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Numerical approximations for fluid flow and heat transfer in the boundary layer with radiation through multiple Lie similarity transformations

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The dependent or independent variables of differential equations may be reduced by applying its associated Lie point symmetries. Seven-dimensional Lie point symmetry algebra exists for differential equations representing heat transfer in a boundary layer flow in the presence of radiation. The linear combinations of these seven Lie symmetries are used first to deduce the invariants and then derive the Lie similarity transformations for the original set of partial differential equations (PDEs). This procedure is repeated for the set of transformed equations to further reduce the system of PDEs into the system of ordinary differential equations (ODEs). Multiple exact similarity transformations are obtained using this procedure. All these transformations map the system of three PDEs with three independent variables of flow and heat transfer under the specified set of conditions into two-dimensional systems of equations with only one independent variable, the system of ODEs. Approximate solutions for these reduced systems are established using the finite difference method to illustrate the effects of unsteadiness, Prandtl number, and radiation on the boundary layer thickness, flow, and heat transfer. This type of study was conducted under the effect of these parameters previously with a different set of similarity transformations. However, the Lie similarity transformations deduced in this work, which have not been employed, lead to different types of reduced systems of ODEs, thereby providing different velocities and temperature profiles and providing valid solutions for previously unexplored regions for unsteadiness in the fluid flow and heat transfer. Some of these transformations and their resulting systems provide results that contradict the flow and heat transfer in real fluids.

KEYWORDS

boundary layer, radiation, Lie transformations, Lie similarity transformation, numerical solutions

1 Introduction

Heat transfer in thin films has garnered significant attention in various manufacturing processes. For example, the process of cooling thin films during the extrusion of polymer sheets, metal sheets, wire coatings, painting, polishing, and many other processes involves heat transfer in thin liquid films. Moreover, some industrial processes, such as surface paint and heat treatments on ceramics, involve radiation treatment to control the temperature of the fluid and boundary layer thickness without affecting the temperature of the surface. In many of these applications, the final product requires a smooth surface finish, which is attained by controlling the rate of heat transfer in these films. With advancements in manufacturing techniques and processes, more accurate methods are required to predict the physics of heat transfer in these types of fluid flows. In some industries, radiation treatments are performed to control the temperature, unsteadiness, and rate of heat transfer in the fluid by altering the surface temperature, such as surface paints on metal sheets in the automobile industry, surface polishing on ceramic products, and thin-walled solar water heaters. These applications require applying thermal radiation effects in energy equations while modeling fundamental boundary layer flows.

Crane [1] investigated the fluid flow driven on a semi-infinite linearly stretching surface, which Wang [2] extended to include the unsteady effects of hydrodynamics in thin-film stretching sheets. Andersson et al. [3] modeled the non-Newtonian fluid flow in a thin film on an unsteady stretching sheet using a power law. Andersson et al. [4] studied this phenomenon further by incorporating heat transfer. Moreover, on an unsteady stretching surface, Chen [5] studied non-Newtonian fluid flow; Dandapat et al. [6] included thermocapillary effects; Chen [7] illustrated viscous dissipation effects on heat transfer in a thin-film flow of a non-Newtonian fluid; Wang [8] obtained analytical solutions for the problem considered in [4] using the homotopy analysis method (HAM); and Dandapat et al. [9] explored the heat transfer in thin films with variable thermal conductivity, viscosity, and thermocapillarity. Several other authors [10–15] developed numerical and analytical solutions to similar problems with additional physical conditions and constraints. Liu and Megahed [16] illustrated the effects of thermal radiation, variable thermal conductivity, and viscosity on heat transfer and fluid flow in a thin film on an unsteady stretching sheet. Furthermore, Kumar [17] scrutinized the 3D flow and non-linear radiative heat transfer of non-Newtonian nanoparticles over an exponentially stretching sheet. Kumar [18] analyzed the flow and heat transfer of non-Newtonian nanofluid over a stretching sheet by considering the slip factor. Reddy et al. [19] demonstrated the transverse magnetic flow over a Reiner–Philippoff nanofluid by considering solar radiation. Kumar [20] studied the ferromagnetic hybrid nanofluid effects on heat transfer under solar radiation. Azam et al. [21] examined the transient bioconvection and activation energy impacts on Casson nanofluid with gyrotactic microorganisms and non-linear radiation. Puneeth et al. [22] considered a 3D flow of a nanofluid with non-linear thermal radiation and multi-slip conditions. Sudharani et al. [23] analyzed the influence of slip flow and linear radiation on a hybrid and tri-hybrid nanofluid. Naik et al. [24] investigated heat transfer under the influence of magnetic dipole. In all these studies, the similarity transformations remained the same. In such boundary layer problems,

