in pleural pressure and radius change of compliant airways.

To determine the length of airways, it is assumed that the length change of airways is proportional to the size change of their surrounding parenchyma. The parenchyma model is described in Parenchymal Tethering.

### III. Acinus Component

The morphological information of the representative acinar regions connected to the terminal airways of the lung is based

on the octahedral models depicted in Fujioka et al. (2013). We represent the behavior of a block of alveoli ( $\sim 1,200$  alveoli representing  $\sim 1.7 \times 10^{-3}$  cc of tissue) by a pressure–volume relationship derived from simulation results of this block. We follow the form suggested by Venegas et al. (1985) that successfully models whole-lung mechanics. As such, the pressure–volume relationship of this model is governed by

$$\frac{V_{AC}}{V_{RV}} = a + \frac{b}{1 + \exp[-(P_{TM,AC} - c)/d]}, \quad (8)$$

where  $V_{AC}$  is the acinar volume,  $V_{RV}$  is the acinar volume at residual volume (RV),  $P_{TM,AC}$  is the acinar transmural pressure defined in Equation (2),  $a$ – $d$  are constants that describe the mechanical characteristics of the parenchyma. Since we add the dynamic surface tension to the Laplace pressure drop in our form of  $P_{TM,AC}$  in Equation (11), this structural component is based upon parameters describing the tissue behavior only (zero surface tension model) with  $a = 1.03$ ,  $b = 4.95$ ,  $c = 5.04$ ,  $d = 1.02$ .

The external and internal acinar pressure are

$$P_{ext,AC} = P_{PL}, \text{ and} \quad (9)$$

$$P_{int,AC} = P_{AC} - \frac{2\gamma}{R_{ALV}}, \quad (10)$$

where  $P_{AC}$  is the acinar pressure,  $P_{PL}$  is pleural pressure,  $\gamma$  is the surface tension of the liquid lining and  $R_{ALV}$  represents the mean radius of the interior surface of the alveolar lining fluid inside the acinus. At this stage, alveoli are assumed to be spherical. From Equations (9) and (10), Equation (2) can be rewritten as

$$P_{TM,AC} = P_{AC} - \frac{2\gamma}{R_{ALV}} - P_{PL}, \quad (11)$$

#### IV. Parenchymal Tethering

We utilized the parenchyma model from Ryans et al. (2019) to describe the tethering pressure. In that model, a cylindrical “hole” is surrounded by an annular region of parenchyma. An airway is laminated inside this parenchymal hole. Without the laminated airway, the equilibrium hole radius is defined as  $R_H$  so that when the strain in the annular parenchyma is uniform, this yields  $P_{ext,AW} = P_{PL}$ . For non-uniform strain, following Lai-Fook et al. (1978), we define the effective parenchyma shear modulus  $G_{eff}$  by

$$\frac{\Delta R}{R} = \frac{R_{AW} - R_H}{R_H} = \frac{P_{ext,AW} - P_{PL}}{2G_{eff}}, \quad (12)$$

where  $R_{AW}$  is the airway radius,  $P_{ext,AW}$  is the peri-airway pressure,  $P_{PL}$  is the pleural pressure. From analyses performed by Ryans et al. (2019), we assume the equilibrium hole radius is proportional to the cubic root of the weighted average of acinus volume within a distance of  $5R_{AW,0}$  from the airway axis, where  $R_{AW,0}$  is  $R_{AW}$  at zero transmural pressure. This behavior is consistent with the finite-element model by Ma et al. (2013). We also assumed the equilibrium hole radius  $R_{H,FRC}$  is equal to  $R_{AW,FRC}$  when the surrounding acinus volume is at the Functional Residual Capacity,  $V_{FRC}$ . Since the exact value of FRC is unknown before the simulation,  $R_{H,FRC}$  and  $R_{AW,FRC}$  are estimated from the isolated airway and acini model. We note that the equilibrium hole radius setpoint at FRC is an assumption that should be experimentally validated and is related to positive strain-deviation of terminal airways, as described in section Parenchymal Tethering and Strain Deviation.

From computational simulations as described from Ryans et al., the effective parenchyma shear modulus  $G_{eff}$  is empirically determined as a function of mean transpulmonary pressure (Ryans et al., 2019). The transpulmonary pressure and effective parenchyma shear modulus can be expressed as

$$\overline{P_{TP}} = \overline{P_{ALV}} - P_{PL}, \text{ and} \quad (13)$$

$$G_{eff} = Ae^{b\overline{P_{TP}}^3}, \quad (14)$$

where  $\overline{P_{TP}}$  is average transpulmonary pressure,  $\overline{P_{ALV}}$  is the weighted average of surrounding acinar pressures within a distance of  $5R_{AW,0}$  from the airway axis,  $A = 4.75 \text{ cmH}_2\text{O}$ ,  $B = 5.17 \times 10^{-4} \text{ cmH}_2\text{O}^{-3}$ .

#### Air Component

##### I. Air Conductance

We assume that all air flows are laminar and fully developed. Airflow throughout the lung model is described using a Poiseuille relationship at each airway. From Poiseuille's law, the conductance of a compliant airway is prescribed as a function of its radius and length:

$$C_{AW} = \frac{\pi R_{in,AW}^4}{8\mu L}, \quad (15)$$

where  $C_{AW}$  is the conductance of airway,  $R_{in,AW}$  is the radius from the center line of the airway to the interior surface of the liquid lining,  $\mu$  is the viscosity of air,  $L$  is the length of the airway. We acknowledge that this is inaccurate when Reynolds numbers are high, as in the central airways (trachea and mainstem bronchi) and first generations of the model of the lung. We also neglect the loss of pressure at bifurcations.

##### II. Network Flow Dynamics

In our model, the axial component of the pressure gradient inside each airway is assumed to be a constant. We also assume that all air flows through airways are fully developed and without turbulence. The flow rates at the airway level are determined by

$$Q_{AW,i} = C_{AW,i} (P_{UP,i} - P_{DN,i}), \quad (16)$$

where  $Q_{AW,i}$  is the flow rate of the airway,  $C_{AW,i}$  is the conductance of the airway,  $P_{UP,i}$  and  $P_{DN,i}$  are the upstream and downstream pressure of the airway, respectively.

At the terminal end of the system (acinus), the flow changes the acinus volume as

$$Q_{AW,i} = C_{AW,i} (P_{UP,i} - P_{AC,i}) = \frac{dV_{AC,i}}{dt}, \quad (17)$$

where  $P_{AC,i}$  is the acinus pressure,  $V_{AC,i}$  is the acinus volume.

We assume that there is no pressure loss at the bifurcations. Conservation of flow rate at each bifurcation is satisfied by an equation of the form

$$Q_{AW,P} + Q_{AW,D1} + Q_{AW,D2} = 0, \quad (18)$$

where  $P$  stands for the parent airway, and  $D$  stands for the daughter airways.

Equations (16)–(18) are applied to each acinus, airway and bifurcation to build the differential-algebraic equation system. We note that we neglect the loss of pressure at the airway bifurcation (Filоче et al., 2015).

#### Liquid Components

##### I. Conservation of Liquid Phase

We assume the amount of liquid is conserved within each airway/alveolus. Thus the liquid film thickness has to varies with time due to changes in radius of airway/alveolus. A parameter which characterizes this change is defined as

$$\varepsilon = \frac{R_{out} - R_{in}}{R_{out}}, \quad (19)$$

where  $R_{out}$  is the airway/alveolus radius,  $R_{in}$  is the radius from the center(line) to the liquid lining that determines the Laplace pressure drop. The change in the volume of the airways and alveolus therefore modulates the film thickness, which feeds back to the stress balance Equations (7) and (11). We note that the change of airway caliber as well as length is accounted for in the conservation of mass calculation for determining the dynamic film thickness.

## II. Surfactant Physicochemical Interactions

The mechanism of surfactant transport was based on the multilayer surfactant behavior analysis done by Krueger and Gaver (2000). Soluble surfactant in the liquid lining of airways/acini exists in the bulk fluid and two surface layers: primary and secondary layers. The primary layer is in direct contact with the air-liquid interface, while the secondary layer is created by collapse of the primary layer and resides between the primary layer and the bulk fluid. Adsorption/desorption can only happen between the bulk liquid and the primary layer. Only the surfactant in the primary layer can reduce the surface tension. The surface tension of water  $\gamma_0 = 72 \frac{\text{dyne}}{\text{cm}}$ . From Krueger and Gaver (2000), the equilibrium surface tension  $\gamma_\infty = 22 \frac{\text{dyne}}{\text{cm}}$  at the equilibrium surfactant concentration  $\Gamma_\infty = 3 \times 10^{-4} \frac{\text{mg}}{\text{cm}^2}$ . The minimum surface tension  $\gamma_{\min} = 4 \frac{\text{dyne}}{\text{cm}}$  occurs at the maximum surfactant concentration  $\Gamma_{\max} = 3.3 \times 10^{-4} \frac{\text{mg}}{\text{cm}^2}$ . We assumed the relationship between the primary layer surfactant concentration and surface tension is linear from  $(0, \gamma_0)$  to  $(\Gamma_\infty, \gamma_\infty)$  and from  $(\Gamma_\infty, \gamma_\infty)$  to  $(\Gamma_{\max}, \gamma_{\min})$  with a slope of  $m$  and  $m'$ , respectively. The surface tension equation of state can be expressed as

$$\gamma = \begin{cases} m\Gamma_1 + \gamma_0, & \text{if } \Gamma_1 < \Gamma_\infty \\ m'(\Gamma_1 - \Gamma_{\max}) + \gamma_{\min} & \text{if } \Gamma_1 \geq \Gamma_\infty \end{cases}, \quad (20)$$

where  $m = -1.7 \times 10^5 \frac{\text{dyne}}{\text{cm}} \cdot \frac{\text{cm}}{\text{mg}}$ ,  $m' = -5.3 \times 10^5 \frac{\text{dyne}}{\text{cm}} \cdot \frac{\text{cm}}{\text{mg}}$ . **Figure 5** demonstrates an example hysteresis

mass to the secondary layer ( $\Gamma_2$ ). At the bottom right corner, the primary layer concentration reaches  $\Gamma_{\max}$ . The speed of collapse increases by an order of magnitude when  $\Gamma_1 > \Gamma_{\max}$ . Therefore  $\Gamma_1 \sim \Gamma_{\max}$  as the contraction continues, highly enriching the secondary layer. At the bottom left corner, the alveolar unit starts to expand. The surface tension increases during this expansion due to the decreasing concentration of the primary layer. When the concentration of the primary layer begins to fall below  $\Gamma_\infty$ , respreading starts from the secondary layer to the primary layer, and surfactant molecules are once again adsorbed from the bulk. This hysteresis loop is a key characteristic relating surfactant physicochemical behavior to the stabilizing properties associated with dynamic surface tension in the healthy lung (Notter, 2000).

The governing equations of the surfactant transport are

$$\begin{aligned} \frac{dM_1}{dt} &= (-j_c + j_r + j_a - j_d) A \\ \frac{dM_2}{dt} &= (j_c - j_r) A, \\ \frac{dM_b}{dt} &= (-j_a + j_d) A \end{aligned} \quad (21)$$

where  $M_1$  is the surfactant mass in the primary layer,  $M_2$  is the surfactant mass in the secondary layer,  $M_b$  is the surfactant mass in the bulk liquid,  $A$  is the surface area of the air-liquid interface,  $j$  terms represent the transport between bulk and surface layers. Terms for collapse and respreading are defined as

$$j_c = \begin{cases} C_{\text{collapse}} \frac{\Gamma_1^2}{\Gamma_1^2 + \Gamma_{\max}^2} \max\left(\frac{\Gamma_1 - \Gamma_\infty}{\Gamma_\infty}, 0\right), & \text{if } \Gamma_\infty < \Gamma_1 < \Gamma_{\max} \\ \exp\left[1000 \cdot \left(\frac{\Gamma_1}{\Gamma_{\max}} - 1\right)\right] \cdot C_{\text{collapse}} \frac{\Gamma_1^2}{\Gamma_1^2 + \Gamma_{\max}^2} \max\left(\frac{\Gamma_1 - \Gamma_\infty}{\Gamma_\infty}, 0\right), & \text{if } \Gamma_1 > \Gamma_{\max} \end{cases}, \text{ and} \quad (22)$$

$$j_r = C_{\text{respread}} \frac{\Gamma_2^2}{\Gamma_1^2 + \Gamma_{\text{mls}}^2} \max\left(\frac{\Gamma_\infty - \Gamma_1}{\Gamma_\infty}, 0\right) \frac{\Gamma_2}{\Gamma_\infty}, \quad (23)$$

behavior of alveolar unit as determined from Equations (21) to (25) below.

In **Figure 5**,  $\Gamma_{\max} = 4.2 \times 10^{-4} \frac{\text{mg}}{\text{cm}^2}$  is the maximum surfactant concentration,  $\gamma_{\min} = 2 \frac{\text{dyne}}{\text{cm}}$  is the surface tension when  $\Gamma_1 = \Gamma_{\max}$ ,  $\Gamma_\infty = 3 \times 10^{-4} \frac{\text{mg}}{\text{cm}^2}$  is the surfactant concentration at equilibrium state,  $\gamma_\infty = 22 \frac{\text{dyne}}{\text{cm}}$  is the surface tension when  $\Gamma_1 = \Gamma_\infty$ .

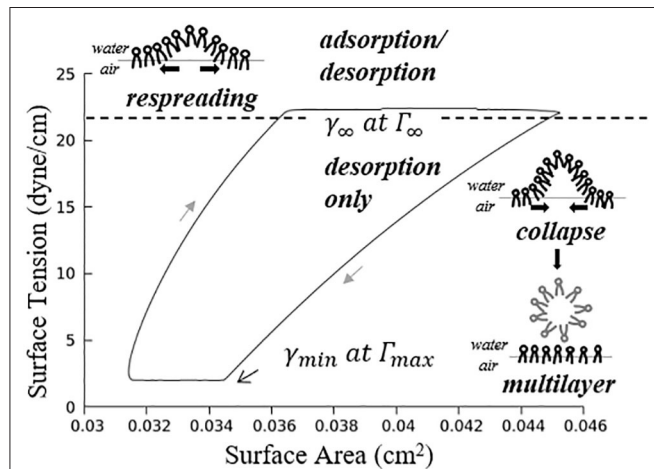
As described by **Figure 5**, the alveolar unit starts contracting from the maximum volume point (top right corner). During the contraction, the surface tension decreases as the monolayer surfactant concentration increases with simultaneous adsorption/desorption occurring between the surface and bulk phases. When the monolayer surfactant concentration exceeds  $\Gamma_\infty$ , the adsorption from the bulk stops. At this time, the monolayer cannot sustain further compression without collapsing to create a multi-layer with surfactant molecules exuded from the primary to the secondary layer as the alveolar unit continues contracting. Desorption between the primary layer and bulk fluid continues as  $\Gamma_1$  exceeds  $\Gamma_\infty$  and simultaneously the primary layer ( $\Gamma_1$ ) collapses to transport

where  $\Gamma_1$  is the primary layer surfactant concentration,  $\Gamma_2$  is the secondary layer concentration,  $C_{\text{collapse}} = 2 \times 10^{-4} \left(\frac{\text{mg}}{\text{s} \cdot \text{cm}^2}\right)$ ,  $C_{\text{respread}} = 5 \times 10^{-2} \left(\frac{\text{mg}}{\text{s} \cdot \text{cm}^2}\right)$ ,  $\Gamma_{\text{mls}} = 2.34 \frac{\text{mg}}{\text{cm}^2}$  is the multilayer respreading concentration (corresponds to  $\gamma_{\text{mls}} = 33 \frac{\text{dyne}}{\text{cm}}$ ),  $\max\left(\frac{\Gamma_1 - \Gamma_\infty}{\Gamma_\infty}, 0\right) / \max\left(\frac{\Gamma_\infty - \Gamma_1}{\Gamma_\infty}, 0\right)$  serve as a switch to turn on the collapse/respreading when  $\Gamma_1$  is above/below  $\Gamma_\infty$ , and describes the relationship between concentration and speed of transport together with the sigmoidal function  $\frac{\Gamma_1^2}{\Gamma_1^2 + \Gamma_{\max}^2}$  and  $\frac{\Gamma_2^2}{\Gamma_2^2 + \Gamma_{\text{mls}}^2}$ . The collapse term increases exponentially when  $\Gamma_1$  is greater than  $\Gamma_{\max}$  based on the experimental evidence (Clements, 1957; Horn and Davis, 1975; Schurch, 1995; Krueger and Gaver, 2000). Note that we have modified the collapse and respreading terms from that originally introduced by Krueger and Gaver (2000) in order to stabilize the computations. In the present model we assume that collapse can be initiated (albeit slowly) as soon as the primary layer concentration exceeds  $\Gamma_\infty$ , and this collapse rate increases substantially as  $\Gamma_1$  increases to  $\Gamma_{\max}$ . Likewise, respreading initiates when the primary layer concentration falls below  $\Gamma_\infty$ , and the respreading rate increases substantially near  $\Gamma_{\text{mls}}$ .

Terms for adsorption and desorption are defined as

$$j_a = \begin{cases} K_a c_{bulk} (\Gamma_\infty - \Gamma_1) \left(1 - \frac{\Gamma_1}{\Gamma_\infty}\right), & \text{when } \Gamma_1 < \Gamma_\infty, \text{ and} \\ 0, & \text{otherwise} \end{cases} \quad (24)$$

$$j_d = K_d \Gamma_1 \left(1 - \frac{\Gamma_1}{\Gamma_\infty}\right), \quad (25)$$



**FIGURE 5 |** Example hysteresis loop of an alveolus.  $\Gamma_1$  is inversely proportional to the interfacial area. The primary layer begins to collapse when  $\Gamma_1 \geq \Gamma_\infty$ , forming a secondary layer between the bulk and primary layer. When  $\Gamma_1 < \Gamma_\infty$ , the secondary layer dynamically respreads, which stabilizes the surface tension.

where  $c_{bulk}$  is the bulk concentration,  $K_a = 1.7(\frac{cm^3}{mg \cdot s})$ ,  $K_d = 1.7 \times 10^{-2}(\frac{1}{s})$ ,  $(1 - \frac{\Gamma_1}{\Gamma_\infty}) A$  is the effective surface area.

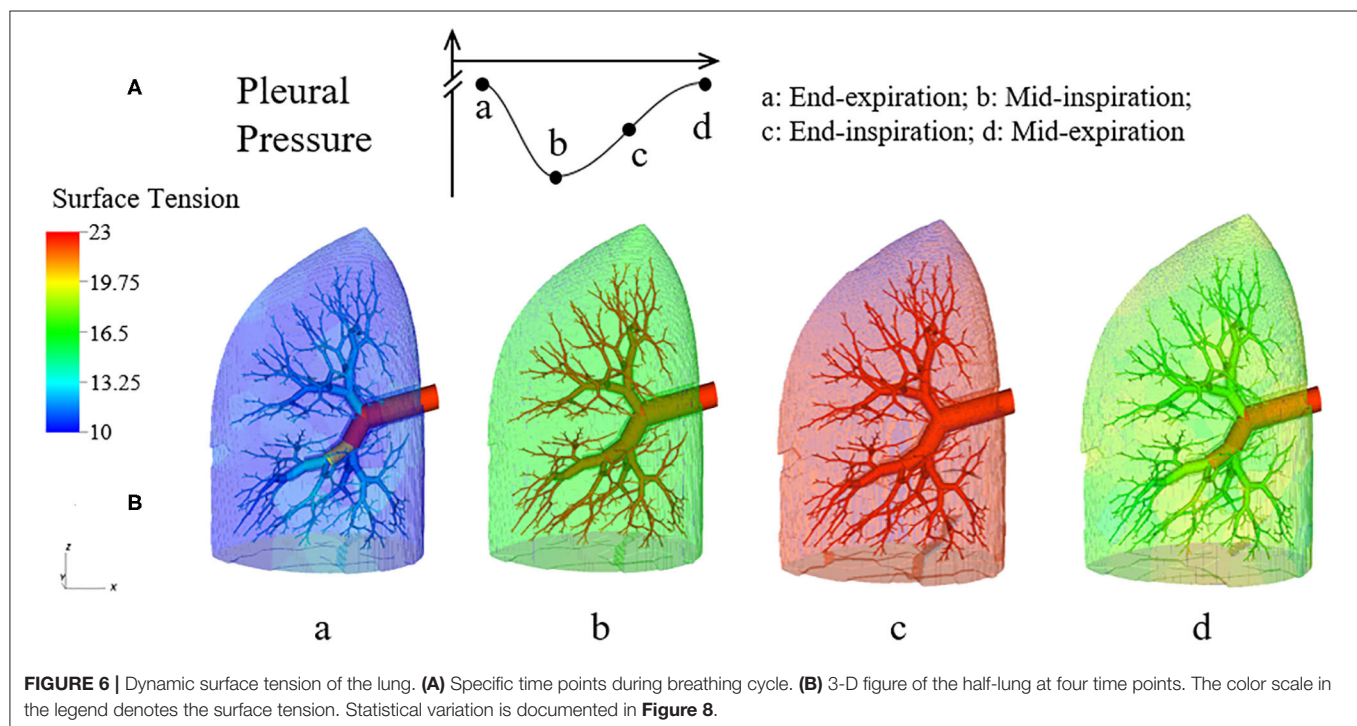
## Computational Methods

High-performance computing simulations were conducted on Tulane's Cypress supercomputer. The code was constructed in C++ and utilized MPI library. The differential-algebraic equation systems solver used in the code was SUNDIALS IDAS solver with adaptive time stepping (Hindmarsh et al., 2005). The simulation utilizes 8 Intel Xeon E5-2680 v2 CPUs and 128 GB of RAM. Total CPU time for one simulation (180 s of breathing) is  $\sim 5$  h.

## RESULTS AND DISCUSSION

### Overview

In this study, pleural pressure forcing was assumed to be periodic with  $-5 \leq P_{PL} \leq -8.2$  cmH<sub>2</sub>O and a frequency of 12 min<sup>-1</sup> to simulate tidal breathing (Swan et al., 2012). The inhalation–exhalation time ratio is assumed to be 1:2. As an initial condition, the dimensionless liquid film thickness  $\varepsilon$ , and the total amount of surfactant,  $M_{total} = M_1 + M_2 + M_b$  were prescribed at each airway as well as each acinus when the lung is at its residual volume (RV). In this study, we assumed the minimum alveolar radius equals 100  $\mu m$ , and the alveolar liquid film thickness equals 0.1  $\mu m$  at residual lung volume (Bastacky et al., 1985), so  $\varepsilon = 1 \times 10^{-3}$  at RV in the acinus components. For airway components, the initial  $\varepsilon$  is assumed to be 0.02 (Cassidy et al., 1985). We initially apply a uniform bulk surfactant concentration  $c_{airway} = 6 \frac{mg}{ml}$  for airway components, and  $c_{alveolus} = 35 \frac{mg}{ml}$  for acinar components. During initialization, the equilibrium



**FIGURE 6 |** Dynamic surface tension of the lung. **(A)** Specific time points during breathing cycle. **(B)** 3-D figure of the half-lung at four time points. The color scale in the legend denotes the surface tension. Statistical variation is documented in Figure 8.



surface concentrations are determined according to the defined bulk concentration and the physicochemical description above. True surfactant concentration values in the healthy lung are not known, but  $c_{alveolus}$  equals the concentration of the exogenous surfactant Infasurf (ONY, Inc; Amherst, NY).

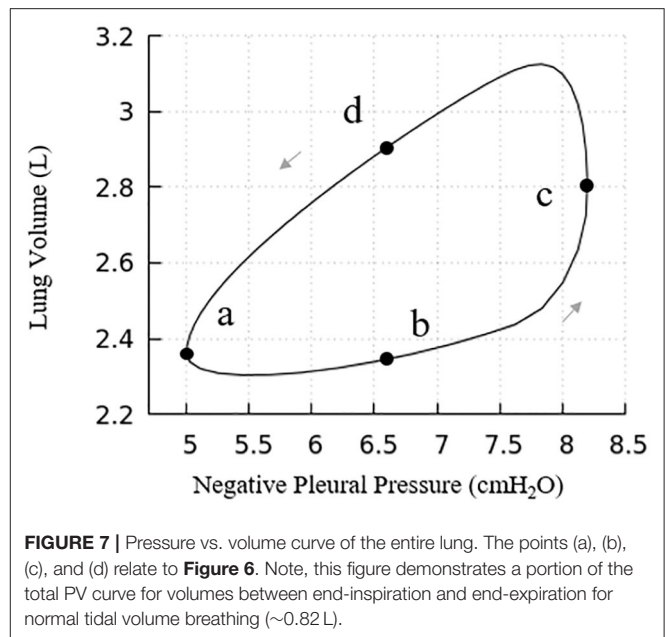
During the simulation, states of each component are recorded to track the evolution of the system. For visualization, a 3-D figure of the half-lung was generated. This figure reflects the space distribution of each airway and acinus as well as their real-time states. Our simulation was performed for several breathing cycles until stationary states were achieved.

**Figure 6** demonstrates the changes of surface tension in the lung (consisting of airways and acini) at four different time points (a–d) during a breathing cycle. Starting with end-exhalation (a), the surface tension in acini and small airways is as small as 8 dynes/cm, which is far below the equilibrium surface tension (22 dynes/cm) and can be achieved only due to the dynamic transport of surfactant. This low surface tension occurs because the air-liquid interface in each component contracts, increasing the primary layer interfacial surfactant concentration, and decreasing the surface tension (as surfactant also loads the secondary layer). As the lung volume increases during inspiration (b), the surface tension increases, implying a decrease of primary layer surfactant concentration. At the end of inspiration (c), the surface tension attains close to a maximum value in both acini and airways. During expiration (d), the volume of the lung decreases and thus the inner surface area of acini and airways are decreased, reducing the surface tension.

We note that at points a and c, the lung volumes and surface tensions are not respectively the minimum and maximum due to the airway network resistance and the Laplace pressure drop explained in the Pressure–Volume Curve section. Likewise, the lung volumes as well as the surface tensions at points b and d are not identical, even though these represent identical  $P_{PL}$  values. The differentials in lung volume and surface tension are related to the phase-lag that occurs in the system, described below.

## Pressure–Volume Behavior

The pressure-volume behavior described here reflects both lungs, that is twice the size of our computational domain. Our lung model has a full lung residual volume (RV) of 1.0 L. Assuming homogeneous acinar behavior, following Equation (8) the total lung capacity (TLC) is 6.0 L. The dynamic properties of the lung are determined by pressure cycling and **Figure 7** presents the pressure-volume (PV) relationship for the entire lung. Under the given pleural pressure range investigated for normal breathing, the tidal volume (TV) equals 0.82 L, with a functional residual capacity (FRC) of  $\sim 2.30$  L. From these simulations of normal breathing, the maximum flow rate at the trachea is  $\sim 0.92$  L/s. The average compliance of the lung during tidal breathing is  $\sim 0.25$  L/cmH<sub>2</sub>O, while the accepted normal value is 0.2 L/cmH<sub>2</sub>O in human lungs (Harris, 2005). TV and compliance of our model is higher than the normal values because the simulated airway resistance is unrealistically low due to the assumptions of laminar, fully developed flow in “Modeling Implementation” as described in “Limitations”. The total airway resistance excluding upper airways ranges from 0.6 to 0.9 cmH<sub>2</sub>O/L/s with lung volume



oscillating between 2.30 L (38% of TLC) and 3.12 L (52% of TLC), which is less than the predicted flow resistance at low equivalent lung volumes predicted by Pedley et al. (1970).

Our model presents a typical PV hysteresis behavior, i.e., the compliance of the lung ( $\Delta \text{volume}/\text{pressure}$ ) is different between the inspiration and expiration phase. The PV phase lag that is demonstrated in **Figure 6** is evident from points a–d in **Figure 7**.

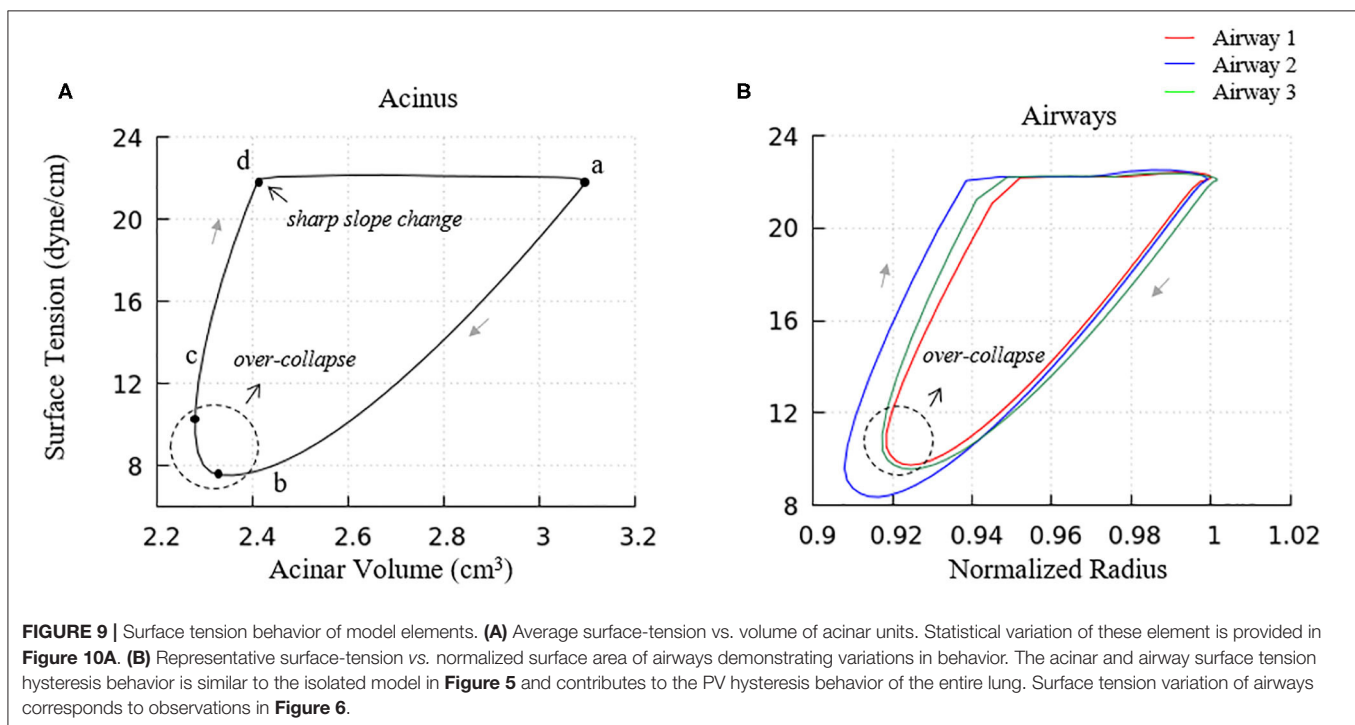
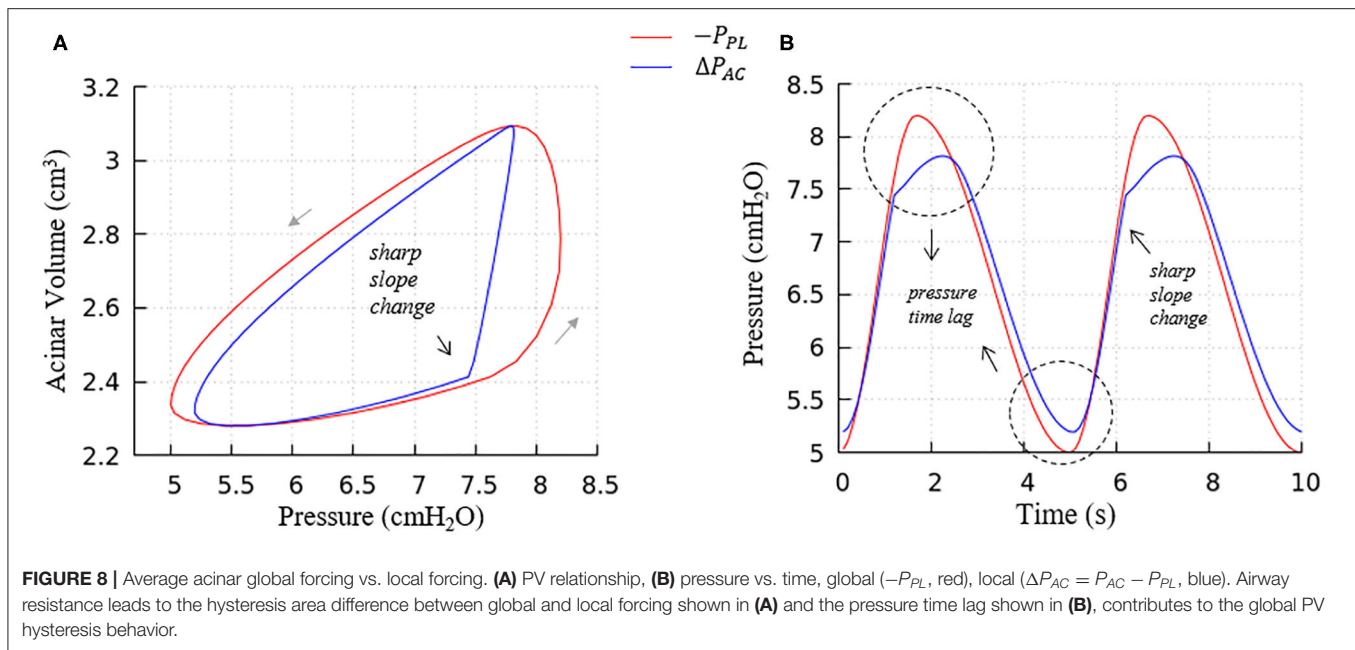
**Figure 8** further elucidates the acinar contributions to PV hysteresis behavior—here we present the behavior in terms of local forcing ( $\Delta P_{AC} = P_{AC} - P_{PL}$ , represented by the blue curve), and global forcing ( $P_{PL}$ , represented by the red curve). The global forcing demonstrates a rounded behavior similar to the full lung in **Figure 7**. However, the behavior of a specific acinus is best understood from the local forcing,  $\Delta P_{AC}$ .

