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EDITED BY

Jiaru Shi,
Tsinghua University, China

REVIEWED BY

Kiki Theodorou,
University of Thessaly, Greece
Lanchun Lu,
The Ohio State University, United States

*CORRESPONDENCE

J. H. Pensavalle,
✉ jakeharold.pensavalle@gmail.com
G. Felici,
✉ giuseppefelici1971@gmail.com

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Standard requirements for clinical very high energy electron and ultra high dose rate medical devices

J. H. Pensavalle^{1*}, F. Di Martino^{1,2,3}, A. Cavalieri⁴, M. Celentano^{1,3}, A. De Gregorio^{5,6}, M. Di Francesco⁷, G. Franciosini^{6,8}, L. Galluzzo⁷, L. Masturzo^{1,3}, G. Milluzzo⁹, P. Montay-Gruel^{10,11}, F. Paiar^{2,4,12}, M. Pantaleoni¹³, V. Patera^{6,8}, S. Pioli¹⁴, P. Poortmans^{15,16}, F. Romano^{9,17}, A. Sarti^{6,8}, A. Subiel^{18,19}, A. Vannozzi¹⁴ and G. Felici^{7*}

¹Azienda Ospedaliero Universitaria Pisa (AOUP), Fisica Sanitaria, Pisa, Italy, ²Centro Pisano Multidisciplinare Sulla Ricerca e Implementazione Clinica Della Flash Radiotherapy (CPFR@CISUP), Pisa, Italy, ³National Institute of Nuclear Physics (INFN), Section of Pisa, Pisa, Italy, ⁴Center for Instrument Sharing University of Pisa (CISUP), University of Pisa, Pisa, Italy, ⁵Dipartimento di Fisica, Sapienza Università di Roma, Roma, Italy, ⁶Istituto Nazionale di Fisica Nucleare (INFN) Sezione di Roma I, Roma, Italy, ⁷SIT Sordina IORT Technologies, Aprilia, Italy, ⁸Dipartimento di Scienze di Base e Applicate per l'Ingegneria, Sapienza Università di Roma, Roma, Italy, ⁹Istituto Nazionale di Fisica Nucleare (INFN), Sezione di Catania, Catania, Italy, ¹⁰Center for Oncological Research (CORE), Integrated Personalized and Precision Oncology Network (IPPON), Faculty of Medicine and Health Sciences, University of Antwerp, Wilrijk, Belgium, ¹¹Iridium Network, Radiation Oncology, Antwerp, Belgium, ¹²Department of Translational Research and New Technologies in Medicine and Surgery, University of Pisa, Pisa, Italy, ¹³Maytal International Ltd – Global Med Dev Expertise, London, United Kingdom, ¹⁴Laboratori Nazionali Frascati-Istituto Nazionale di Fisica Nucleare (LNF-INFN), Frascati, Italy, ¹⁵Department of Radiation Oncology, Iridium Network, Antwerp, Belgium, ¹⁶Faculty of Medicine and Health Sciences, University of Antwerp, Antwerp, Belgium, ¹⁷Particle Therapy Research Center (PARTREC), Department of Radiation Oncology, University Medical Center Groningen, University of Groningen, Groningen, Netherlands, ¹⁸National Physical Laboratory, Teddington, London, United Kingdom, ¹⁹University College London, London, United Kingdom

Very High-Energy Electrons (VHEE) present a promising innovation in radiation therapy (RT), particularly for the treatment of deep-seated tumors using Ultra High Dose Rate (UHDR) within the framework of FLASH-RT. VHEE offers significant advantages, such as improved tumor targeting, reduced treatment times, and potential utilization of the FLASH effect, which may minimize normal tissue toxicity. However, the lack of an international technical standard for VHEE systems, especially for UHDR applications, remains a critical challenge. Current standards for radiation therapy equipment, such as IEC 60601-2-1 and IEC 60601-2-64, do not encompass VHEE technology. This regulatory gap underscores the need for developing a structured international standard to ensure the basic safety and essential performance of VHEE medical devices. Addressing this challenge requires overcoming complex dose delivery issues, such as the interaction of multiple fields and beam conformality and incorporating novel techniques like broad beam or pencil beam scanning. Establishing comprehensive regulatory standards is essential to ensure patient safety, consistent treatment practices, and the successful clinical integration of VHEE systems. These standards must encompass design guidelines, radiation protection protocols, and integration

with existing oncology practices. Collaborative research and development efforts are crucial to formulating evidence-based guidelines, fostering the safe and effective use of VHEE in clinical settings. By addressing these challenges, VHEE technology has the potential to revolutionize cancer therapy, particularly for deep-seated tumors, while enhancing therapeutic outcomes for patients.

KEYWORDS

VHEE radiotherapy, FLASH radiotherapy, UHDR, regulatory standards, IEC (international electrotechnical commission)

Introduction

Very High-Energy Electrons (VHEE) represent a promising advancement in radiation therapy (RT), particularly for treating deep-seated tumors using Ultra High Dose Rate (UHDR) in the context of FLASH-RT. However, the lack of an international technical standard governing VHEE systems, especially for UHDR applications, poses a significant challenge.

To design future VHEE medical devices, it is essential to consider the following current evidence [1–3]:

- UHDR VHEE is a promising and likely alternative to other UHDR External Beam RT (EBRT) modalities for treating deep-seated tumors, as electrons, even at very high energies, offer advantages in terms of easier high-current beam acceleration and potential cost reductions in clinical linear accelerator (linac) implementation.
- Optimizing VHEE dose delivery requires addressing challenges beyond conventional radiation oncology, factoring in beam temporal structure and the interaction of overlapping beams.
- Unlike single-field, lower-energy potential FLASH treatments (e.g., in the framework of Intra Operative RT (IORT) or dermatological treatments), VHEE conformality requires multiple fields, utilizing either broad beam and/or pencil beam scanning techniques.

