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Dynamic behavior of a two-mass nonlinear fractional-order vibration system

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The two-mass nonlinear vocal cord vibration system (VCVS) serves as a mechanical representation of the fundamental vocalization process. Traditional models of the VCVS, which are based on integer-order dynamics, often overlook the impact of memory effects. To address this limitation and enhance the accuracy of simulations, this study incorporates the memory effects of vocal cord vibrations by integrating the Grunwald–Letnikov fractional derivative into the two-mass nonlinear VCVS framework. Initially, a high-precision computational scheme is formulated for the two-mass nonlinear fractional-order VCVS. Subsequently, the model undergoes a comprehensive series of numerical simulations to investigate its dynamic characteristics. The findings reveal that the dynamics of the fractional-order VCVS exhibit a significantly higher complexity compared to the conventional integer-order models, with the emergence of novel chaotic behaviors that were previously unobserved.

KEYWORDS

fractional-order vibration system, novel chaotic dynamic behavior, high-precision numerical method, vibration system, vocal cord vibration system

1 Introduction

With the continuous development and improvement of computer technology and numerical simulation methods, the application of nonlinear vibration technology has been widely used in many fields and has become one of the hot topics in various fields.

Nonlinear dynamics can not only be used to analyze and explore certain natural phenomena and physical processes but can also be applied to other fields such as medicine, acoustics, ecology, and economics. Nonlinear vibration is very important in the study of MEMS oscillators [1, 2] and their interaction with structures. MEMS oscillators have a wide range of applications, including consumer electronics, automotive, healthcare, industries, aerospace, and many other fields. In recent years, vocal cord computer simulation technology has been used in the diagnosis of laryngeal diseases, can use the vocal cord pronunciation function [3], acoustic analysis to reflect the lesions of the vocal band. The study of the vocal cord vibration model [4] can reveal the characteristics of vocal band vibration and help understand the mechanism of vocal cord vibration. This study provides theoretical guidance for laryngeal pathology, artificial organs, voice therapy, and other medical fields and has practical application value. Researchers have also been trying to mimic human sound production by not only developing mechanical and mathematical models to describe the human organs associated with sound production but also studying the process of producing sound.



Numerical simulation of time series plots at $\alpha = [1, 1, 1, 1]$, and $\alpha = [0.99, 1.01, 0.95, 0.95]$, $h = 0.01, T = 1000, r_1 = 0.01, r_2 = 0.5, k_1 = 0.9, k_2 = 0.1, k_c = 0.5, c = 0.2, B = 0.2$.



Vocal cord vibration can be simplified into various physical models, and the mass model represented by the spring mass block is a typical physical model of the vocal cord. These vocal cord vibration models represent vocal cord and polyp vibration with different numbers of spring mass blocks, such as the single-mass block model [5], the two-mass vocal cord model [6], three-mass vocal cord model, and H-C model. Latest research on the vocal cord vibration model involves the single-mass block model [5]. One of the simplest models is the single-degree-of-freedom single-mass model, which was first proposed by Dr. Flanagan and has





since been studied by many researchers in related fields. Dr. Flanagan uses electricity acoustic analysis [7] which describes the dynamic knowledge of vocal cords and proposes a vocal cord model of a single-mass vibration system, in which self-excited vibration is caused by air flow that changes with

pressure. [6] introduced the nonlinear properties of vocal cord organization into the two-mass model of vocal cords and proposed an improved nonlinear two-mass model of symmetrical vocal cords. In this model, the two vocal cords are assumed to be identical and move symmetrically relative to the glottic midline.





