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X-ray detector requirements for laser–plasma accelerators

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Laser–plasma interactions (LPIs) are an emerging source of a range of energetic radiation. LPI experiments drive ultra-short (< ps) and brilliant sources of X-rays from keV to MeV energies. Designing detectors to maximise the sensitivity and resolution achievable with these sources is paramount to optimising laser-driven accelerators. In this article, we explore the key parameters associated with laser-driven X-ray sources and the detector systems required to characterise them. We present a concise approach to modelling the sensitivity and resolution for indirect detector systems factoring in both the optical collection and the X-ray attenuation within the scintillator.

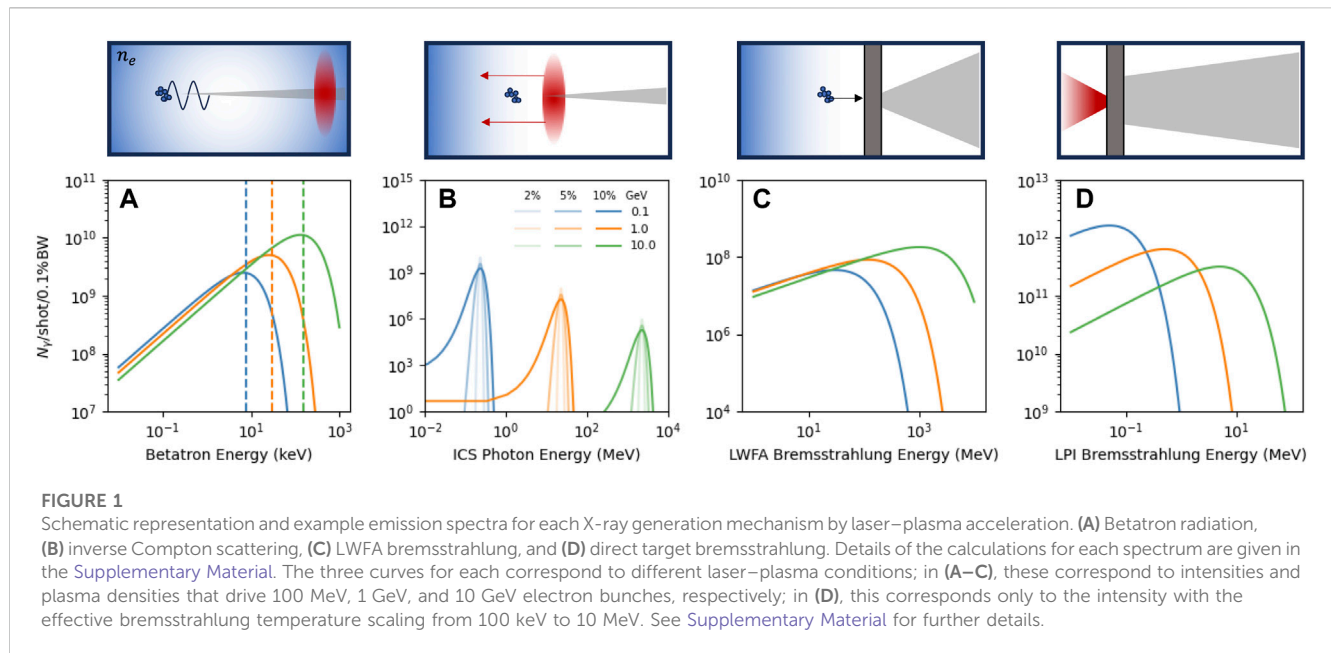
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laser–plasma interactions, bremsstrahlung, betatron, inverse Compton scattering, laser wakefield, high-intensity laser, X-ray generation

1 Introduction

A unique aspect of high-intensity laser–plasma interactions (LPIs) is the ability to generate broad ranges of energetic radiation by tuning the plasma and laser conditions. The different radiation types share a common set of characteristics: they are of short pulse (< ps) [1–3], emanate from a small source (100 nm–1 mm) [4–8], and can be tuned by subtle variations in the laser parameters or target [9–13]. In general, when high-intensity lasers are focussed on a target (either gas, liquid, or solid), atoms are ionised, and the freed electrons are accelerated to high energies [14, 15]. These electrons continue to radiate via one of the mechanisms described below or seed secondary reactions such as collisional ionisation, prompting further emission. A schematic diagram of these mechanisms is shown in [Figure 1](#), with the expected photon emission characteristics for a PW (30 J, 30 fs) laser system to establish a baseline—a full description of each calculation is given in [Supplementary Material](#). These energies and conditions are considered to mirror the upcoming high-repetition laser facility EPAC at the Central Laser Facility [16].