Current standards, such as IEC 60601-2-1 [4], which covers electron RT equipment up to 50 MeV, and IEC 60601-2-64 [5], which addresses light ions, do not encompass VHEE technology. This regulatory gap underlines the necessity for a structured approach to establish an international technical standard that ensures the basic safety and essential performance of VHEE-capable medical equipment.

The development of such a standard would provide the foundation for safe clinical application of VHEE systems. Given that basic safety and essential performance are already determined for other forms of RT, including electron and proton systems, it becomes clear that the objective is not merely to address technological advancements, but to establish a clear regulatory framework. This would guide the design, manufacturing, and clinical use of VHEE systems in a way that prioritizes patient safety while maximizing therapeutic efficacy.

From a clinical perspective [6], VHEE holds great promise for improving outcomes in several challenging cancer types. Preclinical studies on FLASH-RT delivered with ultra-high high dose rate intermediate energy electrons (4–20 MeV) have shown encouraging

results in multiple organs and tumor types. If confirmed with VHEE, this technology could be a game changer for multiple indications in radiation oncology.

For instance, in the treatment of multiple brain metastases or primary brain tumors such as high-grade gliomas, current methods are often limited by the radiosensitivity of healthy brain tissue [7, 8]. These tumors typically require large-volume irradiation [9], yet delivering curative doses is often impossible without damaging surrounding brain structures [10]. FLASH-RT with intermediate energy electrons showed a significant advantage over conventional dose rate RT in the brain tissues, particularly in preserving cognitive function in animal models, suggesting that neurocognitive sparing might be possible with FLASH-RT in adult [11–14] and juvenile animals [15]. If these effects are confirmed in human trials, it could open the door for dose-escalation studies aimed at enhancing local control of intracranial disease and potentially improving overall survival rates.

Locally advanced non-small cell lung cancer (NSCLC) is another area where VHEE could provide a breakthrough. In cases where surgery is not an option, RT plays a critical role, but long-term survival remains low, with only 15%–20% of patients surviving 5 years post-diagnosis [16, 17]. The challenge lies in delivering curative radiation doses while sparing healthy lung tissue, as the limiting toxicities—acute pneumonitis and late fibrosis—are directly related to the volume of lung exposed to radiation [18–20]. Preclinical data suggest that FLASH-RT delivered with intermediate energy electrons induces significantly less lung fibrosis compared to similar doses of conventional dose rate RT [21, 22]. This positions VHEE as a potentially game-changing modality for lung cancer treatment, enabling higher tumoricidal doses with reduced risks of debilitating side effects.

Recent studies in various preclinical models suggest that, compared to conventional dose-rate RT (CONV), FLASH-RT has distinct effects on circulating immune cells, the tumor immune microenvironment, cytokine production, and inflammatory responses [23–25]. Based on these findings, FLASH-RT could be an ideal complement to immunomodulating drugs, potentially enhancing the therapeutic window of current radioimmunotherapy strategies.

Vertebral metastases, which often affect patients requiring palliative RT, represent another potential application for VHEE. The main challenge is protecting the radiosensitive spinal cord while delivering optimal doses to the vertebra [26]. Exceeding the maximum tolerated dose to the spinal cord can lead to irreversible damage, making it difficult to treat metastatic tumors effectively. Although preclinical studies on the FLASH effect in spinal tissues are still needed, VHEE could allow higher therapeutic

doses to be delivered while minimizing spinal cord risk. This makes vertebral metastases an ideal candidate for early clinical trials of VHEE, given the straightforward treatment geometry and high therapeutic potential. For pancreatic cancer, where prognosis remains poor due to local recurrence and early metastasis [27], VHEE could have a profound impact. The proximity of critical organs like the duodenum and small intestine limits RT, making high tumoricidal doses difficult to deliver without severe gastrointestinal complications [28]. While stereotactic ablative RT (SABR) has been explored, complication rates remain high. Emerging data on the protective effects of FLASH-RT on intestinal tissues provide a compelling rationale for investigating VHEE in this context. If validated, this approach could allow higher doses and/or volumes to be delivered safely, without increasing the possible side-effects, and thereby potentially improving local control and survival outcomes in pancreatic cancer patients and other challenging intra-abdominal tumor locations. As we move toward clinical translation, several technological challenges must be addressed. Firstly, there is no clinically certified VHEE linear accelerator available. Moreover, the existing methods of beam delivery for high-energy electrons differ from those for low-energy electrons. Importantly, no pre-clinical study pertaining to the FLASH effect has employed VHEE. Similar to other multiple-beam VHEE applications, understanding the “volume effect” and whether time delays between field transitions could affect the FLASH effect (FE) will be critical for the safe and effective use of VHEE in the clinic.

While FLASH-RT has generated substantial interest in the radiation oncology community, the key to its widespread adoption, together with the technological development and radiobiological knowledge advancement, will be the establishment of a comprehensive international technical standard for VHEE systems. Such a standard would determine the basic safety and essential performance requirements, ensuring that VHEE technology can be implemented safely and effectively in clinical settings.

The complexities associated with VHEE dose delivery, particularly in the context of UHDR modalities, necessitate a thorough understanding of basic safety and essential performance metrics as outlined in IEC standards, specifically IEC 60601-2-1, which governs medical electrical equipment, including electron linacs up to 50 MeV.

Towards a VHEE medical device

VHEE therapy, operating in the range of 50–300 MeV, presents unique challenges that differ significantly from conventional radiation oncology techniques. Traditional methods primarily focus on optimizing conformality—the precision with which the radiation dose conforms to the shape of the tumor. In contrast, VHEE treatments require an integrated approach that considers both the temporal beam structure and the spatial overlap of multiple beams. This dual consideration is particularly critical given that UHDR VHEE modalities can deliver high doses rapidly, which may enhance tumor targeting while minimizing damage to surrounding healthy tissues [3].