This analysis demonstrates that the hysteretic behavior is reflected by two factors:

- The flow resistance of airways. As seen in **Figure 8A**, the hysteresis area of the  $\Delta P_{AC}V$  curve is much smaller than  $P_{PL}V$ , which results from the network airflow resistance. The time lag between the global and local pressure changes caused by the airway network resistance can be observed in **Figure 8B**, and causes the lung volume to lag the changes in  $P_{PL}$ , as demonstrated by **Figure 6**.
- The Laplace pressure drop. The hysteresis area of the local PV curve ( $\Delta P_{AC}$ , represented by the blue curve) results from the behavior of surfactant transport as shown in **Figure 5**, as described in the next section.

## Surfactant Transport

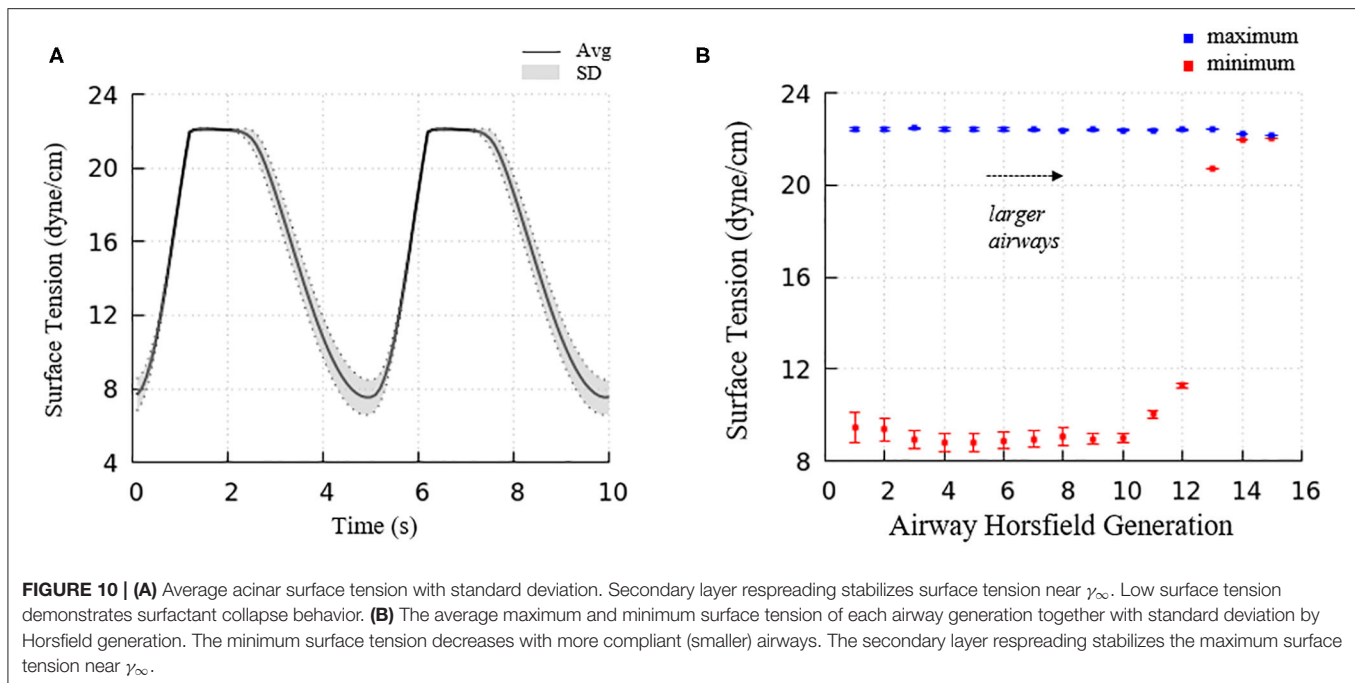
In order to understand the PV relationships in **Figure 8**, it is necessary to explore the dynamic surface tension behavior at the alveolar and airway levels (**Figure 9**). As seen in **Figure 9A**, the surface tension hysteresis behavior of acinus components



is similar to the isolated interface model (**Figure 5**) except that a minimum surface tension plateau does not exist at the lowest acinar volumes. This deviation occurs because the surfactant concentration of the acinus model does not approach  $\Gamma_{max}$  under the breathing conditions imposed by this simulation. In this model, “collapse” refers to the transport of surfactant from the primary to secondary layers. This transport occurs if  $\Gamma_1 > \Gamma_\infty$ , and occurs at a greater rate

as  $\Gamma_1$  increases, to a point where saturation will occur if  $\Gamma_1 \geq \Gamma_\infty$ . In our full-lung model, the rate of interfacial contraction is not large enough to hyper-concentrate the alveolar primary layer to a level that leads to secondary layer saturation. Nevertheless, a significant secondary layer does exist in acinus components.

We note that there is a sharp slope change in the local PV curve in **Figure 8A**. This abrupt change in compliance is due to



the secondary layer respreading, which reduces surface tension and work of breathing. This sharp slope change corresponds to the slope change at point d in **Figure 9A**.

Airways (**Figure 9B**) in our model have surface tension hysteresis behaviors similar to acini. Airways exhibit hysteresis areas that varies due to geometrical as well as tethering pressure difference. This corresponds to observations in **Figure 6**.

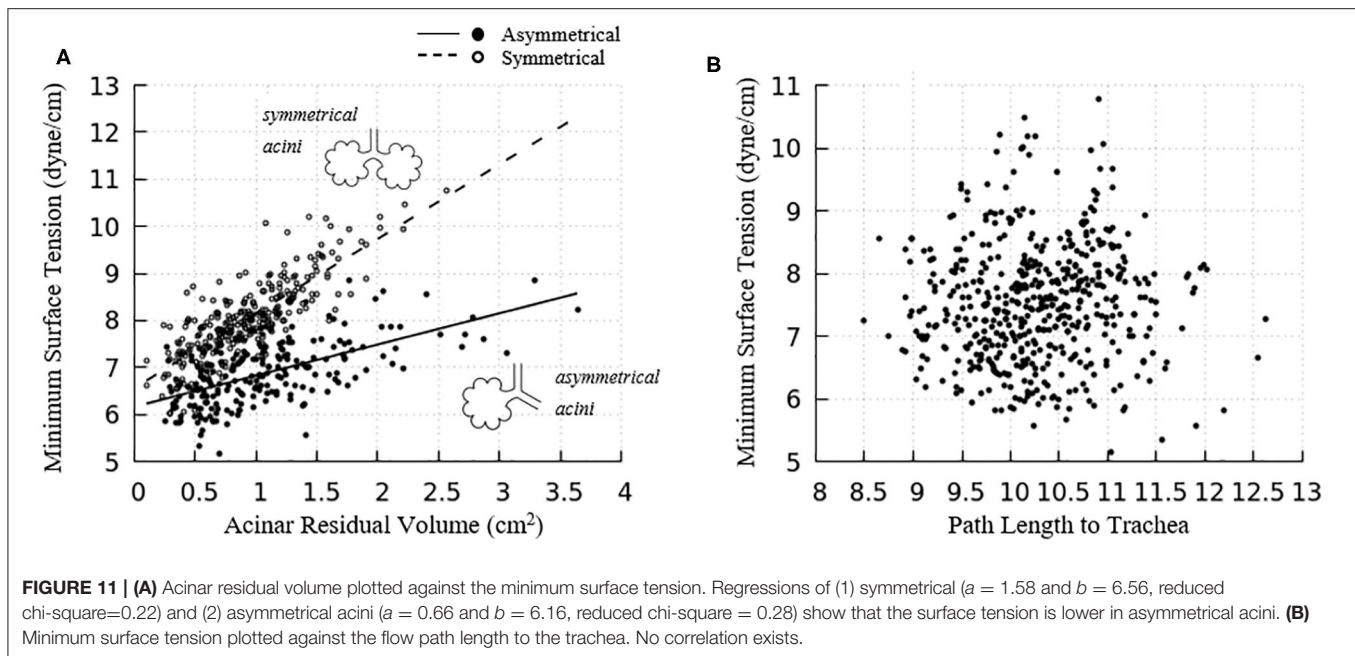
We also note that the surface tension increases slightly prior to alveolar and airway expansion (dotted circles), which is likewise observed in the acinar PV relationship (**Figure 8A**). We attribute this behavior to surfactant over-collapse. In our model, the direction of transport between the primary and secondary layer is only determined by the value of  $\Gamma_1$ . During most of the phase a–b–c–d in **Figure 9A**, the primary layer concentration exceeds  $\Gamma_{\infty}$ , so surfactant transport from the primary to secondary layer occurs. However, as described above, this rate of transport is not large enough to saturate the secondary layer. Nevertheless, the secondary layer is able to respread to the primary layer during the phase d–a in **Figure 9A**. In phase a– and c–d, the surface concentration is dominated by the surface area change, i.e., the surface concentration increases/decreases as the surface area decreases/increases. However, due to the sinusoidal pleural pressure, the change rate of the surface area in phase c–d decreases dramatically, while the collapse term in Equation (22) does not have any abrupt changes. Here, the surface concentration becomes transport-dominated, i.e., the surface concentration decreases as surfactant being exuded from the primary layer.

**Figure 6** demonstrated the surface tension in our model and shows spatial variation. This variation is due to physiologically based heterogeneity that is inherent in our model. For example, there are geometrical differences that exist from generation

to generation based upon the space-filling algorithm used to construct the airway tree (Tawhai et al., 2000). Acini are likewise non-uniform because they fill different-sized regions of the lung depending upon the location of the terminal airways. The local surface tension depends upon the lining fluid/surfactant that is distributed within the alveolar components of the acini. While this is assumed to be a uniform concentration, the local strain-field is nonuniform. The physicochemical interactions from variable strain result in transport behavior that leads to non-uniform heterogeneous surface tensions in this dynamic model. **Figure 10A** demonstrates the average and standard deviations of the acinar surface tension. This figure demonstrates an upper limit of surface tension near  $\gamma_{\infty}$  with an insignificant variation. This occurs as the secondary layer respreads, and is indicated by point d in **Figure 9A**. In contrast, at low surface tension the variation is much greater.

The acinar minimum surface tension is found to be correlated to its residual volume, as shown in **Figure 11A**. We subdivide the data into two groups: (1) symmetrical acini that are created at the ends of two equivalent daughter terminal airways, and (2) an asymmetrical acinus that develops from a single terminal airway, with the other daughter airway non-terminal (see figure inset). We investigate the linear regressions using the form  $\gamma_{min} = aV_{RV} + b$ . On average, symmetrically produced acini have higher the surface tensions than asymmetric acini. We also explored the influence of central airway-to-acinus path length on the surface tension (**Figure 11B**) and found no correlation between these values.

For airways, the surface tension heterogeneity also exists. **Figure 10B** shows the relationship between airway generation (Horsfield) and maximum/minimum airway surface tension. The points represent the average value of all the airways in



that generation in one breathing cycle, and the bars represent the standard deviation. Similar to acini, the variation of the maximum surface tension is insignificant due to the surfactant transport mechanism, while a much greater variation of the minimum exists in each generation. The difference among generations can be found to correlate with the tube law defined by Equation (3) and Table 1.

To investigate the impact of a sigh to enhance surfactant surface-layer sorption, we introduced a sigh-like maneuver by temporarily tripling the magnitude of pleural pressure (from 3.2 to 9.6 cmH<sub>2</sub>O), and doubling the time period (from 5 to 10 s per breath). During this cycle, the maximum lung volume increased to 5.96 L. As shown in Figure 12, this high increment of lung volume temporarily depletes the secondary layer and reduces the surfactant concentration of the primary layer, and allows for greater sorption from the bulk to the interface. Upon exhalation, the primary layer is highly concentrated and significantly reduces the surface tension to very low values (<5 dynes/cm). Simultaneously, transfer to the secondary layer occurs, and this leads to a lower surface tension on the following inspiration compared to that observed during the stationary state of tidal breathing.

## Parenchymal Tethering and Strain Deviation

As the red curve in Figure 13A shown, airways in our model has a hysteresis pressure-radius behavior similar to the acini. As discussed in the previous sections, this hysteresis behavior is a result from the flow resistance of the airway network and the surfactant behavior (same mechanics as in acini), and more importantly, the pressure-related tethering force. To describe the tethering effect of the parenchyma, we rewrite Equation (12) and

define  $\Delta Strain$  as

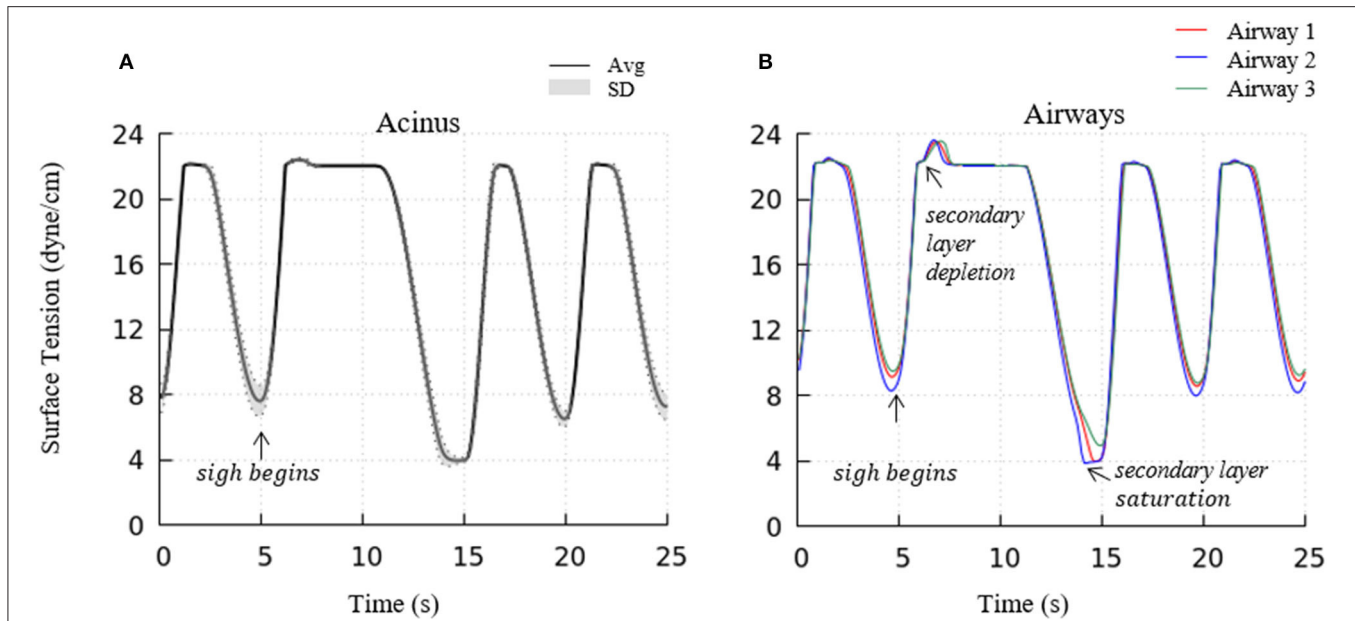
$$\Delta Strain = \frac{R_H - R_{AW}}{R_H}, \quad (26)$$

where  $R_H$  is the hole radius of the parenchyma,  $R_{AW}$  is the airway radius. If  $\Delta Strain$  is negative, it means  $R_H < R_{AW}$ , and the tethering force is compressing the airway. Likewise, if  $\Delta Strain$  is positive,  $R_H > R_{AW}$ , and the tethering force is pulling the airway open. In Figure 14, the strain deviation at four different time point of the breathing cycle are shown.

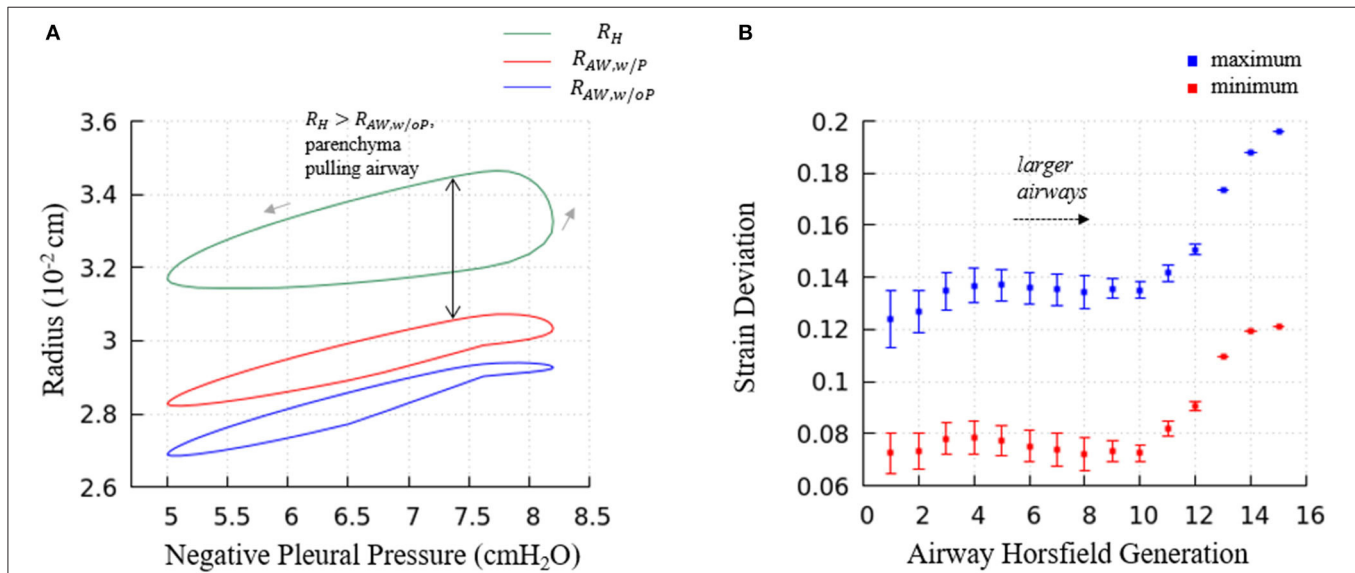
It can be observed in Figure 14 that  $\Delta Strain$  is positive almost all the time, which indicates that airways are pulled outward by parenchyma. To elucidate this stabilizing force, we investigate the parenchyma effect  $[2G_{eff}(\frac{\Delta R}{R})]$  and airways' own properties  $[P_{AW} - P_{PL}(t) \frac{\gamma}{R_{in,AW}(t)}]$  in Equation (7) separately. We simulate the system without tethering, i.e., forcing  $2G_{eff}(\frac{\Delta R}{R}) = 0$  in Equation (7).

Figure 13A demonstrates the terminal airway radius with and without tethering ( $R_{AW, \frac{w}{p}}$ , and  $R_{AW, \frac{w}{o}}$ , respectively) compared to the size of the hole radius,  $R_H$ . This figure shows that  $R_H$  is greater than the size of the terminal airways. This induces an outward tethering stress that increases the airway radius, so  $R_{AW, \frac{w}{p}} > R_{AW, \frac{w}{o}}$ . This stent-like behavior depends upon the set-point for the equilibrium hole-radius (set at  $V_{FRC}$ ) as described in "Parenchymal Tethering." This assumption leads to physiologically reasonable positive strain-deviations during normal breathing for nearly all generations of airways, indicating that the parenchymal tethering supports the airway structure in this healthy lung model. We found that reducing the set-point of the equilibrium hole-radius to volumes below  $V_{FRC}$  results in negative-strain deviation





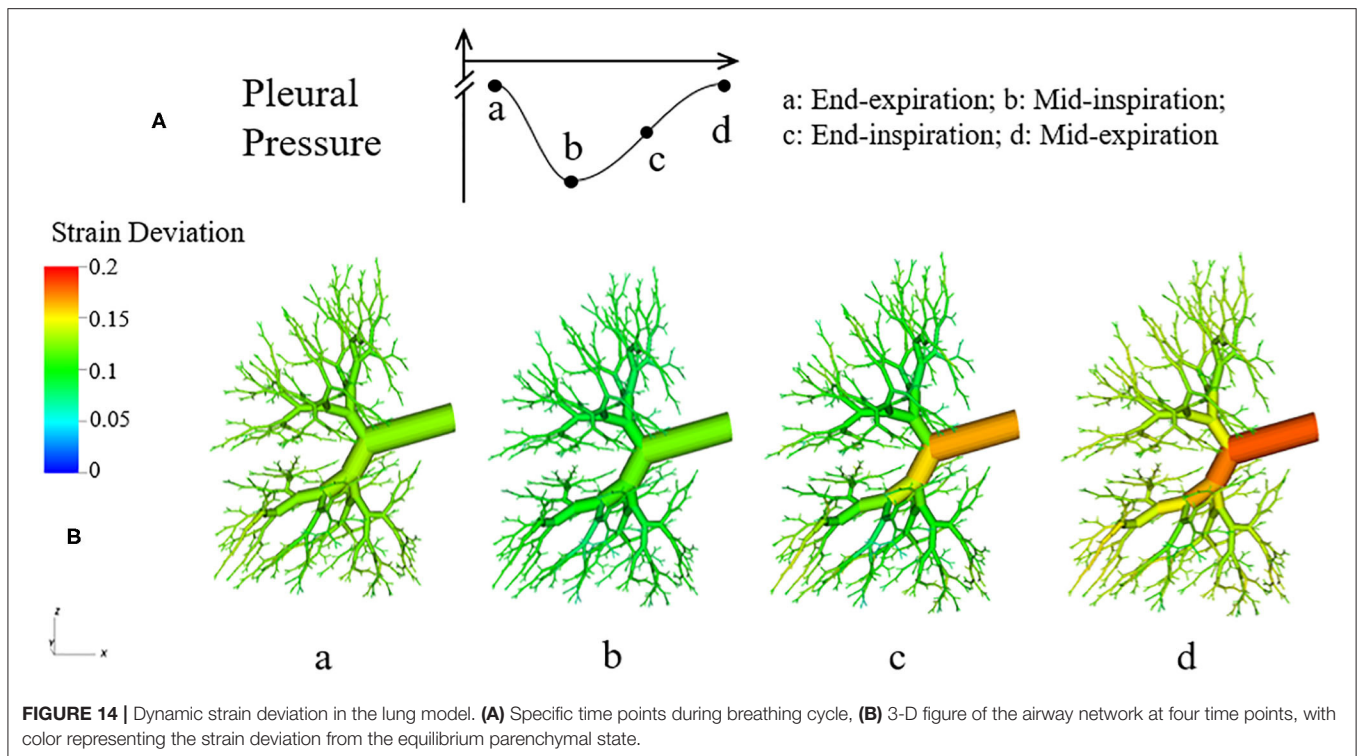
**FIGURE 12 |** Acinar (A) and representative airways, (B) surface tension after a deep sigh. The secondary layer respreading stabilizes the surface tension around  $\gamma_{\infty}$ . In airways, secondary layer depletion can be seen where the surface tension rises rapidly again after being stabilized around  $\gamma_{\infty}$  for a short period. Compared to the stationary tidal breathing state, the additional surfactant in the primary layer by respreading from the secondary layer and adsorption from the bulk during sigh leads to a lower surface tension at end-expiration. The representative airways are the same as those shown in Figure 9.



**FIGURE 13 |** (A) Predictions of terminal airway radius with and without parenchymal tethering. Parenchymal hole radius  $R_H$  (green), airway radius with parenchymal tethering,  $R_{AW,w/P}$  (red), and predicted airway radius without parenchymal tethering,  $R_{AW,w/oP}$  (blue). This figure demonstrates the important feature that in this healthy lung model,  $R_H > R_{AW,w/oP}$ . This implies that parenchyma provides an outwardly directed mechanical stress that stabilizes compliant airways. (B) The average maximum and minimum strain deviation of each Horsfield airway generation. Bars represent the standard deviation.

during portions of the ventilation cycle for mid-generation and terminal airways (data not shown). This behavior could be destabilizing because it would reduce the caliber of compliant airways and lead to an enhanced proclivity for airway obstruction. This parenchymal support behavior is consistent

with earlier simulations conducted by Ryans et al. (2019). The tethering force is important to stabilize the open airway and maintain air flow, though surfactant deficiency can still lead to airway closure or meniscus obstruction in the unhealthy lung (Notter, 2000; West, 2012).



**FIGURE 14 |** Dynamic strain deviation in the lung model. **(A)** Specific time points during breathing cycle, **(B)** 3-D figure of the airway network at four time points, with color representing the strain deviation from the equilibrium parenchymal state.

**Figure 13B** demonstrates the relationship between airway generation (Horsfield) and strain deviation Equation (26). The points represent the average value of all airways in that generation in one breathing cycle, and the bars represent the standard deviation. Small strain deviations exist in the most compliant airways, and this deviation is due to time-dependence in the acinar response related to Equation (17), since the compliance of the airways is approximately equal to the acini. In contrast, for larger airways, significantly positive strain deviation exists due to several factors: (1) a compliance differences between the acinus and airway, (2) the pressure differences associated with large path-lengths between the large airways and surrounding acinus, and (3) the time-dependence in the acinar response.

## Limitations

While this model provides a useful tool for simulating the multi-scale interactions of the lung, there are significant limitations due to the assumed idealized conditions. For example, we neglect gravitational effects and assume a uniform pleural pressure distribution. As such, this model cannot yet simulate ventilation dependency that is linked to orientation. This model also neglects smooth muscle biomechanics that may be neuromodulated. Furthermore, we neglect important pressure losses due to turbulence and entrance-flow effects (Filоче et al., 2015). Our simulations of normal breathing induce a maximum flow rate of  $\sim 0.92$  L/s in the trachea. The Reynolds number is large ( $Re > 2,000$ ) in airways of generations  $n \leq 3$  and the Womersley parameter indicates unsteady flow in generations  $n \leq 4$ . Furthermore, we have assumed fully developed flow,

which does not occur near bifurcations. Thus, we can expect that these regions will have greater pressure-drops than those predicted by this model. We also assume that each airway and acinus is initialized with the same dimensionless film thickness  $\varepsilon$  and a uniform surfactant concentration, and we do not allow for inter-airway or airway-to-acinar transport. Since this is a model of a healthy lung, we do not incorporate interfacial instabilities that can create plugs or regions of atelectasis. Despite these limitations, this multi-scale model a significant step in the development of a multi-scale model of the entire lung, and is capable of reproducing physiologically realistic behavior.

It should be noted that there are a large number of parameters in our system. Some of these are simple physical constants such as viscosity, equilibrium surface tension, adsorption/desorption rates, etc. that can be determined independently. Other parameters include physiological model constants related to the tube law, the set-point for tethering between parenchyma and airways, airway parent-daughter branch angles, etc. Some of these are better known than others, and could be patient specific. These might be considered “tunable” in the sense that they can be subject to revision when more information is available. With present technology, we cannot hope to create patient-specific geometric models of all branching airways and alveoli, lining fluid distributions and regionally dependent surfactant physico-chemical behavior. Despite the inability to define this type of specific information, when fully developed for healthy and pathological states, we will seek to determine the sensitivity of physiological behavior to key measurable parameters. This could provide insight into pathophysiological behavior and system interdependency that is not available from simpler systems. With

this understanding, the step toward patient-specific analyses will become clearer.

## CONCLUSIONS

We have developed and investigated a computational 3-D lung model that simulates multi-scale pulmonary interactions under healthy conditions. This model includes the airflow between airways and acini, surfactant transport in the liquid lining, and parenchymal tethering between the acini that surrounds airways. As shown above, these simulations demonstrate physiologically realistic macroscale PV relationships and predict microscale strain distributions that deviate from the uniform strain state (Ma et al., 2013). This deviation occurs due to ventilation-induced airflow pressures and non-equilibrium Laplace pressures resulting from surfactant physicochemical interactions (West, 1977, 2012; Krueger and Gaver, 2000; Notter, 2000). In the future, this model will provide a baseline for the study of pathological conditions; for example, airway closure and liquid plug movement that may be important contributors to the etiology of ARDS and ventilator-induced lung injury. Simulations of pathophysiological conditions may foster the

development of improved methods of ventilation (Kollisch-Singule et al., 2014; Gaver et al., 2020).

## DATA AVAILABILITY STATEMENT

The datasets generated for this study are available on request to the corresponding author.