In laser wakefield acceleration, the laser is focussed onto a gas target at low ($\sim 10^{18-19}n_e/\text{cm}^3$) [9] density, which ionizes the gas and forms a plasma channel. The ponderomotive potential [14] of the laser drives electrons out of the focus and forms a plasma “wake” behind the laser pulse. This displacement of electrons sets up a strong electric field gradient, and electrons, injected into the wakefield, are accelerated to high energies. As the electrons are accelerated, they oscillate within the channel due to the background positive ion population and emit a synchrotron-like emission, betatron radiation [[Figure 1A](#)] [17–21], which is near-collimated and emanates from a small source area. For narrow-band X-ray emission, we can utilise inverse Compton scattering (ICS) ([Figure 1B](#)), where a secondary laser irradiates the relativistic electron beam and laser photons interacting with the electrons are upshifted by $\sim 4\gamma^2$, where γ is the electron Lorentz factor [22–25]. By



controlling the electron energies and focus of the scattering laser, the resultant X-ray emission can have a narrow spectral distribution at MeV energies and small divergence [23, 25–27]. Alternatively, the electron population can be accelerated into a solid converter foil to produce laser-wakefield bremsstrahlung (Figure 1C). This emission can be tuned by varying the thickness and material of the converter target [12, 28–30].

In laser–solid (overdense) interactions, the laser is again focussed on the target where electrons are ionised from the surface and accelerated up to MeV energies within the laser field before being driven into the target. Electrons accelerated by this mechanism generally have a broad Maxwell- or Boltzmann-like distribution of energies, and when interacting with the solid target, atoms produce a similarly broad distribution of laser–solid bremsstrahlung (Figure 1D) extending up to the peak energies of the electrons [4, 31–33]. The emission can be optimised by tuning the target material and thickness [34], lateral dimensions [4], and incident laser parameters [10, 33, 35]. The X-rays are typically more divergent than the laser-wakefield mechanisms but can still emanate from < 100- μ m source sizes [4, 6, 10, 33].

This article outlines the primary approaches to spatially resolving the emission from laser-driven sources, a brief introduction to two distinct methods we can use to detect X-rays, and then a discussion on how to apply these techniques to each of the different sources discussed above. Here, we distinguish between detectors (i.e., the sensor/substrate/scintillator that records the incident X-ray radiation) and diagnostics which translate the measured signal into a useful characteristic of the beam. As there are numerous regimes laser-driven sources can produce, we consider that no single solution/detector will suffice and, instead, describe the necessary parameters across three case studies.

- High-resolution imaging with betatron radiation—3.1
- High-energy imaging with ICS and bremsstrahlung radiation—3.2

- High instantaneous flux with direct or proximity-focussing detectors—3.3

The expected photon parameters, where necessary, are taken from the scaling shown in Figure 1.

2 X-ray imaging approaches for laser-driven sources

With the adoption of higher-repetition high-power laser facilities, there has been considerable effort by the community to produce high-stability interactions. There are several recent proposals using LPI as the initial accelerator for FELs [36], ion beamlines [37], and compact ICS sources [26]. Maier *et al.* demonstrated significant improvements in the stability of laser-driven sources [38], and new facilities are being built and designed with mechanical and machine stability in mind, including active feedback to ensure long-term stability of the driving laser. However, especially during commissioning of new facilities, detectors and diagnostics need to be able to fully characterise the emission on a single-shot basis and not integrate or scan, assuming that the emission is constant. The requirement for single-shot acquisitions limits what diagnostic techniques are possible; for example, super-resolution methods [39] and single-event processing techniques [40] are not possible. This requirement is, therefore, an important factor in detector design for laser-driven sources.

2.1 Direct detection

Indirect and direct detection schemes are both useful in laser–plasma interactions. For direct-detection schemes, electrons within the substrate material are freed by incident radiation and swept towards an electronic readout. The total charge is then

digitised by an ADC. High-grade Si, CdTe, and CZT semiconductors are often used for direct detection. Detectors based on this mechanism have demonstrated sub-% energy resolution [41], large area [42–44], and X-ray energies of up to MeV [45]. Typically, these devices are operated in an integrating mode where the counts after the ADC correspond to an amount of charge deposited in the pixel. This can be interpreted as either the number of photons at a given energy or the energy of an individual photon. With the latter mode, it is, therefore, possible to retrieve spectroscopic information as well. Recent efforts with direct-detector systems aimed to increase the full frame rate of the camera beyond MHz repetition rates [46–48] for use in high average brilliance facilities. As the pulse duration for high-intensity laser sources is typically on the order of femto- to pico-seconds, increases in the frame rate of the detector have a limited impact on reducing the number of photons per frame. Instead, the area of the pixels must be considered to control the chance of interactions per pulse, the thickness of the substrate to tune the stopping power, and the full-well capacity of the readout to maximise the total energy that can be measured.