TABLE 1 Physical observables for Basic Safety and Essential Performance, conventional RT and VHEE UHDR.

Basic safety and essential performance – physical observables	
Conventional	VHEE UHDR
Ionizing Radiation (X, e, p, \dots)	TIME (Total Irradiation time, time of pulse, etc.) T, t_p
Beam Energy E	Rates (what rates? Average? Instantaneous?) D/t
Beam Fluence φ	Dose (Total, per fraction, per pulse) D_T, D_F, D_p
Dose (Total, per fraction) D_T, D_F	Beamlet Position and Divergence X, Θ

Temporal and spatial considerations

The temporal dynamics of UHDR VHEE beams, characterized by their ultra-short pulse delivery, can influence the biological effectiveness of the treatment. Research indicates that the FLASH effect—whereby high doses delivered in very short time frames reduce damage to normal tissues while maintaining tumor control—can be particularly useful in VHEE therapies. This necessitates a comprehensive evaluation of how these time dynamics interact with spatial dose distributions, especially in multi-beam configurations.

Safety and performance metrics

Basic Safety and Essential Performance consist in properly setting (via Human Machine Interface–HMI), monitoring (using a monitoring systems in conjunction with HMI) and reporting on the HMI the physical observables involved in the dose delivery and essential for guaranteeing both safety and quality of and during the treatment. For conventional therapy machines, the observables are the type of radiation (X-rays, electrons, protons, etc.), beam energy E , beam fluence φ and dose (total or for each fraction). With UHDR, also the temporal beam structure should be included in the physical observables, and for VHEE, depending on the delivery technology, also beamlet position and/or divergence. In Table 1 the physical observables are summarized.

Additional safety requirements

According to IEC 60601-2-1, basic safety also encompasses the protection of patients and operators from electrical, mechanical, and radiation hazards. Also, for VHEE systems, this should include the following requirements:

- Radiation Leakage: The system must minimize radiation exposure to non-target areas, ensuring compliance with strict limits on leakage radiation.

- **Electrical Safety:** All electrical components must be designed to prevent electric shock and ensure safe operation under fault conditions.
- **Mechanical Integrity:** The equipment must maintain structural integrity to prevent accidents or malfunctions during operation.

Performance requirements

Essential performance refers to the equipment's ability to operate as intended without compromising safety. For conventional medical accelerators, this is defined by IEC 60976 [29]. Although much of this standard may be applicable, modifications are necessary to account for the temporal beam structure for VHEE systems. Thus, an analogous standard for VHEE systems should take into consideration the following:

- **Dose Delivery Accuracy:** The system must accurately deliver the prescribed dose to the target while minimizing exposure to surrounding organs at risk (OARs). This requires accurate calibration and real-time monitoring of dose delivery.
- **Conformality and Homogeneity:** VHEE treatments should achieve a high degree of dose conformality and homogeneity, particularly when treating complex tumor geometries. Studies have shown that VHEE beams can provide superior dose distribution compared to conventional photon beams, leading to better sparing of OARs and enhanced tumor coverage [3].
- **Temporal Control:** The ability to modulate the dose rate and timing of beam delivery is crucial for optimizing treatment effectiveness and minimizing side effects. This includes the implementation of advanced treatment planning systems capable of accounting for the unique temporal characteristics of VHEE beams.

Additionally, periodic tests to assure the integrity of essential performance are mandatory. The IEC 60977 standard [30] describes the type tests required for conventional linacs, but adaptations are necessary for the higher energy and unique temporal beam structure.

The integration of basic safety and essential performance metrics, as defined by IEC standards, is vital for the successful implementation of VHEE therapy. As the field of RT advances with modalities like VHEE, establishing comprehensive standards to address these unique challenges posed by these systems will be key to ensuring both patient safety and treatment efficacy. The interplay of temporal and spatial factors in VHEE dose delivery underscores the need for continued research and development to refine treatment protocols and enhance clinical outcomes.

VHEE medical device certification process

In this article, we will only discuss the essential elements of the certification process in the European context (CE marking), although with the entry in force of the EU Medical Device Regulation (MDR) 2017/745 [31], the evidence supporting this process is quite similar to that in other major economic areas (United States, Canada, United Kingdom, Japan, China, etc.).

The certification process for a Medical Device (MD) is based on two conditions that are both necessary: a "technical" verification, whose focus is essentially product safety, and clinical evaluation, which integrates clinical safety and expected clinical performance for the product.

The "technical" verification is essentially based on compliance with technical regulations applicable to the medical device, based on its intended use.

These standards are issued by standardization bodies such as IEC [32].

Dealing with medical accelerators, the reference standard is IEC 60601-1 [33], a general standard that applies to all electro-medical devices, flanked by other collateral standards such as 60601-1-2 [34] for electromagnetic compatibility, 60601-1-6 [35] for usability etc., and particular standards dependent on the type of accelerator (60601-2-8 [36] X ray in the range 10 kV up to 1 MV, 60601-2-1 [4] for electrons between 1 and 50 MeV, 60601-2-64 [5] light ions).

From this it follows that although there will be, in the near future, for VHEE accelerators a particular technical standard, to the analogous IEC 60601-2-1, which is used today for electron accelerators in the class between 1 and 50 MeV, this standard will only be the first necessary step to provide the basis for getting to clinical use of a VHEE system, but it will not be a sufficient condition.

Indeed, it will be necessary for the manufacturer of a MD for VHEE to also demonstrate clinical efficacy for target tumors and areas through a clinical evaluation in compliance with MDR. This pathway will be equally challenging.

Indeed, the clinical evaluation of a medical device, and particularly an innovative medical device such as a device for VHEE, will have to demonstrate the safety and clinical performance of the device, now inferred from various pre-clinical studies in *in vitro* and/or animal models, on humans.