When the glottis is open, the equation for vocal cord movement can be written as follows:

$$\begin{cases} m_1 \ddot{x}_1 + b_1 (x_1, \dot{x}_1) + s_1 (x_1) + k_c (x_1 - x_2) = f_1, \\ m_2 \ddot{x}_1 + b_2 (x_2, \dot{x}_2) + s_2 (x_1) + k_c (x_2 - x_1) = f_2, \end{cases}$$
(1)

where x_i is the displacement and m_i is the quality of the Equation 1. $b_i(x_i, \dot{x_i})$ is the damping force, and $s_i(x_i)$ is the elastic force. In this model (1), Lucero and Koenig introduced the cubic characteristics of biological tissue elasticity [8], as shown in Equation 2:

$$s_i(x_i) = k_i x_i (1 + 100 x_i^2), \quad i = 1, 2.$$
 (2)

On the other hand, for damping forces, instead of using the usual linear term $r_i x_i$, nonlinear properties are used:

$$b_i(x_i, \dot{x}_i) = r_i(1 + 150|x_i|)\dot{x}_i, \quad i = 1, 2.$$
 (3)

 r_i represents the damping coefficient, and k_i, k_c represent all coefficients in Equation 3.

The nonlinear term is used because when the width of the glottis increases, it is necessary to limit the amplitude of vocal cord vibration to ensure the effectiveness of the simulation.

As is known, there are many kinds of fractional derivatives, such as the Caputo fractional derivative, Caputo fractional derivative, Grünwald–Letnikov fractional derivative, and two-scale fractal derivative [9, 10] [11–13]. Fractional derivatives are widely used in many fields, such as engineering, physics, signal processing, and

biomathematics. Some fractional derivatives have memory and nonlocality. In the VCVS, memory refers to the ability of the system to retain information about past events and use it to influence future behavior. Because of the memory of vocal cord vibration, the integer-order VCVS ignores the influence of memory. Therefore, in order to ensure the effectiveness of the simulation, the following fractional-order VCVS is considered in this paper:

$$\begin{cases} m_1 D_t^{\alpha_1 + \alpha_3} x_1 + b_1 (x_1, D_t^{\alpha_1} x_1) + s_1 (x_1) + k_c (x_1 - x_2) = f_1, \\ m_2 D_t^{\alpha_2 + \alpha_4} x_1 + b_2 (x_2, D_t^{\alpha_2} x_2) + s_2 (x_1) + k_c (x_2 - x_1) = f_2, \end{cases}$$
(4)

where $D_t^{\alpha} x_1$ is the Grünwald–Letnikov differential derivative. $\alpha = 1$; the fractional-order model (4) is the integer-order model (1).

The Grünwald–Letnikov fractional calculus is named after the Czech mathematician Anton Karl Grünwald and Russian mathematician Aleksey Vasilievich. They defined Grünwald–Letnikov fractional calculus in 1867 and 1868, respectively. In the finite difference scheme of integer derivative, when calculating the derivative value of a node, the function value at the first few nodes is needed, or the function value at the next few nodes is needed. In contrast, the calculation of fractional derivatives requires the function values at all nodes before or after a certain point in time, so fractional calculus is assumed to have memory properties.

Some scholars have applied the fractional microproduct to memory modeling damping vibration systems. [14] focused on investigating the



chaotic behavior of a 2-D vocal dynamical system using fractional-order Caputo difference operators, both commensurate and incommensurate. The methodology involves a dynamical analysis of the discrete fractional-order system, employing bifurcation theory, Lyapunov exponents, and coexisting attractors to understand the dynamical behavior. [15] gave a high-precision numerical approach to solving the space fractional Gray–Scott model. [16] gave some novel patterns for a class of fractional reaction–diffusion models with the Riesz fractional derivative. [17] researched on the pattern dynamics behavior of a fractional vegetation-water model in an arid flat environment. [18] researched the chaotic dynamic behavior of fractional-order financial systems with constant inelastic demand. [19] solved two-sided fractional super-diffusive partial differential equations with variable coefficients in a class of new reproducing kernel spaces. [20] studied the low frequency property of a fractal vibration model for a concrete beam. The fractal dimension formulation



[21] made the fractal theory accessible to porous media and discontinuous time. [22] implemented the homotopy perturbation method for fractal duffing oscillators with arbitrary conditions. [23, 24] applied Li-He's modified homotopy perturbation method for the doubly clamped electrically actuated microbeam-based microelectromechanical system and the dropping shock response of a tangent nonlinear packaging system. [25] studied autonomous ordinary differential systems. [26] studied the Kaup-Newell system. [27] studied the nanobeam-based N/MEMS system, and [28] studied the fractal pull-in motion of electrostatic MEMS resonators. This paper introduces a numerical approach for the fractional-order vocal cord vibration model. [29] used the discontinuous Galerkin finite element method for the Caputo-type nonlinear conservation law. [30] used nonuniform L1/discontinuous Galerkin approximation for the timefractional convection equation with a weak regular solution and the time fractional convection-diffusion-reaction Equation [31], and so on fractional systems [32, 33].