2.2 Indirect detection

In contrast to direct detection, indirect detection uses scintillators to convert the X-ray radiation into optical light that is then imaged with a standard optical camera and lens system. By tuning the scintillator and the optical relay, we can optimise detection as needed. The optical collector is either a lens or a fibre-optic plate. For imaging, the typical lenses considered are either microscope objectives or camera/machine vision lenses. Both options are compound lenses with many elements to correct aberrations or minimise distortion; however, the microscope objectives are generally of high numerical aperture with a magnification greater than unity, whereas machine vision lenses are typically of lower numerical aperture and demagnify the image onto the sensor. Critically, with either option, we must factor in the distance to the scintillator, (d_o), and opening aperture, D , of the optic to determine the effective numerical aperture ($NA = D/2d_o$) of the system with the magnification (M_o) to determine what the collection efficiency and resolution will be. There have been several studies on the relationship between these parameters [32, 49, 50]; in general, resolution and collection efficiency are inversely proportional. The resolution limit in the optically limited regime can be approximated as follows:

$$R[\mu\text{m}] = \sqrt{\underbrace{\left(\frac{p}{NA}\right)^2}_{\text{Diffraction}} + \underbrace{(q\ell NA)^2}_{\text{Defect of focus}} + \underbrace{\left(\frac{2dx}{M_o}\right)^2}_{\text{Sampling}}}, \quad (1)$$

where p and q are fitting parameters determined by Koch *et al.* [49] and ℓ is the thickness of the scintillator. Throughout this article, we define the resolution as 90% of the integrated line-spread-function to mirror the work by Koch *et al.* [49]. This is notably larger than the full-width half-maximum, and so, features below the limits given here could still be visible—albeit at a lower contrast. The first term in Eq. 1 relates to the cumulative effects of diffraction and spherical aberrations stemming from the scintillator–air interface,

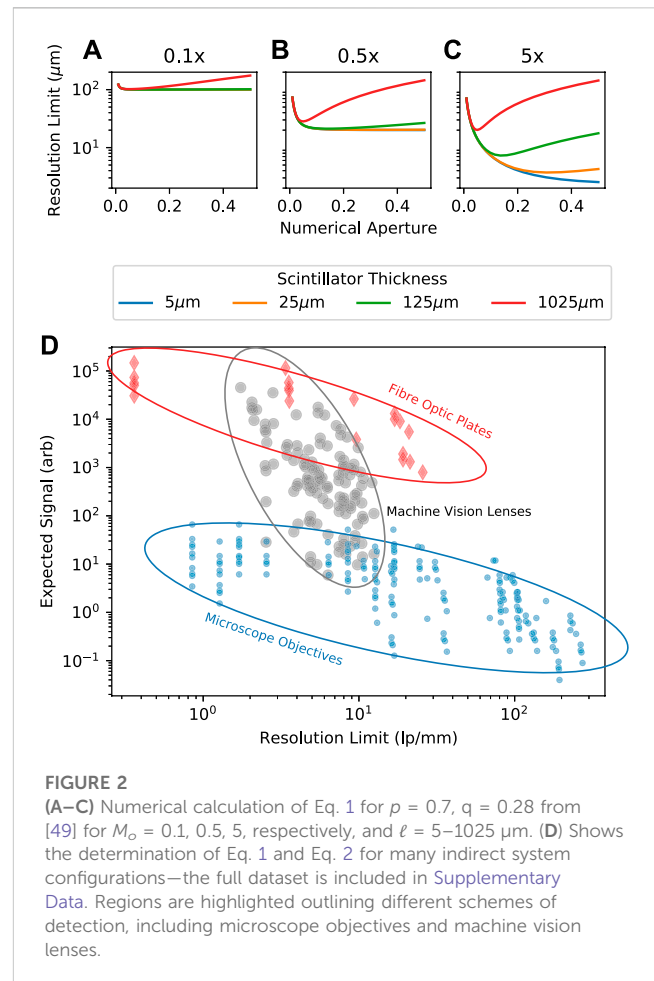


FIGURE 2 (A–C) Numerical calculation of Eq. 1 for $p = 0.7$, $q = 0.28$ from [49] for $M_o = 0.1, 0.5, 5$, respectively, and $\ell = 5\text{--}1025 \mu\text{m}$. (D) Shows the determination of Eq. 1 and Eq. 2 for many indirect system configurations—the full dataset is included in [Supplementary Data](#). Regions are highlighted outlining different schemes of detection, including microscope objectives and machine vision lenses.