Without a clinical evaluation according to the requirements of MDR2017/745, demonstrating that what has already been achieved in pre-clinical testing is replicable in humans in a safe and effective manner, there can be no DM on the market that can be authorized for use in humans for VHEE.

In fact, the MD regulatory landscape in Europe, prescribes that the clinical evaluation to be based on clinical data obtained by a scientifically valid method from a critical review of the currently available scientific literature on the issues of safety, performance, design characteristics and intended use of the device, and/or a critical analysis of the results of all available clinical investigations and a review of any alternative treatment options currently available for the same purpose (ref. to Art.61 of the MDR).

All this clinical data must demonstrate that the proposed device, such as the device for VHEE, is capable of providing the intended benefit (e.g., treatment of target tumors) with a benefit-to-risk ratio that is equal to or less than currently commercially available treatment options.

For clinical evaluations to be performed in humans (clinical investigations) the MDR 2017/745, in order to protect the health of the patients involved, prescribes specific authorization pathways by the National Competent Authorities (Italian Health Ministry in Italy, BfArm in Germany etc.), and due to the very nature of the target diseases to be treated, clinical investigations can only be lengthy, since post-treatment follow-ups will necessarily require important, time-consuming and clinically complex observations.

From these considerations, therefore, it is clear that it cannot be overlooked that while there is extremely interesting pre-clinical data on Flash technology today, the need to obtain clinical confirmations on humans will be a major challenge from all parties (manufacturers, scientific community) who would like to confirm the validity of this technology on humans. A challenge as necessary as of defining a particular standard to be used for verification of radiogenic safety, similar to 60601-2-1, and no less complicated, indeed.

Proposed standards for VHEE systems

Future standards for Very High Energy Electron (VHEE) therapy must focus on ensuring optimal Dose Volume Histograms (DVH) and Dose Rate Volume Histograms (DRVH) on a voxel-by-voxel basis [37], specifically tailored to the unique characteristics of each dose delivery mechanism. This approach is essential for accurately assessing treatment plans and improving patient outcomes.

Establishing thresholds

To effectively implement these standards, a double threshold must be established:

- Energy Threshold: The lower threshold should be set at 50 MeV, as this is the point beyond which IEC 60601-2-1 standards do not apply. This regulation ensures that equipment used for VHEE therapy meets stringent safety and performance criteria, which are crucial for high-energy applications.
- Average/Instantaneous Dose Rate and Dose per Pulse Threshold: The second threshold should focus on average/instantaneous dose rates and/or dose per pulse metrics. This is particularly important for UHDR modalities, where the delivery of high doses in short time frames can significantly impact treatment efficacy and normal tissue sparing.

Mathematical definitions of UHDR

Defining precise mathematical parameters for UHDR in the context of VHEE is essential, as current definitions designed for proton therapies may not directly apply. This requires the development of new models and algorithms that consider the unique interactions and physical characteristics of VHEE beams, including their energy deposition patterns and biological effects. The relationship between the quantities measured by the beam monitoring system, those verified through quality assurance, and those calculated by the treatment planning system is particularly complex.

In conventional RT, the physical observable is the delivered dose, monitored by the monitoring system (monitor chamber, electrometer, HMI). However, in the case of UHDR, it is critical to not only define the delivered dose but also account for the temporal characteristics of each beam delivery within the different radiation fields. This ensures:

- Accurate evaluation of radiobiological effects: The treatment planning system must be able to correctly assess the radiobiological impact of the dose delivery.
- Real-time monitoring of quality and conformity: During treatment, the beam monitoring system must verify that the delivery aligns with the calculated plan in terms of quality and dose conformity both spatially and temporally.