## AUTHOR CONTRIBUTIONS

HM, HF, and DG conceived, designed research, analyzed data, interpreted results of experiments, prepared figures, and drafted manuscript. HM and HF performed experiments. HM, HF, DH, and DG edited, revised manuscript, and approved final version of manuscript. All authors contributed to the article and approved the submitted version.

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**Conflict of Interest:** The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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# Hidden Microatelectases Increase Vulnerability to Ventilation-Induced Lung Injury

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Mechanical ventilation of lungs suffering from microatelectases may trigger the development of acute lung injury (ALI). Direct lung injury by bleomycin results in surfactant dysfunction and microatelectases at day 1 while tissue elastance and oxygenation remain normal. Computational simulations of alveolar micromechanics 1-day post-bleomycin predict persisting microatelectases throughout the respiratory cycle and increased alveolar strain during low positive end-expiratory pressure (PEEP) ventilation. As such, we hypothesize that mechanical ventilation in presence of microatelectases, which occur at low but not at higher PEEP, aggravates and unmasks ALI in the bleomycin injury model. Rats were randomized and challenged with bleomycin (B) or not (H = healthy). One day after bleomycin instillation the animals were ventilated for 3 h with PEEP 1 (PEEP1) or 5 cmH<sub>2</sub>O (PEEP5) and a tidal volume of 10 ml/kg bodyweight. Tissue elastance was repetitively measured after a recruitment maneuver to investigate the degree of distal airspace instability. The right lung was subjected to bronchoalveolar lavage (BAL), the left lung was fixed for design-based stereology at light- and electron microscopic level. Prior to mechanical ventilation, lung tissue elastance did not differ. During mechanical ventilation tissue elastance increased in bleomycin-injured lungs ventilated with PEEP = 1 cmH<sub>2</sub>O but remained stable in all other groups. Measurements at the conclusion of ventilation showed the largest time-dependent increase in tissue elastance after recruitment in B/PEEP1, indicating increased instability of distal airspaces. These lung mechanical findings correlated with BAL measurements including elevated BAL neutrophilic granulocytes as well as BAL protein and albumin in B/PEEP1. Moreover, the increased septal wall thickness and volume of peri-bronchiolar-vascular connective tissue in B/PEEP1 suggested aggravation of interstitial edema by ventilation in presence of microatelectases. At the electron microscopic level, the largest surface area of injured alveolar epithelial was observed in bleomycin-challenged lungs after PEEP = 1 cmH<sub>2</sub>O ventilation. After

bleomycin treatment cellular markers of endoplasmic reticulum stress (p-Perk and p-EIF-2 $\alpha$ ) were positive within the septal wall and ventilation with PEEP = 1 cmH<sub>2</sub>O ventilation increased the surface area stained positively for p-EIF-2 $\alpha$ . In conclusion, hidden microatelectases are linked with an increased pulmonary vulnerability for mechanical ventilation characterized by an aggravation of epithelial injury.

**Keywords:** microatelectases, alveolar interdependence, ventilation-induced lung injury, surfactant, blood-gas barrier

## INTRODUCTION

The clinical picture encompassing refractory blood deoxygenation, decrease in respiratory system's compliance and bilateral infiltrates in conventional chest X-ray has been described originally as acute respiratory distress syndrome (ARDS) by Ashbaugh et al. (1967). For those patients suffering from ARDS, mechanical ventilation represents the decisive lifesaving therapeutic intervention. On the other hand, mechanical ventilation has also been identified to be an independent trigger for the progression of acute lung injury (ALI) through a process referred to as ventilator-induced lung injury (VILI) (Slutsky and Ranieri, 2013) and a substantial fraction of ARDS patients develop the complete picture of the ARDS during mechanical ventilation (Nieman et al., 2015). Moreover, mechanical ventilation in presence of surfactant abnormalities plays a central role in the development of an ARDS/ ALI (Albert, 2012; Rühl et al., 2019).

The underlying pathomechanisms involve abnormalities in alveolar micromechanics. Alveolar micromechanics can be defined as the dynamic changes of alveoli in size and shape during a respiratory cycle (Knudsen and Ochs, 2018). In healthy lungs the alveolar airspaces are stabilized by connective tissue elements located within the inter-alveolar septal walls as well as the intra-alveolar surfactant layer at the gas-liquid interface which reduces surface tension during expiration (Wilson and Bachofen, 1982; Knudsen and Ochs, 2018). In presence of a functional surfactant system the stresses are balanced and roughly homogeneously distributed within the lung (Mead, 1961; Mead et al., 1970). During a respiratory cycle the strains and stresses acting on the inter-alveolar septa (e.g., the blood-gas barrier) are therefore minimized (Knudsen and Ochs, 2018). Direct or indirect lung injury results in inflammation, edema formation, and surfactant dysfunction that cause severe organ dysfunction. These pathologies introduce heterogeneous ventilation and abnormal alveolar micromechanics. Surfactant dysfunction results in intra-tidal alveolar recruitment and derecruitment (Schiller et al., 2001), an abnormality which, in presence of high surface tension, injures the epithelium and is therefore named atelectrauma (Slutsky and Ranieri, 2013; Cressoni et al., 2017; Rühl et al., 2019). The inter-alveolar walls of those alveoli which remain open are subject to increased strain and overdistension. This volutrauma further injures the very thin and delicate blood-gas barrier by rupturing the endothelial or alveolar epithelial cells (Dreyfuss and Saumon, 1998; Vlahakis et al., 2002; Cong et al., 2017). A more insidious mechanism of

volutrauma results from the concept of alveolar interdependence (Mead et al., 1970; Makiyama et al., 2014). In this situation, microatelectases act as stress concentrators that impose tethering forces on surrounding inter-alveolar septal walls so that these areas of lung parenchyma are prone to overdistension and therefore volutrauma (Albert, 2012; Albert et al., 2019).

Ruptures of the plasma membrane of alveolar epithelial cells increase cytoplasmic Ca<sup>2+</sup> levels which are responsible for activation of the cellular integrated stress response (ISR) (Dolinay et al., 2017, 2018). Stretch-induced ISR is initiated by Ca<sup>2+</sup> dependent auto-phosphorylation of protein kinase RNA-like endoplasmic reticulum kinase (Perk). Phosphorylated Perk (p-Perk) moreover phosphorylates eukaryotic translation initiating factor 2 $\alpha$  (EIF-2 $\alpha$ ), a step critical to switch off the protein biosynthesis machinery of the cell (Harding et al., 2000). If the ISR lingers on then cell death is initiated by selective expression of CCAAT/Enhancer binding Protein homologous Protein (CHOP) (Günther et al., 2012; Dolinay et al., 2018).

Intratracheal instillation of bleomycin is a common animal model of dose-dependent direct acute lung injury and fibrosis (Bonniaud et al., 2018). We have previously characterized the alveolar micromechanics of this model in detail during disease progression. The first abnormality observed after 24 h was a slight surfactant dysfunction linked with pathological alterations in alveolar micromechanics (Lutz et al., 2015; Steffen et al., 2017; Knudsen et al., 2018) where a decrease in airway opening pressure below 5 cmH<sub>2</sub>O on expiration resulted in a derecruitment of alveoli. At a light microscopic level, further pathologies including edema formation or inflammation were virtually absent (Lutz et al., 2015; Knudsen et al., 2018). Moreover, at this very early stage of injury the lung mechanical properties, including organ scale tissue elastance within a range of PEEP levels from 1 to 5 cmH<sub>2</sub>O as well as oxygen saturation, did not significantly differ from healthy subjects. Due to the fact that pressures needed to recruit alveoli were much higher than those needed to prevent their derecruitment, computational simulations of alveolar micromechanics suggested that in this model there was only little intra-tidal alveolar recruitment and derecruitment during ventilation with PEEPs between 0 and 15 cmH<sub>2</sub>O and a tidal volume of 10 ml/kg bodyweight (Knudsen et al., 2018). Instead, ventilation with PEEP below 5 cmH<sub>2</sub>O was associated with permanent alveolar derecruitment (=microatelectases) combined with increased tidal alveolar volume changes indicating an increased dynamic alveolar strain. In addition, the open alveoli were characterized by lower individual elastance, a phenomenon explainable by outward

tethering forces imposed by nearby derecruited alveoli. Based on these observations, we considered the bleomycin-injured lung to be at risk for VILI when PEEP is below 5 cmH<sub>2</sub>O due to the presence of microatelectases. Since neither tissue elastance nor blood oxygenation differed from healthy controls there were no clinical signs of ALI at the organ scale. The microatelectases were therefore considered to be hidden.

In order to investigate the hypothesis whether these hidden microatelectases are linked with an increased susceptibility to VILI, bleomycin challenged lungs were ventilated with a PEEP of 1 (=microatelectases present) or 5 cmH<sub>2</sub>O (=microatelectases absent) and compared to healthy controls. After a period of 3 h of mechanical ventilation ALI was unmasked in bleomycin challenged lungs if ventilated with PEEP of 1 but not 5 cmH<sub>2</sub>O based on tissue elastance measurements, alveolar edema, ultrastructural signs of injury of alveolar epithelial cells and markers of ISR.

## MATERIALS AND METHODS

### Subjects and Study Design

The animal experiments were approved by the Niedersächsisches Landesamt für Verbraucherschutz und Lebensmittelsicherheit (LAVES, Oldenburg, Lower Saxony, Germany, approval number 17/2068) which house the German equivalent of an institutional animal care and use committee, according to the European Animal Welfare Regulations. In total 50 male Fisher 344/DuCrI rats (Charles River, Sulzfeld, Germany) aged 11 to 13 weeks with body weights ranging between 208 and 250 g were randomly assigned to a healthy group (H;  $n = 23$ ) and a bleomycin-injured group (B;  $n = 27$ ). The bleomycin group received intratracheal instillation of 4.5 U/kg bodyweight of bleomycin dissolved in 0.9% NaCl solution. One day later animals were further randomized to the subgroups which were either not ventilated (groups H/No ventil,  $n = 9$ , and B/No ventil,  $n = 8$ ) or ventilated with PEEP = 1 cmH<sub>2</sub>O (groups H/PEEP1,  $n = 7$ , and B/PEEP1,  $n = 9$ ) or PEEP = 5 cmH<sub>2</sub>O (groups H/PEEP5,  $n = 7$ , and B/PEEP5,  $n = 10$ ). The animals were anesthetized by intraperitoneal injection of Ketamine (80 mg/kg bodyweight) combined with Xylazine (5 mg/kg bodyweight) and tracheotomized. Those animals assigned to “no ventilation” were directly subjected to bronchoalveolar lavage, and instillation fixation or vascular perfusion fixation as outlined below. Those animals assigned to ventilation groups were ventilated with room air, initially with PEEP = 3 cmH<sub>2</sub>O, tidal volume = 10 ml/kg bodyweight and an inspiratory-to-expiratory ratio of 1:2. The respiratory rate was 90/min. The choice of these parameters was geared to previous studies applying similar volumes per minute and kg bodyweight during mechanical ventilation (Allen et al., 2005). The baseline lung mechanical properties were measured using derecruitability tests administered with a *newFlexiVent-System* (SCIREQ®, Montreal). These derecruitability tests included 2 deep inflations consisting of a continuous ramp of airway opening pressure from 3 to 30 cmH<sub>2</sub>O over 3 s and an end-inspiratory plateau at 30 cmH<sub>2</sub>O for 3 s. The deep inflations, or recruitment maneuvers, were

followed by 10 repetitive forced oscillation perturbations (FOT) over a period of 4.5 minutes with the first FOT performed 2 seconds after the recruitment. The impedance spectra measured by FOT over a frequency range between 1 and 20.5 Hz were fit to the constant-phase model in order to calculate tissue elastance  $H$  (Hantos et al., 1992). The first tissue elastance value of this derecruitability test was referred to as  $H_1$  and reflected lung mechanical properties at the highest degree of recruitment. The mean of the last three measurements of the tissue elastance was referred to as  $H_s$  and reflected steady state conditions between 3.5 and 4.5 min after recruitment. The increase of tissue elastance over time after recruitment maneuver has been linked with progressive derecruitment of distal airspaces and was calculated as  $\Delta H = H_s - H_1$ . After assessments of baseline lung mechanical properties, the PEEP was set to either 1 cmH<sub>2</sub>O (PEEP1 groups) or 5 cmH<sub>2</sub>O (PEEP5 groups). Anesthesia was maintained by inhalation narcosis using 1% isoflurane in room air combined with subcutaneous injection of 2 mg/kg bodyweight butorphanol (Torbugesic®). The tidal volume, inspiratory-to-expiratory ratio and respiratory rate remained unchanged. Derecruitability tests were performed every 60 min as described above with a PEEP, and FOT onset pressure, set according to the ventilation pattern (1 or 5 cmH<sub>2</sub>O). After 3 h of mechanical ventilation a final derecruitability test was conducted at PEEP = 3 cmH<sub>2</sub>O. Since the PEEP value has an impact on the lung mechanical properties (Knudsen et al., 2018) the measurements before and after the 3 h period of either PEEP = 1 or 5 cmH<sub>2</sub>O ventilation could be compared between study groups so that differences in tissue elastance reflected the degree of lung injury. Monitoring of animals during mechanical ventilation was based on transcutaneous pulse oximetry using a rodent oximeter (MouseOx Plus, Rat Foot Sensor, Starr Life Sciences Corp., United States) and the oxygen saturation as well as heart rate was documented every 30 min. In addition the pressure in the ventilator cylinder (Pcycl) of the flexiVent system and airway opening at the expiratory limb (Pao) was recorded continuously in  $n = 3$  animals per experimental group to describe the time course of the peak inspiratory pressure (PIP) during mechanical ventilation.

### BAL and Tissue Processing

After ventilation, all rats were euthanized with Ketamine (80 mg/kg bodyweight) combined with Xylazine (5 mg/kg bodyweight, Rompun®) and the opening of the abdominal aorta. Except for 1–2 lungs per study group all were subjected to BAL and instillation fixation. For this purpose, the right lungs received three repetitions of a 4 ml bronchoalveolar lavage (BAL) using 0.9% sodium chloride (NaCl). Left lungs were fixed by instillation fixation (1.5% Paraformaldehyde, 1.5% Glutaraldehyde, 0.15 M HEPES buffer) at a hydrostatic instillation pressure of 25 cmH<sub>2</sub>O. The lung volumes of fixed lungs were determined before a systematic uniform sampling for light and electron microscopic assessments was performed based on established methods (Tschanz et al., 2014). This sampling process resulted in 5–6 slices sampled for analyses at light microscopical level and at least 6 tissue blocks sampled for analyses at electron microscopic level. Samples were embedded in Technovit 8100

(Kulzer GmbH, Wehrheim, Germany) or epoxy resin (Epon®, Polyscience, Hirschberg an der Bergstraße, Germany) for light and electron microscopy, respectively (Mühlfeld et al., 2013). Within each study group the remaining lungs ( $n = 1-2$ ) were fixed by vascular perfusion fixation at an end-inspiratory hold during PEEP = 1 cmH<sub>2</sub>O ventilation using 0.1% glutaraldehyde and 4% paraformaldehyde in 0.2 M Hepes buffer solution. This “fixation from behind” allows assessment of the air-filled lung and therefore the effects of high surface tension on lung structure, e.g., the occurrence of microatelectases or intra-alveolar edema formation, are maintained. This fixative has also been used for immunolabeling since it maintains antigenicity and molecular identity of cells (Hsia et al., 2010). Perfusion fixed lungs were sampled for Technovit embedding and structural investigations as well as O.C.T. (optical cutting temperature) embedding for cryosections and immunolabeling of cellular stress markers.

## BAL Analyses

For protein and cellular analysis, the BAL components were separated by centrifugation. The protein concentration inside the BAL fluid was analyzed by a protein assay (Pierce™ BCA Protein Assay, Fisher Scientific, Hampton, VA, United States) based on the manufacturer's instructions. Albumin concentration in the BAL was measured via ELISA (Rat Albumin ELISA Kit, Bethyl Laboratories, Montgomery). The BAL samples were diluted 1:1000 and compared to the standard curve according to the manufacturer's protocol. For cellular analysis, the BAL cells were separated from the rest of the BAL via centrifugation. Cytospin slides (Thermo Shandon Cytospin 3, Marshall Scientific, Hampton VA, United States) were prepared with 50.000 cells per BAL diluted in 100 µl phosphate buffer (PBS). Lymphocytes, macrophages and neutrophilic granulocytes were differentiated after staining the Cytospins with DiffQuik. Using Visiopharm® Software a systematic uniform area sampling was performed and at least 100 to 200 cells were categorized and counted using a primary magnification of 40×. Furthermore, we assessed the concentration of IL-6 within the BAL using an ELISA Kit (DuoSet® ELISA Rat IL-6, R&D Systems, Minneapolis, MI, United States). We utilized 96 well-plates and photometric measurements for cytokine concentration. Calculations were made with Magellan Software.

## Design-Based Stereology

For stereology, lungs fixed by airway instillation were used. Initially we performed a volumetry based on the Archimedes principle for the whole left lung to obtain the volume of the reference space, the lung volume, for further structural assessments (Scherle, 1970). Embedded tissue for light microscopic analyses was cut into 1.5 µm sections by a microtome (Leica RM 2165, Leica Biosystems, Wetzlar, Germany). Afterward, a toluidine blue staining was performed. The slides for light microscopy were scanned (AxioScanZ.1) and 10% of the area of each slide was randomly sampled with the use of Visiopharm® Software to obtain between 60 and 200 representative fields of view per lung. The pictures were examined by using the STEPanizer stereology tool (Tschanz et al., 2011) or the newCAST Visiopharm software. Following a cascade sampling design (Ochs, 2006)

non-parenchyma (nonpar) was initially differentiated from parenchyma (par) and volume fractions of these compartments ( $V_V(\text{par/lung})$  and  $V_V(\text{nonpar/lung})$ ) within the lung were determined by point counting. Parenchyma was defined as regions of the lung that contribute to diffusive gas exchange so that this compartment included alveolar and ductal airspaces as well as interalveolar septal walls. Non-parenchyma included the conducting airways (bronchi and bronchioles), larger vessels (excluding capillaries and corner vessels within the septa) and the peri-bronchiolar-vascular connective tissue. In a second step the components within the non-parenchyma and parenchyma were further differentiated by means of point-counting. Taking the non-parenchyma compartment as reference space, the volume fractions within non-parenchyma of conducting airways ( $V_V(\text{airway/nonpar})$ ), larger vessels ( $V_V(\text{ves/nonpar})$ ) and peri-bronchiolar-vascular connective tissue ( $V_V(\text{pbvtis/nonpar})$ ) were determined. Within parenchyma, alveolar ( $V_V(\text{alv/par})$ ) and ductal airspaces ( $V_V(\text{duct/par})$ ) as well as interalveolar septa ( $V_V(\text{sep/par})$ ) were distinguished. Volume fractions were, in general, calculated by dividing the number of test points falling on the structure of interest (e.g., non-parenchyma) and the test points hitting the reference space (e.g., the total lung volume). Volume fractions were converted to absolute volumes of the structures of interest per lung by multiplication with the volume of the reference space. In addition, the surface area density of alveolar walls within the lung parenchyma ( $S_V(\text{alv/par})$ ) was determined by intersection counting based on established methods (Knudsen et al., 2010). The surface density was converted into a total surface area per lung ( $S(\text{alv,par})$ ) by multiplication with the reference volume, in this case the volume of lung parenchyma ( $V(\text{par,lung})$ ). For all structures of interest between 100 and 200 counting events per lung were generated since this has been shown to result in a sufficiently high precision of stereological estimators (Gundersen and Jensen, 1987). The mean arithmetic thickness of interalveolar septal walls ( $t(\text{sep})$ ) was calculated as a volume-to-surface ratio (Mühlfeld and Ochs, 2013).

Electron microscopy (FEI Morgagni transmission electron microscope, Eindhoven, The Netherlands) was used to investigate the health of the alveolar epithelium based on ultrastructural criteria (Dreyfuss and Saumon, 1998; Fehrenbach et al., 1999; Lutz et al., 2015; Rühl et al., 2019). The samples for electron microscopy were embedded in epoxy resin and cut into 80 nm sections (Ultracut S, Leica Reichert, Wetzlar, Germany). Six sections per lung were analyzed and 100 to 200 fields of view per lung were imaged within a systematic uniform area sampling process (Tschanz et al., 2014). Test lines were superimposed on each image and intersections of the test line with the epithelial basal lamina were counted. At each intersection, the covering epithelial cell was categorized as alveolar epithelial type I (AEI) or type II (AE2) cell. Based on ultrastructural criteria, the corresponding epithelial cell was further categorized as being either “intact” or “injured.” The criteria for an injured epithelial cell were as follows: clearing and swelling of the cytoplasmic ground substance (in relation to the other cells in the septum), blebbing and fragmentation of cells, or denudation of the epithelial basal lamina. The surface densities of the basal lamina



covered by the differently categorized epithelial cells were then calculated. By multiplication of the surface densities with the reference volume, in this case the total volume of interalveolar septa ( $V(\text{sep,par})$ ), absolute surface areas of the basal lamina covered by intact ( $S(\text{AE1\_intact,par})$ ;  $S(\text{AE2\_intact,par})$ ) or injured AE1 or AE2 cells ( $S(\text{AE1\_injure,par})$ ;  $S(\text{AE2\_injure,par})$ ) could be determined (Lutz et al., 2015; Rühl et al., 2019). The light and electron microscopic images used for design-based stereology in this study are available on <https://zenodo.org> (Albert et al., 2020, DOI: 10.5281/zenodo.3738928).

## Immunohistochemistry and Immunofluorescence of Cellular Stress Markers

Cryosections with a thickness of 5  $\mu\text{m}$  were cut for immunohistochemistry of cellular stress markers (p-Perk and p-EIF-2 $\alpha$ ). Sections were pre-treated for 7 min at 37°C with 0.01% trypsin in 0.1% CaCl and repetitively washed with phosphate buffer (PBS). Endogenous peroxidases were blocked with 0.06% hydrogen peroxide in PBS. Primary antibodies (Rabbit anti p-EIF-2 $\alpha$ , Cell Signaling Technologies #3398; Rabbit anti p-Perk, Cell Signaling Technologies #3179) were diluted 1:200 in PBS and used for incubation at 4°C in a moist chamber overnight. Staining with an isotype control antibody (Rabbit mAb, IgG, Cell Signaling Technologies, #3900) were used as a negative control according to the manufacturer's recommendations. Biotinylated mouse-anti-rabbit antibody was used as the secondary antibody. For detection, a streptavidin – HRP – DAB reaction system was applied and the color development observed. Counterstaining was carried out by means of hematoxylin. For quantification of the percentage of the alveolar surface area covered by p-EIF-2 $\alpha$  positive cells a systematic uniform area sampling was performed on four sections per group to obtain at least 200 pictures. Test-lines were randomly projected on the fields of view and intersections of the test lines with brown or not brown colored surfaces were counted. The surface fraction of brown colored surface after p-EIF-2 $\alpha$  ( $S_s(\text{pEIF2}\alpha/\text{sep})$ ) staining was calculated as the ratios of intersections with brown surfaces and all surfaces.

## Statistics

Statistical analysis of the data was done using *GraphPad Prism Version 7* (GraphPad Software, San Diego, CA, United States). A two-way ANOVA was used to take the influencing factors “pre-treatment” (Bleo) and “ventilation pattern” (vent: no ventilation vs. PEEP 1 vs. PEEP 5) or “duration of ventilation” as well as their interaction into account. In case of significant differences based on the two-way ANOVA the Bonferroni *post hoc* test for multiple comparisons and adjustment of the p-level was added. Correlation analyses were performed using Pearson's test. In general, *p* values below 0.05 were considered as statistically significant. The raw data measured during mechanical ventilation while performing the FOT perturbations were fit to the constant phase model. If the coefficient of determination of the model fit to the raw data (impedance spectra) was below 0.9 the data were excluded from further consideration.

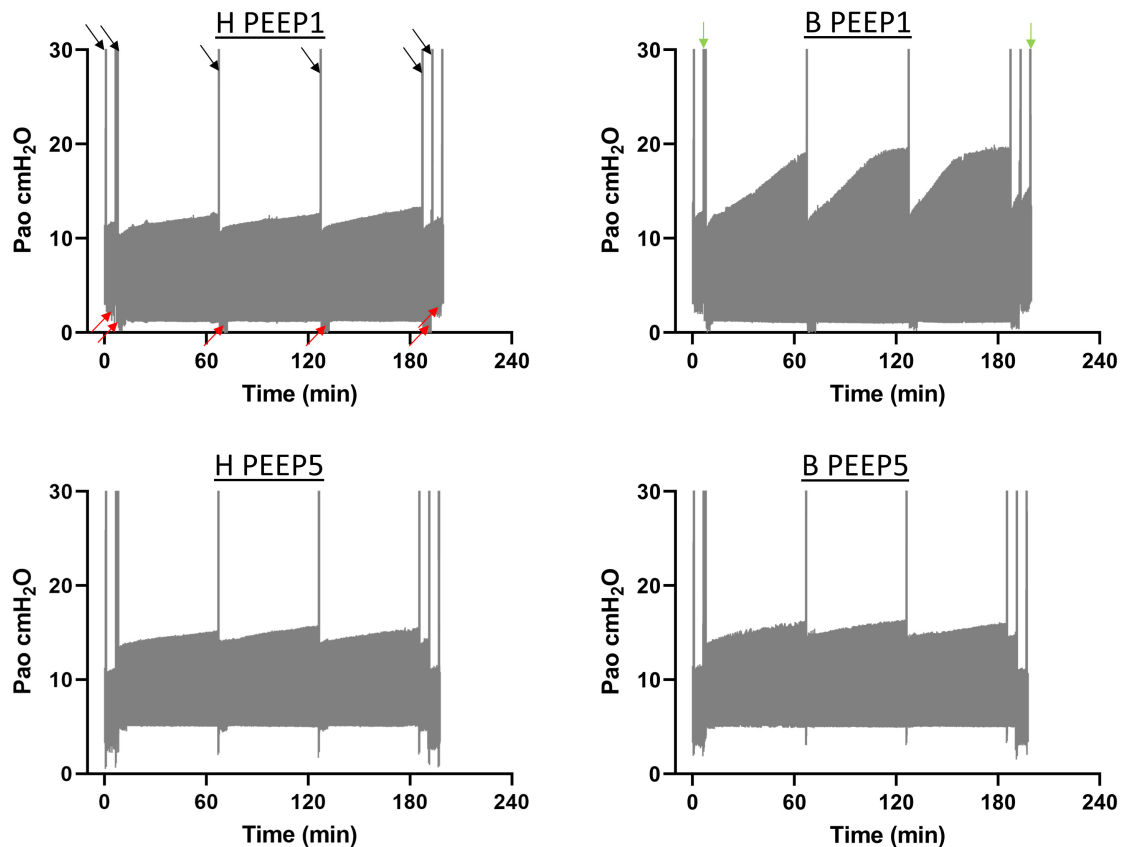
## RESULTS

### Effects of Mechanical Ventilation on Lung Function and Mechanics

During mechanical ventilation oxygen saturation ( $\text{SO}_2$ ) was measured as a functional parameter. No significant differences could be detected between the study groups both at the beginning and at the end of the 3 h period of mechanical ventilation. Initially, the mean and standard deviation of  $\text{SO}_2$  were 98.8% (0.3%), 98.8% (0.6%), 98.8% (1.3%), and 98.6% (1.5%) for H/PEEP1, H/PEEP5, B/PEEP1 and B/PEEP5, respectively. At the end of the mechanical ventilation  $\text{SO}_2$  data were 98.7% (0.72%), 97.3% (1.6%), 96.2% (2.5%), and 97.7% (1.3%) for H/PEEP1, H/PEEP5, B/PEEP1, and B/PEEP5, respectively.

Continuous recording of the airway opening pressure ( $P_{ao}$ ) describes the time course of the peak inspiratory pressure (PIP) during mechanical ventilation. Representative examples of the recorded  $P_{ao}$  data are illustrated in **Figure 1**. In general, in all recorded datasets the PIP increased between the derecruitability tests and could be reduced by a deep inflation (= recruitment manoeuvre). The increase in PIP between derecruitability tests was most pronounced in B/PEEP1. However, in none of the datasets did the peak inspiratory pressures exceed 20  $\text{cmH}_2\text{O}$ . Derecruitability tests were performed at PEEP = 3  $\text{cmH}_2\text{O}$  both before and after the 3-hour period of mechanical ventilation. Since the PEEP level has significant effects on tissue elastance (Knudsen et al., 2018), these measurements were necessary to obtain lung mechanical data under exactly the same conditions for comparison between study groups. The data of the 4 study groups during PEEP = 3  $\text{cmH}_2\text{O}$  ventilation are illustrated in **Figure 2A** (baseline) and **Figure 2B** (outcome after mechanical ventilation). H1 did not show any differences between study groups and the factor “Bleo” did not affect H1 at baseline according to the two-way ANOVA. However, the tissue elastance increased during the time course of the derecruitability test in particular in the bleomycin group. Hence, the level of tissue elastance values at the end of the derecruitability test ( $H_s$ ), was slightly higher in the groups having been challenged with bleomycin (groups B/PEEP1 and B/PEEP5) compared to those which were healthy (groups H/PEEP1 and H/PEEP5) before starting either PEEP = 1 or 5  $\text{cmH}_2\text{O}$  ventilation. Accordingly, the two-way ANOVA demonstrated a significant effect of the factor “Bleo” on  $H_s$  during PEEP = 3  $\text{cmH}_2\text{O}$  ventilation ( $p < 0.01$ ). No differences between the groups which were randomized to either PEEP1 or PEEP5 ventilation could be detected at baseline so that the study groups entered the different ventilation protocols with comparable lung mechanical properties.

After 3 h of mechanical ventilation the tissue elastance data in the B/PEEP1 group was significantly elevated above the other groups including B/PEEP5 as is shown in **Figure 2B**. With this regard, both bleomycin challenge ( $p = 0.001$ ) as well as the PEEP level ( $p = 0.009$ ) had a significant effect on  $H_s$  and these two factors demonstrated a significant interaction ( $p = 0.028$ ). The study design also allowed within-group comparison of  $H_s$  before and after the 3 h period of mechanical ventilation. Using a student's *t*-test for dependent measurements a highly



**FIGURE 1 |** The airway opening pressure (Pao) at the expiratory limb of the rodent ventilator were continuously recorded during the mechanical ventilation in  $n = 3$  lungs per experimental group. The graphs illustrate representative examples of the range of Pao for the different study groups. The lower limit represents the PEEP level while the upper limit corresponds to the peak inspiratory pressures. The black arrows indicate pressure increases during recruitment maneuvers (=deep inflations) which were followed by repetitive measurements of tissue elastance using the forced oscillation perturbation (FOT, red arrows). The green arrows indicate recording of pressure controlled pressure volume loops with a stepwise increase of Pao up to a maximum of 30 cmH<sub>2</sub>O (quasistatic PV-loops). Hence, the second bar is a combination of quasistatic PV-loops and deep inflations. The peak inspiratory pressures increased between the recruitment maneuvers in all study groups but did in none of the recorded datasets exceed 20 cmH<sub>2</sub>O.