the flow originates from the origin, and the stretching of the elastic sheet causes it to flow in a plane parallel to its motion. Restriction of the stretching sheet velocity and temperature, namely, when $U(x, t)$ and $T(x, t)$ depend on the x -distance from the origin and time, enables the mapping of systems of boundary layer partial differential equations (PDEs) into systems of ordinary differential equations (ODEs) [2]. The systems of equations thus obtained are non-linear and coupled; therefore, analytic and approximate solution schemes are employed to construct the velocity and temperature profiles.

In this study, we used the Lie symmetry method [25–27] to derive similarity transformations. Safdar et al. [28] proposed Lie similarity transformations for an unsteady flow in a thin film over a stretching sheet and constructed analytic solutions using Lie point symmetries. In their work, instead of using $U(x, t) = bx/(1 - at)$ to obtain the fluid velocity, the invariance of the obtained Lie symmetry algebra was used to derive a general form for $U(x, t)$ along with the stretching sheet temperature $T_s(x, t)$ and film thickness $h(t)$. Bilal et al. [29] recently proposed a method to obtain the Lie similarity transformations for heat transfer in boundary layer flow with additional parameters. For a system of differential equations (DEs), the Lie point symmetry offers reduction based on functions that remain invariant under the action of these generators. For a PDE system, these invariants reduce the number of dependent and independent terms. Such consecutive reductions in the independent variables of the flow PDEs resulted in a system of ODEs. In this study, we found seven Lie point symmetry generators for a system of PDEs describing the boundary layer flow and heat transfer in a thin film on an unsteady stretching surface in the presence of radiation, with three dependent and three independent terms. In the next step, we reduced one independent variable of the system by applying invariants associated with the linear combinations of the obtained symmetries. Consequently, we let the reduction procedure dictate the form of the velocity components using specific boundary conditions. Another reduction was achieved through the invariants of the symmetries of the once-reduced system. This double reduction revealed a system of ODEs corresponding to the flow and heat transfer PDEs. Similarity transformations were attained using the invariants derived in both cases. This directly mapped the flow and heat transfer equations to the same systems of ODEs obtained through separate reductions. We showed that five similarity transformations exist for flow and heat transfer equations. These transformations corresponded only to linear combinations of the Lie point symmetries for which both the velocity and temperature of the stretching sheet were retained as functions of space x and time t . These new similarity transformations revealed more than one type of ODE system. Hence, the Lie symmetry procedure led to more than one class of system of equations for studying the flow and heat transfer. We used finite-difference approximations to draw the velocity and temperature profiles for the systems of the ODEs extracted from the flow model via similarity transformations.

Previous studies on flow and heat transfer have primarily focused on the solution method(s) or analysis with additional parameters by utilizing the pre-existing basic similarity transformations given by [2,8]. Single reductions of systems of differential equations representing steady flows are performed using such similarity transformations, whereas double reductions through these transformations are performed for unsteady fluid flows. In these transformations, the velocity of the elastic sheet is considered $U(x, t) = bx/(1 - at)$, which later directly ensures the fluid velocity u -velocity is a component in these transformations,

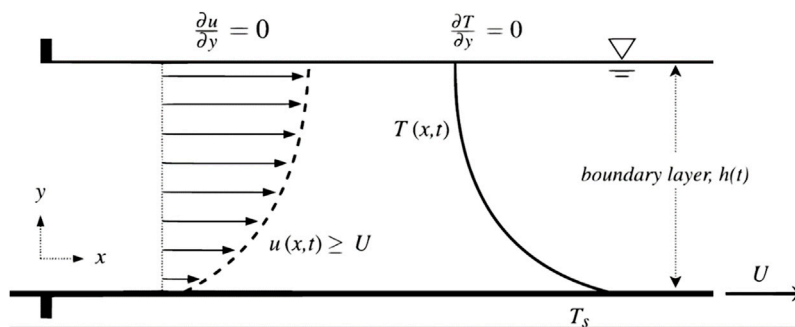


FIGURE 1
Fluid flow and heat transfer in the boundary layer.

such that $u = bx f'(\eta)/(1 - at)$. This is problematic when a real-world problem is modeled using velocity and temperature as inputs, where the velocity of the flow exceeds that of the stretching sheet (most real-world flows).