and the second term is due to planes beyond the point of best focus contributing. We include the third term factoring in the pixel size dx and the optical magnification M_o to account for the limit in the low-magnification domain. In addition, this relationship holds assuming a pencil-like deposition throughout the scintillator. For the purposes of this discussion, we omit effects due to non-uniform attenuation throughout the scintillator [49] and large electron cascades with high-energy incident X-rays [51]. Assuming that we have a relatively thin ($\ell < \lambda_{\text{mfp}}$) scintillator and a limited electron cloud radius, Eq. 1 sets the resolution at the detector plane, and so, by controlling the geometric magnification, M_g , the system resolution, can exceed this for samples or images. The signal detected in each pixel, however, is dependent on the attenuation of the scintillator, the conversion efficiency into optical photons κ , the collective power of the lens system, and the magnified area of pixels:

$$\text{Signal} \left[\frac{\text{Counts}}{px} \right] = \underbrace{\frac{E_{\text{dep}}}{\text{mm}^2} \kappa}_{\text{Photons Produced}} \cdot \underbrace{QE(\lambda) \frac{NA^2}{4n^2}}_{\text{Collection}} \cdot \underbrace{\frac{A_{px}}{M_o^2} G}_{\text{Sampling}}, \quad (2)$$

where $QE(\lambda)$ is the quantum efficiency of the chosen sensor at the wavelength of emission, κ is the yield in photons per deposited energy for the scintillator material, n is the refractive index of the scintillator material (see [Supplementary Material](#) for collection efficiency derivation), and G a linear gain term to convert the

number of photons to counts recorded by the sensor. This equation is similar in form to that determined by Cardarelli et al. [32]; however, the F-stop terms they used are replaced by terms for the effective numerical aperture and optical magnification directly. Where the deposited energy per mm^2 is dependent on both the incident spectral shape, $f(E)$, and the attenuation of the scintillator, to a first order, this can be expressed using the Beer–Lambert model for transmission as

$$\frac{E_{dep}}{\text{mm}^2} = \int_0^{\infty} f(E) (1 - \exp^{-\rho \ell \sigma(E)}) dE, \quad (3)$$

where ρ is the density of the scintillator and σ is the attenuation cross section. Eq. 1 and Eq. 2 are both dependent on the length of the scintillator, ℓ , the numerical aperture of the lens system, and the optical magnification, resulting in a complex trade off of parameters between lens choices.

We demonstrate the calculation of both the signal and the resolution at the plane from parameters for typical systems, using both microscope objectives and camera lenses to image scintillators of different thicknesses, as shown in Figures 2A–C; we set the pixel size to $5 \mu\text{m}$ for each magnification and vary the numerical aperture of the lens to demonstrate the scaling. It is clear from evaluating Eq. 1 that the magnification and pixel size act as a hard limit on the resolution. When operating with high magnification, there becomes a significant dependence on the thickness of the scintillator and numerical aperture of the system. However, if we consider only the numerical aperture of the system, a clearer picture emerges—with a low numerical aperture; therefore, with a small angle being observed, there is little dependence on scintillator thickness, whereas with a high numerical aperture, the scintillator thickness becomes paramount to the achieved resolution. Figure 2D summarises how different commercially available optics vary in terms of achievable resolution and expected signal. The full dataset used is detailed in Supplementary Material. The data points assume a Gaussian X-ray distribution with a 100-keV centre and a full-width half-maximum of 40 keV.

3 Imaging case studies

In the following sections, we outline three distinct imaging challenges with laser-driven sources where advancements in detector characteristics would enhance the potential applications of laser-driven sources.

3.1 Single-shot high-resolution imaging with laser-driven betatron radiation

Laser-wakefield betatron sources have sub-micron source sizes [8]; however, typically, the smallest resolvable element achieved in experiments is much higher than this and is, instead, limited by the detector [52]. To achieve a high resolution at the detector plane, the best route is to use high-magnification objectives, as shown in Figure 2D; however, this limits the expected signal due to spreading over many pixels. Microscope objectives exhibit a general scaling between the numerical aperture and optical