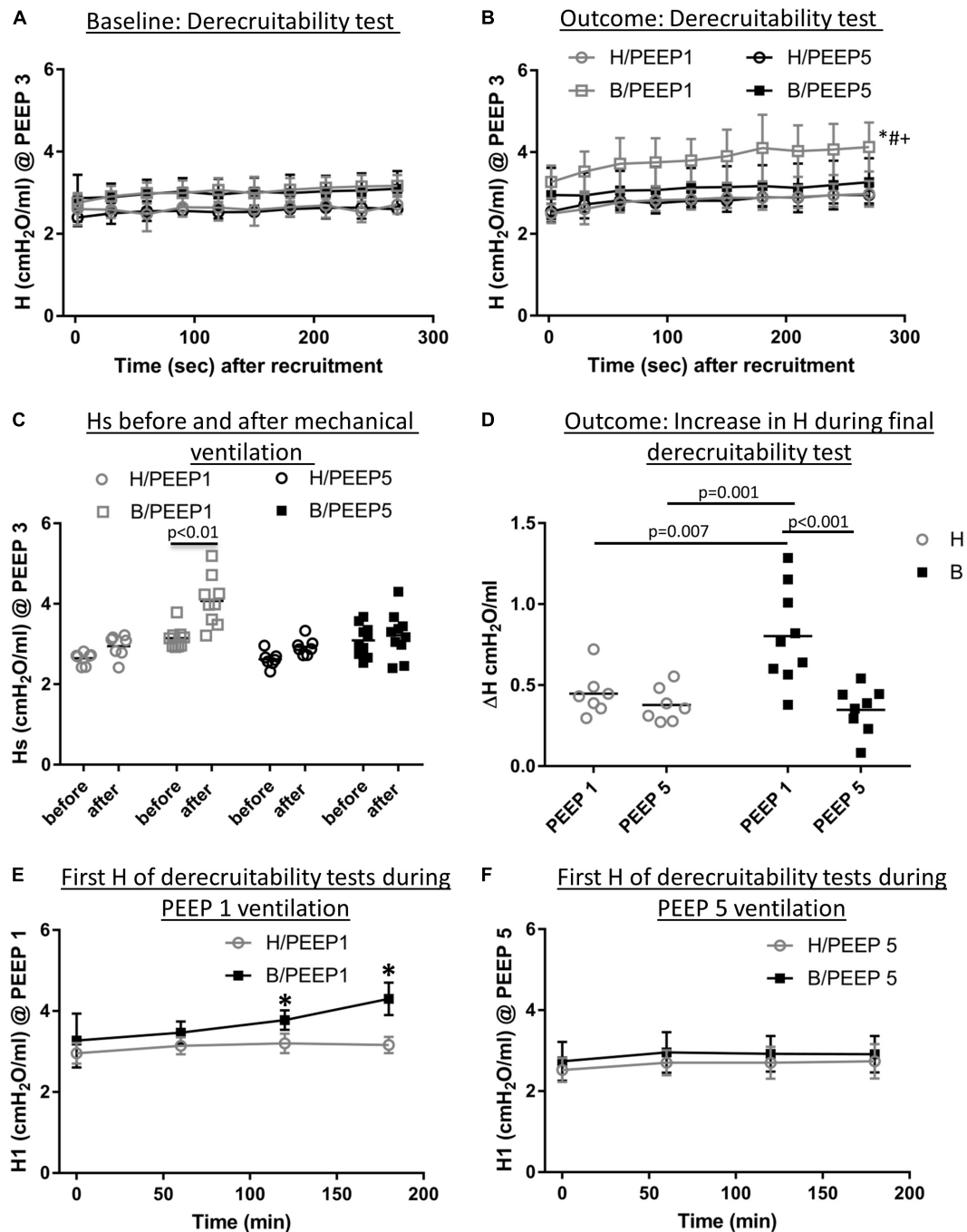
significant increase in Hs was observed in the B/PEEP1 group but not in the other three groups B/PEEP5, H/PEEP1 and H/PEEP5 (**Figure 2C**). The increase of tissue elastance during the observational period after the recruitment manoeuvre,  $\Delta H$ , was significantly increased in B/PEEP1 compared to the other three groups (**Figure 2D**) indicating increased progressive stiffening in B/PEEP1 after recruitment compared to the other groups. Derecruitability tests were also performed every 60 min during mechanical ventilation with PEEP = 1 or 5 cmH<sub>2</sub>O. **Figures 2E,F** illustrate the initial tissue elastance after recruitment manoeuvre, H1, as a function of time of mechanical ventilation during PEEP = 1 and 5 cmH<sub>2</sub>O ventilation. Changes in the first tissue elastance measurement after recruitment manoeuvre have been shown to correlate with the degree of alveolar epithelial injury based on quantitative ultrastructural data (Smith et al., 2017; Hamlington et al., 2018). During PEEP = 1 cmH<sub>2</sub>O ventilation the first tissue elastance after recruitment remained roughly stable in healthy lungs (H/PEEP1) but demonstrated a significant increase with time in the bleomycin challenged lungs (B/PEEP1) (**Figure 2E**, bleomycin effect  $p = 0.003$ , time effect  $p < 0.001$ ,

interaction  $< 0.001$ ). Of note, both H/PEEP1 and B/PEEP1 started at the same level without any significant differences. On the other hand, during PEEP = 5 cmH<sub>2</sub>O both bleomycin challenged (B/PEEP5) as well as healthy lungs (H/PEEP5) did not show a temporal increase in H1. The level of H1 differed between PEEP = 1 cmH<sub>2</sub>O and PEEP = 5 cmH<sub>2</sub>O ventilation in both B and H and this is the effect of the increased onset pressure the FOT started (Knudsen et al., 2018).

Taken together, during and after the 3 h period of mechanical ventilation, there is a significant increase in tissue elastance in bleomycin challenged lungs ventilated with PEEP = 1 cmH<sub>2</sub>O. In the other study groups, tissue elastance remained comparably stable. In none of the study groups a relevant respiratory failure in terms of deoxygenation could be detected.

## Effects of Mechanical Ventilation on Lung Architecture

Left lungs were instillation fixed and available for qualitative and quantitative structural assessments. Additional pairs of lungs per



**FIGURE 2 |** Lung mechanical data. **(A)** Derecruitability tests at baseline: Tissue Elastance (cmH<sub>2</sub>O/ml) was measured repetitively after first recruitment maneuver for 10 times before the onset of mechanical ventilation. H1 did not differ between study groups while Hs demonstrated significant Bleomycin effects. The data show that there was no difference present before subjects were assigned to the different ventilation protocols. Mean and standard deviation of at least seven independent measurements per group are given. **(B)** Shows derecruitability tests during PEEP = 3 cmH<sub>2</sub>O ventilation after 3 h of mechanical ventilation. Hs was significantly increased in B/PEEP1 compared to the other groups, including B/PEEP5. Mean and standard deviation of at least seven independent measurements per group are given. **(C)** Compares Hs data before and after mechanical ventilation in the different study groups. A statistical significant increase was only observed in B/PEEP1. **(D)** The increase in tissue Elastance ( $\Delta H$ ) was calculated from derecruitability tests after mechanical ventilation. Compared to the other groups, a significantly larger  $\Delta H$  was observed in B/PEEP1. **(E)** The development of H1 is presented for H/PEEP1 and B/PEEP1 during mechanical ventilation. Whereas H1 increased significantly ( $p < 0.05$ ) in B/PEEP1, H1 remained stable in H/PEEP1. The same measurements are shown for H/PEEP5 and B/PEEP5 in **panel F**, where no increase can be identified in any of study groups. In **(E,F)** the mean and standard deviation of at least seven independent measurements per group are given. Statistics is based on two-way ANOVA followed by Bonferroni's *post hoc* adjustment of the *p*-value in all graphs except for C where a dependent *t*-test was used. The level of statistical significance was  $p < 0.05$ . Hs: tissue elastance at steady state (mean of last 3 tissue elastance measurement of derecruitability test), H1: first tissue elastance after recruitment,  $\Delta H = H_s - H_1$ .

study group were fixed by vascular perfusion at end-inspiration to describe microatelectases and intra-alveolar edema fluid at light microscopic level. These pathological alterations are usually not preserved in lungs fixed by airway instillation (Hsia et al., 2010; Lutz et al., 2015). Representative images of instillation fixed lungs are illustrated in **Figures 3, 4D** while images of perfusion fixed lungs are shown in **Figure 5D**. The healthy lungs, independent of ventilation pattern, did not show any evidence of increased numbers of inflammatory cells within the airspaces or the peri-bronchiolar-vascular connective tissue compartment (**Figure 3**). The interalveolar septa were not thickened and the distal airspaces were open. The bleomycin-challenged lungs which were either not mechanically ventilated or ventilated with PEEP 5 cmH<sub>2</sub>O looked very similar to the healthy lungs (**Figure 3**). In contrast, PEEP = 1 cmH<sub>2</sub>O ventilation of bleomycin-challenged lungs was characterized by more inflammatory cells within the distal airspaces as well as in the peri-bronchiolar-vascular connective tissue compartment. In addition, in some areas of lung parenchyma, the interalveolar septal walls appeared to be thickened (**Figure 3**).

Instillation fixed lungs were subjected to stereological analyses at light microscopic level. These data are presented in **Table 1** and illustrated in **Figure 4**. The total lung volume ( $V(\text{lung})$ ) was not affected by bleomycin or the mechanical ventilation pattern. On the contrary, the total volume of lung parenchyma ( $V(\text{par, lung})$ ) as well as non-parenchyma ( $V(\text{nonpar, lung})$ ) per lung demonstrated significant bleomycin effects:  $V(\text{par, lung})$  was reduced while  $V(\text{nonpar, lung})$  was increased. Within the bleomycin-treated lungs, the Bonferroni *post hoc* comparison demonstrated significantly lower  $V(\text{par, lung})$  in B/PEEP1 compared to B/No ventil ( $p = 0.047$ ). On the other hand  $V(\text{nonpar, lung})$  was largest in B/PEEP1 but no significant differences from B or B/PEEP5 were identified. The parenchyma was divided into the compartments of alveolar airspaces ( $V(\text{alv, par})$ ), ductal airspaces ( $V(\text{duct, par})$ ) and interalveolar septa ( $V(\text{sep, par})$ ). With regard to  $V(\text{alv, par})$  a significant effect of the factor “bleomycin treatment” could be identified resulting in a decrease. Within the bleomycin challenged groups a significant reduction of  $V(\text{alv, par})$  could be identified in B/PEEP1 compared to B/No ventil while no significant difference existed between B/PEEP5 and B/No ventil or B/PEEP1 (**Figure 4A**). In a further step, the alveolar surface area ( $S(\text{alv, par})$ ) within the lung was determined and this parameter was affected by both the bleomycin treatment and the mechanical ventilation pattern.  $S(\text{alv, par})$  was reduced by bleomycin pre-treatment and mechanical ventilation resulted in an additional reduction, which was most prominent in B/PEEP1. Compared to B/No ventil,  $S(\text{alv, par})$  was significantly reduced in B/PEEP1 ( $p = 0.014$ ) but also in B/PEEP5 ( $p = 0.033$ ). The arithmetic mean thickness of interalveolar septa [ $t(\text{sep})$ ] was calculated as a volume-to-surface ratio and data are illustrated in **Figure 4B**. While the bleomycin-challenge itself had a significant effect on this parameter, the Bonferroni test revealed that  $t(\text{sep})$  was significantly higher in B/PEEP1 compared to B/PEEP5 ( $p = 0.022$ ), indicating a ventilation effect on this parameter.

The different compartments of non-parenchyma were categorized into the total volumes of vessels ( $V(\text{ves, nonpar})$ ),

conducting airways ( $V(\text{airway, nonpar})$ ) and peri-bronchiolar-vascular connective tissue ( $V(\text{pbvtis, nonpar})$ ).  $V(\text{ves, nonpar})$  and  $V(\text{airway, nonpar})$  did not show any significant differences. However,  $V(\text{pbvtis, nonpar})$  was clearly effected by both the bleomycin-challenge and the mechanical ventilation pattern (**Figure 4C**). Prior to mechanical ventilation, bleomycin pre-treatment (group B/No ventil) resulted in a near doubling of  $V(\text{pbvtis, nonpar})$  compared to healthy controls (group H/No ventil). Mechanical ventilation with PEEP1 in addition to bleomycin challenge (B/PEEP1) resulted in a further increase so that  $V(\text{pbvtis, nonpar})$  became significantly larger compared to B/No ventil ( $p = 0.015$ ) but also compared to B/PEEP5 ( $p = 0.003$ ). A closer look at the peri-bronchiolar-vascular connective tissue compartment demonstrated an increased infiltration with inflammatory cells but also very prominent, enlarged lymphatic vessels in B/PEEP1 in comparison to the other study groups (**Figure 4D**). The adjacent interalveolar septa of infiltrated and thickened connective tissue cuffs around airways and vessels appeared to be thickened (**Figure 4D**). In healthy lungs, mechanical ventilation did not have any effects on the peri-bronchiolar-vascular connective tissue compartment.

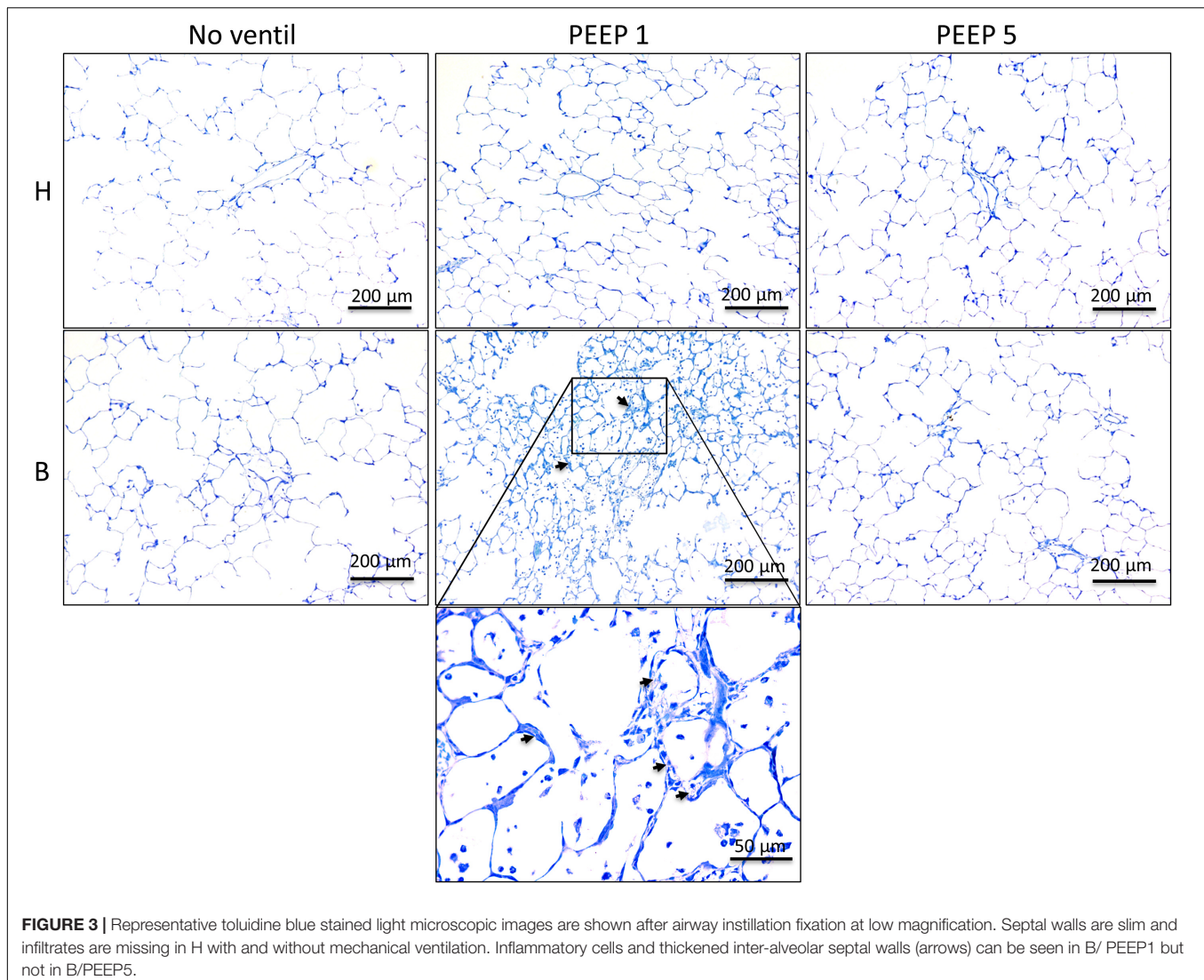
Taken together, low PEEP mechanical ventilation of bleomycin pre-treated lungs resulted in an additional decrease in the volume of alveolar airspaces and surface area of alveoli. The interalveolar septa were thickest and the total volume of peri-bronchiolar-vascular connective tissue largest in B/PEEP1.

## BAL Measurements

The right lungs were subjected to broncho-alveolar lavage. Altogether 12 ml of 0.9% NaCl solution were instilled per lung and between 10 and 11 ml were recovered. **Figures 5A–C** illustrates the data obtained from the BAL measurements. While the total numbers of alveolar macrophages and lymphocytes per BAL did not differ between the study groups (data not shown), the number of neutrophilic granulocytes was markedly increased and was influenced by both the bleomycin pre-treatment ( $p < 0.001$ ) and the mechanical ventilation pattern ( $p = 0.003$ ). No significant interaction between the factors bleomycin pre-treatment and PEEP level were observed ( $p = 0.131$ ). Within the healthy lungs, however, the mechanical ventilation did not show statistical significant differences. In bleomycin pre-treated lungs on the other hand highest numbers of neutrophilic granulocytes were found in B/PEEP1 and this was statistically significant compared to both B/No ventil and B/PEEP5 (**Figure 5A**). Hence, PEEP 1 ventilation but not PEEP 5 ventilation resulted in an additional increase in neutrophilic granulocytes after bleomycin pre-treatment.

The levels of protein (**Figure 5B**) and albumin (**Figure 5C**) were measured within the BAL as surrogate markers for leakage of the blood-gas barrier. Bleomycin pre-treatment ( $p \leq 0.001$ ) and PEEP level ( $p < 0.001$ ) had significant effects on protein and albumin levels and also demonstrated relevant interactions with regard to these parameters ( $p < 0.001$ ). Bleomycin challenge without ventilation significantly increased protein ( $p < 0.001$ ) and albumin ( $p < 0.001$ ) levels. Investigation of the effects of the ventilation pattern within the bleomycin challenged group showed elevated BAL protein in B/PEEP1 compared to both

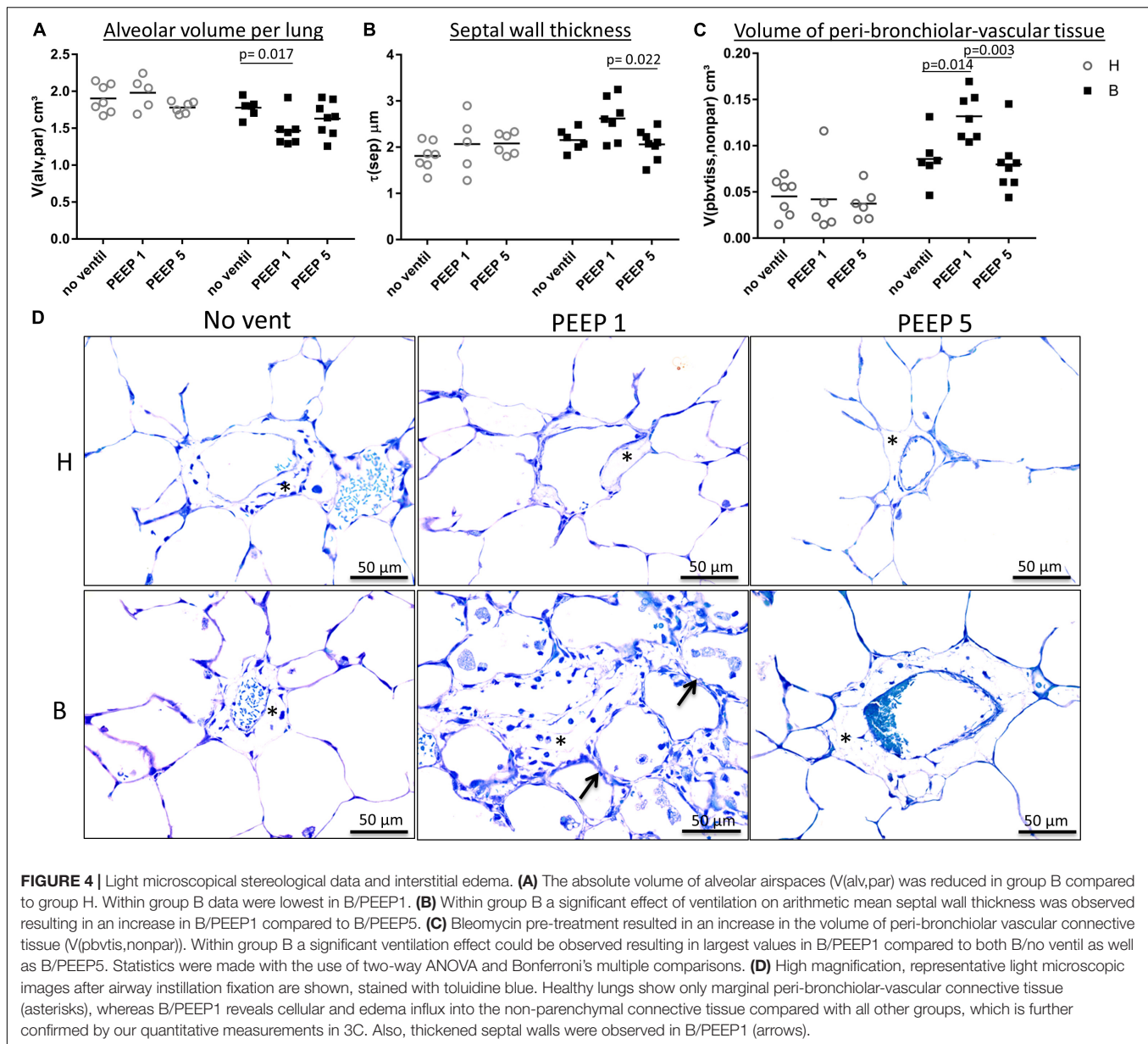




B/No ventil ( $p < 0.001$ ) and B/PEEP5 ( $p < 0.001$ ). Within the healthy lungs BAL protein trended higher in H/PEEP1 compared to H ( $p = 0.069$ ). The BAL albumin level behaved differently from the protein level (**Figure 5C**). PEEP 1 ventilation after bleomycin challenge did not result in an additional increase in albumin level so that there are no statistical differences between B and B/PEEP1. On the other hand, B/PEEP5 had significant lower albumin levels compared to B ( $p < 0.001$ ) and B/PEEP1 ( $p < 0.001$ ). Within initially healthy lungs, PEEP = 1 cmH<sub>2</sub>O ventilation resulted in a significant increase in albumin levels ( $p = 0.01$ ), a finding which could not be observed after PEEP = 5 cmH<sub>2</sub>O ventilation. Measurements of IL-6 were performed in the BAL since this parameter has been shown to correlate with the outcome in an animal model of VILI (Szabari et al., 2019). While in healthy control, the level of IL-6 was underneath the detection level, mechanical ventilation resulted in an increase which was more pronounced in H/PEEP1 [mean = 522 (SD = 238) pg/ml] than in H/PEEP5 [mean = 179 (SD = 115) pg/ml]. Bleomycin challenge resulted in measureable IL-6 levels in BAL [mean = 123 (SD = 54)

pg/ml] which increased in B/PEEP1 [mean = 779 (SD = 246) pg/ml] and B/PEEP5 [mean = 959 (SD = 739) pg/ml] groups to a similar degree.

Taken together, PEEP1 but not PEEP5 ventilation of bleomycin pre-injured lungs aggravated markers of lung injury including the number of BAL granulocytes and BAL protein level. From previous studies it is known that the volume of edema fluid one day after bleomycin-induced lung injury is increased based on electron microscopic assessments but cannot be detected at light microscopic level since the protein rich edema covering the alveolar walls is too thin and beyond light microscopic resolution (Knudsen et al., 2018). In the present study we investigated lungs at light microscopic level which were fixed during PEEP = 1 cmH<sub>2</sub>O ventilation at an end-inspiratory arrest by vascular perfusion fixation (**Figure 5D**). The goal was to identify microatelectases and intraalveolar edema fluid. Healthy lungs, independent of mechanical ventilation did not show any signs of microatelectases or intraalveolar edema. On the other hand, all bleomycin pre-treated lungs during PEEP = 1 cmH<sub>2</sub>O

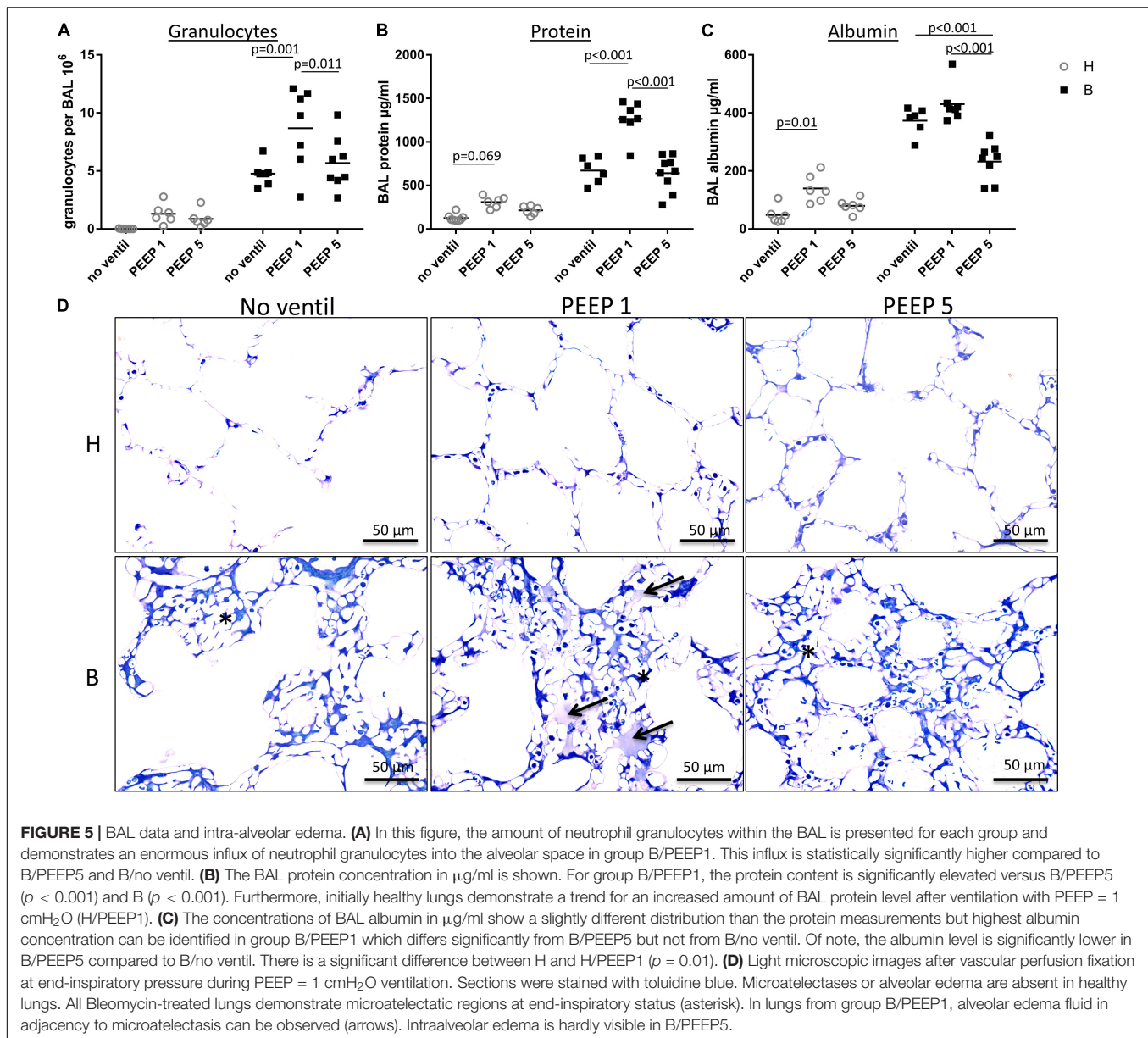


ventilation demonstrated end-inspiratory microatelectases as a common finding. No intraalveolar edema fluid could be detected in lungs after PEEP5 ventilation or those which were not mechanically ventilated. After PEEP1 ventilation, however, there were traces of intraalveolar edema fluid visible in some regions at light microscopic level and these were in general co-located with areas of microatelectases. Hence, mechanical ventilation of bleomycin pre-injured lungs with PEEP1 but not with PEEP5 seems to aggravate intraalveolar edema fluid so that it becomes clearly detectable at light microscopic level.

### Injury of the Blood-Gas Barrier

Microatelectases have been suggested to function as stress concentrators and might induce volutrauma in neighboring interalveolar septa during mechanical ventilation via alveolar

interdependence. This mechanism would result in ruptures of the cellular components of the blood-gas barrier (Cong et al., 2017) followed by leakage. Accordingly, the blood-gas barrier was investigated for ultrastructural signs of injury in the present study. Representative micrographs are provided in **Figure 6**. Signs of injury of the alveolar epithelial type 1 (AE1) cells were found in all ventilated lungs and, in addition, in unventilated bleomycin treated lungs. Except for group B/PEEP1 the injury was characterized by a swelling of AE1 cells combined with a clearing of their cytoplasmic ground substance. In group B/No ventil this was the typical ultrastructural presentation of the injury of the blood-gas barrier and more severe signs of injury were hardly present, reproducing previous observations in this animal model (Lutz et al., 2015). In B/PEEP1, however, complete denudations of the epithelial basal lamina were observed quite



frequently (Figure 6). This was accompanied by thickening of the interalveolar septa and a divergence of the formed extracellular components such as the collagen fibrils due to interstitial fluid accumulation. The degree of injured epithelial cells was quantified by determining the total surface area of the basal lamina covered by healthy or injured AE1 cells as well as AE2 cells (Figure 7). Bleomycin and the ventilation pattern had both a significant effect on the surface area covered by injured AE1 cells (Table 1). While in bleomycin pre-injured lungs the PEEP = 1  $\text{cmH}_2\text{O}$  ventilation resulted in an additional, although not significant ( $p = 0.056$ ), decrease in surface area covered by intact AE1 cells (Figure 7A) combined with an increase in surface area covered by injured AE1 cells (Figure 7B), this was not the case with PEEP = 5  $\text{cmH}_2\text{O}$  ventilation where no difference from non-ventilated bleomycin lungs were

observed. In the healthy lungs, both PEEP levels resulted in a slight, although statistically not significant increase in the surface area of injured AE1 cells. In general, the effect of bleomycin and/or mechanical ventilation on ultrastructural AE2 cell injury markers was much less pronounced compared to AE1 cells. In all study groups the ratio of injured AE2 cells to intact AE2 cells was much smaller compared to the ratio of injured AE1 cells and intact AE1 cells. Neither bleomycin nor mechanical ventilation demonstrated an effect on the surface area covered by intact AE2 cells (Figure 7C). On the other hand, bleomycin, but not the ventilation pattern, demonstrated an effect on the surface area covered by injured AE2 cells (Figure 7D). Within the group of bleomycin challenged lungs no significant differences in AE2 injury attributable to ventilation pattern were observed.