Bilal et al. [30] recently conducted a detailed heat transfer analysis of boundary layer flow in the presence of radiation using two different types of transformations. It was observed that the valid transformation obtained using Lie point symmetries yields results in the different regions compared with the existing transformations. The comparison showed that the previously existing transformation is valid only for steady and marginally accelerating fluid (unsteadiness). However, the Lie transformations provide a valid solution for any range of unsteadiness in the fluid. In addition, the previous transformations are valid for a specific time interval, which depends on a range of unsteadiness parameters. However, the Lie similarity transformations provide valid solutions at any given time. This motivates the author to derive all the Lie point similarity transformations associated with the system of PDEs representing the flow and heat transfer in the boundary layer in the presence of radiation.

The remainder of this study is organized as follows: Section 2 describes the mathematical formulation and Lie point symmetry transformations/generators of the flow. The numerical solutions are presented in Section 3. The results and discussion based on the velocity and temperature profiles are presented in Section 4, and conclusions are presented in Section 5.

2 Mathematical formulation and construction of similarity transformations

Consider a fully developed, viscous, nonvolatile, unsteady, incompressible, two-dimensional fluid flowing on a thin horizontal elastic surface and emerging from a hole (shown in Figure 1) that emerges from the origin of the (x, y) coordinate system. The fluid viscosity was unaffected by temperature changes, and the buoyancy effects were negligible. The velocity and temperature changed with time t and x -coordinate, and the streamwise diffusion terms were neglected. The smoothness of the thin film surface was assumed to be free of any type of wave. Considering all these assumptions, we obtained the following boundary layer equations:

$$\begin{aligned} u_x + v_y &= 0, \\ u_t + uu_x + vv_y - \frac{\mu}{\rho} u_{yy} &= 0, \\ T_t + uT_x + vT_y - \frac{\kappa}{\rho C_p} T_{yy} - \frac{1}{\rho C_p} q_y^r &= 0, \end{aligned} \tag{1}$$

such that

$$\begin{aligned} y = 0: u &= U(x, t), v = 0, T = T_s(x, t), y = h(t): u_y = T_y = 0, \\ v &= h_t(t). \end{aligned} \tag{2}$$

In the aforementioned equations, the u - and v -velocities are in the x - and y -directions, respectively. T and t denote the temperature and time, respectively. μ is the dynamic viscosity; ρ is the density of the fluid; C_p is the specific heat of fluid at constant pressure; κ is the thermal conductivity; q^r is the heat flux under the radiation, and $h(t)$ is the boundary layer film thickness. The subscripts in (Eqs 1, 2) represent partial derivatives; for example, v_y denotes the y derivative of the v -velocity. The velocity of the stretching surface in x -direction is denoted by $U(x, t)$. Wang [2] provided the following form of the stretching velocity $U(x, t)$ by restricting the motion to

$$U(x, t) = \frac{bx}{1 - at}, \tag{3}$$

According to [4], the surface temperature $T_s(x, t)$ is expressed as

$$T_s(x, t) = T_0 - T_{ref} \left(\frac{d\rho x^2}{2\mu} \right) (1 - at)^{-\frac{3}{2}}. \tag{4}$$

According to the Rosseland approximation [31], q_r is

$$q^r = -\frac{4\sigma}{3k_a} T_y^4. \tag{5}$$

In Eqs 3, 4, a, b , and d are constants; the first two possess the dimensions of $time^{-1}$, whereas the third is a constant of proportionality. Moreover, T_0 and T_{ref} denote the ambient and reference temperatures, respectively. In Eq. 5, k_a and σ represent the mean absorption coefficient and Stefan-Boltzmann constant, respectively. Raptis [32] expressed the temperature as a linear function for small variations in it. By expanding T^4 about T_0 with diminishing higher order terms of the Taylor series, we obtain

$$T^4 \cong 4TT_0^3 - 3T_0^4. \tag{6}$$

The formulas of $U(x, t)$ - surface velocity (Eq. 3) and $T_s(x, t)$ - temperature (Eq. 4) lead to the following similarity transformations:

$$\eta = \frac{1}{\sqrt{\frac{\rho b}{(1-at)\mu}}} \frac{y}{\beta}, u = \frac{bx}{1-at} f'(\eta), v = \beta \sqrt{-\frac{b\mu}{\rho(1-at)}} f(\eta),$$

$$T = T_0 - T_{ref} \left(\frac{d\rho x^2}{2\mu} \right) (1-at)^{-\frac{3}{2}} \vartheta(\eta), \tag{7}$$

where η and ϑ represent the stream function, similarity variable, and dimensionless temperature, respectively, whereas β denotes the unknown dimensionless film thickness. Substituting the similarity transformations Eq. 7 into Eq. 1, the transformed system can be written as

$$f''' + \lambda \left(f f'' - f'^2 - S f' - \frac{S\eta f''}{2} \right) = 0,$$

$$\frac{\vartheta''}{Pr} (1 + R) + \lambda \left(f \vartheta' - 2 f' \vartheta - \frac{S\eta \vartheta'}{2} - \frac{3S\vartheta}{2} \right) = 0. \tag{8}$$