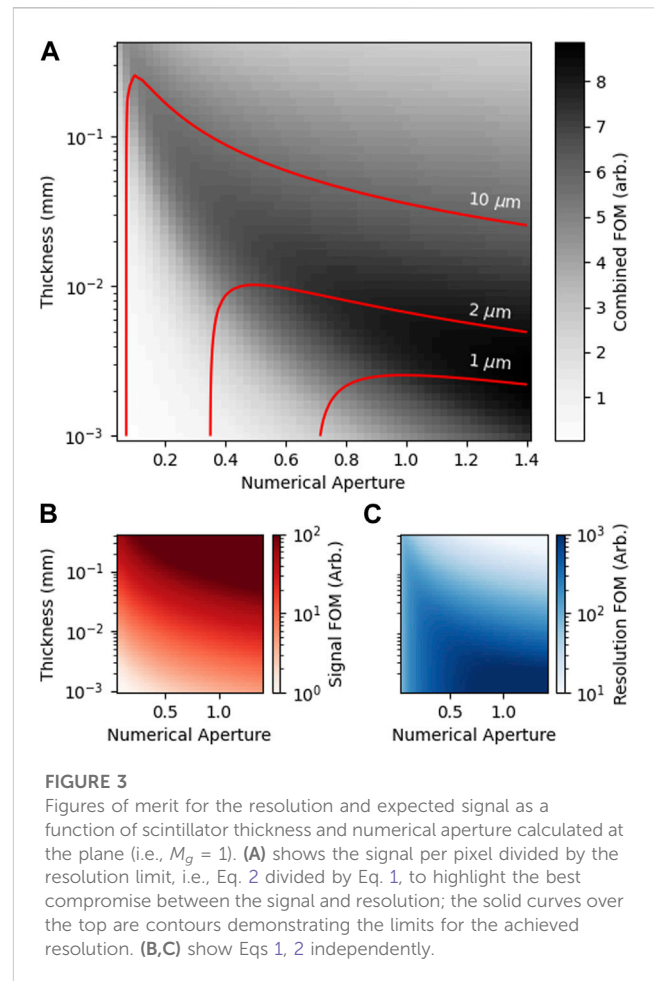


FIGURE 3

Figures of merit for the resolution and expected signal as a function of scintillator thickness and numerical aperture calculated at the plane (i.e., $M_o = 1$). (A) shows the signal per pixel divided by the resolution limit, i.e., Eq. 2 divided by Eq. 1, to highlight the best compromise between the signal and resolution; the solid curves over the top are contours demonstrating the limits for the achieved resolution. (B,C) show Eqs 1, 2 independently.

magnification of the form $M_o \propto \sqrt{\text{NA}}$. Then, for a given spectral distribution and scintillator material, we can express Eq. 1 and Eq. 2 as a function of the numerical aperture and scintillator thickness, respectively. The result of these two functions is shown in Figures 3B,C, and a combination figure of merit, calculated as the signal per pixel divided by the resolution limit, i.e., Eq. 2 divided by Eq. 1, is shown in Figure 3A. The contours on the first panel demonstrate the fundamental limits in resolving power for different numerical apertures. Achieving a sub-micron resolution at the plane requires both a high ($\text{NA} > 0.7$) numerical aperture and an ultra-thin ($\ell < 5 \mu\text{m}$) scintillator.

Betatron emission is divergent, albeit narrowly, ($\theta \approx \text{mRad}$), and so, the geometric magnification can increase the system resolution. This is also true of conventional X-ray tube sources; however, as their source area is typically large [53, 54] (excluding micro- and nano-focus systems [55]), the resolution is fundamentally limited by the extent of the source. The divergence of betatron emission combined with a small source opens up additional pathways to achieve sub-micron imaging, and we can look at the trade-offs between different optical systems by considering how the resolution and sensitivity vary as a function of each variable in 1–2.

Figure 4 shows the variation in the resolution and effective signal due to several parameters—numerical aperture (green), optical magnification (orange), geometric magnification (blue), and scintillator length (pink)—for a selection of microscope

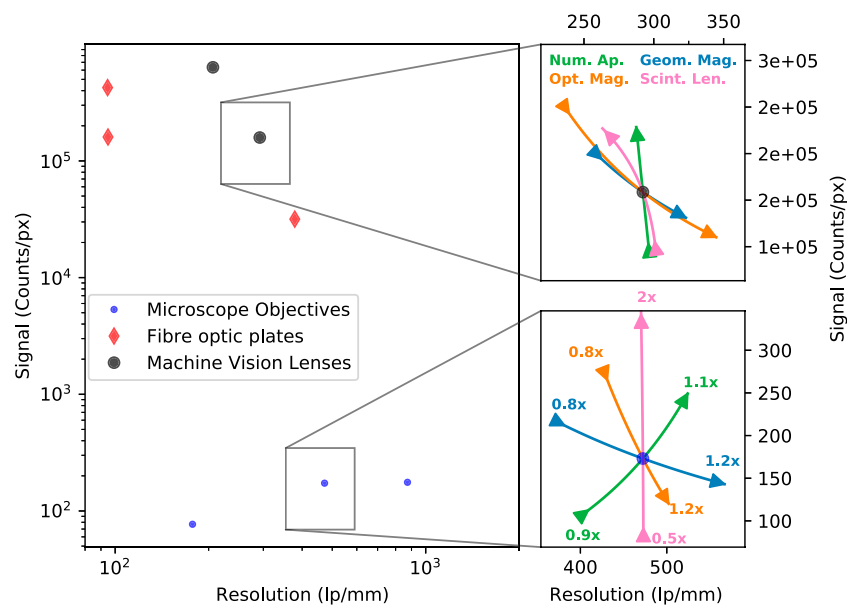


FIGURE 4

Expected signal (counts/px) and resolution (lp/mm) for microscope objectives, fibre-optic plates, and machine vision lenses, calculated by Eqs 1, 2.