**TABLE 1** | Summarized stereological data are given as mean (standard deviation).

Parameter	H			B			Two-way ANOVA		
	No ventil	PEEP1	PEEP5	No ventil	PEEP1	PEEP5	Bleo	Vent	inter
V(lung) cm <sup>3</sup>	2.72 (0.24)	2.80 (0.29)	2.71 (0.15)	2.74 (0.17)	2.52 (0.29)	2.55 (0.27)	0.10	0.56	0.313
V(par, lung) cm <sup>3</sup>	2.47 (0.27)	2.58 (0.28)	2.53 (0.12)	2.49 (0.15)	2.16 (0.28)*	2.29 (0.23)	0.006	0.53	0.068
V(nonpar, lung) cm <sup>3</sup>	0.25 (0.1)	0.22 (0.1)	0.17 (0.04)	0.26 (0.05)	0.36 (0.08)	0.26 (0.1)	0.005	0.12	0.128
V(alv, par) cm <sup>3</sup>	1.90 (0.19)	1.98 (0.22)	1.78 (0.08)	1.78 (0.12)	1.47 (0.22)*	1.63 (0.23)	<0.001	0.15	0.027
V(duct, par) cm <sup>3</sup>	0.44 (0.08)	0.47 (0.06)	0.63 (0.07)*#	0.58 (0.07)	0.56 (0.1)	0.54 (0.09)	0.099	0.033	0.003
V(sep, par) cm <sup>3</sup>	0.12 (0.02)	0.13 (0.04)	0.12 (0.02)	0.13 (0.01)	0.14 (0.03)	0.11 (0.02)	0.779	0.151	0.379
S(alv, par) cm <sup>2</sup>	1299 (79)	1306 (120)	1191 (62)	1232 (81)	1066 (126)*	1089 (104)*	<0.001	0.009	0.089
τ(sep) μm	1.81 (0.3)	2.07 (0.63)	2.08 (0.24)	2.15 (0.24)	2.62 (0.46)	2.06 (0.32)*#	0.022	0.062	0.169
V(airway, nonpar) mm <sup>3</sup>	131 (74)	128 (32)	126 (28)	127 (22)	173 (63)	143 (48)	0.247	0.559	0.483
V(ves, nonpar) mm <sup>3</sup>	58.4 (31.7)	45.3 (46.1)	20.7 (8.7)*	42.9 (8.4)	56.0 (6.8)	40.1 (22.2)	0.536	0.057	0.17
V(pbvts, nonpar) mm <sup>3</sup>	45.2 (20.4)	42.0 (42.0)	37.5 (17.6)	85.8 (27.3)	131.9 (25.3)*	79.9 (30.2)*#	<0.001	0.041	0.058
S(AE1_intact, par) cm <sup>2</sup>	918 (274)	792 (103)	820 (192)	421 (115)	263 (92)	504 (177)*#	<0.001	0.108	0.275
S(AE1_injure, par) cm <sup>2</sup>	60 (36)	128 (93)	201 (122)	305 (79)	455 (187)*	204 (111)*#	<0.001	0.017	0.012
S(AE2_intact, par) cm <sup>2</sup>	57.4 (39.4)	41 (24)	94.2 (47.5)	24.1 (25.6)	40.6 (31.3)	125 (180)	0.951	0.083	0.647
S(AE2_injure, par) cm <sup>2</sup>	0 (0)	1.0 (2.3)	3.0 (3.5)	6.7 (6.0)	12.6 (8.7)	11.6 (13.2)	0.001	0.389	0.795

A two-way ANOVA on ranks was performed to take the factors of treatment (bleomycin effects, B vs. H) and ventilation (no ventil vs. PEEP1 vs. PEEP5) as well as their interaction (inter) into consideration. Within each treatment group (B and H) an adjustment of the p-level for multiple testing using the Bonferroni post hoc test was added. Within each group (B and H) statistical significant differences of ventilation effects are indicated as follows: \* $p < 0.05$  vs. no ventil; # $p < 0.05$  vs. PEEP1. H, healthy; B, bleomycin pre-treatment; Vent, ventilation pattern; V, volume; S, surface area;  $\tau$ , arithmetic mean thickness; par, lung parenchyma; nonpar, non-parenchyma; alv, alveolar airspace; duct, ductal airspace; sep, interalveolar septa; airway, conducting airway; ves, blood vessel; pbvts, peri-bronchiolar-vascular connective tissue; AE1, alveolar epithelial type 1 cell; AE2, alveolar epithelial type 2 cell.

Taken together, mechanical ventilation of a bleomycin pre-injured lung with a low PEEP increased the surface area of epithelial basal lamina covered by of abnormal appearing AE1 cells. This behavior could not be observed during mechanical ventilation with PEEP = 5 cmH<sub>2</sub>O.

## Cellular Stress Markers of Alveolar Epithelial Cells

*In vitro* models of increased epithelial stretch demonstrated that the integrated stress response is activated by mechanical stress of primary alveolar epithelial cells (Dolinay et al., 2017, 2018). Therefore, we performed immunohistochemical staining of p-Perk and p-EIF-2 $\alpha$  in four sections per experimental group. Staining with isotype control antibody (rabbit IgG) did not show any evidence of unspecific binding of the primary antibodies used against p-Perk or p-EIF-2 $\alpha$  (Supplementary Figure S1). Regarding p-Perk, positive cells could occasionally be detected in healthy lungs independent of whether or not the lungs were mechanically ventilated. These positive cells were predominantly found within the septal wall. After bleomycin and mechanical ventilation, alveolar epithelial p-Perk expression demonstrated a marked increase (Figure 8). p-EIF-2 $\alpha$  was not detectable in healthy lungs before or after mechanical ventilation. After bleomycin instillation, however, alveolar epithelial cells were positive for p-EIF-2 $\alpha$ . Mechanical ventilation of bleomycin-treated lungs appeared to increase the fraction of p-EIF-2 $\alpha$  positive cells particularly in and in close proximity to microatelectases (Figure 9). For quantification, the fraction of the alveolar surface area which stained positive for p-EIF-2 $\alpha$  was

determined by means of intersection counting. Since healthy lungs did not show any positive cell this investigation was only performed in bleomycin challenged experimental groups. The mean and standard deviation of the fraction of alveolar surface area covered by p-EIF-2 $\alpha$  positive cells of  $n = 4$  sections per study group were 0.23 (0.04), 0.35 (0.07), and 0.21 (0.03) for B/No ventil, B/PEEP1 and B/PEEP5, respectively. In B/PEEP1 a trend for a significantly larger surface fraction was found compared to B/No ventil ( $p = 0.055$ ).

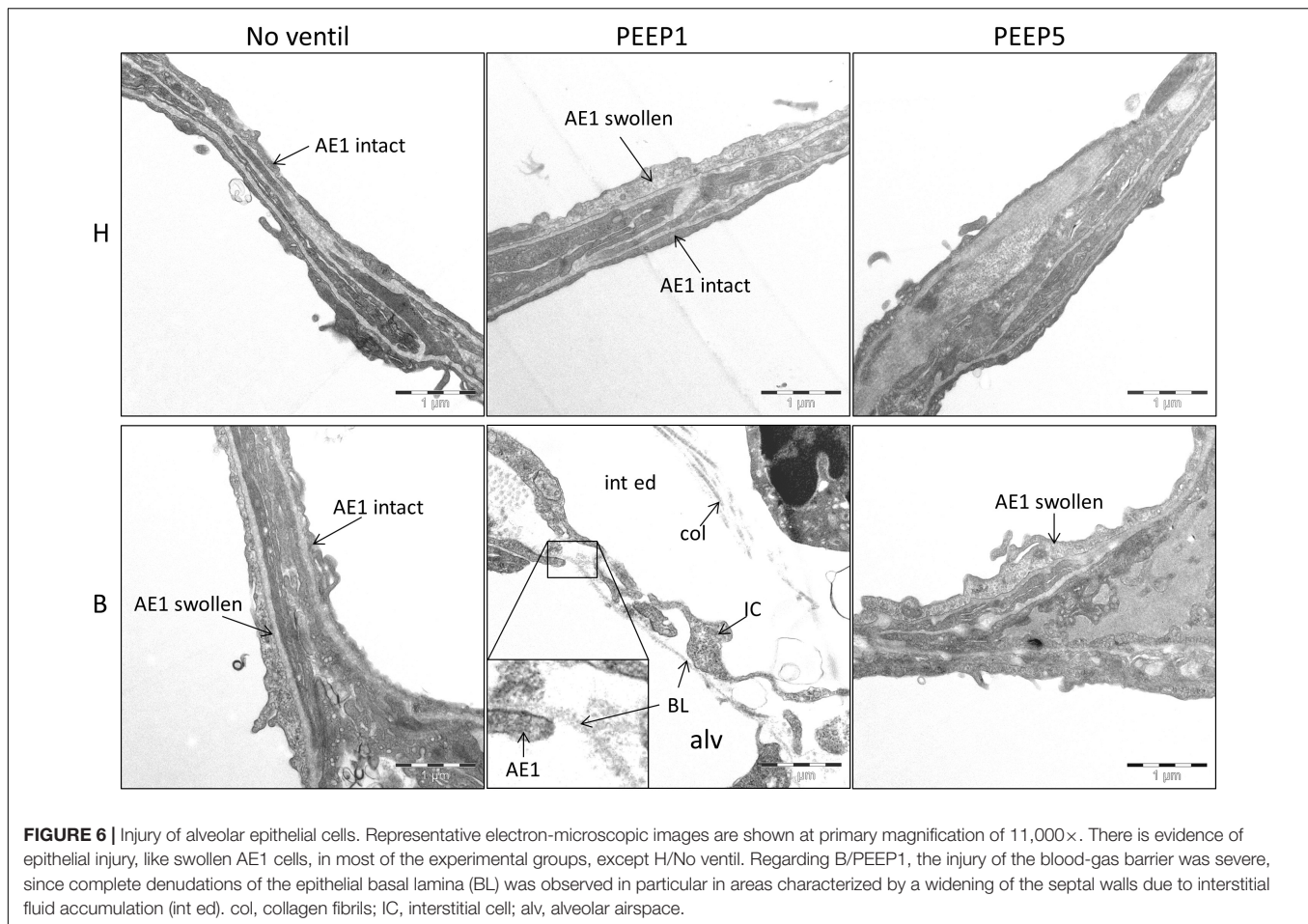
In summary, mechanical ventilation with PEEP1 increased the surface fraction of p-EIF-2 $\alpha$  positive epithelial cells by trend, a finding which correlated with the occurrence of p-Perk positive epithelial cells.

## Correlation Analyses

During mechanical ventilation with PEEP = 1 cmH<sub>2</sub>O, H1 increased with time in the bleomycin pre-treated lungs while it remained stable in the healthy lung. With the goal to investigate which abnormalities in lung structure and BAL measurements were best linked with this increase in H1, correlation analyses were performed. The total volume of peri-bronchiolar-vascular connective tissue per lung (V(pbvts, nonpar), Figure 10A), protein and albumin levels in BAL (Figure 10B), the surface area of basal lamina covered by injured alveolar epithelial cell as well the volume of alveolar airspaces (Figure 10C) demonstrated highly significant ( $p < 0.01$ ) correlations with H1 measured at PEEP = 1 cmH<sub>2</sub>O.

Hs measured at the conclusion of ventilation during PEEP = 3 cmH<sub>2</sub>O ventilation demonstrated significant correlations with





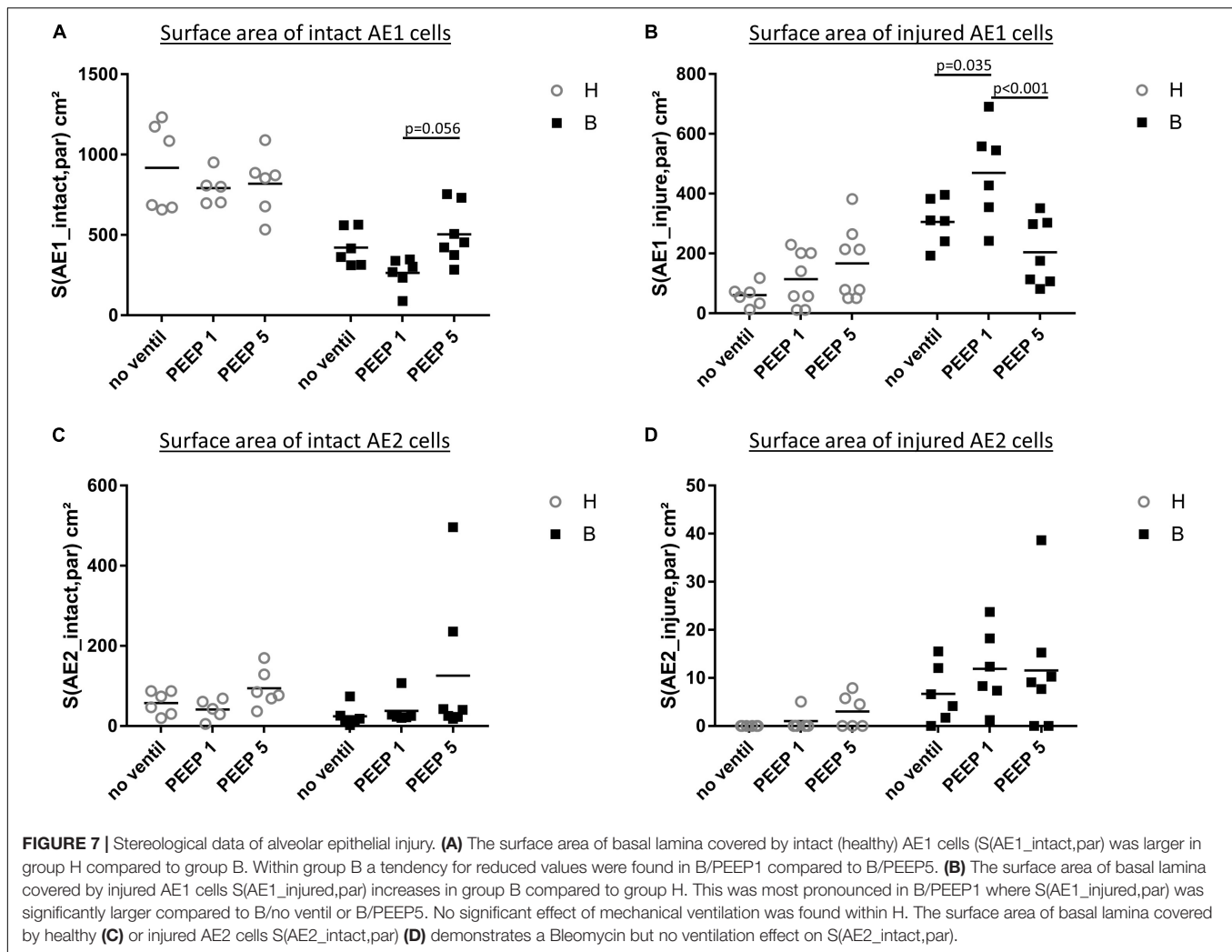
arithmetic mean thickness of septal walls [ $t(\text{sep})$ ,  $r = 0.575$ ,  $p < 0.01$ ] and peri-bronchiolar-vascular connective tissue ( $V(\text{pbvtis}, \text{par})$ , **Figure 10D**) but also the mean volume of alveolar airspaces ( $V(\text{alv}, \text{par})$ ,  $r = 0.619$ ,  $p < 0.01$ ). The most statistical correlation with Hs, however, could be established for BAL protein (**Figure 10E**) and albumin level ( $r = 0.788$ ,  $p < 0.01$ ). The increase in tissue elastance during 4.5 min of low tidal volume, PEEP = 3 cmH<sub>2</sub>O ventilation following a recruitment manoeuvre ( $\Delta H$ ) demonstrated statistically significant correlations with BAL protein (**Figure 10F**) and BAL albumin ( $r = 0.616$ ,  $p < 0.01$ ) levels only while correlations with structural data were, at best, moderate. The BAL protein or albumin level were highly correlated to the total volume of peri-bronchiolar-vascular connective tissue as well as to the surface area of the epithelial basal lamina covered by injured epithelial type I cells (data not shown).

## DISCUSSION

Abnormalities of alveolar micromechanics may not always be reflected in measurements at the organ scale such as arterial blood oxygenation or lung mechanical properties (Knudsen et al., 2018; Grune et al., 2019). On the other hand, it

has been shown that abnormal alveolar micromechanics can aggravate acute lung injury during mechanical ventilation by atelectrauma and volutrauma (Knudsen and Ochs, 2018). The mechanisms of atelectrauma and volutrauma are linked with each other via alveolar interdependence. Derecruited alveoli act as stress concentrators and could increase dynamic strain and therefore micromechanical volutrauma in adjacent, open alveoli (Mead et al., 1970; Makiyama et al., 2014; Albert et al., 2019). In healthy lungs both atelectrauma (e.g., a PEEP of 0 cmH<sub>2</sub>O) and volutrauma (e.g., high tidal volume of 30 ml/kg bodyweight) are required in combination to produce VILI in mice (Seah et al., 2011).

In the present study we tested the hypothesis whether hidden microatelectases increase VILI susceptibility during mechanical ventilation that does not harm healthy lungs. Such microatelectases have been shown to occur at end-expiratory airway pressures below 5 cmH<sub>2</sub>O in the early stage of bleomycin-induced lung injury (Knudsen et al., 2018). We termed these microatelectases one day after bleomycin instillation as “hidden” since oxygenation and tissue elastance, which represent typically available organ scale measurements during mechanical ventilation, were virtually unchanged compared to healthy controls (Knudsen et al., 2018). During mechanical ventilation of bleomycin challenged lungs with PEEP = 1 cmH<sub>2</sub>O the

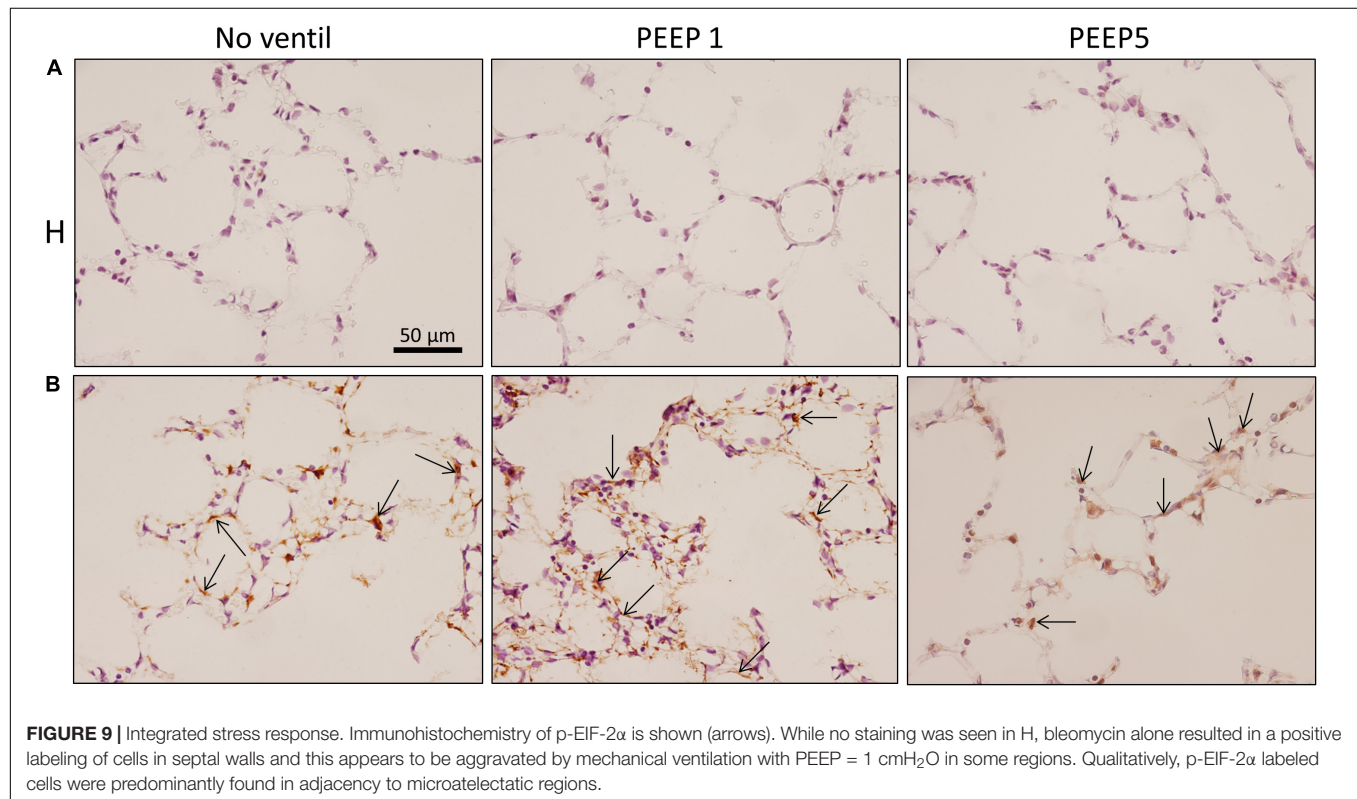
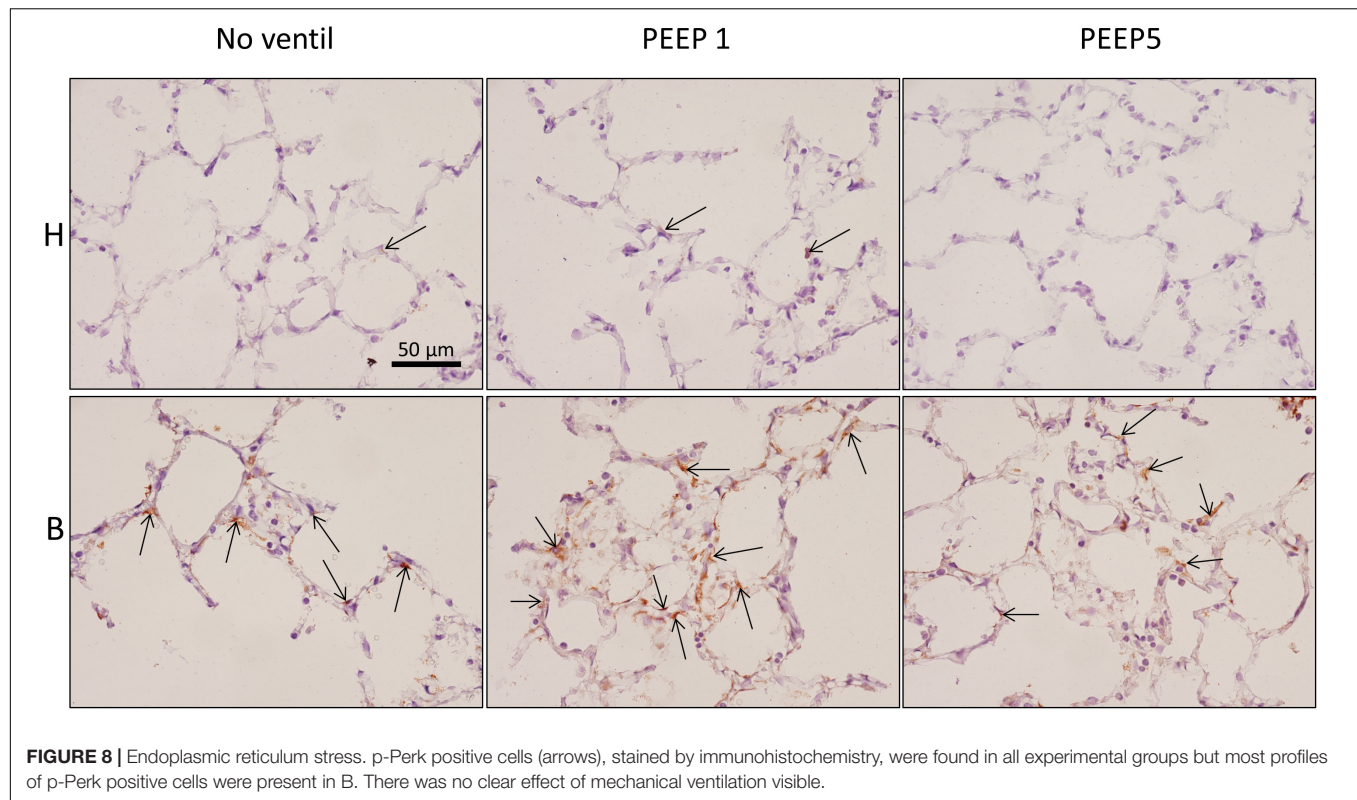


peak inspiratory pressure was at the very beginning within the range found in healthy lungs. However, with time the peak inspiratory pressure demonstrated a considerable and progressive increase in the bleomycin pre-treated lungs (Figure 1) so that the pre-existing injury became manifest at the organ level. The increase in peak inspiratory pressure could be reduced by recruitment manoeuvres and might therefore reflect the occurrence of progressive but still recruitable atelectasis during low PEEP mechanical ventilation (Allen et al., 2005).

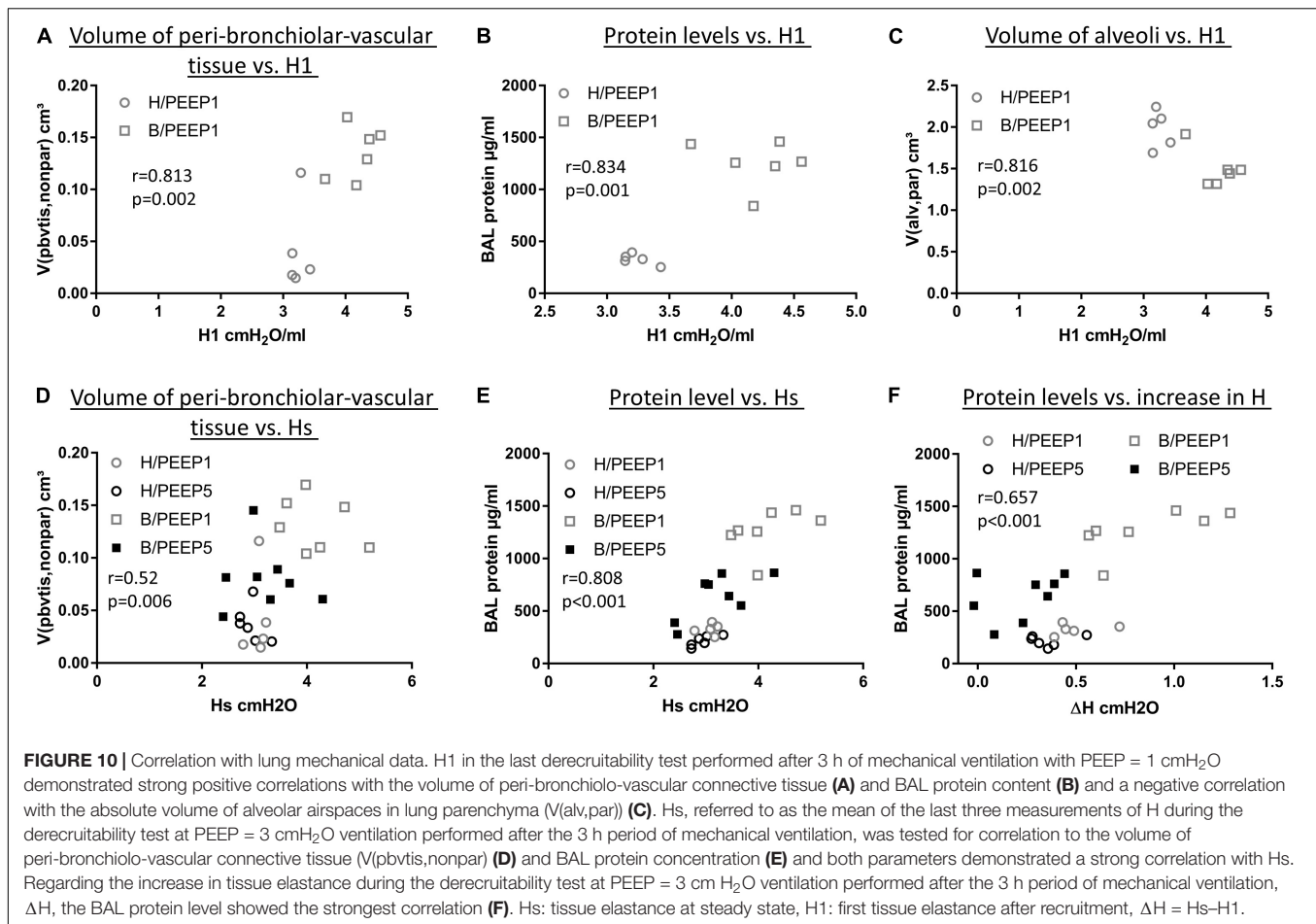
In the current study we demonstrate that the presence of microatelectases during mechanical ventilation for 3 h is linked with increased interstitial edema (Figures 4B,C), pulmonary inflammation (Figure 5A), protein levels in BAL (Figure 5B), and (based on ultrastructural criteria) injury of the alveolar epithelial cells (Figures 6, 7). This ventilation-induced exacerbation of occult injury is reflected in organ-scale lung mechanics as shown in tissue elastance during and after the 3 h period of mechanical ventilation (Figure 2). During mechanical ventilation with PEEP = 1 cmH<sub>2</sub>O in presence of microatelectases (B/PEEP1) the first tissue elastance measured 2 s after a recruitment manoeuvre (H1) is characterized by a progressive increase with ventilation

time (Figure 2E). This behavior was not observed in the lungs where we have previously not observed any microatelectases such as H/PEEP1 and B/PEEP5. Since H1 was measured immediately after recruitment it can be considered as a parameter reflecting lung mechanical properties at highest degree of recruitment and therefore components of lung injury which are not responsive to deep inflations (Massa et al., 2008; Smith et al., 2017). The increase in H1 during PEEP = 1 cmH<sub>2</sub>O ventilation was highly correlated with structural parameters reflecting interstitial edema such as the volume of peri-bronchiolar vascular connective tissue (Figure 10A).

In addition, markers reflecting pulmonary inflammation (the number of neutrophilic granulocytes per BAL) or leakage of protein into the airspace (protein and albumin levels) were highly correlated with H1 during PEEP = 1 cmH<sub>2</sub>O ventilation. The BAL data indicate progressive, protein-rich alveolar edema formation in B/PEEP1 and this is supported by qualitative light microscopical observations in lungs fixed by vascular perfusion at end-expiratory airway opening pressure of 1 cmH<sub>2</sub>O that show interposing alveolar edema within areas of microatelectases (Figure 5D). Since it has been previously shown







that protein-rich alveolar fluid accumulation in the context of high surface tension reduces the recruitability of distal airspaces (Rühl et al., 2019) it can be speculated that in the present study the progressive increase in H1 with time reflects reduced alveolar recruitment. This can be a consequence of altered alveolar lining fluid rheology and/ or progressive inactivation of pulmonary surfactant by plasma proteins (Seeger et al., 1993). In addition, increased dynamic strain of alveoli adjacent to microatelectases has also the potential to inactivate surfactant, e.g., by increased conversion from biophysically active large aggregates to inactive small aggregates (Veldhuizen et al., 1996; Albert, 2012). The increased dynamic alveolar strain might result in ruptures of the surfactant layer giving plasma proteins the opportunity to compete with the surfactant at the air-liquid interface ending up in a further destabilization of distal airspaces (Lopez-Rodriguez and Pérez-Gil, 2014).