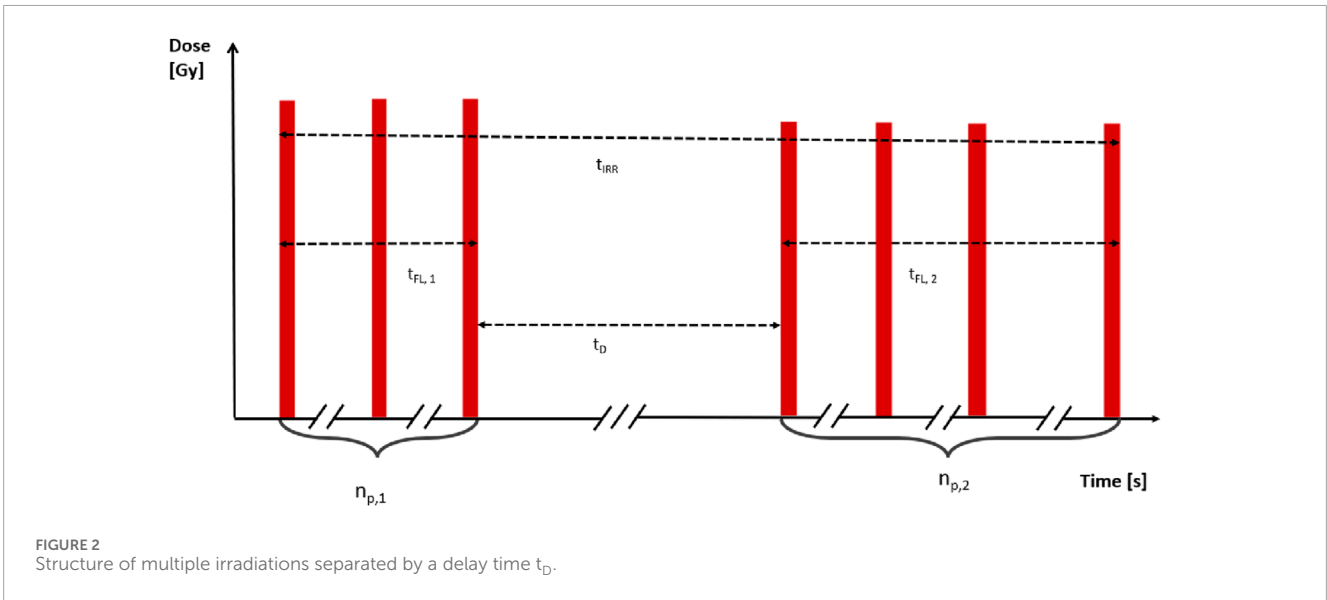
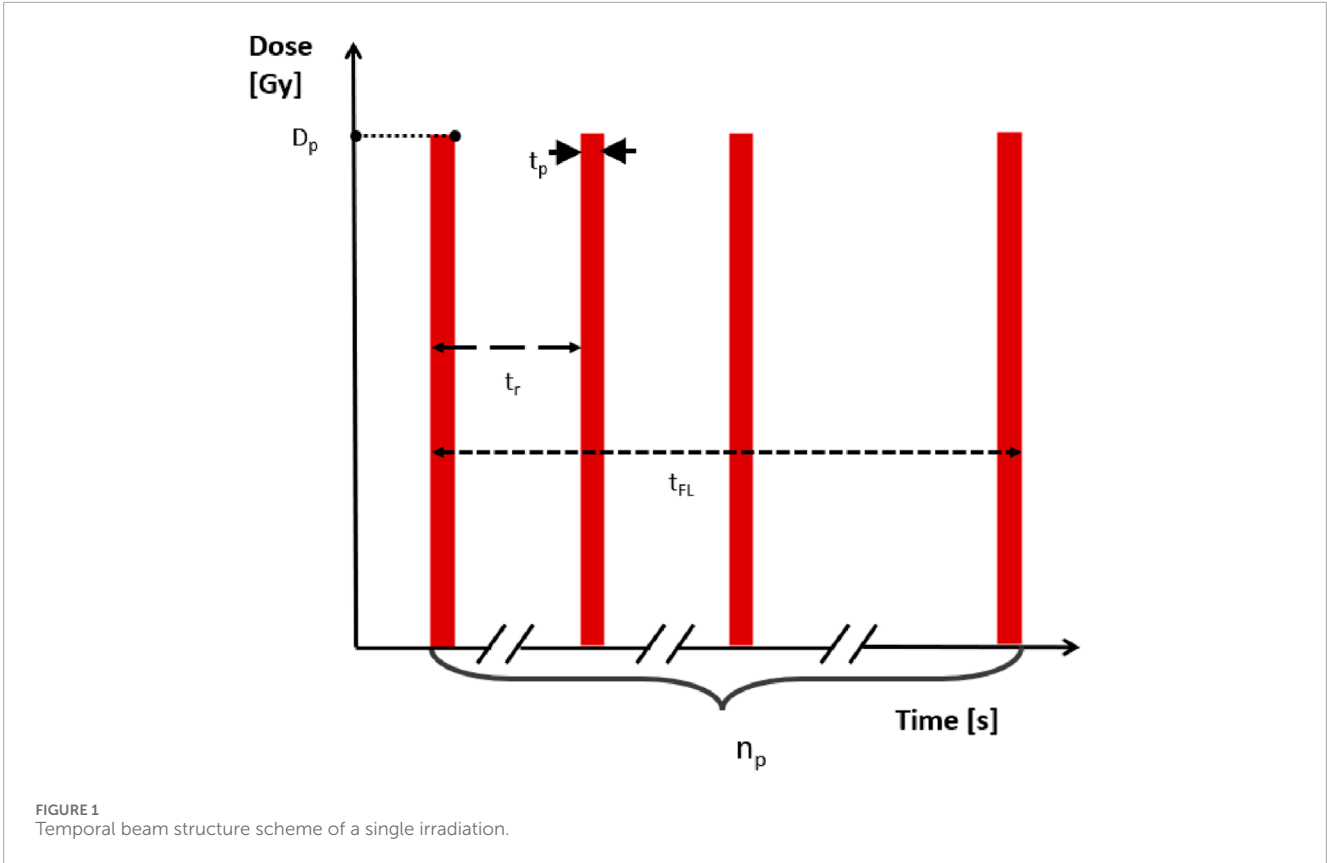
In addition, for pencil beam scanning, a new formalism must be developed to manage beamlet penumbra and scanning time, similar to the approach used for protons [38].

Temporal beam structure

There are two conditions which seem to trigger the FLASH effect: average dose rate greater than 40 Gy/s and a total irradiation time less than 0.2 s [39, 40]. Nevertheless, the temporal beam structure is quite complex, and these two parameters are not enough to fully describe it [41–43]. Given the relationship between VHEE and UHDR, it is crucial to establish standard definitions for the beam's temporal structure, along with the mathematical relationships between these parameters:

- Temporal beam structure: The temporal sequence of the beam delivery. It is identified by the entire set of Dose per pulse, Pulse duration, Time between pulses, Pulse Repetition Frequency, Number of Pulses, Irradiation Time, and Delay Time.
- Dose per pulse (D_p): Dose of a single pulse at the Equipment reference point (ERP).
- Pulse duration (t_p): Temporal width of a single pulse.
- Time between pulses (t_r): Time between two pulses in a sequence of pulses of irradiation.
- Pulse repetition frequency (PRF): Frequency of repetition of the pulses in a sequence of pulses of irradiation.
- Number of pulses (n_p): Number of pulses in a sequence of pulses of the irradiation.
- Irradiation time (t_{FL}): Temporal duration of a sequence of pulses of the irradiation.
- Delay time (t_D): Time separation between two subsequent sequences of pulses of the irradiation.
- Delivered dose (DD): Total delivered dose at ERP during t_{FL} .
- Total irradiation time (t_{IRR}): The sum of all irradiation and delay times.
- Total delivered dose (TD): Total delivered dose at ERP during t_{IRR} .
- Average Dose rate (DR): Dose rate during a sequence of pulses of the irradiation at ERP. The ratio of Delivered Dose (DD) and Irradiation Time (t_{FL}).
- Intra-pulse Dose rate (DR_p): Dose rate within the pulse at ERP. The ratio of Dose per Pulse (D_p) and Pulse Duration (t_p).
- Instantaneous Dose rate (IDR): Dose rate value at a specific moment of time within the pulse at ERP.