The subplots demonstrate the variation in performance due to numerical aperture (green), optical magnification (orange), geometric magnification (blue), and scintillator length (pink).

objectives, fibre-optic plates (FOPs), and high numerical aperture machine vision lenses. These three approaches represent distinct options for optical imaging. Generally speaking, microscope objectives have a numerical aperture between 0.1 and 0.5 and high magnification, fibre-optic plates of a high numerical aperture >0.7 and $\sim \times 1$ magnification, and machine vision lenses have lower numerical aperture ~ 0.1 and typically demagnify the image ($M_o < 0.5$). However, what is interesting between these different approaches is how subtle changes in their respective parameters can change the resultant system performance. It is clear that the complex interplay between parameters makes it challenging to identify the *ideal* candidate. In the inset plots of Figure 4, we vary each parameter independently to demonstrate its effect. The arrows indicate the direction of increasing value for each parameter.

Interestingly, due to the difference in their initial values, increasing the numerical aperture for the highlighted machine vision lens results in a decrease in the expected resolution, leading to a significant increase in the highlight microscope objective. Conversely, if we consider increasing the thickness of the scintillator, we would observe an increase in the signal with no loss in resolution for the microscope objective, and yet, for the machine vision lens example, we observe a decrease in the resolution with minimal gains to the expected signal. Whilst these contradictions make it difficult to identify a general pattern, we note that the system resolution for the microscope objectives can be matched using the machine vision lenses but with a much greater signal. Since geometric magnification depends on the *sample* position rather than just the *detector* position, we can design systems to use lower optical magnification and increase the system resolution by reducing the sample position. The signal values are calculated assuming 7×10^{11} photons with a

divergence of 5 mRad and a critical energy of 50 keV—the parameters given for the example distribution in Figure 1A. For a single shot, it is clear that high-magnification objectives will result in a low signal-to-noise ratio, and so, many shots would likely need to be combined to achieve sufficient imaging quality.

In summary, to achieve a maximum signal with high-resolution imaging with betatron radiation, the best approach is to use relatively low optical magnification combined with high geometric magnification and keep the detector plane at the smallest distance from the source. In laser-wakefield acceleration (LWFA) experiments, the highly relativistic electron bunch must be deflected prior to interacting with the sample to minimise background contributions or damage to the sample. In practice, this sets a lower limit on the sample position ($Z \approx 1$ m), and therefore, a compromise will need to be sought for different experimental configurations. In addition, objectives that exceed the $M_o \propto \sqrt{NA}$ scaling offer potential routes to offset the losses in the signal due to magnification.

3.2 MeV imaging with ICS and laser-driven bremsstrahlung

It is pertinent to consider at this point the extreme case, where instead of a few hundred microns of the scintillator, we require thousands to ensure sufficient stopping power. Laser-driven sources can readily generate X-rays greater than 1 MeV via either inverse Compton sources or bremsstrahlung processes with energies extending up to 100 s of MeV for LWFA mechanisms. At these energies, the dominant X-ray attenuation mechanisms are no longer photo-electric absorption or scattering but nuclear and electronic-pair production [56]. This significantly alters the effects on resolution. No longer can we consider only the optical spreading

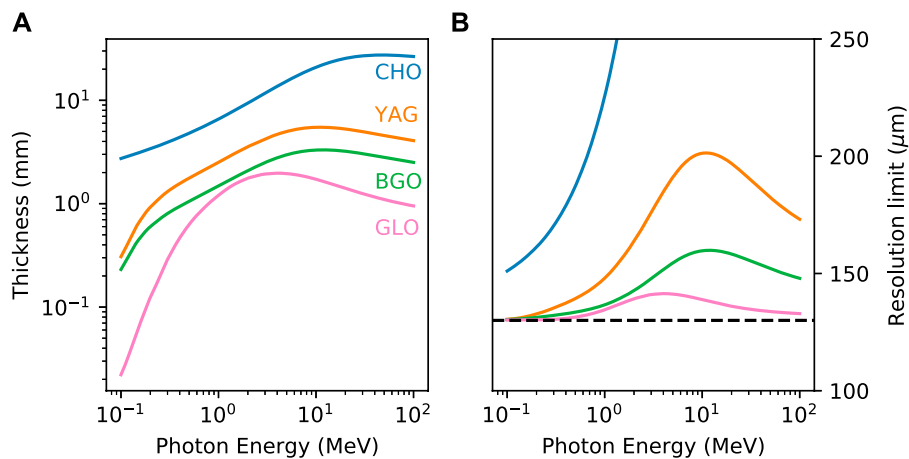


FIGURE 5

(A) Attenuation length for 10% absorption in each scintillator and (B) equivalent resolution limit for a scintillator of that length. Calculated via the NIST data tables [56] as a function of incident X-ray energy.