Fractional calculus has become a fundamental tool for modeling memory phenomena. However, due to the complexity and the nonlocality of fractional calculus, numerical methods are often used to approximate solutions to fractional differential equations, especially when analytical solutions are not feasible. The numerical computation of solving fractional differential equations is both cumbersome and time-consuming. Developing numerical and analytical methods for solving nonlinear fractional differential equations is currently a hot research topic. This paper introduces a high-precision method to study a class of fractional-order vocal cord vibration model.

2 Numerical method

Definition 2.1: [34] The Grünwald–Letnikov fractional derivative for the function $\mathbf{x}(t)$ with respect to $t \in [0, T]$ of order α is defined as follows:

$$D_t^{\alpha} \mathbf{x}(t) = \lim_{h \to 0} \frac{1}{h^{\alpha}} \sum_{j=0}^m \frac{(-1)^j \Gamma(\alpha+1)}{\Gamma(j+1) \Gamma(\alpha-j+1)} \mathbf{x}(t-jh),$$
(5)

where h = T/m is the step size. Let

$$\Psi_{j}^{(\alpha)} = (-1)^{j} {\alpha \choose j} = \frac{(-1)^{j} \Gamma(\alpha + 1)}{\Gamma(j + 1) \Gamma(\alpha - j + 1)}, \quad j = 0, 1, \dots, m.$$
(6)

Using Newton's binomial theorem. get $(1-z)^n = \sum_{j=0}^n (-1)^j {n \choose j} z^j = \sum_{j=0}^n \Psi_j^{(n)} z^j, \text{ and } \sum_{j=0}^\infty \Psi_j^{(\alpha)} z^j = (1-z)^{\alpha}.$ Combining Equations 5, 6, we obtain the following Theorem 2.2.

Theorem 2.2: [34] The Grünwald–Letnikov fractional derivative for the function $\mathbf{x}(t)$ with respect to $t \in [0, T]$ of order α can be calculated directly by the following formula:

$$D_t^{\alpha} \mathbf{x}(t) = \lim_{h \to 0} \frac{1}{h^{\alpha}} \sum_{j=0}^m \Psi_j^{(\alpha)} \mathbf{x}(t-jh),$$
(7)

where $\Psi_j^{(\alpha)} = (1 - \frac{\alpha+1}{j})\Psi_{j-1}^{(\alpha)}, \Psi_0^{(\alpha)} = 1.$ According to Equation 7, let $D_t^{\alpha}x_1 = x_3, D_t^{\alpha}x_2 = x_4$, then Equation 4 can be converted to Equation 8

$$\begin{cases} D_t^{\alpha_1} x_1 = x_3, \\ D_t^{\alpha_2} x_2 = x_4, \\ D_t^{\alpha_3} x_3 = \frac{f_1 - b_1(x_1, x_3) - s_1(x_1) - k_c(x_1 - x_2)}{m_1}, \\ D_t^{\alpha_4} x_4 = \frac{f_2 - b_2(x_2, x_4) - s_2(x_2) - k_c(x_2 - x_1)}{m_2}, \end{cases}$$
(8)