Likewise, the boundary conditions (Eq. 2) are transformed to

$$\eta = 0: f(\eta) = 0, \vartheta(\eta) = f'(\eta) = 1,$$

$$\eta = 1: f(\eta) = \frac{S}{2}, \vartheta'(\eta) = f''(\eta) = 0, \tag{9}$$

where

$$R = \frac{16\sigma T_0^3}{3k_a \kappa}. \tag{10}$$

The aforementioned approach serves as a reference procedure for converting a system of PDEs into a system of ODEs. The transformed system (8) is valid only when $t < a^{-1}$. In Eqs (8) and (9), the prime (') indicates a derivative with respect to the similarity variable η ; the dimensionless film thickness is denoted by $\lambda = \beta^2$; $Pr = \mu \frac{C_p}{\kappa}$ is the Prandtl number; R denotes the radiation parameter; and $S = a/b$ is the dimensionless unsteadiness parameter.

2.1 Lie symmetries and symmetry transformations

Lie developed an algebraic approach for constructing Lie point symmetries associated with differential equations [25–27]. These point transformations map the dependent and independent variables of a differential equation into new dependent and independent variables. These mappings leave the differential equations form-invariant such that their properties (e.g., linearity/non-linearity, order, and type) remain unaltered. Here, for the system of PDEs considered (1), we followed the procedure described by [28] for such systems and their associated conditions (2). The Lie point symmetry associated with system (1) in the general form can be written as

$$\mathbf{X} = \xi_1 \frac{\partial}{\partial x} + \xi_2 \frac{\partial}{\partial t} + \xi_3 \frac{\partial}{\partial y} + \phi_1 \frac{\partial}{\partial T} + \phi_2 \frac{\partial}{\partial u} + \phi_3 \frac{\partial}{\partial v}, \tag{11}$$

where ξ_i, ϕ_i , for $i = 1, 2, 3$, are known as infinitesimal coordinates that are functions (x, t, y) . System (1) and related conditions (2) possess partial derivatives up to order two; hence, $\mathbf{X}^{[1]}$ - first

TABLE 1 Lie symmetries and transformations.

Symmetry generator	Symmetry transformation
$X_1 = \frac{\partial}{\partial t}$	$t = \tilde{t} + \epsilon$
$X_2 = \frac{\partial}{\partial x}$	$x = \tilde{x} + \epsilon$
$X_3 = \frac{\partial}{\partial T}$	$T = \tilde{T} + \epsilon$
$X_4 = t \frac{\partial}{\partial x} + \frac{\partial}{\partial u}$	$x = \tilde{x} + \epsilon \tilde{t}, u = \tilde{u} + \epsilon$
$X_5 = T \frac{\partial}{\partial T}$	$T = \tilde{T} e^\epsilon$
$X_6 = x \frac{\partial}{\partial x} + u \frac{\partial}{\partial u}$	$x = \tilde{x} e^\epsilon, u = \tilde{u} e^\epsilon$
$X_7 = t \frac{\partial}{\partial t} + \frac{y}{2} \frac{\partial}{\partial y} - u \frac{\partial}{\partial u} - \frac{v}{2} \frac{\partial}{\partial v}$	$t = \tilde{t} e^\epsilon, y = \tilde{y} \sqrt{e^\epsilon}, u = \tilde{u} e^{-\epsilon}, v = \frac{\tilde{v}}{\sqrt{e^\epsilon}}$

extension and $\mathbf{X}^{[2]}$ - second extension of the generator (11) are required to establish the invariance of (1) and (2) under (11). These extensions can be obtained from

$$\mathbf{X}^{[2]} = \mathbf{X} + \phi_k^t \frac{\partial}{\partial \zeta_{k,t}} + \phi_k^x \frac{\partial}{\partial \zeta_{k,x}} + \phi_k^y \frac{\partial}{\partial \zeta_{k,y}} + \phi_k^{tt} \frac{\partial}{\partial \zeta_{k,tt}} + \phi_k^{xx} \frac{\partial}{\partial \zeta_{k,xx}} + \phi_k^{yy} \frac{\partial}{\partial \zeta_{k,yy}}. \tag{12}$$