determined by Koch et al. [49] (Eq. 1); we must now also factor in the lateral diffusion that occurs as the X-ray deposits energy through a scintillator. Solving these additional factors requires in-depth Monte Carlo simulations to be conducted. However, we can determine some useful bounds from the aforementioned equations. First, we consider that for a given energy, we can calculate the required thickness, ℓ , as a function of the desired absorption, i.e., $\ell = -\log(T)/\sigma\rho$. Second, we wish to calculate what the intrinsic (i.e., PSF limited) resolution would be for that thickness to inform how we select scintillator materials. The calculation of this is shown in Figure 5 for a plastic scintillator (CHO, e.g., EJ260, BC422q), YAG:Ce, BGO, and the high-Z and high-density GLO scintillator [57]. For each material, the effective resolution limit determined in Figure 5 could then be further refined by Monte Carlo simulations adding a fourth term to Eq. 1 to account for the radial spreading as the X-rays deposit their energy. The energy spreading in materials is also dependent on the density and effective- z , and so, whilst the scattering at higher energies will reduce the resolution, this effect will be reduced with higher-density materials [58, 59].

This scaling with density and atomic number underlines why research on the GLO scintillator is beneficial to high-energy X-ray imaging; the higher density is intrinsically linked to the minimum thickness and relative attenuation to high-energy X-rays. Consequently, continued research and development into exotic scintillators and their manufacture will greatly benefit radiography with high-energy X-rays [60].

3.3 High instantaneous X-ray flux imaging

In the previous cases, we considered an optical system to image the scintillation onto the sensor. However, the lens system introduces significant losses in the collection efficiency, and by switching to either direct detection, the sensor in contact with the scintillator, or the proximity focussing of FOPs, we can consider a far more efficient detection method for imaging the X-rays. With the losses from the optical system minimised, the

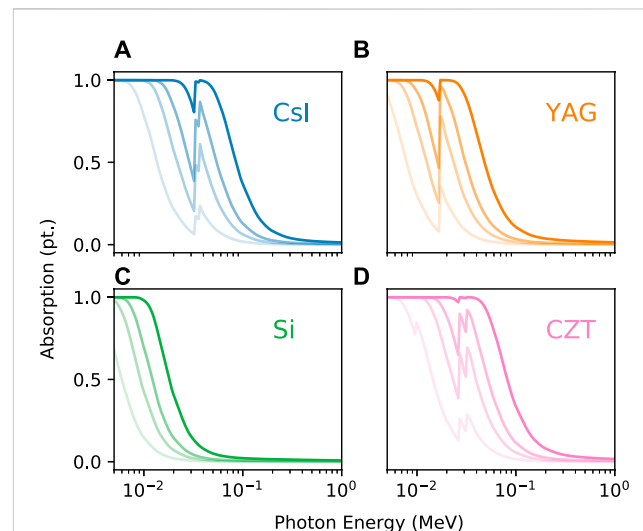


FIGURE 6

Absorption fraction for scintillators and direct-detector substrates, and the transparency of the line corresponds to the thickness of the layer—the order of increasing opacity corresponds to 20, 70, 150, and 500 μm thickness, respectively. Calculated via the NIST data tables [56] for (A) CsI, (B) YAG:Ce, (C) Si, and (D) CZT.

detection efficiency can be calculated directly from NIST-XCOM data tables [56] and the Beer–Lambert law [61]. Figure 6 shows that the efficiency of stopping in the material can be up to 100% for betatron-like energies (~50 keV) of X-rays for both scintillators (CsI and YAG) and thick direct-detection sensors such as CZT. The resolution for the direct detection is dependent on the pixel size and on PSF of the incident photon energy, whereas the FOP method is limited by the spreading in the scintillator, similar to Eq. 1.

One desired application for such a detector is to measure the unattenuated beam in a single shot. The number of X-ray photons arriving per pixel is dependent on the emitted number, the divergence of the emission, and the solid angle subtended by each pixel. With