Of note, the protein and albumin levels in the BAL fluid did not follow the same trend after mechanical ventilation of bleomycin challenged lungs. While PEEP = 1 cmH<sub>2</sub>O ventilation increased the protein level (Figure 5B) the albumin level remained roughly stable (Figure 5C). The protein level (but not the albumin level) correlated with the surface area of the epithelial basal lamina covered by injured type I alveolar epithelial cells (Figure 6B). The increase in BAL protein in B/PEEP1 can

therefore hardly be explained by leakage of albumin from the blood into the alveolar space. Based on the ultrastructural findings the endothelial cells were unaffected by the mechanical ventilation so that the barrier function on the blood side seemed to be still intact and prevented an additional leakage of albumin into the airspace. Since the protein level correlates with ultrastructural signs of injury of alveolar epithelial cells leakage of intracellular proteins into alveolar space in combination with increased inflammation appears to be an important source for protein accumulation after PEEP 1 ventilation of bleomycin pre-injured lungs.

The largest increase in tissue elastance over the observational period of 4.5 min after a recruitment manoeuvre was found in the group B/PEEP1 ( $\Delta H$ , Figure 2D). This behavior can be the consequence of an increased time-dependent derecruitment of distal airspaces (Massa et al., 2008; Smith et al., 2012) and therefore, in the context of the present study, a result of increased alveolar instability due to surfactant inactivation. The increase in  $\Delta H$  was highly correlated to the albumin and protein levels in the BAL (Figure 10E), an observation which is in line with previous observations in a VILI mouse model (Smith et al., 2017). As opposed to Hs,  $\Delta H$  demonstrated at best moderate correlations (e.g.,  $r < 0.5$ ) to structural data and this could be a consequence of the fact that  $\Delta H$  reflects the dynamic,



time-dependent alterations which have their foundation in the properties of the air-liquid interface, e.g., high surface tension or redistribution of alveolar liquid which is dependent on alveolar protein content but not represented in the stereological data. Hs, e.g., the tissue elastance under steady state conditions after recruitment manoeuvre, on the other hand is dependent on both the mechanical properties of the inter-alveolar septa (Knudsen et al., 2015) and the characteristics of the air-liquid interface (Mead, 1961).

In the current study, quantitative structural data were generated in lungs which were fixed by airway instillation at a hydrostatic pressure of 25 cmH<sub>2</sub>O. In these liquid-filled lungs the air-liquid interface has been abolished so that the effects of surface tension on lung structure, such as microatelectases or the location of intra-alveolar edema, cannot be investigated (Gil et al., 1979; Wilson and Bachofen, 1982). The fact that the volume of alveolar airspaces as well as the surface area of alveoli was significantly reduced in bleomycin injured lungs ventilated with PEEP = 1 cmH<sub>2</sub>O (**Figure 4A** and **Table 1**) indicates that the mechanical properties of the interalveolar septa were altered due to the mechanical ventilation of lungs suffering from microatelectases, independent of the surface tension at the air-liquid interface. At the electron microscopic level we observed interstitial edema at the thick side of the blood-gas barrier where the epithelial and endothelial basal laminae are separated by interstitial tissue including collagen fibrils and fibroblasts (**Figure 6**). Here, a diverging of collagen fibrils was seen. At light microscopic level this observation was linked with an increase of the mean septal wall thickness. Hence, an interstitial edema-related stiffening of the inter-alveolar septa is assumed to occur due to a disarrangement of collagen fibrils.

The presented data suggest a causal relationship between the existence of microatelectases during mechanical ventilation and the progression of VILI, although they do not provide a definite proof. This causality is supported by theoretical considerations using spring models to simulate the distribution of septal stresses and strains within a network of elastic elements (Mead et al., 1970; Makiyama et al., 2014; Albert et al., 2019). As long as the mechanical properties of the spring elements are similar the distribution of stresses and strains, and therefore the tissue deformation, is homogenous. In presence of springs with increased stiffness e.g., due to alveolar derecruitment the stresses on surrounding elements have been calculated to be increased 16-fold (Makiyama et al., 2014). Albert and co-workers simulated the strain of alveoli adjacent to derecruited alveoli and found that in dependence of the number of derecruited alveoli (which was in that model between 1 and 7) there could be an increase in septal wall strain of 30 to 50% at resting volume (Albert et al., 2019). Those predictions were in agreement with previous physiology-based, non-linear multi-compartment model simulations of mean static and dynamic alveolar strain during mechanical ventilation in bleomycin-treated rats at PEEPs where microatelectases were observed in tissue sections (Knudsen et al., 2018). Taken together, those simulations suggest that although there is no increased strain at the organ scale there might be local increased dynamic and static strain of a cohort of alveoli due to stress concentration in a lung which suffers from microatelectases (=group of derecruited alveoli).

There are several imaging studies which support the concept of the injurious potential of microatelectases creating locally increased strain via alveolar interdependence. Using functional magnetic resonance imaging (MRI) to determine the apparent diffusion coefficient (ADC), evidence for airspace overdistension in close proximity to atelectasis due to low PEEP ventilation or surfactant removal was established (Cereda et al., 2013, 2016). The ADC correlates very well with the mean linear intercept length of acinar airspaces measured at light microscopic level (Woods et al., 2006). However, the mean linear intercept length has to be interpreted with caution in terms of alveolar pathophysiology since it depends on both the dimension of the ductal and the alveolar airspaces (Knudsen et al., 2010). The use of the mean linear intercept length or ADC as a marker for alveolar or septal wall strain is therefore not appropriate and it is difficult to conclude whether or not there is injurious septal wall strain due to atelectases from those studies. Nevertheless, in spite of normal strain at the organ level, increased regional tidal strain of distal airspaces, as measured from the distribution of a tracer by means of positron emission tomography, has been shown to correlate with the degree of neutrophilic inflammation after invasive mechanical ventilation indicating induction of regional ventilation-induced lung injury (Wellman et al., 2014). Using an *ex vivo* approach and confocal microscopy to resolve individual alveolar septa, Wu and co-workers directly analyzed the effects of alveolar interdependence during mechanical ventilation by observing the interactions between an alveolus filled with protein-rich edema and a healthy alveolus (Wu et al., 2014). Although the strain at the organ scale was considered to be harmless, injury of the healthy alveolus, as measured by leakage of tracer into alveolar airspace, was induced and correlated to surface tension in the flooded alveolus (Wu et al., 2014).

Dolinay and co-workers demonstrated in a primary alveolar epithelial cell culture model that a bi-axial strain of 25%, which corresponds to ventilation with 15 ml/kg bodyweight (Tschumperlin and Margulies, 1999), the unfolded protein response is activated in a Ca<sup>2+</sup> dependent manner. These findings could be reproduced *in vivo* in a rat model ventilated with a tidal volume of 20 ml/kg bodyweight and an *ex vivo* porcine model ventilated with a tidal volume of 15 ml/kg bodyweight (Dolinay et al., 2017, 2018). The investigators suggested that a stretch-induced cytosolic increase in Ca<sup>2+</sup> concentration resulted in an autophosphorylation of Perk which in a further step phosphorylated EIF-2 $\alpha$ . By p-Perk inhibition experiments, the authors also demonstrated that this pathway was of relevance for dysfunction of the blood-gas barrier resulting in a leakage of proteins into the alveolar space. In the present study, we used immunohistochemistry to localize phosphorylated EIF-2 $\alpha$  within lung parenchyma and observed that in the healthy lung there was hardly any staining while after bleomycin challenge, approximately 23% of the alveolar surface area was covered by positive cells. While during PEEP 5 cmH<sub>2</sub>O this fraction remained roughly stable, PEEP = 1 cmH<sub>2</sub>O ventilation increased that fraction up to 35%. Of note, positive cells were predominantly observed in adjacent to microatelectases so that increased static and dynamic strain of alveoli appears to be a plausible explanation for this observation. Furthermore, this observation suggests that microatelectases

could be the spatiotemporal origin for spreading of the integrated stress response.

The present study has several limitations. Based on the functional data described in this study the bleomycin injured lungs did not develop a severe respiratory failure after 3 h of mechanical ventilation with PEEP = 1 cmH<sub>2</sub>O. The transcutaneously measured oxygen saturation did not illustrate a substantial desaturation although lung mechanical properties as well as structural and BAL parameters measurably deteriorated. Hence, long term experiments expanding the duration of mechanical ventilation to allow further worsening of lung function are necessary to embed the relevance of our observations into the context of ARDS. As an alternative the PEEP could be reduced to zero (=ZEEP). This adjustment in the experimental protocol would result in an aggravation of microatelectases (Knudsen et al., 2018) and could potentially increase the vulnerability to ventilation-induced lung injury in this animal model even with shorter periods of mechanical ventilation. Moreover, in order to monitor the mechanical ventilation we used the oxygen saturation which demonstrated for all study groups under the given conditions sufficient gas exchange. However, we did not monitor arterial partial pressure of CO<sub>2</sub>, bicarbonate and pH during mechanical ventilation which would have provided an additional assessment of ventilation adequacy. While the measured oxygen saturation at room air makes a relevant hypoventilation unlikely we cannot exclude a hyperventilation with subsequent respiratory alkalosis which as such might have had an impact on our read-out parameters. However, the volumes of ventilated air per minute were comparable between the different PEEP levels and study groups (900 ml/min/kg bodyweight). Based on ultrastructural criteria, we quantified the degree of injury of the alveolar epithelial cells in lungs fixed by airway instillation and observed that after bleomycin challenge without mechanical ventilation approximately 42% of the epithelial basal lamina was covered by cells which showed ultrastructural criteria for injury. Using exactly the same stereological approach for quantification of alveolar epithelial injury (Lutz et al., 2015) used lung tissue fixed via vascular perfusion and found one day after bleomycin instillation a surface fraction of injured alveolar epithelium of 27%. Hence, the route of fixation might have had an impact on this parameter in a way that airway instillation of the fixative e.g., via fluid-induced shear stress aggravated the ultrastructural signs of epithelial injury in the present study.

In conclusion, we could demonstrate that bleomycin-induced microatelectases, which are hard to detect using organ-scale lung mechanical and functional data, are linked with an increased susceptibility for VILI during ventilation with tidal volumes that are not injurious to the initially healthy lung. Through the mechanism of alveolar interdependence these microatelectases might elevate local septal strains (in absence of abnormal strain at the organ-scale) to cause volutrauma of adjacent open alveoli which is characterized by progressive injury of the blood-gas barrier, reduced recruitability, and increased instability of distal airspaces. The role of the activated integrated stress response in the tethering-induced expansion

of microatelectases and the progression of VILI warrants further investigation.

## DATA AVAILABILITY STATEMENT

All datasets generated for this study are included in the article/**Supplementary Material**. The original virtual microscopic slides which were investigated in this study are also available as a repository under the first reference in the reference list: Albert et al. (2020).

## ETHICS STATEMENT

The animal study was reviewed and approved by Niedersächsisches Landesamt für Verbraucherschutz und Lebensmittelsicherheit (LAVES, Oldenburg, Lower Saxony, Germany, approval number 17/2068).

## AUTHOR CONTRIBUTIONS

KA contributed to the conception and design, acquisition of data, analysis and interpretation of data, drafting and revising of the manuscript. J-MK contributed to the conception and design, acquisition of data, analyses and interpretation of data, revising of the manuscript. AP contributed to the conception and design, analysis and interpretation of data, revising of the manuscript. SW contributed to the conception and design, acquisition, analysis and interpretation of data, revising of the manuscript. EL-R contributed to the conception and design, analysis and interpretation of data, revising of the manuscript. AB contributed to the conception and design, analysis and interpretation of data, revising of the manuscript. BS contributed to the conception and design, analysis and interpretation of data, drafting and revising of the manuscript. LK contributed to the conception and design, acquisition of data, analysis and interpretation of data, drafting and revising of the manuscript.

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## SUPPLEMENTARY MATERIAL

The Supplementary Material for this article can be found online at: <https://www.frontiersin.org/articles/10.3389/fphys.2020.530485/full#supplementary-material>

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# Modeling Lung Derecruitment in VILI Due to Fluid-Occlusion: The Role of Emergent Behavior

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Ventilator-induced lung injury (VILI) is driven by the processes of volutrauma and atelectrauma, which can act synergistically to compromise the blood-gas barrier. We have postulated that this synergy arises through a rich-get-richer mechanism whereby atelectrauma causes holes to form in the blood-gas barrier while concomitant volutrauma causes susceptible holes to progressively enlarge as VILI worsens. We previously developed an analytical model based on this idea that accurately predicts the progressive increases in lung elastance seen immediately following a recruitment maneuver as VILI progresses over the course of hours. In the present study we extend this model to account for the rate of change of elastance, due to closure of lung units, in the minutes following a recruitment maneuver. We found that the distribution of unit closing velocities throughout the lung can be described by a power law with an exponent of  $-2$  that matches previously published power laws associated with the dynamics of lung recruitment. Our model thus reveals lung collapse as an example of emergent complex behavior and links the dynamics of altered function in the injured lung to structural damage in a way that explains the mechanisms of injury progression arising from the ongoing stresses and strains applied by mechanical ventilation.

**Keywords:** acute lung injury, analytical model, alveolar flooding, surface tension, lung elastance

## INTRODUCTION

Mechanical ventilation plays a major role in critical care, providing life support to patients in respiratory failure. However, because of the stresses and strains it imposes on the tissues of the lung, mechanical ventilation can also cause ventilator-induced lung injury (VILI) (Dos Santos and Slutsky, 2000; Gattinoni et al., 2003; Slutsky and Ranieri, 2013). The two principle injury mechanisms of VILI are over-distension of the tissues that gives rise to volutrauma, and cyclic recruitment and derecruitment of lung units that gives rise to atelectrauma (Parker et al., 1993; Dreyfuss and Saumon, 1998). Volutrauma and atelectrauma are both involved in compromising the blood-bas barrier of the lung, which allows plasma-derived fluid and proteins to leak into the airspaces. This disrupts surfactant function, which then decreases lung compliance and thus increases the tissue stresses associated with mechanical ventilation, making the leak worse. At the same time, the lung becomes progressively more derecruited, which places the remaining open lung regions at greater risk of over-distension

(Gattinoni and Pesenti, 2006; Gattinoni et al., 2016). Patients with pre-existing lung injury, particularly acute respiratory system distress syndrome (ARDS), are highly susceptible to VILI (Slutsky and Ranieri, 2000; Dreyfuss and Hubmayr, 2016). Various ventilation strategies have been proposed to manage ARDS and prevent VILI, but once underway it is difficult to break out of the vicious cycle of progressing injury (Slutsky and Ranieri, 2013).

We have shown in a number of studies in mice (Seah et al., 2011; Smith et al., 2013, 2017) that the nature and degree of lung injury is reflected in what we term the *derecruitability* of the lung. Derecruitability is measured by applying a recruitment maneuver (deep inflation) to maximally open closed airspaces followed immediately by a period (typically 3 min) of mechanical ventilation at a designated tidal volume ( $V_t$ ) and level of positive end-expiratory pressure (PEEP). Lung stiffness ( $H$ ) rises progressively during the ventilation period to a degree that is modest (perhaps 20%) in a normal lung, but is dramatically enhanced in the injured lung to an extent that reflects the degree of injury (Smith et al., 2013). Some of the post-recruitment increase in  $H$  in the normal lung likely reflects changes in surface tension arising from the dynamics of surfactant at the air-liquid interface and viscoelastic adaptation of tissue stress, but the highly exaggerated increases in  $H$  seen in the injured lung are largely the result of progressive derecruitment of airspaces (Massa et al., 2008; Smith et al., 2017; Hamlington et al., 2018b).

We denote as  $D_{\text{rate}}$  the mean rate of increase in  $H$  over the 3 min following recruitment, while  $H_1$  is the first measurement of  $H$  made immediately after recruitment (Smith and Bates, 2013; Smith et al., 2013). Both  $D_{\text{rate}}$  and  $H_1$  increase with the severity of lung injury, but they do not mirror each other exactly.  $D_{\text{rate}}$  quantifies derecruitment dynamics that manifest over a timescale of minutes, probably reflecting instabilities in the fluid layer lining the small airways and alveoli (Smith et al., 2013).  $H_1$ , on the other hand, quantifies either much more rapid derecruitment phenomena or an inability to recruit at all, more likely explicable on the basis of rapid alveolar flooding by accumulated edema fluid and/or unstable collapse of lung units caused by high surface tension in the air-liquid interface (Smith et al., 2013).  $D_{\text{rate}}$  and  $H_1$  together thus comprise a pair of sensitive biomarkers of lung injury (Smith et al., 2013).

We have previously shown in mice that, as VILI develops, the time-course of  $H_1$  can be accurately accounted for in terms of the accumulated leak of plasma-derived material through holes in the blood-gas barrier (Mori et al., 2018). These holes appear to be generated by both atelectrauma and volutrauma acting synergistically in a rich-get-richer fashion (Hamlington et al., 2018a). The rate of accumulation of edema in the airspaces, and thus the displacement of air that results, is a function of the number and sizes of these holes, both of which increase with time during injurious mechanical ventilation. In the present study, we extend this analysis to  $D_{\text{rate}}$  in order to establish a consistent theory of derecruitability of the injured lung that links both  $H_1$  and  $D_{\text{rate}}$  to the biophysical processes taking place during the development of VILI.

## MATERIALS AND METHODS

### Model Development

In the following model development we take a similar analytical approach to our previous study of the dependence of  $H_1$  on degree of lung injury, this time focusing on the complementary parameter  $D_{\text{rate}}$ . To account for the progressive increase in  $D_{\text{rate}}$  that accompanies the development of VILI, it is necessary to model events taking place over two different scales of time. The longer time scale, on the order of minutes to hours, concerns the progression of VILI itself. The shorter time scale, on the order of seconds to minutes, involves the dynamic recruitment and derecruitment of alveoli and small airways that are reflected in our periodic assessments of VILI. In order to avoid ambiguity between these two time scales in the following mathematical development, events taking place over the shorter time scale (seconds to a few minutes) will be referenced to time denoted by  $\tau$  while events taking place over the longer time scale (many minutes to hours) will be referenced to time denoted by  $t$ .

We first consider the short time-scale assessment of VILI, which is based on the computational model of recruitment/derecruitment dynamics proposed by Bates and Irvin (2002) consisting of a parallel distribution of lung units. Each unit has its own airway to which is applied the same pressure. The units open and close according to their randomly assigned critical opening and closing airway pressures ( $P_o$  and  $P_c$ , respectively). These pressures are drawn from probability distribution  $f_{P_o}(P_o)$  and  $f_{P_c}(P_c)$ , respectively. However, a unit does not necessarily open or close as soon as it traverses its particular value of either  $P_o$  or  $P_c$ . Rather, a latency is built into the process by associating with each unit a *virtual trajectory* variable  $x$  that can assume any value between 0 (corresponding to the unit being definitively closed) and 1 (definitively open). An open unit remains open until  $x = 0$ , while a closed unit remains closed until  $x = 1$ . Movement of  $x$  along the virtual trajectory occurs to the right (i.e., toward increasing values of  $x$ ) when  $P > P_o$ , and to the left when  $P < P_c$ , with the rate of change  $x$  being proportional to the amount by which  $P$  either exceeds  $P_o$  or is less than  $P_c$ . The constants of proportionality that determine the velocity of  $x$  rightward and leftward are  $s_0$  and  $s_c$ , respectively. That is,

$$\begin{aligned}\frac{dx}{d\tau} &= (P - P_o) s_0; \quad \text{for } P \geq P_o \\ &= (P - P_c) s_c; \quad \text{for } P \leq P_c \\ &= 0; \quad \text{for } P_c < P < P_o\end{aligned}\quad (1)$$

where  $0 \leq x < 1$ . The velocity constants  $s_0$  and  $s_c$  for each unit are drawn from probability distributions  $f_{s_0}(s_0)$  and  $f_{s_c}(s_c)$ , respectively.

Following the original model (Bates and Irvin, 2002), we assume that  $P_o$  and  $P_c$  are distributed according to Gaussians with variances  $\sigma_0$  and  $\sigma_c$ , and means  $\mu_0$  and  $\mu_c$ , respectively. In accord with the findings of Massa et al. (2008) in acid-injured mice, we set the two variances to be equal (i.e.,  $\sigma_0 = \sigma_c = \sigma$ ) and the two

means separated by  $\delta P$  such that the opening pressures are greater than the closing pressures (i.e.,  $\mu_0 = \mu_c + \delta P$ )

$$f_{P_c}(P_c) = \frac{1}{\sigma\sqrt{2\pi}} e^{-\frac{1}{2}\left(\frac{P_c - \mu_c}{\sigma}\right)^2} \quad (2)$$

and

$$f_{P_o}(P_o) = \frac{1}{\sigma\sqrt{2\pi}} e^{-\frac{1}{2}\left(\frac{P_o - \mu_c - \delta P}{\sigma}\right)^2} \quad (3)$$

We assume that  $\sigma$  and  $\delta P$  do not change with increasing injury, so the progression of VILI is reflected entirely in the way that  $\mu_c$  increases with time.

The velocity distributions  $f_{s_o}(s_o)$  and  $f_{s_c}(s_c)$  were originally specified on purely empirical grounds as conforming to hyperbolic functions (Bates and Irvin, 2002), motivated by the ubiquitous appearance of such functions in naturally occurring complex systems (West, 1990; Robertson et al., 2000; West et al., 2000). Solving the model analytically using such functions is not possible, however, because hyperbolas are not finite-integrable over  $s \in (0, \infty)$ , but finite integrals can be obtained by having the exponent of the power law be different from unity and by specifying a small positive lower limit,  $s_m$ , for integration. Accordingly, we set

$$f_{s_c}(s_c) = \frac{\alpha - 1}{s_m} \left(\frac{s_c}{s_m}\right)^{-\alpha} \quad (4)$$

where  $0 < s_m < s_c < \infty$  and  $\alpha > 1$ .

When modeling how the fraction of closed lung,  $F_{\text{closed}}$ , changes during a derecruitment test, we avoid having to consider  $f_{s_o}(s_o)$  specifically by assuming, as did Albert et al. (2009), that it is only derecruitment that takes place to any significant extent during the 3 min following a recruitment maneuver. That is, we assume that the fully recruited lung derecruits progressively during these 3 min as if exposed to an effective pressure,  $P_{\text{derecruit}}$ , that is fixed throughout the breath and that reflects the mean airway pressure applied by the mechanical ventilator.  $P_{\text{derecruit}}$  is determined by the applied level of PEEP plus some positive  $\Delta P$  that depends on the ventilation regimen that is applied on top of the PEEP. As the lung becomes progressively more injured, and thus stiffer, mean airway pressure increases. This pressure increase is offset to some extent, however, by the compliance of the gas in the piston and connecting tubing of the flexiVent ventilator (Scireq, Montreal, Canada) that was used to collect the experimental data. While the effect of this compliance on calculation of  $H$  was compensated for digitally (Schuessler and Bates, 1995), it still absorbed an increasing fraction of the pressure increases as the lung stiffened (Smith et al., 2013). Mean airway pressure also increases somewhat over the course of a single derecruitment test. However, in order to obtain an analytical solution to our model we assumed that  $P_{\text{derecruit}}$  remains unchanged over each of the 3 min derecruitment maneuvers. This is clearly not precisely the case, but we take it to be a reasonable first-order approximation since tidal volume is quite low during the tests.

For a unit to have the possibility of closing during a derecruitment test it must therefore satisfy the condition  $P_c >$

$P_{\text{derecruit}}$ . Whether or not a particular unit actually closes during the test, however, depends on whether it moves along its virtual trajectory rapidly enough for  $x$  to reach a value of 0 before the 3 min test is complete and that there is no significant retrograde motion of  $x$  during the inspiratory portions of the test. If the duration of the test were to continue indefinitely, the asymptotic value to which  $F_{\text{closed}}$  would tend is that which satisfies the above condition, which is

$$F_{\text{closed}}(\infty) = \int_{P_{\text{derecruit}}}^{\infty} \left[ \frac{1}{\sigma\sqrt{2\pi}} e^{-\frac{1}{2}\left(\frac{P_c - \mu_c}{\sigma}\right)^2} \right] dP_c \quad (5)$$

This situation is never actually achieved, of course, because the derecruitment test is terminated after 3 min.

We assume that the recruitment maneuver establishes an initial condition for which all units open and are positioned at  $x = 1$  along their respective virtual trajectories. As derecruitment proceeds during the test, the various units in the model close sequentially. The time,  $\tau$ , at which a given unit closes is determined by how quickly it traverses the length of its virtual trajectory from  $x = 1$  to  $x = 0$ , which is given by

$$\tau = \frac{1}{s_c |P_{\text{derecruit}} - P_c|} \quad (6)$$

which means that the units that have closed by time  $\tau$  are those that have closing pressures satisfying  $\frac{1}{\tau(P_c - P)} < s_c$ . Assuming, as did Albert et al. (2009), that  $f_{P_c}(P_c)$  and  $f_{s_c}(s_c)$  are statistically independent,  $F_{\text{closed}}(P, \tau)$  is given by

$$F_{\text{closed}}(P, \tau) = \int_P^{\infty} \int_{[(P_c - P)\tau]^{-1}}^{\infty} \frac{1}{\sigma\sqrt{2\pi}} e^{-\frac{1}{2}\left(\frac{P_c - \mu_c}{\sigma}\right)^2} \cdot \frac{\alpha - 1}{s_m} \left(\frac{s_c}{s_m}\right)^{-\alpha} dP_c ds_c \quad (7)$$

A detailed step-by-step solution of Eq. 7 is presented in the **Supplementary Material**.

Solving Eq. 7 we find that  $\alpha = 2$  and Eq. 4 of thus becomes

$$f_{s_c}(s_c) = \frac{1}{s_m} \left(\frac{s_c}{s_m}\right)^{-2} \quad (8)$$

Massa et al. (2008) found  $\sigma = 3$  in mice with acute lung injury caused by hydrochloric acid instillation. Smith et al. (2013) found  $\mu_c(t) = kt$ , where  $k$  is a constant, in injuriously ventilated mice. Since PEEP is zero and  $H$  is measured using small-amplitude perturbations in lung volume, we assume that  $P = 0$  to a first approximation (Mori et al., 2018).  $D_{\text{rate}}$  can thus be written as:

$$D_{\text{rate}}(t) = \frac{H_1(t) s_m}{\sqrt{2\pi}} \left[ \sqrt{\frac{\pi}{2}} 3kt \left( \text{erf}\left(\frac{kt}{3\sqrt{2}}\right) + 1 \right) + 9e^{-\frac{1}{2}\left(\frac{kt}{3}\right)^2} \right] \quad (9)$$

From our previous proposed model (Mori et al., 2018) we can relate Eq. 9 to  $H_1$  when  $t$  is sufficiently large:

$$\lim_{t \rightarrow \infty} D_{\text{rate}}(t) = 3ks_m \frac{1}{\sqrt{a}} \left( H_1(t) - \frac{H_0}{2} \right) \quad (10)$$

## Experimental Data

We tested the predictions of the above model against a set of data collected in mice and published previously (Smith et al., 2013). A detailed description of the experimental method used, as well as animals ethics approval, are given in this previous publication. Briefly, healthy 8- to 10-week-old female BALB/c mice (18.3–24.4 g) were anesthetized with 90 mg/kg intraperitoneal sodium pentobarbital and then connected to a computer-controlled mechanical ventilator (flexiVent, Scireq, Montreal, Canada). Following paralysis (0.5 ml/kg IP injection of pancuronium bromide) animals received a 21 min protocol starting with 16.5 min of injurious ventilation delivered at zero PEEP with a very large  $V_t$  (1.0, 1.1, 1.2, and 1.3 ml in 4 different groups of animals) followed by a derecruitability test (4.5 min protocol consisting of a deep inflation followed by ventilation at zero PEEP with  $V_t = 0.25$  ml during which elastance was measured every 20 s). This 21 min protocol was repeated continuously for 4 h or until the animal died. The way that the lungs derecruit over time during the derecruitment test is reflected in the way that  $H$  increases with time (Allen and Bates, 2004). Finally, the resulting estimations of  $D_{\text{rate}}$  from the derecruitability tests were fitted to Eq. 15, and the 95% joint confidence regions for  $s_m$  and  $k$  were determined as described by Mori et al. (2018).

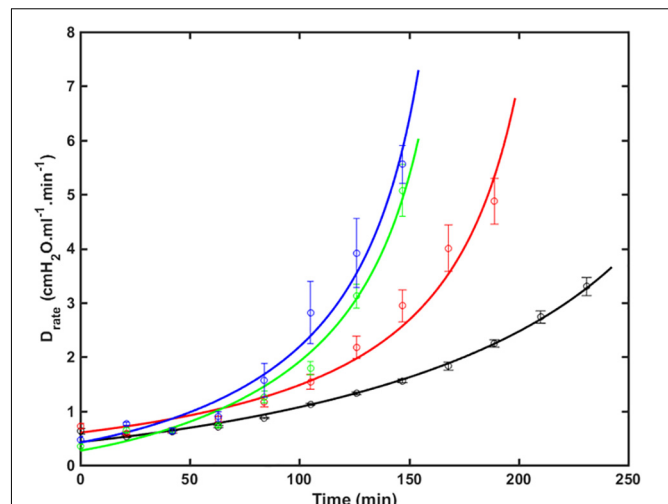
It should be pointed out that we also measured parameters related to the resistance of both the conducting airways and the respiratory system tissues in these mice. We focus here exclusively on the elastance parameter  $H$  in our model because it scales inversely with the fraction of lung that remains open, provided intrinsic tissue stiffness does not change, thus serving as a convenient biomarker of derecruitment. Lung tissue resistance scales similarly to elastance (Smith et al., 2020) and therefore adds no new information, so we did not include it in our model. Airway resistance tends to correlate less well with lung derecruitment because the proximal branches of the airway tree, which contribute much to airway resistance, mostly remain patent even when significant portions of the lung periphery derecruit (Smith et al., 2020).

## Model Fitting

The model described by Eq. 9 was fit to the elastance data versus time collected within each derecruitment maneuver with MATLAB (The Mathworks, Natick, MA, United States) using a non-linear least squares method (trust-region algorithm) for each animal individually in all 4 groups, resulting in a pair of values of  $s_m$  and  $k$  for each animal. The maximum number of evaluations and iterations were set to 600 and 400, respectively, and the termination tolerance value of the cost function (mean squared residual) was  $10^{-6}$ . Finally, the 95% joint confidence regions for  $s_m$  and  $k$  were determined as described by Mori et al. (2018).