The coefficients in these extensions are obtained from

$$\phi_k^n = D_n \phi_k - \zeta_{k,t} D_n(\xi_1) - \zeta_{k,x} D_n(\xi_2) - \zeta_{k,y} D_n(\xi_3), \tag{13}$$

where $n \in \{t, x, y\}$ and $k = 1, 2, 3$. The second extension coefficients are derived using

$$\phi_k^{tt} = D_t \phi_k^t - \zeta_{k,tt} D_n(\xi_1) - \zeta_{k,tx} D_n(\xi_2) - \zeta_{k,ty} D_n(\xi_3),$$

$$\phi_k^{xx} = D_x \phi_k^x - \zeta_{k,tx} D_n(\xi_1) - \zeta_{k,xx} D_n(\xi_2) - \zeta_{k,xy} D_n(\xi_3),$$

$$\phi_k^{yy} = D_y \phi_k^y - \zeta_{k,ty} D_n(\xi_1) - \zeta_{k,xy} D_n(\xi_2) - \zeta_{k,yy} D_n(\xi_3). \tag{14}$$

The subscript in D_i is a total derivative with respect to t , which expands as

$$D_n = \frac{\partial}{\partial n} + \zeta_{k,n} \frac{\partial}{\partial k} + \zeta_{k,m} \frac{\partial}{\partial k, n} + \dots, \tag{15}$$

where $n \in \{t, x, y\}$ and $k = 1, 2, 3$. To determine the infinitesimal coordinates ξ_k and ϕ_k of operator (11), its second-order extension $\mathbf{X}^{[2]}$ is applied to the system of PDEs (1). For instance, its application to the continuity equation in (1) requires the following invariance criterion:

$$\mathbf{X}^{[2]} \left(\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} \right) \Big|_{\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0} = 0. \tag{16}$$

This criterion is evaluated using the continuity equation of system (1). The partial derivatives and coefficients of u, v , and T in the resulting equation are zero. Solving these systems simultaneously yields the system of PDEs, which contains ξ_k and ϕ_k and their partial derivatives. By solving these systems of PDEs, we obtain

$$\xi_1 = \delta_6 t + \delta_1, \xi_2 = \delta_4 x + \delta_5 t + \delta_2, \xi_3 = \frac{\delta_6 y}{2},$$

$$\phi_1 = (\delta_4 - \delta_6)u + \delta_5, \phi_2 = -\frac{\delta_6 v}{2}, \phi_3 = \delta_3 T + \delta_7, \tag{17}$$

where $\delta_1, \delta_2, \dots, \delta_7$ are constants that yield the seven Lie point symmetry generators given in Table 1.

MAPLE offers a built-in code, “Infinitesimals,” for computing Lie point symmetries in its package “PDEtools.” We use the same method to obtain the symmetry transformations for system (1), which form a Lie algebra. These symmetry generators X_1, \dots, X_7 and their linear combinations leave system (1) form-invariant.

To obtain similarity transformations using symmetry generators, condition (2) must remain form-invariant when operated by generators. Both velocity and temperature are functions of the time t and x -coordinate. However, when we use a single symmetry X_1, \dots, X_7 , (considering one at a time), both the velocity $U(x, t)$ and temperature $T_s(x, t)$ in (2) become functions of only the time t or x -coordinate. However, both must remain functions of the time t and x -coordinate. Therefore, $U(x, t)$ and $T_s(x, t)$ in (2) become the desired functions when linear combinations of X_1, \dots, X_7 are used considering two at a time. In the present study, five valid combinations in which both boundary conditions with $U(x, t)$ and $T_s(x, t)$ became functions of the time t and x -coordinate, were obtained.