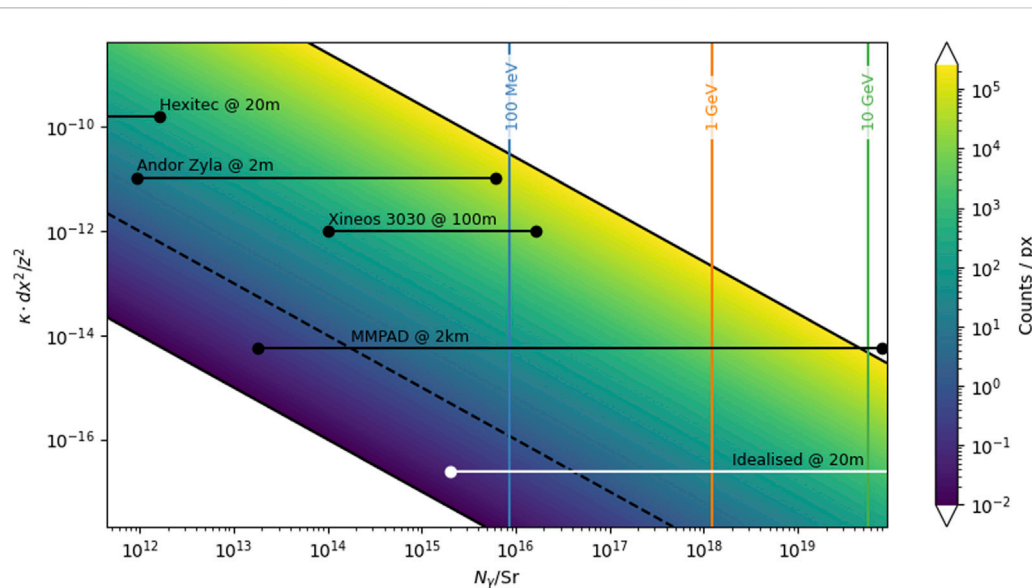


FIGURE 7

Calculated number of counts per pixel as a function of incident photons per Sr, and the relative pixel area (dx^2/z^2) and effective efficiency/gain (K) for a given detector system. The vertical lines correspond to the emission characteristics given in Figure 1A. The solid horizontal lines correspond to the effective dynamic range of the labelled detectors at representative distances, taking the background level and saturation point from the respective datasheets [42, 62–64].

these criteria and the photon distributions shown in Figure 1, we can generate the plot shown in Figure 7, showing the effective number of counts as a function of the incident photon intensity and the effective signal (Eq. 2) of a given detector. Here, we express the y-axis as Kdx^2/z^2 , where K is the overall efficiency term from incident photons per pixel to counts. Expressing Eq. 2 like this provides a clear route to improving detector performance. Figure 7 shows the approximate dynamic ranges for various detectors [42, 62–64] available that can operate in the desired range; additionally, we include an “idealised” detector that operates with a high dynamic range similar to the MM-Pad diagnostics [64] but a pixel size of $dx = 10 \mu\text{m}$ at a distance of $z = 20 \text{ m}$ and $K = 10^{-4}$ [Counts/ γ_x] to compensate. Additionally, we include a dashed line at 1 count/px to indicate the relative threshold for single-photon spectroscopy techniques. Current detector systems, at reasonable distances ($< 100 \text{ m}$), cannot operate in the single-photon mode in the direct beam, leading to secondary scattering techniques to utilise such detectors [65]. Reducing the pixel size can, in principle, work; however, this approach is fundamentally limited since the charge cloud, the energy deposition volume, and lateral diffusion through the substrate will start to dominate as the pixel size is reduced. Extending the propagation further might be possible in certain facilities; however, it is impractical to consider kilometre-scale propagation distances in the near future, and since the divergence of betatron radiation is expected to drop with increasing electron energy [17], this approach will rapidly become impractical. In practice, to access the higher incident intensities, relatively inefficient systems, where $K \ll 1$, become the only realistic route to ensure sufficient sampling of the directly emitted beam. This is not to say thin scintillators and lossy lens systems are the only route to achieve it as this would result in significant disparity between low- and high-energy X-ray sensitivity. Instead, a high-attenuation substrate paired with a variable gain register [66] would provide a more appropriate solution for highly instantaneous flux environments.

4 Summary

Herein, we demonstrated, using analytical equations for resolution (Eq. 1) and signal (Eq. 2), approaches to X-ray imaging with laser-driven sources. The variety of X-ray energies and fluences poses a challenge to detectors but provides an opportunity for a wide variety of applications. Taking advantage of the diverging X-ray emission and the proximity to the source location, we can exploit geometric magnification to maximise the signal collected for a given resolution. With improvements to scintillator materials, we can design efficient scintillators for high-energy ($> \text{MeV}$) X-ray imaging while maintaining a $\sim 100\text{-}\mu\text{m}$ resolution as laser-driven source intensity increases further, i.e., by increasing the total flux per pulse and reducing the emission divergence.

Data Availability Statement

The original contributions presented in the study are publicly available. This data can be found here: <https://edata.stfc.ac.uk/handle/edata/945>.

Author contributions

CDA: Conceptualization, Investigation, Methodology, Writing—original draft. GS: Conceptualization, and Writing—review and editing. SR: Conceptualization, Investigation, and Writing—review and editing. JP: Writing—review and editing. KF: Writing—review and editing. RG: Conceptualization, Investigation, Methodology, and Writing—review and editing. KW: Supervision, and Writing—review and editing. PR: Funding acquisition, Investigation, Supervision, and Writing—review and editing.

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Conflict of interest

The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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Supplementary material

The Supplementary Material for this article can be found online at: <https://www.frontiersin.org/articles/10.3389/fphy.2023.1286442/full#supplementary-material>

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