In general, medical linacs inherently generate pulsed beams; each irradiation event encompasses a sequence of pulses, each pulse of the duration t_p of a few microseconds. The pulses are spaced apart by a time interval denoted as t_r , which typically ranges in the order of tenths of milliseconds. The value of t_r is inversely



related to the *Pulse Repetition Frequency (PRF)*, determining the rate at which pulses are delivered. A representation of this general scheme is depicted in [Figure 1](#). An irradiation can also consist in a series of multiple sub-irradiations separated by a delay time t_D . A representation of this general scheme is depicted in [Figure 2](#).

Where:

– $D_p^{(n),k}$ dose of n^{th} pulse in the k^{th} irradiation at the ERP [Gy]

- t_p^k time width of a single pulse in the k^{th} irradiation [s]
- t_r^k time between two pulses in the k^{th} irradiation [s]
- PRF^k Pulse Repetition Frequency in the k^{th} irradiation [s^{-1}]
- $n_{p,k}$ Number of pulses of the k^{th} irradiation
- t_{FL}^k irradiation time of the k^{th} irradiation [s]
- t_D^k delay time, time separation between the k^{th} and $(k+1)^{\text{th}}$ irradiations [s]
- DD^k delivered dose at ERP during t_{FL}^k [Gy]

- t_{IRR} Total irradiation time [s]
- TD total delivered dose at ERP during t_{IRR} [Gy]
- DR^k Average Dose Rate during the k^{th} irradiation at ERP [$Gy\ s^{-1}$]
- $DR_p^{i,k}$ Dose rate within the i^{th} pulse during the k^{th} irradiation at ERP [$Gy\ s^{-1}$]
- $IDR^{i,k}$ Instantaneous Dose Rate within the i^{th} pulse during the k^{th} irradiation at ERP [$Gy\ s^{-1}$]

In case of a single irradiation (Figure 1), the following relations hold:

$$PRF = \frac{1}{t_r}$$

$$t_{FL} = \frac{n_p - 1}{PRF} + t_p \cong \frac{n_p - 1}{PRF}$$

$$TD = \sum_{i=1}^{n_p} D_p^i = n_p \cdot \overline{D_p}, \text{ where } \overline{D_p} = \frac{1}{n_p} \sum_{i=1}^{n_p} D_p^i$$

$$DR = \frac{TD}{t_{FL}} = \frac{1}{t_{FL}} \sum_{i=1}^{n_p} D_p^i \cong PRF \cdot \overline{D_p}$$

$$DR_p = \frac{D_p}{t_p}; DR_p = \frac{t_r}{t_p} DR$$

$$D_p = \int_0^{t_p} IDR(t) dt = DR_p \cdot t_p; DR_p = IDR \leftrightarrow \frac{dIDR(t)}{dt} = 0 \forall t \in (0, t_p)$$

If the irradiation consists of multiple sub-irradiations (Figure 2), the previous equations can be easily generalized and the additional relations hold:

$$t_{IRR} = t_{FL}^1 + t_D^1 + \dots + t_D^{N-1} + t_{FL}^N,$$

being N the total number of sub-irradiations

$$TD = \sum_{i=1}^N DD^i$$

Correlation between e-beam current and its kinetic energy

To reach the fluences required in for UHDR mode, electron beam current accelerated is increased respect to the current electron accelerators. In these conditions, the power absorbed by e-beam becomes comparable with the power absorbed by the accelerating waveguide; therefore, any e-beam current variation implies a variation in the kinetic energy [44]. Let be W the power generated by the radiofrequency, it is

$$W_{TOT} = W_{LINAC} + W_{BEAM} + W_{LOSS}$$

The power absorbed by the accelerated waveguide, and thus the electric field, can be calculated as

$$W_{LINAC} = \frac{\left(\int_0^{S_{LINAC}} E_0(s) \cdot ds \right)^2 \cdot T^2}{Z_{LINAC}}$$

where E_0 is the on axis electric field inside the accelerating waveguide, S its overall length, T the transit time factor and Z_{LINAC} its shunt impedance.

The power absorbed by the electron beam can be calculated as

$$W_{BEAM} = E(eV)I_{BEAM}(A)$$

In the following example, consider the case of a high current VHEE linac [45]:

- Nominal energy $E_0 = 130\ MeV$
- Beam Current $I_{BEAM} = 0.2\ A$
- Linac length $S_{LINAC} \cong 5\ m$

Assuming a shunt impedance per unit length of $100\ M\Omega/m$, resulting in $Z_{LINAC} \sim 500\ M\Omega$, it follows that:

$$W_{LINAC} = \frac{\left(\int_0^{S_{LINAC}} E_0(s) \cdot ds \right)^2 \cdot T^2}{Z_{LINAC}} \cong \frac{130^2}{500} MW = 34\ MW$$

And

$$W_{BEAM} = E(eV)I_{BEAM}(A) \cong (130 \cdot 10^6 eV \cdot 0.2A) = 26\ MW$$

Therefore, the two terms are comparable; any variation in the beam current implies a fluctuation in beam energy as well. Hence both beam current and beam energy should be measured independently, and an additional interlock on beam energy could be considered.

Beam monitoring and temporal structure

Importance of beam monitoring

Effective beam monitoring is vital for ensuring treatment accuracy and safety. The **temporal structure** of VHEE beams, along with the potential spatial overlap of individual beamlets in pencil beam scanning delivery, must be meticulously monitored. Therefore, alternatives to conventional ionization chambers and detectors, which are susceptible to saturation at ultra-high dose rates [44] must be considered [46, 47].