## RESULTS

**Figure 1** shows the fits of Eq. 9 to experimental data from four groups of over-ventilated mice ( $V_t = 1.0, 1.1, 1.2$ , and  $1.3$  ml, with zero PEEP), together with the experimental data. The model fits



**FIGURE 1** |  $D_{\text{rate}}$  (average  $\pm$  SE) versus time as VILI developed in the 4 groups of mice (symbols) together with the model fits to Eq. 9 (lines). Black:  $V_t = 1.0$  ml (RMSE = 0.35); Red:  $V_t = 1.1$  ml (RMSE = 0.64); Green:  $V_t = 1.2$  ml (RMSE = 0.36); Blue:  $V_t = 1.3$  ml (RMSE = 0.65). The data were collected in a previous study (Smith et al., 2013) (RMSE – root mean squared residual.).

pass within one standard error either side of the data points in most cases, and are very close to these ranges in the other cases. The  $R^2$  values for all fits were greater than 0.85. This demonstrates that the model accurately accounts for the way that injury, as reflected by  $H$ , accelerates over time and how this acceleration increases with increasing  $V_t$ .

**Figure 2** shows the two model parameters in Eq. 9,  $s_m$  and  $k$ , versus  $V_t$ . There was no dependence of  $s_m$  on  $V_t$  by ANOVA ( $p = 0.11$ , **Figure 2A**), whereas  $k$  was significantly greater for the lungs exposed to the two higher  $V_t$  compared to the two lower  $V_t$  ( $p < 0.001$ , **Figure 2B**). Normality of the distributions of all parameter groups was supported by the Shapiro-Wilk test ( $p > 0.05$ ). The Bonferroni *post hoc* test was performed to assess inter-groups differences for  $k$ . All statistical tests were performed in MATLAB 2019b (The Mathworks, Natick, MA, United States).

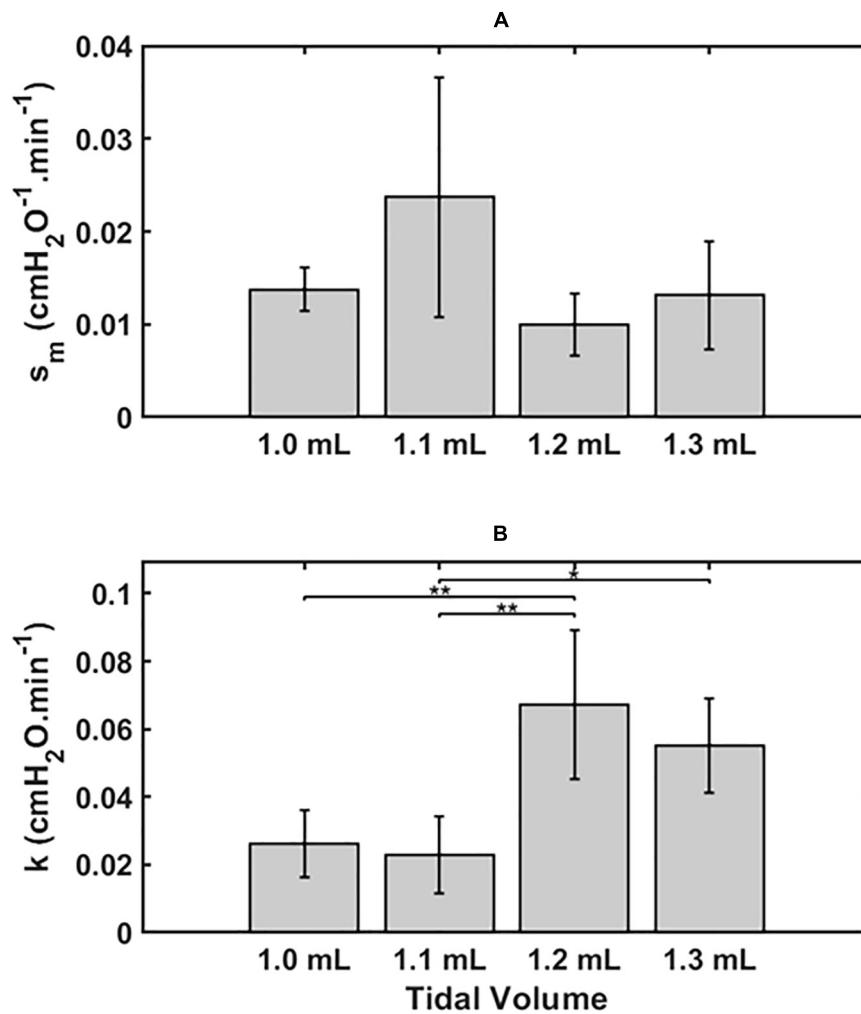
The joint 95% confidence intervals show clean separation between the parameter pairs for the four groups of mice (**Figure 3**).

**Figure 4** shows plots of  $D_{\text{rate}}(t)$  versus  $H_1$  for all animals studied. Also shown are the model predictions of  $D_{\text{rate}}(t)$  from Eq. 9 versus  $H_1$  calculated according to Mori et al. (2018). Lastly, **Figure 5** shows, in a Bland-Altman plot, the difference between modeled and measured  $D_{\text{rate}}$  values as a function of  $H_1$ .

## DISCUSSION

We have developed an analytical model of the time-course of derecruitment in the injured lung that mimics observations of how lung derecruitability evolves during the development of VILI. This analytical model is based on our previous numerical approach of ascribing recruitment and derecruitment dynamics



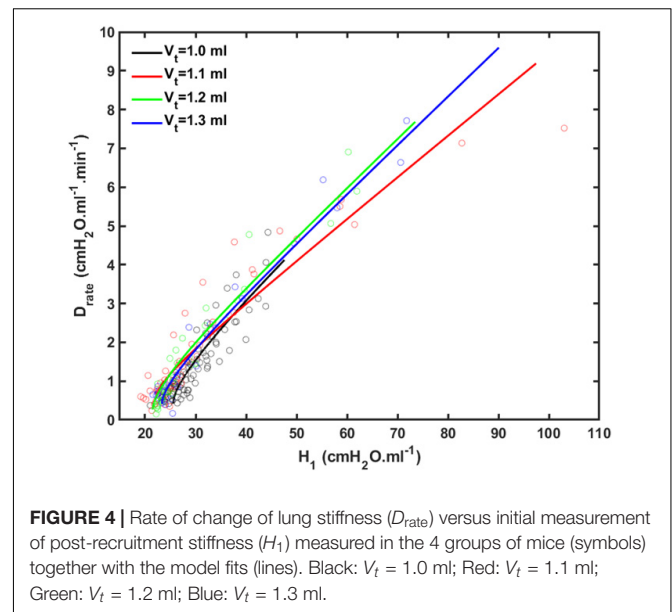
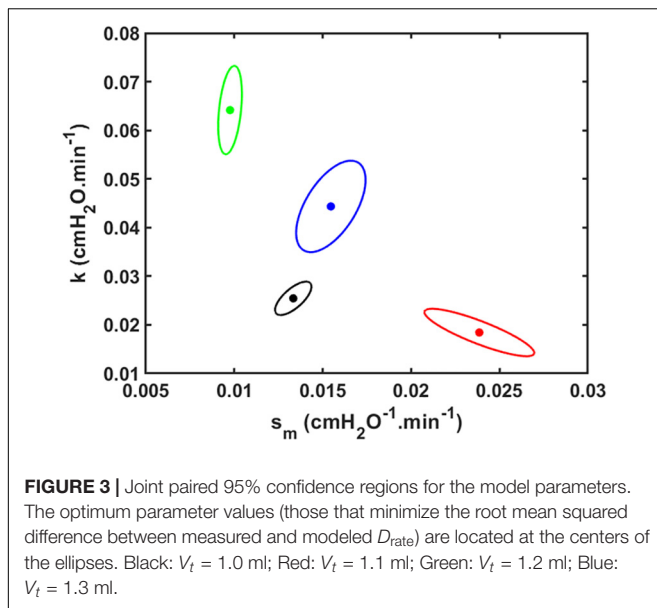


**FIGURE 2** | Mean  $\pm$  2 SEM for the two key model parameters  $s_m$  (A) and  $k$  (B) and for the 4 groups, 1.0 ml ( $n = 6$ ), 1.1 ml ( $n = 6$ ), 1.2 ml ( $n = 5$ ) and 1.3 ml ( $n = 4$ ). Statistically significant differences between groups are indicated by: \* $P < 0.05$ , \*\* $P < 0.01$ .

to the behavior of a virtual trajectory associated with various lung units (Bates and Irvin, 2002; Massa et al., 2008). This model uses a similar analytic approach to our recent study that examined how  $H$  measured immediately after a recruitment maneuver ( $H_1$ ) increases as a function of worsening lung injury (Mori et al., 2018). In this sense, the present study complements our previous model analysis since together they provide a complete analytic description of how a deep inflation of the injured lung recruits closed lung units and then how these units derecruit again over time as governed by the values of the three fixed parameters  $\alpha$ ,  $s_m$ , and  $k$ , where  $\alpha$  and  $k$  depend on  $V_t$ . The model of the present study accurately predicts the manner in which the temporal evolution of  $D_{rate}$  varies with both time and injurious  $V_t$  (Figure 1), dependencies that are embodied in a single parameter,  $k$ , thought to largely reflect how surface tension increases with time (Figure 2). Surface tension elevation is a consequence of surfactant dysfunction, itself caused either by direct damage to the surfactant or by the presence of material that has leaked from

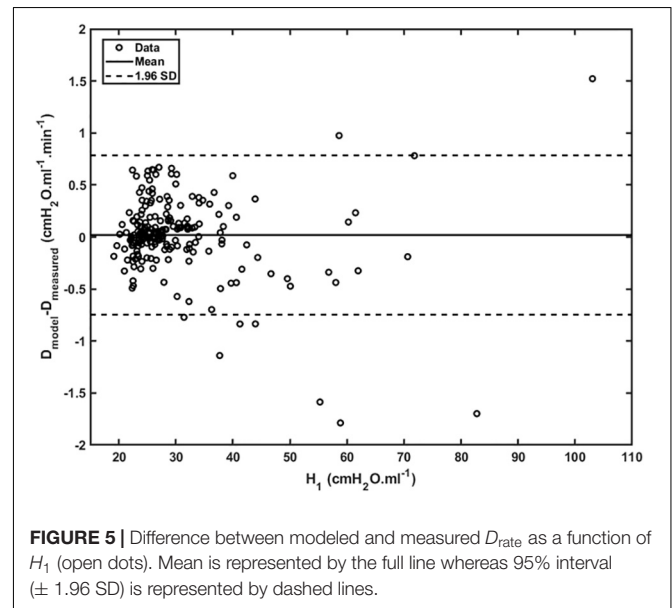
the vasculature into the airspaces of the lung.  $H$  can also increase as a result of accumulated fluid that floods alveoli. This model thus links developments in physical injury of the parenchyma tissue to the dynamics of lung function derangement via the physiologic mechanism of airspace derecruitment.

Analytical models generally do not have the same flexibility as numerical models to describe the complex details of experimental data. On the other hand, when the model equations are based on putative underlying mechanisms, as in the present case, analytical models may offer insight of a general nature that more empirical models cannot. In this regard, the model in the present study supports the suitability of a power-law function as describing the velocity distribution along virtual trajectories (Eq. 4). The parameter  $s_m$  sets the minimum closing velocity, which corresponds to those units that close so slowly they remain open throughout the entire derecruitability test. It is possible that these units would eventually close if the derecruitability tested lasted long



enough, but they make no contribution to the data when the tests last only 3 min. Interestingly, the exponent of the power law was found to be  $-2$  purely on the basis of the empirically observed linear increase in lung stiffness following a recruitment maneuver at zero PEEP. In other words, this exponent value comes from the qualitative behavior of the data rather than the fit of a particular model. This is significant because power laws have been invoked in a previous model of lung recruitment during lung inflation to account for avalanches of sequential opening events along the airway tree that are triggered when critical opening pressures are surpassed (Suki et al., 1994, 2000). Moreover, both inter-crackle intervals and terminal air space sizes that are linked by avalanches throughout the airway tree are characterized by power-law distributions having an exponent of  $-2$  (Suki et al., 2000; Alencar et al., 2001). The similarity between the probability distribution for  $s_c$  and these other avalanche-based mechanisms in the lung might not be a coincidence, but rather might follow in some way from the fractal branching structure of the airway tree. Thus, although our model consists of a parallel collection of respiratory units that cannot open in the kinds of cascades observed in the airway tree (Suki, 2002), the fractal structure of the lung is embedded in our model through the power-law form of the distribution of  $s_c$  (Eq. 4) and thus conforms to previous work by Suki et al. (1994, 2000), Alencar et al. (2001), and Suki (2002).

Having the geometry of the airway tree be implicit in our model in the functional form for  $s_c$  could also explain the findings of Massa et al. (2008) that  $f_{s_0}(s_0)$  and  $f_{s_c}(s_c)$  are unchanged following lung injury. That is, although lung injury would be expected to damage the alveolar parenchyma and the airway epithelium, there is no reason to suppose it would alter the branching structure of the airway tree, which would leave the functional form for  $s_c$  preserved. On the other hand, we do expect that injury would increase the mean values of the distributions



for  $P_c$  and  $P_o$  (Eqs 2 and 3, respectively) on the basis of increases in surface tension at the air-liquid interface within the lungs as a result of blood-gas barrier perforation and the subsequent airspace accumulation of fluid and protein (Massa et al., 2008; Smith et al., 2013). This conveniently allows us to account for the progression of lung injury largely in terms of the evolution of the value of a single parameter,  $k$  in Eq. 9 (Figures 2, 3).

We previously reported an apparent master relationship between  $D_{rate}$  and  $H_1$  (Smith et al., 2013). The model developed in the present study, however, suggests this is not quite the case because rate of change of  $D_{rate}$  with injury (Eq. 10) is predicted to depend on  $k$ , which depends on  $V_t$  (Figure 2B), even though the initial value of  $D_{rate}$  (Eq. 10

of the **Supplementary Material**) does not (**Figure 2A**). On the other hand, the dependence of  $dD_{\text{rate}}/dH_0$  on  $V_t$  is rather subtle (**Figure 4**), and is easily masked by noise in the data, so the notion of a single master relationship may still be a useful approximation. Also, both  $H_1$  (Mori et al., 2018) and  $D_{\text{rate}}$  (**Figure 4**) exhibit exponential growth over the time-scale of our experiment (up to 4 h), but they are unlikely to continue to increase indefinitely beyond this point because this would correspond to derecruitment of the entire lung. Even if this was a possibility, however, forcing a sizeable  $V_t$  into an ever shrinking lung would eventually lead to pressures that would cause rupture of the tissues. In any case, it appears that neither eventually would ever be realized because the mice died when about 75% of the lung became derecruited, at which point  $H_1$  and  $D_{\text{rate}}$  were still increasing exponentially.

Another feature of the relationship between  $D_{\text{rate}}$  and  $H_1$  is the early transient seen in **Figure 4**, which shows that  $D_{\text{rate}}$  to begin to increase early in the development of lung injury before  $H_1$  changes noticeably. We have previously postulated (Smith et al., 2013) that increases in  $D_{\text{rate}}$  are due to increases in surface tension that give rise to derecruitment dynamics manifesting over a timescale of minutes, while increases in  $H_1$  reflect flooded alveoli that have become permanently derecruited. This being the case, the relationship between  $D_{\text{rate}}$  and  $H_1$  in **Figure 4** suggests that surfactant deactivation by plasma-derived fluid and proteins starts to occur as soon as this material arrives in the airspaces whereas a certain volume of fluid as to accumulate in the airspaces before it can cause noticeable alveolar flooding. It also suggests that  $D_{\text{rate}}$  is more directly related to the “rich-get-richer” hypothesis of VILI that we have previously advanced (Hamlington et al., 2018a; Mori et al., 2018) and thus may be the more sensitive marker of the onset of lung injury. On the other hand, even though the model errors for  $D_{\text{rate}}$  do not appear to depend on  $H_1$  (**Figure 5**), at large  $t$ ,  $D_{\text{rate}}$ , and  $H_1$  become linearly dependent on each other (Eq. 10) suggesting that both variables ultimately embody the same pathophysiological information, although the fits of the present study are not as good at this end of the data range compared to those of our previous study (Smith et al., 2013) which curve over and follow the data better. Regardless, both  $D_{\text{rate}}$  and  $H_1$  are increased by fluid accumulation in the airspaces, so some kind of monotonic relationship between the two parameters is to be expected.

Our model has a number of limitations. For example, although we have characterized derecruitability of the lung in terms of only two parameters,  $H_1$  and  $D_{\text{rate}}$ , the increase in  $H$  with time during a derecruitability test is only approximately linear in its early stages; eventually,  $H$  begins to plateau (Allen et al., 2002; Allen and Bates, 2004; Massa et al., 2008). Such a plateau is inevitable as only those lung units for which  $P < P_c$  will eventually close as  $\tau \rightarrow \infty$ .  $D_{\text{rate}}$  is thus an empirical characterization of only part of a more complex relationship. We also neglected intra-breath variations in the pressures applied to the lungs by mechanical ventilation, as well as the way they depend on the degree of lung injury. We assumed a constant pressure for derecruitment in order to be able to solve the

model equations analytically (Eq. 7) and so gain the benefits of insight that a closed-form solution provides. In reality of course, these pressures are not constant because mean airway pressure rises for a given  $V_t$  as the lung becomes progressively more consolidated, so more quantitatively accurate predictions would require the numerical solution of a computational model in which airway pressures are allowed to vary in a realistic manner. This may partly explain why the ellipse areas of the joint parameter confidence regions in **Figure 3** tend to be greater for larger  $V_t$  (i.e., greater VILI); we would generally expect a simple analytical model to fit better to data from normal or mildly injured lungs compared to those that are severely injured. We also waived details concerning alveolar micromechanics such as interactions between neighboring respiratory units, although we recognize the potentially important role of such interactions in lung injury (Knudsen and Ochs, 2018). Finally, we have assumed that the dynamics of derecruitability in the lung are accurate indicators of the degree of lung injury, but they are not direct measures of such. Nevertheless, numerous prior studies from our laboratory have established a tight link between derecruitability and direct measures of damage to the blood-gas barrier (Allen and Bates, 2004; Allen et al., 2005; Smith et al., 2017; Hamlington et al., 2018a,b).

In summary, we have developed an analytical version of our previously developed computational model of the dynamics of lung derecruitment following a recruitment maneuver. We found that the distribution of velocity constants defining rates of movement along the virtual trajectories associated with the pulmonary airways follows a power-law with the same exponent of  $-2$  as found in other investigations into the dynamics of lung recruitment and derecruitment. We speculate that this may reflect the fractal-like structure of the airway tree throughout which recruitment and derecruitment may take place as cascades of open and closing events. Our study also suggests that the rate of change in lung stiffness represented by the parameter  $D_{\text{rate}}$ , to the extent that this remains constant during a 3 min derecruitability test, is a particularly sensitive marker of the degree of lung injury.

## DATA AVAILABILITY STATEMENT

The datasets generated for this study are available on request to the corresponding author.

## ETHICS STATEMENT

The animal study was reviewed and approved by Institutional Animal Care and Use Committee of the University of Vermont.

## AUTHOR CONTRIBUTIONS

VM developed the model analysis, coded the simulations, and drafted the manuscript. BJS, BS, and JB contributed to the development of the model concept, checked the mathematics,

and edited and approved the manuscript. All authors contributed to the article and approved the submitted version.

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## SUPPLEMENTARY MATERIAL

The Supplementary Material for this article can be found online at: <https://www.frontiersin.org/articles/10.3389/fphys.2020.542744/full#supplementary-material>

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The remaining authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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# The Development of Integrin Alpha-8 Deficient Lungs Shows Reduced and Altered Branching and a Correction of the Phenotype During Alveolarization

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Lung development involves epithelial–mesenchymal interactions and integrins represent one of the key elements. These extracellular matrix receptors form hetero-dimers of alpha and beta subunits. The integrin  $\alpha 8 \beta 1$  is highly expressed in mouse tissues, including lung. It forms a cellular receptor for fibronectin, vitronectin, osteopontin, nephronectin, and tenascin-C. This study aims to investigate the role of the integrin  $\alpha 8$ -subunit ( $\alpha 8$ ) during lung development. Wild type and  $\alpha 8$ -deficient lungs were explanted at embryonic days 11.5/12.5. After 24–73 h in culture  $\alpha 8$ -deficient lung explants displayed reduced growth, reduced branching, enlarged endbuds, altered branching patterns, and faster spontaneous contractions of the airways as compared to wild type. Postnatally, a stereological investigation revealed that lung volume, alveolar surface area, and the length of the free septal edge were significantly reduced in  $\alpha 8$ -deficient lungs at postnatal days P4 and P7. An increased formation of new septa in  $\alpha 8$ -deficient lungs rescued the phenotype. At day P90  $\alpha 8$ -deficient lungs were comparable to wild type. We conclude that  $\alpha 8 \beta 1$  takes not only part in the control of branching, but also possesses a morphogenic effect on the pattern and size of the future airways. Furthermore, we conclude that the phenotype observed at day P4 is caused by reduced branching and is rescued by a pronounced formation of the new septa throughout alveolarization. More studies are needed to understand the mechanism responsible for the formation of new septa in the absence of  $\alpha 8 \beta 1$  in order to be of potential therapeutic benefit for patients suffering from structural lung diseases.

**Keywords:** integrin alpha 8, lung development, branching morphology, alveolarization, transgenic mice, integrin

**Abbreviations:**  $\alpha 8$ ,  $\alpha 8$  integrin subunit; E, embryonal; P, postnatal; WT, wild type; KO,  $\alpha 8$  deficient mice or lungs; KO+  $\alpha 8$  deficient mice or lungs with phenotype; KO–,  $\alpha 8$  deficient mice or lungs without phenotype.

## INTRODUCTION

### Lung Development

The lungs are the main organ of respiration present in human, mice, and higher vertebrates. They provide a large internal surface area where the inspired air and the capillary blood get in close contact to each other to allow an efficient exchange of gases. To achieve this goal, during lung development, six important and overlapping stages occur: organogenesis, pseudoglandular stage, canalicular stage, saccular stage, alveolarization, and microvascular maturation. Successful development and function of the lung also involves the biochemical development of the surfactant system required for the stability and immune defense of the large respiratory surface area (Schittny, 2017).

During the pseudoglandular and canalicular stage, large parts of the pulmonary airways are formed prenatally by branching morphogenesis. In humans, monkeys, dogs and others, the bronchial tree is formed by a repetitive dichotomous branching of the future airways whereas in rodents, branching follows a monopodial pattern (Woods and Schittny, 2016).

Mostly postnatally in rodents and human the gas exchange surface of the lungs is enlarged during alveolarization; new septa are lifted off of pre-existing ones subdividing the most distal airspaces (Mund et al., 2008; Schittny et al., 2008). Alveolarization is a process, which does not finish during early childhood but continues until young adulthood (for a review see Schittny, 2017, 2018). Throughout lung postnatal development of rodents the size of the alveoli first decreases and later increases (Mund et al., 2008; Tschanz et al., 2014). Therefore, the alveolar surface area, the number of alveoli, and the total length of free septal edge does not increase in parallel with the increase of the lung volume.

### Integrins

Cellular and extracellular signaling networks orchestrate lung development. In the past the extracellular matrix was mainly viewed as the structural element of tissue. In the last two decades it became obvious that the extracellular matrix represents a dynamic and functional active zone that contributes to the establishment of cellular phenotypes. The contact to specific extracellular matrix proteins precisely modulates differentiation, migration, proliferation, and programmed cell death (Streuli, 1999). Extracellular matrix proteins like elastin, collagens, laminins and tenascin-C contribute to pre and postnatal development. These proteins are recognized by specific receptors such as integrins,  $\alpha$ -dystroglycan and other collagen receptors (Arnaout et al., 2005). Integrins are a large family of heterodimeric transmembrane glycoproteins containing a single  $\alpha$  and a single  $\beta$  subunit non-covalently linked. The expression, distribution, and role of the different integrins present on airway epithelial cells have been characterized *in vivo* and *in vitro* (Coraux et al., 1998; Sheppard, 2003).

### $\alpha 8 \beta 1$ Integrin

The integrin  $\alpha 8$  subunit exclusively associates with the integrin  $\beta 1$  subunit to form receptors for fibronectin, vitronectin, nephronectin, osteopontin, and tenascin-C (Muller et al., 1995;

Schnapp et al., 1995a,b; Brandenberger et al., 2001). In the lung the presence of  $\alpha 8 \beta 1$  appears prenatally diffusely in the mesenchyme except for cells surrounding the branching and growing ends of the future airways. Postnatally,  $\alpha 8$  keeps its diffuse mesenchymal distribution, but co-localizes with fibronectin and also with alpha smooth muscle actin (Chiquet-Ehrismann and Tucker, 2011). It has been shown that integrin  $\alpha 8 \beta 1$  mediates signals from the extracellular matrix to alveolar myofibroblasts and contributes to secondary septation (Wagner et al., 2003).

### $\alpha 8 \beta 1$ Integrin Knock Out Mice

In 1997 Müller and coworkers created an integrin  $\alpha 8$ -deficient mouse line by inactivating the gene encoding the  $\alpha 8$  subunit by gene targeting (Muller et al., 1997). They demonstrated that  $\alpha 8 \beta 1$  plays a crucial role in epithelial-mesenchymal interactions during kidney morphogenesis. This explains renal agenesis or dysgenesis at birth in homozygote mice. The penetration of this phenotype varies between two normal kidneys and no kidneys at all. Further investigations were necessary to discover that they have inner ear defects (Littlewood and Muller, 2000), and in the lung, anomalies in airway division and fusion of the medial and caudal lung lobes (Benjamin et al., 2009). The spatiotemporal expression pattern in lung development has been studied (Wagner et al., 2003) but detailed morphometric studies during prenatal and postnatal lung development have never been done.

### Aim of the Study

The aim of this study is to investigate the role of the integrin  $\alpha 8$  subunit during lung development. We hypothesized that the  $\alpha 8$  subunit plays an essential role in two important mechanisms: branching morphogenesis and alveolarization. To test these hypotheses, we have performed lung organ culture and morphometric studies during prenatal and postnatal lung development. We observed reduced branching, an altered branching pattern, and a higher frequency of spontaneous contractions of the future airways during prenatal development of  $\alpha 8$  deficient lungs resulting in a reduced lung volume, surface area, and length of the free septal edge at postnatal day 4. A tremendous amount of septa are formed to rescue the prenatal phenotype of  $\alpha 8$ -deficient mice until adulthood. We conclude that integrin  $\alpha 8 \beta 1$  takes part in the control of branching morphogenesis and that during alveolarization an incompletely developed lung may be rescued by an increased alveolarization.

## MATERIALS AND METHODS

### Animals

The  $\alpha 8$ -deficient mouse strain, kindly gift from Dr. Müller, was used (Muller et al., 1997). Wild type (WT) 129/Sv mice were used as age matched controls. 12.5 days old fetuses were obtained from heterozygote and the 11.5 days old ones from homozygote breeding (Table 1). Postnatal lungs were obtained from homozygote breeding. All animal studies were approved by and conducted in accordance with the Veterinary Service of the

**TABLE 1** | Summary of lung organ experiments.

	Number of explants			Penetration of branching phenotype
	KO+	KO–	WT	
Experiment 1 (E12.5)	6	3	20	66%
Experiment 2 (E11.5)	5	2	3	57%
Experiment 3 (E11.5)	6	2	4	75%
Total	17	7	27	71%

The number of used explants and the penetration of phenotype is given. KO+, explants with reduced branching, KO–, explants showing similar numbers of branches as the wild type (WT) explants.

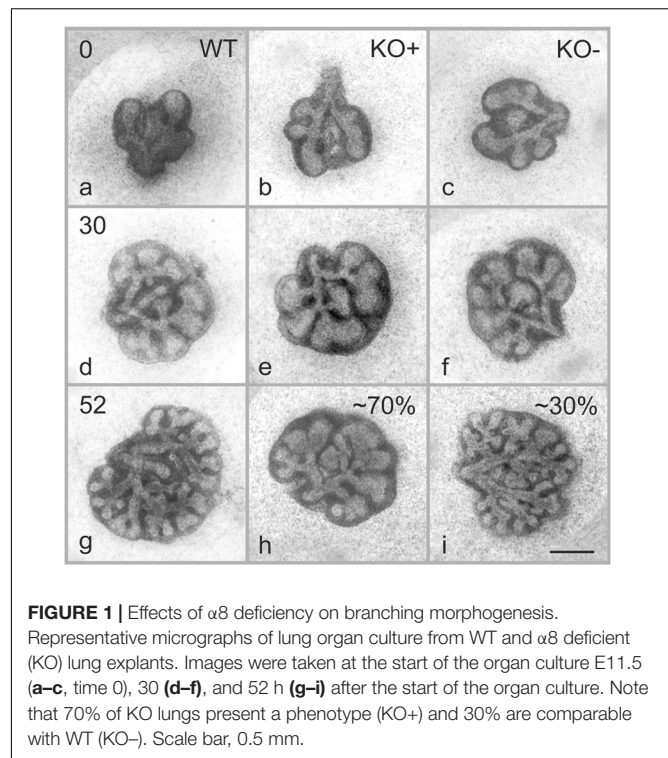
Canton of Bern and the Canton of Basel, Switzerland and the Swiss Federal Agency for Environment, Forest and Landscape.

## Lung Organ Culture

Fetal mouse lungs were obtained at day E11.5 or E12.5 under sterile conditions and cultured as described previously (Schittny et al., 2000; Roth-Kleiner et al., 2004). Depending on the size of the lungs they were either explanted as entire lungs (E11.5) or their lobes were separated (E12.5) in sterile phosphate buffered saline (127 mM NaCl, 10 mM Na<sub>2</sub>HPO<sub>4</sub>, pH 7.4). In both cases, the explants were cultured individually at the air-culture medium interface on a floating filter (TSTP Isopore filter, 13 mm diameter, 3 μm pore size; Millipore, Bedford, MA, United States) in a 24 well plate (Falcon-Becton Dickinson, Lincoln Park, NJ, United States) at 37°C in 5% CO<sub>2</sub>/air. Lungs obtained at E11.5 were explanted undissected. The medium, Dulbecco's modified eagle medium (GibcoBRL-Life Technologies, Basel, Switzerland), was enriched with 10% fetal calf serum (GibcoBRL), 5 μg/ml bovine insulin (Sigma Chemicals Company, St. Louis, MO, United States), 2 mM glutamine (Sigma), 75 μg/ml Streptomycin (Sigma), and 100 μg/ml Penicillin (Sigma). Three explants were transferred onto each filter and the filters were placed in a well containing 350 μl medium. The distance between the three explants was large enough to ensure the tissues did not touch during growth. The explants were fed daily by adding 200 μl of fresh medium per well. Images of the explants were taken twice daily using an inverted microscope (Diaphot-TMD, Nikon, Tokyo, Japan).