Using Theorem (2.2), we can obtain the numerical calculation scheme for Equation 8, which is Equation 9:

$$\begin{cases} x_{1}(t_{k}) = h^{\alpha_{1}}x_{3}(t_{k-1}) + x_{1}(0) - \sum_{j=1}^{m} \Psi_{j}^{\alpha_{1}}(x_{1}(t_{k-j}) - x_{1}(0)), \\ x_{2}(t_{k}) = h^{\alpha_{2}}x_{4}(t_{k-1}) + x_{2}(0) - \sum_{j=1}^{m} \Psi_{j}^{\alpha_{2}}(x_{2}(t_{k-j}) - x_{2}(0)), \\ x_{3}(t_{k}) = h^{\alpha_{3}}\frac{f_{1}(t_{k}) - b_{1}(x_{1}(t_{k}), x_{3}(t_{k-1})) - s_{1}(x_{1}(t_{k})) - k_{c}(x_{1}(t_{k}) - x_{2}(t_{k})))}{m_{1}} \\ + x_{3}(0) - \sum_{j=1}^{m} \Psi_{j}^{\alpha_{3}}(x_{3}(t_{k-j}) - x_{3}(0)), \\ x_{4}(t_{k}) = h^{\alpha_{4}}\frac{f_{2}(t_{k}) - b_{2}(x_{2}(t_{k}), x_{4}(t_{k-1})) - s_{2}(x_{2}(t_{k})) - k_{c}(x_{2}(t_{k}) - x_{1}(t_{k}))}{m_{2}} \\ + x_{4}(0) - \sum_{j=1}^{m} \Psi_{j}^{\alpha_{4}}(x_{4}(t_{k-j}) - x_{4}(0)). \end{cases}$$
(9)

In Ref. [35, 36] gave the construction method of generating function of any order in order to obtain high accuracy, and then gave the high-precision recursive formula of fractional derivative.

Theorem 2.3: [35] The Grünwald–Letnikov fractional derivative for the function $\mathbf{x}(t)$ with respect to $t \in [0, T]$ of order α of the generating function for arbitrary p is shown in Equation 10:

$$D_t^{\alpha} \mathbf{x}(t) = \lim_{h \to 0} \frac{1}{h^{\alpha}} \sum_{j=0}^m \Psi_j^{(\alpha,p)} \mathbf{x}(t-jh),$$
(10)

where $\Psi_k^{(\alpha,p)}$ is shown in Equation 11:

$$\begin{cases} \Psi_{0}^{(\alpha,p)} = \mathbf{g}_{0}, \quad k = 0, \\ \Psi_{k}^{(\alpha,p)} = -\frac{1}{\mathbf{g}_{0}} \sum_{i=0}^{k-1} \left(1 - i\frac{1+\alpha}{k}\right) \mathbf{g}_{i} \Psi_{k-i}^{(\alpha,p)}, \quad k = 1, 2, \dots, p-1, \\ \Psi_{k}^{(\alpha,p)} = -\frac{1}{\mathbf{g}_{0}} \sum_{i=0}^{p} \left(1 - i\frac{1+\alpha}{k}\right) \mathbf{g}_{i} \Psi_{k-i}^{(\alpha,p)}, \quad k = p, p+1, p+2, \dots. \end{cases}$$
(11)

 \mathbf{g}_k is shown in Equation 12:

$$\begin{pmatrix} 1 & 1 & 1 & \cdots & 1 \\ 1 & 2 & 3 & \cdots & p+1 \\ 1 & 2^2 & 3^2 & \cdots & (p+1)^2 \\ \vdots & \vdots & \vdots & \cdots & \vdots \\ 1 & 2^p & 3^p & \cdots & (p+1)^p \end{pmatrix} \begin{pmatrix} \mathbf{g}_0 \\ \mathbf{g}_1 \\ \mathbf{g}_2 \\ \vdots \\ \mathbf{g}_p \end{pmatrix} = - \begin{pmatrix} 0 \\ 1 \\ 2 \\ \vdots \\ p \end{pmatrix}.$$
(12)