Special considerations for beam monitoring

Real-time beam monitoring presents significant challenges, particularly with respect to ultra-high dose rate delivery and the beam's temporal structure of VHEE system. Conventional transmission detectors, such as gas-filled transmission ionization chambers used as golden standard in radiotherapy, encounter issues like ion recombination effect under UHDR exposures [44]. Additionally, these detectors must provide rapid feedback signals to halt the beam once the intended radiation dose has been delivered. However, ionization chambers, which are commonly used as beam monitors in clinical radiotherapy, tend to have slow timing responses with ion collections times on the order of $300\ \mu s$ in $5\ mm$ air gap separation. As a result, new beam monitoring systems may be required for safe delivery of clinical VHEE RT machines.

Currently, no ideal detector exists for monitoring UHDR VHEE beams. Nonetheless, various approaches are being explored to adapt ionization chambers for this purpose. One promising design is the multi-gap ionization chamber proposed by Giordanengo et al. [48].

This instrument features three parallel-plate ionization chambers, each with a different gap width. The charge collected by each chamber exhibits varying levels of ion recombination depending on the electrode spacing, which can be phenomenologically modeled to facilitate corrections for charge collection efficiency.

Ultra-thin silicon detectors have also been investigated as potential beam monitors due to their high sensitivity, exceptional spatial resolution, and strong radiation hardness [49]. Previous studies have demonstrated excellent linearity with dose rates for both photon [50] and proton beams [51]; however, further evaluation is needed to assess their applicability for pulsed electron beams. As such, the design and development of an optimal geometry for silicon detectors are still in progress.

Silicon carbide (SiC) detectors are gaining traction as a promising alternative for dosimetry and monitoring in UHDR beam applications [52]. These detectors offer significant advantages, including strong radiation resistance, rapid response times, high sensitivity, and stability across varying dose rates [53, 54]. However, extensive research is still required to fully harness the capabilities of this technology.

Beam current transformers (BCTs) are non-intercepting, inductive current monitors that have shown potential for real-time monitoring of UHDR electron beams [55–57]. Commonly used in research electron accelerators, they facilitate non-destructive charge measurements of individual beam pulses with high accuracy and reproducibility [58]. However, a key limitation of BCTs is their inability to provide information on beam cross-section and spatial distribution, rendering them ineffective for determining beam dimensions or flatness [29].

Recently, calorimetric methods have emerged as viable options for monitoring UHDR exposures [59]. A significant advantage of calorimetry is its dose-rate independence due to the physical nature of the phenomena. Furthermore, a transmission calorimeter can be designed with multiple sections to effectively detect beam symmetry and flatness. While further development is needed to fully exploit the capabilities of calorimetric methods, they continue to show promise as a technique for monitoring UHDR beams.

Differentiation of beam types

Additionally, it is important to distinguish between the treatment approaches for broad and pencil beams, as each modality presents unique advantages and challenges. Broad beams offer the advantage of quicker implementation since they are more closely aligned with conventional irradiation techniques and single-field UHDR irradiation. The beam monitoring requirements are less stringent, with the primary distinction from IEC 60601-2-1 being the UHDR component. Monitoring for broad beams must focus on the dose delivered, current and energy variations, temporal beam structure, and gantry rotation, which affects the delay between irradiation trains. However, broad beams face significant challenges, particularly because clinical implementation heavily relies on the tissue-sparing effect of FLASH. This is compounded by the fact that broad beams offer less conformality compared to pencil beams and result in a higher surface dose than protons or light ions. Radiation safety can also be a concern, as beam broadening (whether passive or active) and field collimation introduce additional stray radiation

and neutron production due to interactions between high-energy electrons and beamline components.

On the other hand, pencil beams offer greater conformality [60], which reduces the reliance on a stronger FLASH effect and allows for more complex treatments. This approach also minimizes stray radiation through magnetic scanning techniques. However, pencil beam scanning presents a more complex formalism, similar to UHDR protons [38], and necessitates monitoring of the angular divergence of beamlets, as seen in proton therapy (IEC 60601-2-64). Furthermore, pencil beams require a more advanced beam monitoring system to track the position of individual beamlets, necessitating sophisticated technology beyond the integration systems like ACCTs (Alternating-Current Current Transformers) typically used for UHDR delivery [61]. In summary, the development of future standards for VHEE therapy should prioritize the development of comprehensive DVH and DRVH metrics that are energy-specific and dose-rate-focused. By establishing clear thresholds and enhancing beam monitoring capabilities, the treatment planning process can be significantly improved. This approach will ultimately lead to better patient outcomes through optimized dose delivery and reduced risks to healthy surrounding tissues, paving the way for the clinical implementation of VHEE therapies in radiation oncology.

Human-machine interface and radiation protection

The design of the human-machine interface (HMI) and control console for VHEE systems is crucial for ensuring both intuitive operation and robust safety protocols. As VHEE technology advances, it is essential to evaluate how these systems differ from existing standards, particularly concerning radiation protection aspects such as neutron yield and stray radiation.

Human-machine interface design

The HMI for VHEE systems must prioritize user-friendliness to facilitate seamless operation by medical personnel. Key features include:

- **Intuitive Controls:** The interface should provide clear visual indicators and controls that allow operators to easily adjust settings and monitor system performance in real-time.
- **Safety Features:** Built-in safety mechanisms, such as emergency shut-off controls and interlocks, are paramount to protect both patients and staff.

Radiation protection considerations

Differences from existing standards

Current regulations, including IEC 60601-2-1, may not adequately encompass the specific safety requirements presented by VHEE systems. Key areas that require attention include:

- **Neutron Yield:** VHEE systems can produce photoneutrons due to high-energy electron interactions, which poses unique

challenges in radiation protection. Studies indicate that the neutron yield from VHEE systems is comparable to that of conventional proton therapy [62]. However, it is crucial to carefully evaluate the implications for both patient and staff exposure.