## Quantitative Evaluations of Organ Cultures

As a measure for branching, the number of terminal endbuds was counted on micrographs as shown in **Figure 1**. The growth (volume%) was estimated by area measurement of the projected organ pieces by point counting. The growth was calculated by dividing the measured area by the area of the explant at the start of the experiment and multiplying this result by 100. We may take these numbers as an estimation of the volume percentage of the growth, because the quotient of the diameter and the thickness of an individual explant was constant, especially as compared between different explants at one time point, but also between explants at different time points (Schittny et al., 2000; Roth-Kleiner et al., 2004). The α8-deficient lung explants were grouped

**FIGURE 1** | Effects of α8 deficiency on branching morphogenesis.

Representative micrographs of lung organ culture from WT and α8 deficient (KO) lung explants. Images were taken at the start of the organ culture E11.5 (a–c, time 0), 30 (d–f), and 52 h (g–i) after the start of the organ culture. Note that 70% of KO lungs present a phenotype (KO+) and 30% are comparable with WT (KO–). Scale bar, 0.5 mm.

according to their difference to WT explants. If after 48 h in culture the difference between α8-deficient and WT explants was less than 15%, the explants were defined as α8-deficient explants without phenotype (KO–) all other α8-deficient explants were defined as showing a phenotype (KO+).

## Morphology

Lungs were prepared as previously published (Luyet et al., 2002; Mund et al., 2008; Tschanz et al., 2014). Briefly, at postnatal days P4, P7, P10, and P90 the pulmonary blood vessels of five animals per group and day were perfused with phosphate buffered saline (PBS = 10 mM sodium phosphate, containing 127 mM sodium chloride, pH 7.4), containing 5 units/ml heparin, 10 mg/ml procaine and 10 mM EDTA (Fluka Chemie AG, Buchs, Switzerland), and the air space filled with PBS, containing 4% freshly prepared paraformaldehyde (Merck, Darmstadt, Germany) at a constant pressure of 20 cm water column. At this pressure, the lung reaches roughly its total lung capacity (TLC). In order to prevent a recoiling of the lung, the pressure was maintained during fixation of 1 h. After fixation, the five lobes were separated and their volumes were measured by water displacement (Scherle, 1970). The total lung volume was calculated from the five lobar volumes. The specific lung volume was defined as lung volume over body weight (Weibel, 1970). Lungs were embedded in paraffin (Histosec, Merck, Darmstadt, Germany) at 60°C after three washes in PBS, followed by a graded series of ethanol and by three changes of Histoclear (Life Science International, Frankfurt, Germany). Under all conditions no recoil of the lungs was observed. A total of 3.5–5 μm sections were cut, transferred



onto silanized (aminopropyl-trimethoxy-silane) micro slides, air dried over night at 37°C, dewaxed in Histoclear and stained with hematoxylin-eosin.

## Stereology

Stereological measurements were done as previously published by our group (Mund et al., 2008; Schittny et al., 2008; Tschanz et al., 2014) and in compliance with standards for quantitative assessment of lung structure of the American Thoracic Society and the European Respiratory Society (Hsia et al., 2010). Briefly, 40–50 images per animal were taken at a magnification of  $\times 250$  on 10–12 sections of its left lung. Sampling of the sections and the images were done according to a systematic random sampling scheme (Cruz-Orive and Weibel, 1981). The sections were taken at equal distances to each other covering the entire length of the lung. The start of this series of sections was determined randomly. Five left lungs per day and group were analyzed. It was shown that the left lung represents a valid sample for the entire lung (Zeltner et al., 1990; Barre et al., 2016). The volume of the five lobes was measured by water displacement (Scherle, 1970) (see above). Volume densities were estimated by point counting. The lung parenchyma was defined as airspaces and septal tissue, excluding bronchi, bronchioli, and blood vessels  $>20\ \mu\text{m}$  in diameter. Intersection counting was used to estimate the septal (alveolar) surface area density. The length density of the free septal edges was estimated by counting the number of cut free septal edges (tips of the cut septa) in a reference area on 2D paraffin sections. The total length of the free septal edge represents the total length of all alveolar entrance rings. (Mund et al., 2008; Schittny et al., 2008; Roth-Kleiner et al., 2014; Mund and Schittny, 2020). The totals of the parenchymal volume, the septal surface area, and the length of the free septal edge were calculated by multiplying their densities by the total parenchymal lung volume (Weibel, 1984; Howard and Reed, 2005). All calculations were done separately for each animal and each time point. In order to calculate the extent of newly formed alveolar septa, the length density was mathematically corrected for its change due to the growth of the volume of the lung parenchyma. An enlargement of the lung without the addition of new septa will lead to a decrease of the length density of the free edges by a factor of  $\sqrt[3]{(V_x/V_0)^2}$  (where  $V_x$  represents the parenchymal lung volume at the time point  $X$  and  $V_0$  the volume at the start of the growth). We use this correction because volume increases by a factor of  $x^3$  and length only by a factor of  $x^1$ . We corrected the stereologically estimated length densities for its decrease due to isometric growth of the lung parenchyma by multiplying by the factor of  $\sqrt[3]{(V_x/V_0)^2}$  (thereby  $V_0$  was set to the mean value of the parenchymal lung volume at postnatal day 4). During isometric growth of the lung the resulting “growth corrected length density” remains constant and shows an increase or a decrease, if new septa are formed or if septa are degraded, respectively. We calculated the formation of new alveolar septa during lung development and compared it between controls and  $\alpha 8$ -deficient mice by following the increase of the “growth corrected length densities” between postnatal days 4 and 90. In Tschanz et al. (2014) we discuss the method described above in more details and compared the number of alveoli with the length of the free septal edge throughout lung development.

## Statistical Analysis

Statistical analysis was done using 2-way ANOVA and Bonferroni post-test. Significance was defined as  $P < 0.05$  and “highly significant” as  $P < 0.001$  (Altman, 1991). Microsoft Excel (Office 2010, Microsoft Corporation, Redmond, WA, United States) and Prism (version 5.04, GraphPad Software Inc.) were used to calculate the statistics.

## RESULTS

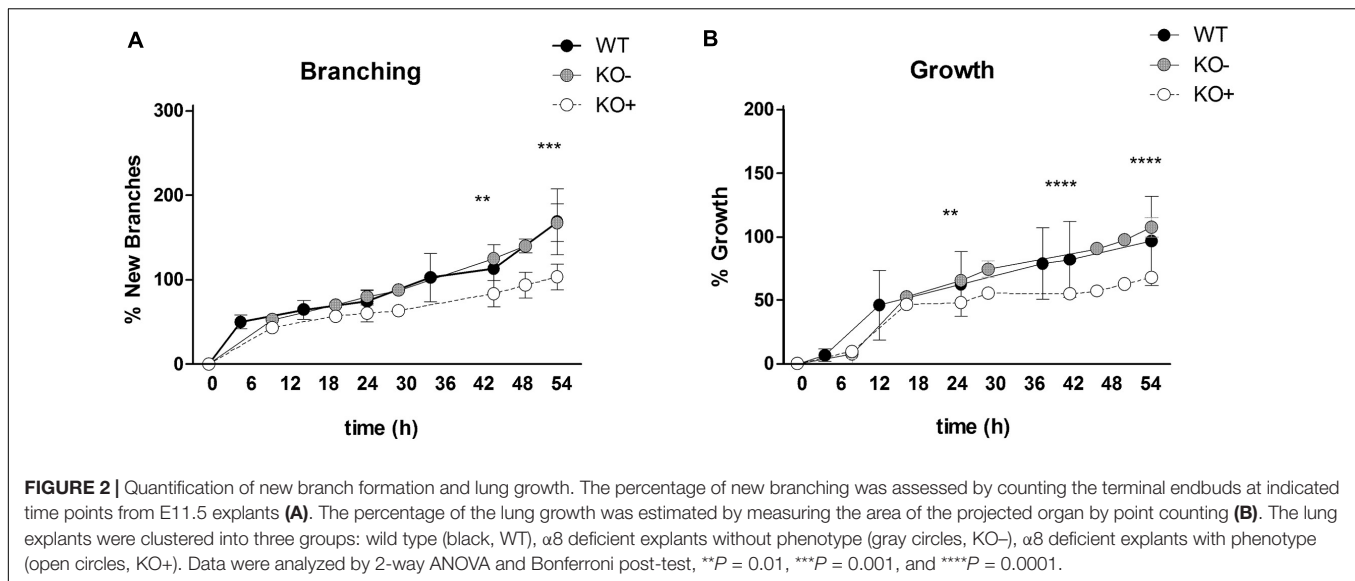
### Integrin $\alpha 8$ -Deficiency Reduces Branching Morphogenesis

To assess the role of the integrin  $\alpha 8$  subunit during branching morphogenesis, we collect explants from wild type (WT) and  $\alpha 8$  deficient mice (KO) at embryonic day E11.5–E12.5 and cultured them for up to 3 days (Table 1). Explants were imaged twice a day (Figure 1). Day E11.5 (embryonic stage) represented the earliest day, where we could start the lung organ culture. We included day E12.5 (pseudoglandular stage) in order to extend the time interval of observation. We did not observe any significant difference between days E11.5 and E12.5 (data of E12.5 not shown).

At time 0, WT and KO explants appeared comparable (Figures 1a–c). After 30 h of organ culture most, but not all of the KO explants showed a small reduction of branches as compared to WT explants (Figures 1d–f). A marked reduction of airway branching was evident in KO explants after 43 h of organ culture (Figures 1g–i, shown for 52 h). The deficiency, as verified by quantification, consists of diverse defects in branching and bud formation. Interestingly, only  $\sim 70\%$  of the KO explants (Figure 1h) showed a pronounced phenotype (KO+) with reduced branching, the remaining  $\sim 30\%$  (Figure 1i) showed the same number of branches (KO–) as WT (Figure 1g). New branching formation was quantified for each explant at different time points and significant differences were detected between WT and KO+ explants after 43 h of lung culture. No difference was observed between WT and KO– (Figure 2A). In addition, we asked whether  $\alpha 8$  deficiency has a direct effect on the lung growth. Lung size was estimated by measuring the area of the projected organ at indicated time points and statistical differences were observed between WT and KO+ groups especially after 24, 42, and 54 h of organ culture (Figure 2B). These data suggest that loss of integrin  $\alpha 8\beta 1$  alters not only the branching morphogenesis but also the overall growth of the lung explant.

### Integrin $\alpha 8$ -Deficiency Shows Altered Branching Patterns

Experiments were performed to evaluate whether the lack of  $\alpha 8$  integrin affects branching pattern during pulmonary development. Lungs from WT and KO obtained at E11.5–E12.5 were cultured and imaged at different time points (Figure 3). All WT lungs showed a normal pattern of branching over time (Figure 3a). Deficiency of  $\alpha 8$ , regardless of the penetrance of the phenotype caused an altered branching pattern (Figures 3b–d). Abnormal branching patterns were observed inside the lobes and



interestingly, none of the five lobes was more affected than the others (Figures 3b–d irregularities are encircle).

### Integrin $\alpha 8$ -Deficiency Affects Lung Spontaneous Contraction and Bud Morphology

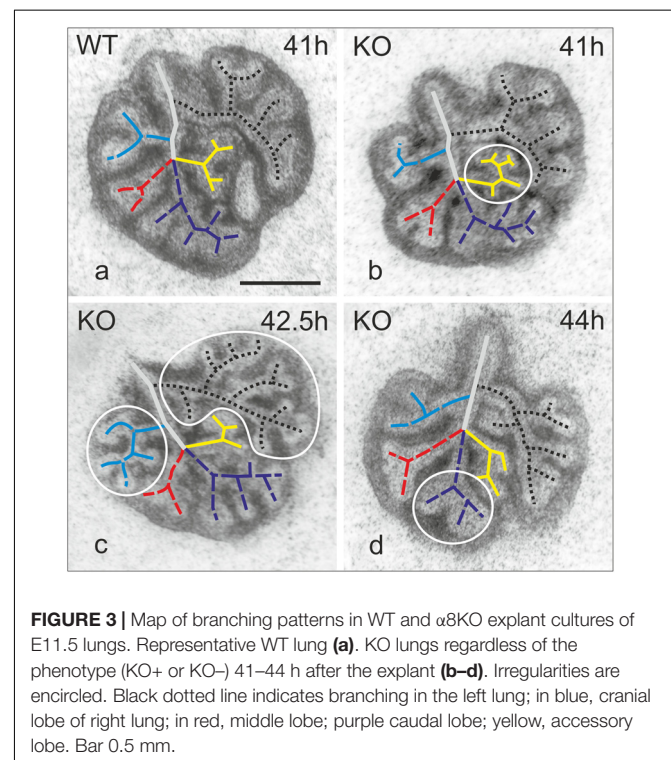
It is known that contractions of the future airways contribute to a normal airway differentiation and branching (Schittny et al., 2000) and  $\alpha 8\beta 1$  is expressed in contractile interstitial cells (CICs) (Levine et al., 2000). To determine whether the lack of  $\alpha 8$  affects this ability to contract, we analyzed and counted the number of contractions per minutes after 53 and 73 h in culture of E11.5 and E12.5 explants (Figure 4A). We found that contractions increased with time in WT and KO independently of the presence of the phenotype. Interestingly KO showed a significantly higher frequency of contractions after 73 h of organ culture. Furthermore, we studied whether the size of terminal endbuds was affected by  $\alpha 8$ -deficiency. Photographs taken at the day of explant (0) and after 24, 43, and 52 h in culture were quantified (Figure 4B). The size of endbuds was similar between WT and KO-, but interestingly KO+ showed larger endbuds than WT.

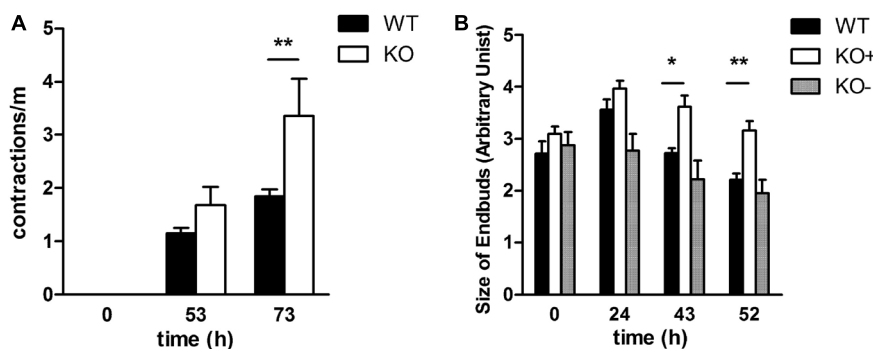
### Anatomical Differences Between WT and $\alpha 8$ Deficient Mice

The pulmonary phenotype of  $\alpha 8$ -deficient mice is characterized by a fusion of the medial and caudal lobe, as a consequence of mesenchymal and mesothelial cell anomalies and defective saccular airway branching (Benjamin et al., 2009). We found the same phenotype as Benjamin et al. (Benjamin et al., 2009) (Figure 5A) in the KO lungs where fusion is evident when compared to WT (Figure 5B). In addition, WT lungs clearly presented a fissure, which was completely missing in KO lungs (Figures 5C,D).

### Integrin $\alpha 8$ Deficiency Induces Prominent Formation of New Septa With a Consequent Rescue of the Phenotype

We asked whether the phenotype observed in KO organ cultures could lead to a characteristic phenotype postnatally (Figures 6, 7). We investigated the impact of  $\alpha 8$  integrin deficiency during alveolarization. Lung sections were compared between WT and KO littermates at postnatal day 4, 7, 10, and



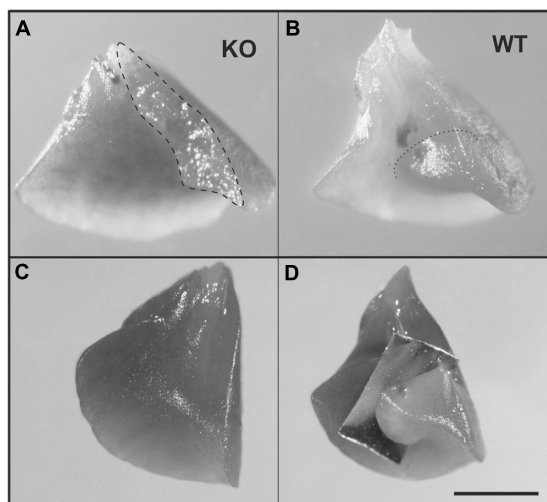


**FIGURE 4 |** Spontaneous contractions and size of terminal buds in E11.5 explant cultures over time. **(A)** Contractions were measured in WT and KO explants at starting point E11.5 and after 53 and 73 h of organ culture **(B)** The size of the endbuds was determined by measuring projected surface area at the start of the culture of WT, KO-, KO+ E11.5 (time 0) explants, as well as after 24, 43, and 52 h of cultivation. Data were analyzed by 2-way ANOVA and Bonferroni post-test, \* $P = 0.05$  and \*\* $P = 0.01$

90. Absolute lung volume and total surface area was significantly reduced in KO lungs as compared to age-matched WT at postnatal day 4 (P4) (**Figures 6A,B**).

During the phase of alveolarization, the increase of structural complexity of the lung parenchyma may be view from two different points of view: we look either to the formation of new alveoli or to the formation of new alveolar septa. Both parameters are well suited to study postnatal rodent lung development (for a comparison see Schittny et al., 2008; Tschanz et al., 2014). We focused on the formation of new alveolar septa and estimated the total length of the free septal edge. This parameter represent the total length of all septa, measured at their upper

free (not connected to anything) edge. In a first approximation, it is equal to the total length of the alveolar entrance rings. A significant reduction of this parameter was detected in KO lungs at P4 and P7 (**Figure 6C**). Interestingly, we found that the phenotype observed at an early stage, P4, did not persist until adulthood (P90): lung volume, total surface area and total length of free septal edge were comparable between WT and KO lungs (**Figures 6A–C**). These findings may be explained by the results of the stereological estimations showing that a significantly larger amount of new septa is formed in KO animals as compared to WT between postnatal days P4 and P90 (**Figure 6D**). In all KO lungs we observed the same postnatal phenotype and rescue. Therefore, postnatally the penetration of the phenotype was complete.



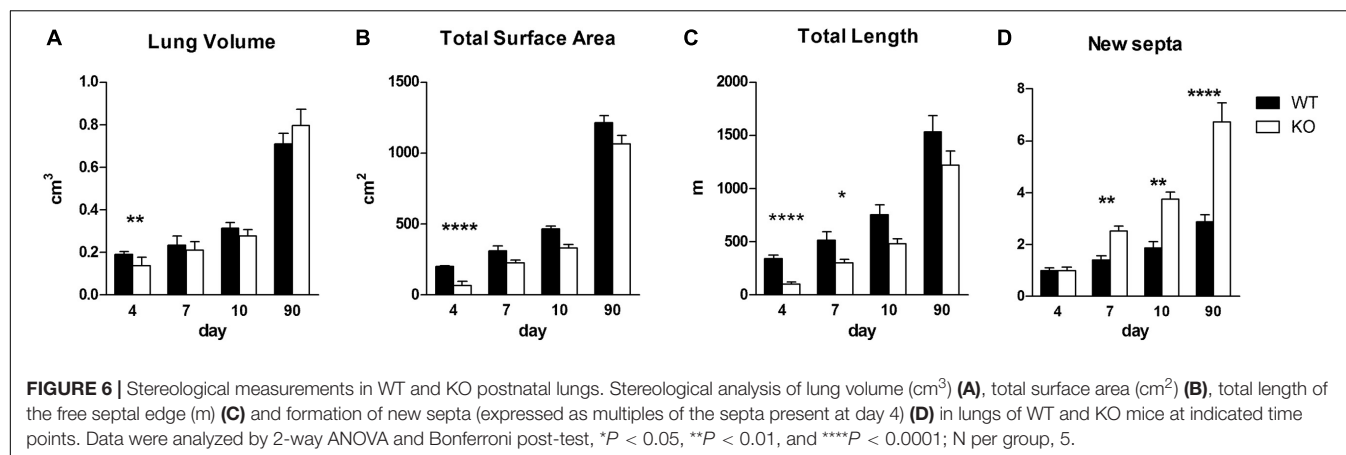
**FIGURE 5 |** Anomalous lung lobation in KO young adult as compared to WT. **(A)** Caudal lobe from KO lung with incomplete separation between the middle and the caudal lobe of the right lung. **(B)** Caudal lobe from WT. **(C)** KO caudal lobe from KO with incomplete or missing fissure **(C)** which is present in WT lungs **(D)**, an aluminum foil demonstrates where the fissure is running). Dashed line represents area of incomplete separation **(A)**; dotted line indicates fissure in WT **(B)**. Scale bar is 2 mm.

## DISCUSSION

### Phenotypes and Its Penetration

In the present study, we demonstrate that integrin  $\alpha 8 \beta 1$  is essential for the proper development of the lung and its absence causes many defects during prenatal and postnatal development. During prenatal lung development of  $\alpha 8$  KO mice, defects include reduced and irregular branching morphogenesis, a higher frequency of spontaneous contractions of the future airways and anomalous lobation. However, in the  $\alpha 8$  KO animals, we observed only ~70% of penetrance of the prenatal branching phenotype. Similar results were found previously (Muller et al., 1997) in the kidney of  $\alpha 8$  KO mice, which are born with different kidney phenotypes. The presence of variable phenotypes is partially explain as a consequence of the two genetic background (129 and C57Bl/6) present in those mice. It is possible that the presence or the absence of genetic modifier locus controls specifics phenotypes. We assume that not only the two genetic backgrounds modulate the penetrance but also a compensatory effect by other integrins during the different steps in lung development. Based on kidney studies it has been hypothesized that  $\alpha 5$  and  $\alpha V$  could compensate the function of  $\alpha 8$ , but it was not the case due to the





negative results obtained (Haas et al., 2003). Moreover, collagens I and III were detected in the glomeruli of  $\alpha 8$  KO mice leading to the assumption that compensation for  $\alpha 8$  function could implicate interactions between collagens with collagen receptors. We speculate that similar mechanisms involved in the

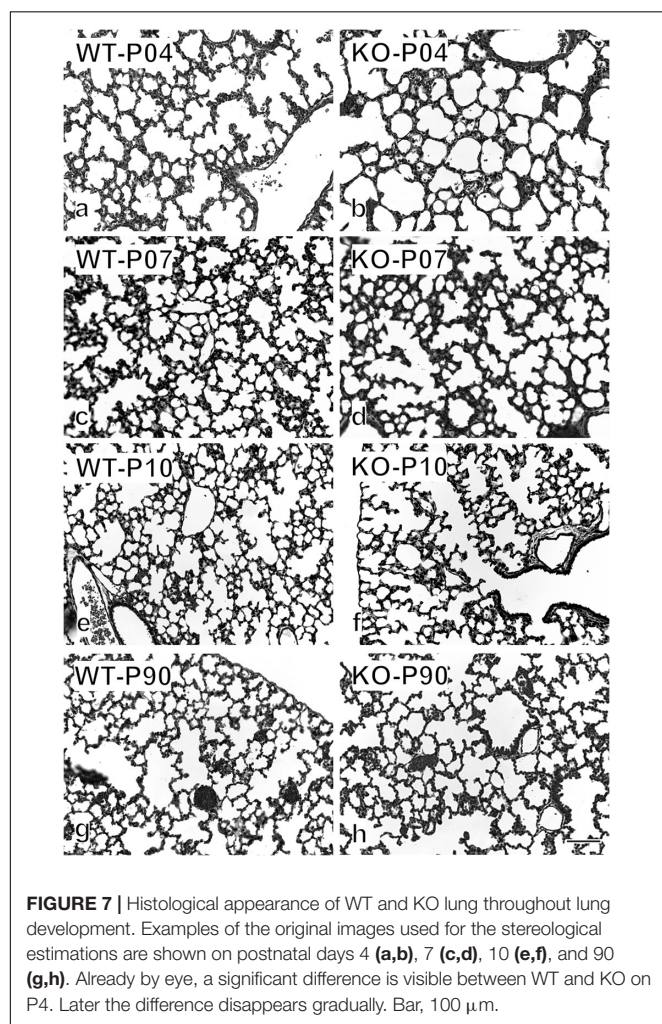
renal phenotypes are also responsible for the lung phenotype, which we observe.

During postnatal development, an increased formation of new septa was observed resulting in a nearly normal lung in adult KO mice (day 90). In opposite to the prenatal phenotype we observed a complete penetration of the postnatal phenotype. Previous studies (Wagner et al., 2003; Benjamin et al., 2009) have shown cellular function and spatiotemporal expression of  $\alpha 8\beta 1$  in the developing lung. However, the specific prenatal and postnatal defects, which were observed in this study, have not been described until now.

## Branching Morphogenesis

Branching morphogenesis is a complex phenomenon regulated by signaling factors that requires epithelial and mesenchymal interactions to form an epithelial bud (Iber and Menshykau, 2013). Only rare variations are seen in lungs of WT mice proving that branching is not random but a very well controlled mechanism (Metzger and Krasnow, 1999). We observed that  $\alpha 8$  KO lungs with a phenotype (KO+) showed fewer branches and reduced growth compared to WT and KO without phenotype (KO−, Figures 1, 2) in lung organ cultures. In addition, all KO lung explants showed an irregularly altered branching pattern (Figure 3). Any culture system has its limits if it is compared to a live animal. However, the phenotype detected in lung organ culture was confirmed by the observation that at postnatal day 4 the lung volume, the total alveolar surface area, and the total length of the free septal edge were reduced in live animals. These results represent a confirmation, because at this time point alveolarization did not start yet (see section “Alveolarization” and Figures 6A–C).

Interestingly, former studies have shown that tenascin-c (TNC) represents a ligand for  $\alpha 8$  integrin (Schnapp et al., 1995b). In addition, previous research in our laboratory (Roth-Kleiner et al., 2004) has demonstrated that TNC deficiency leads to a reduction of branching but showed normal overall growth of the explants and normal branching patterns in deficient mice. Branching and branching patterns are governed by a dynamic process of epithelial–mesenchymal interactions (Morrissey et al., 2013). Because tenascin-C as well as  $\alpha 8$  integrin deficiency





shows similar phenotypes, it may be concluded that both are involved in the epithelial–mesenchymal interactions during lung development. Typically  $\alpha 8$  integrin and TNC-mRNA is expressed by mesenchymal cells, but the TNC-protein was found along the epithelial basement membranes (Zhao and Young, 1995). Therefore, we hypothesized that TNC signals to the epithelial and mesenchymal cells and influences their adherence to their substratum (Chiquet-Ehrismann and Tucker, 2011) and that  $\alpha 8$  recognizes TNC (Schnapp et al., 1995b) and closes at least one loop of interactions.

## Spontaneous Contractions of the Future Airways

During gestation, spontaneous contractions of the future airways have been described (Schittny et al., 2000). The responsible players of those contractions are airway smooth muscles. They contribute to normal lung development and fetal lung growth (Schittny et al., 2000). Murine and rat lung development studies have shown that primitive lung mesenchymal cells retain a generic capacity to differentiate into airway smooth muscle cells, and these cells follow the emergence of the definitive lung bud (Jesudason et al., 2005). In our study, we also noticed spontaneous contractions of the future airways in WT, KO<sup>−</sup>, and KO<sup>+</sup>. Independently from the phenotype, KO lungs showed a significantly increased number of contractions per minute (**Figure 4A**) and this correlates with an increase of the size of the endbuds (**Figure 4B**). We propose that absence of the  $\alpha 8$  subunit could lead to signals, which activate myofibroblasts or reduce an inhibitor pathway with the result of faster contractions.

## Alveolarization

Alveolarization is a complex process coordinated by multiple interactions between extracellular matrix, fibroblasts, epithelial cells, and microvasculature. Deficiencies in one of these elements have consequences on the entire alveolar development. Interestingly, at postnatal day 4,  $\alpha 8$  deficient mice showed a significant reduction in lung volume compared with WT (**Figure 6**). Because at day 4, alveolarization did not yet start, this phenotype is exclusively caused by branching morphogenesis. However, at day 90 KO lungs were comparable to WT (**Figures 6, 7**). Therefore when mice are considered to be adults WT and KO do not show any significant difference. The same holds true for the total surface and total free septal length. The latter represents a measure for alveolarization. Based on morphological measurements we found that KO mice start with one fourth of length of the free septal edge at P4 (**Figure 6C**) and in order to become equal to WT, KO mice compensate with a massive input of new septa (**Figure 6D**). Therefore, the prenatal phenotype of the  $\alpha 8$  deficient mice is rescued by an increased alveolarization during postnatal life.

It may be speculated about the size of the acini during the rescue of the  $\alpha 8$ -phenotype between days 4 and 90. It is likely that in the KO<sup>+</sup> mice branching is as well reduces as the number of acini. Because the number of acini is most likely constant in postnatal mouse lung development (Barre et al., 2014, 2016),

we hypothesize that KO<sup>+</sup> mice possess a smaller number of acini which show a larger volume as compared to wildtype mice. A similar – at the end unanswered question – arise during compensatory growth after pneumonectomy: The remaining lung is able to regrow to its original size and alveolar surface (Hsia et al., 1994; Hsia and Johnson, 2006; Butler et al., 2012). If our data, that the number of acini stays constant after the saccular stage (Barre et al., 2016), are right, the only other known option will be to increase the size of the acini.

Tenascin-C is not only contributing to branching morphogenesis, but also to alveolarization. It involved in hyperoxia- (Olave et al., 2016) and steroid-induced (Roth-Kleiner et al., 2014) abnormal lung development. Furthermore, tenascin-C deficient mice show in both phases of alveolarization (classic and continued) a deceleration and acceleration of alveolarization (Mund et al., 2008; Mund and Schittny, 2020). Therefore, even if tenascin-C is a ligand of  $\alpha 8$  integrins they exhibit different phenotypes during pulmonary alveolarization.

## Conclusion

Taken together our results indicate that  $\alpha 8\beta 1$  integrin plays several roles in distinct phases of lung development. During prenatal lung development, regular spatio-temporal presence of  $\alpha 8\beta 1$  is essential for the normal pattern of branching. Most likely  $\alpha 8$  has a direct effect on branching and on the branching pattern, but in addition an indirect effect by the alteration of the spontaneous contractions of the future airways. From these observations, we conclude that  $\alpha 8\beta 1$  is crucial for lung development at different time points even though the mechanism responsible for the rescue of the lung phenotype is still unknown. But the fact that a rescue takes place during alveolarization shows the enormous potential of the lung to correct early impairments of lung development. We assume that during the development chronic disease (such as emphysema, COPD and fibrosis) the lung is overwhelm by inflammation and activation of specific pathways, which do not consent the correction of septa loss.

Although numerous elements in the process of alveolarization have been determined, more studies are needed in order to clarify the complex interrelationships that are operative during normal lung development.

Our findings strongly suggest the necessity of further studies in order to determine how to improve the mechanism able to correct impairment in the lung and which is the point of no return when this mechanism is not anymore able to correct it.

## DATA AVAILABILITY STATEMENT

The datasets generated for this study are available on request to the corresponding author.

## ETHICS STATEMENT

The animal study was reviewed and approved by Veterinary Service of the Canton of Bern and the Canton of Basel,

Switzerland and the Swiss Federal Agency for Environment, Forest and Landscape.

## AUTHOR CONTRIBUTIONS

TC analyzed the data and drafted the manuscript. AH obtained the postnatal lungs and did the required breeding of the mice. JS conceived and designed the study, performed the lung organ cultures including the videotaping and analysis of the data. In addition, he did of parts of the breeding of the mice, the stereological estimations of postnatal lung development including analysis of data, and contributed to writing. All authors contributed to the article and approved the submitted version.

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