Using Theorem (2.3), we can obtain the following the numerical calculation scheme (Equation 13) of Equation 8:

$$\begin{cases} x_{1}(t_{k}) = h^{a_{1}}x_{3}(t_{k-1}) + x_{1}(0) - \sum_{j=1}^{m} \Psi_{j}^{(a_{1},p)} (x_{1}(t_{k-j}) - x_{1}(0)), \\ x_{2}(t_{k}) = h^{a_{2}}x_{4}(t_{k-1}) + x_{2}(0) - \sum_{j=1}^{m} \Psi_{j}^{(a_{2},p)} (x_{2}(t_{k-j}) - x_{2}(0)), \\ x_{3}(t_{k}) = h^{a_{3}}\frac{f_{1}(t_{k}) - b_{1}(x_{1}(t_{k}), x_{3}(t_{k-1})) - s_{1}(x_{1}(t_{k})) - k_{c}(x_{1}(t_{k}) - x_{2}(t_{k}))}{m_{1}} \\ + x_{3}(0) - \sum_{j=1}^{m} \Psi_{j}^{(a_{3},p)} (x_{3}(t_{k-j}) - x_{3}(0)), \\ x_{4}(t_{k}) = h^{a_{4}}\frac{f_{2}(t_{k}) - b_{2}(x_{2}(t_{k}), x_{4}(t_{k-1})) - s_{2}(x_{2}(t_{k})) - k_{c}(x_{2}(t_{k}) - x_{1}(t_{k}))}{m_{2}} \\ + x_{4}(0) - \sum_{j=1}^{m} \Psi_{j}^{(a_{4},p)} (x_{4}(t_{k-j}) - x_{4}(0)). \end{cases}$$

$$(13)$$

3 Numerical simulation and dynamics analysis

First, we consider the dynamic behavior of the VCVS with linear elasticity and resistance. Then, the dynamic behavior of the VCVS with nonlinear elasticity and resistance is considered. In numerical simulations, we set $m_i = 1$, i = 1, 2, initial values $x_0 = [x_1(0), x_2(0), x_3(0), x_4(0)] = [-0.1, -0.1, -0.3, -0.3]$, the time step $h = 0.01, t \in [0, T]$, $f_i = B \cos(ct)$, i = 1, 2, and $\alpha = [\alpha_1, \alpha_2, \alpha_3, \alpha_4]$.

3.1
$$s_i(x_i) = k_i x_i, b_i(x_i, \dot{x}_i) = r_i \dot{x}_i, \quad i = 1, 2$$

We consider the dynamic behavior of the VCVS with linear elasticity and resistance $s_i(x_i) = k_i x_i$, $b_i(x_i, \dot{x}_i) = r_i \dot{x}_i$, i = 1, 2.

We choose different fractional derivatives and different parameters for numerical simulation. Figure 1 shows numerical simulation results of time series plots at $\alpha = [1, 1, 1, 1]$, and $\alpha = [0.99, 1.01, 0.95, 0.95]$, T = 1000, r1 = 0.01, r2 = 0.5, k1 = 0.9, k2 = 0.1, kc = 0.5, c = 0.2, B = 0.2. From Figure 1, it can be seen that the larger the derivative, the larger the amplitude of vocal cord vibration. At this time, the system is in a chaotic state. Figures 2, 3 show numerical simulation results of phase diagrams. Figure 4 shows numerical simulation results of 3D phase diagrams in different fractional derivatives.

From numerical simulation results in Figure 1, we can observe the fractional derivative can control the amplitude of vocal cord vibration, which will lead to different sounds in the larynx, so as to ensure the effectiveness of the simulation. Figures 2–4 show the chaotic dynamic behavior of the fractional-order VCVS. Unstable and irregular movements of the vocal cords can indicate disease or abnormalities. The dynamic behavior of the fractional-order VCVS is much more complex than that of the integer-order model.

Figure 5 shows the Poincare surface of section at $\alpha = [1, 1, 1, 1], T = 2000\pi/c, tn = 1000, r1 = 0.01, r2 = 0.5, k1 = 0.9, k2 = 0.1, kc = 0.5, c = 0.2, B = 0.2.$

3.2
$$s_i(x_i) = k_i x_i (1 + c_i x_i^2),$$
 $b_i(x_i, \dot{x}_i) = r_i (1 + d_i |x_i|) \dot{x}_i,$ $i = 1, 2$

The nonlinear term is used because it is necessary to limit the amplitude and chaotic behavior of vocal cord vibration as the width of the glottis increases. c_i , d_i are all coefficients.