- **Stray Radiation:** The risk of stray radiation from VHEE systems necessitates additional monitoring and shielding strategies to ensure compliance with safety standards. This is particularly important in clinical settings where multiple treatment areas may be in proximity, in addition to UHDR radiation safety requirements [63].

Need for dedicated standards

A simple amalgamation of existing standards, such as IEC 60601-2-1 and IEC 60601-2-64, is insufficient to guarantee the basic safety and essential performance of VHEE systems. Instead, a dedicated set of standards tailored to the unique characteristics of VHEE technology is required. This includes:

- **Advanced Beam Monitoring Requirements:** Establishing precise standards for real-time beam monitoring systems is critical, especially for UHDR VHEE beams. This includes defining the performance specifications for new detectors, tailored to the ultra-high dose rates and unique temporal structures of VHEE beams. These standards must address rapid feedback mechanisms, accuracy in dose delivery, and spatial beam monitoring to ensure treatment precision and patient safety.
- **Integration with Imaging and Treatment Planning:** Updates to the broader family of radiation oncology systems must encompass imaging, planning, and positioning technologies to accommodate the new VHEE requirements. This integration will enable comprehensive treatment planning that considers both therapeutic and safety aspects.
- **Specific Radiation Protection Guidelines:** Developing guidelines that address the unique neutron and radiation profiles of VHEE systems will enhance safety protocols and operational standards.

The design of the human-machine interface and control console for VHEE systems must balance intuitive operation with stringent safety measures. As VHEE technology progresses, it is crucial to develop dedicated standards that address the unique radiation protection challenges associated with high-energy electron therapy. By focusing on specific guidelines for neutron yield, stray radiation, and comprehensive treatment planning, the medical community can ensure the safe and effective implementation of VHEE systems in clinical practice.

Conclusion

The integration of VHEE technology into clinical practice represents a transformative advancement in the treatment of deep-seated tumors, particularly through the application of Ultra-High Dose Rate (UHDR) modalities. While the potential benefits are substantial, the absence of regulatory standards poses significant challenges that must be addressed through collaborative research and development efforts.

Promising advances in treatment

VHEE technology offers several advantages for radiation oncology, particularly in the treatment of tumors located deep within the body. Key benefits include:

- **Enhanced Tumor Targeting:** VHEE beams can deliver high doses of radiation with precision, allowing for effective treatment of complex tumor geometries while minimizing damage to surrounding healthy tissues.
- **Potential for FLASH Effect:** The ultra-high dose rates associated with VHEE therapy may leverage the FLASH effect, which has been shown to reduce normal tissue toxicity while maintaining tumor control, thus improving patient outcomes.
- **Reduced Treatment Times:** The UHDR capabilities of VHEE systems enable rapid dose delivery, which can improve patient throughput and enhance overall treatment efficiency.

Challenges of regulatory standards

Despite the promising advances in VHEE technology, the absence of established regulatory standards poses several challenges:

- **Safety and Efficacy Concerns:** Without comprehensive standards, there is a risk that VHEE systems may not meet the necessary safety and performance benchmarks, potentially compromising patient safety and treatment efficacy.
- **Variability in Practice:** The lack of standardized protocols can lead to inconsistencies in treatment practices across different institutions, making it challenging to ensure consistent patient care and outcomes.
- **Need for Collaborative Research:** Addressing these challenges necessitates a collaborative effort among stakeholders - including regulatory bodies, manufacturers, and clinical practitioners - to develop evidence-based guidelines that reflect the unique characteristics of VHEE technology.

Establishing comprehensive standards

To facilitate the successful integration of VHEE systems into clinical practice, it is essential to establish a comprehensive set of standards that encompass:

- **Design and Implementation Guidelines:** Clear guidelines for the design and operational protocols of VHEE systems will aid manufacturers in creating equipment that meets safety and performance criteria.
- **Integration with Existing Oncology Practices:** Standards should also consider the integration of VHEE technology with existing imaging, planning, and treatment delivery systems to create a cohesive treatment environment.
- **Radiation Protection Protocols:** Specific protocols addressing the unique radiation profiles of VHEE systems, including neutron yield and stray radiation, are crucial for ensuring the safety of both patients and healthcare providers.

In conclusion, the future of radiation oncology may significantly depend on the successful integration of VHEE technology, contingent upon the development and adoption of essential regulatory standards. By addressing the current challenges through collaborative research and establishing comprehensive guidelines, the medical community can harness the full potential of VHEE systems to enhance the treatment of deep-seated tumors. This proactive approach will not only ensure patient safety and treatment efficacy but also foster innovative advancements in cancer therapy, ultimately improving patients' outcomes worldwide.

Data availability statement

The original contributions presented in the study are included in the article/supplementary material, further inquiries can be directed to the corresponding authors.

Author contributions

JP: Conceptualization, Investigation, Writing—original draft, Writing—review and editing. FD: Conceptualization, Writing—original draft, Writing—review and editing. AC: Writing—review and editing. MC: Writing—review and editing. AD: Writing—review and editing. MD: Writing—review and editing. GF: Writing—review and editing. LG: Writing—review and editing. LM: Writing—review and editing. GM: Writing—review and editing. PM-G: Writing—review and editing. FP: Writing—review and editing. MP: Writing—original draft, Writing—review and editing. VP: Writing—review and editing. SP: Writing—review and editing. PP: Writing—review and editing. FR: Writing—review and editing. ASa: Writing—review and editing. ASu: Writing—original draft, Writing—review and editing. AV: Writing—review and editing. GF: Conceptualization, Investigation, Writing—original draft, Writing—review and editing.

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Conflict of interest

Authors MD, LG, and GF were employed by Sordina IORT Technologies S.p.A. Author MP was employed by Maytal International Ltd. – Global Med Dev Expertise.

The remaining authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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