Figure 6 shows the Poincare surface of section at $\alpha = [1, 1, 1, 1]$, $T = 2000\pi/c$, tn = 1000, r1 = 0.01, r2 = 0.5, k1 = 0.9, k2 = 0.1, kc = 0.5, c = 0.2, B = 0.2, $c_1 = 10$, $c_2 = 0$, $d_1 = 0$, $d_2 = 15$. From Figures 5, 6, we can see that the chaotic behavior of vocal cord vibration can be controlled by adding a nonlinear term to the system.

When there is only one fixed point and a few discrete points on the Poincare section, the system can be judged to be periodically vibrating. When the Poincare section is a closed curve, it can be determined that the system is quasi-periodic vibration. When the Poincare section is a dense piece of points and there is a hierarchical structure, the system motion can be determined to be in a chaotic state. Figure 7 shows time series plots at different fractional derivatives $(\alpha = [1, 1, 1, 1], \alpha = [0.95, 0.95, 0.95, 0.95], \alpha = [1.01, 1.01, 1.01, 1.01]), r_1 = 0.01, r_2 = 1, k_1 = 1.5, k_2 = 0.1, k_c = 1.5, s_i(x_i) = k_i x_i$ $(1 + 100x_i^2), b_i(x_i, \dot{x}_i) = r_i(1 + 150|x_i|)\dot{x}_i$, i = 1, 2. From Figure 8, we can see the fractional derivative can control the amplitude and chaotic behavior of vocal cord vibration.

Figure 8 shows C_0 and spectral entropy complexity at $r_1 \in [0.02, 0.3]$, $\alpha \in [0.95, 1.5]$ and $r_2 = 1, k_1 = 1.5, k_2 = 0.1, k_c = 0.5, c = 0.8, B = 0.8, T = 20\pi/c, [-0.1, -0.1, -0.3, -0.3], <math>s_i(x_i) = k_i x_i (1 + 100x_i^2)$, $b_i(x_i, \dot{x}_i) = r_i (1 + 150|x_i|)\dot{x}_i$, i = 1, 2. From Figure 8, we show the effect of parameter r_1 and fractional derivative α on the complexity of the system. The chaotic behavior of vocal cord vibration cannot be completely controlled by nonlinear dynamics, where $\alpha = \alpha_1 = \alpha_2 = \alpha_3 \alpha_4$. The chaotic and periodic regions of the system can be seen more clearly by using C_0 and spectral entropy complexity.

The dynamic behavior of the system under fractional-order influence is analyzed, and the advantages of introducing fractional-order operators into the vocal cord vibration system are demonstrated. In this paper, a series of numerical simulations are carried out to explore the dynamic behavior of the model. The results show that it is very different from the traditional whole-order model, showing a richer and more complex dynamic landscape. Notably, the introduction of fractional derivatives reveals chaotic behavior in the system that was not previously observed.

4 Conclusion

This paper delves into the study of a two-mass nonlinear fractional-order VCVS, proposing a high-precision control scheme. The incorporation of nonlinear elements and fractional derivatives is motivated by their ability to regulate the amplitude and chaotic tendencies of vocal cord vibrations as the glottis widens. This regulation is essential for producing distinct vocal sounds in the throat, thereby enhancing the efficacy of the simulation. Numerical simulations reveal the system's dynamic behavior and highlight intriguing novel chaotic dynamics. These findings offer innovative insights into the mechanical aspects of the vocal articulation process. In the future, we will study the multi-mass block model of the asymmetric vocal cord vibration system.

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Data availability statement

The original contributions presented in the study are included in the article/supplementary material; further inquiries can be directed to the corresponding author.

Author contributions

Y-XH: formal analysis, software, and writing-original draft. J-XZ: software and writing-original draft. Y-LW: formal analysis, funding acquisition, methodology, and writing-original draft.

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Conflict of interest

The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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