2.2 Double reductions with similarity transformations

In this subsection, successive double reductions of DEs were used to construct similarity transformations using Lie point symmetry generators. We allowed the symmetry procedure to determine the form of the surface velocity using boundary condition (2). We demonstrate the process of reduction considering the symmetries $X_4 + X_5$. All conditions (2) are left form-invariant by the symmetry combination $X_4 + X_5$, with a few exceptions, namely, $h(t)$, $U(x, t)$, and $T_s(x, t)$, which are put in place by the considered linear combination. After substituting these boundary conditions, the invariance criterion is as follows:

$$\begin{aligned} [X_4 + X_5](u - U(x, t))|_{u=U(x,t)} &= 0, \\ [X_4 + X_5](T - T_s(x, t))|_{T=T_s(x,t)} &= 0. \end{aligned} \tag{18}$$

By substituting generators and expanding them at $u = U(x, t)$ and $T = T_s(x, t)$, we obtain the following linear PDEs:

$$x \frac{\partial U}{\partial x} - u = 0, x \frac{\partial T_s}{\partial x} - T + T_0 = 0. \tag{19}$$

Solving the aforementioned linear PDEs, we obtain

$$u = x\bar{U}(t), T = T_0 + x\bar{T}_s(t). \tag{20}$$

To derive invariants, we apply $X_4 + X_5$, on $J(x, t, y, T, u, v)$, which results in a PDE:

$$tJ_x + J_u + TJ_T = 0, \tag{21}$$

whose solution provides the invariants $\{t, y, \frac{u}{x}, v, \frac{T}{x}\}$. These are assigned as the new independent variables:

$$c_1 = t, c_2 = y, \tag{22}$$

and new dependent variables:

$$P = \frac{u}{x}, Q = v, R = \frac{T}{x}. \tag{23}$$

System (1) in these new variables is transformed into

$$\begin{aligned} P + \frac{\partial Q}{\partial c_2} &= 0, \\ \frac{\partial P}{\partial c_1} + P^2 + Q \frac{\partial P}{\partial c_2} &= \frac{\mu}{\rho} \left(\frac{\partial^2 P}{\partial c_2^2} \right), \\ \frac{\partial R}{\partial c_1} + PR + Q \frac{\partial R}{\partial c_2} &= \frac{\kappa}{\rho C_p} \left(\frac{\partial^2 R}{\partial c_2^2} + \frac{16\sigma T_0^3}{3k_a \kappa} \right), \end{aligned} \tag{24}$$

whereas the boundary conditions (2) become

$$\begin{aligned} c_2 = 0: P &= F(c_1), Q = 0, R = G(c_1), \\ c_2 = h(c_1): Q &= \frac{dh}{dc_1}, \frac{\partial P}{\partial c_2} = \frac{\partial R}{\partial c_2} = 0. \end{aligned} \tag{25}$$

For the second successive reduction, the following symmetry generators for Eq. 24 are derived, which admits a three-dimensional Lie algebra:

$$Z_1 = \frac{\partial}{\partial c_1}, Z_2 = R \frac{\partial}{\partial R}, Z_3 = c_1 \frac{\partial}{\partial c_1} + \frac{c_2}{2} \frac{\partial}{\partial c_2} - \frac{Q}{2} \frac{\partial}{\partial Q} - P \frac{\partial}{\partial P}. \tag{26}$$

The combination of $Z_1 + Z_2 + Z_3$ transforms conditions (25) to

$$\begin{aligned} c_2 = 0: P &= \frac{a_1}{1 + c_1}, Q = 0, R = a_2(1 + c_1), c_2 = a_3\sqrt{1 + c_1}: \\ Q = \frac{a_3}{2}, \frac{\partial P}{\partial c_2} &= \frac{\partial R}{\partial c_2} = 0. \end{aligned} \tag{27}$$

The invariants obtained using $Z_1 + Z_2 + Z_3$ are $\left\{ \frac{c_2}{\sqrt{1+c_1}}, P(1+c_1), Q\sqrt{1+c_1}, \frac{R}{1+c_1} \right\}$. Among the listed invariants, the following is considered a new independent variable:

$$\frac{c_2}{\sqrt{1+c_1}} = \chi, \tag{28}$$

whereas the new dependent variables are

$$P(1+c_1) = L, Q\sqrt{1+c_1} = M, \frac{R}{1+c_1} = N. \tag{29}$$

The second reduction is obtained by substituting the variables in (24) and the associated conditions in (25). The transformed system can now be expressed as

$$\begin{aligned} L + M' &= 0, \\ L^2 - L - \frac{\chi}{2}L' + ML' &= \frac{\mu}{\rho}L'', \\ LN + N - \frac{\chi}{2}N' + MN' &= \frac{\kappa}{\rho C_p} \left(N'' + \frac{16\sigma T_0^3}{3k_a \kappa} \right), \end{aligned} \tag{30}$$

and

$$L(0) = a_1, M(0) = 0, N(0) = a_2, M(a_3) = \frac{a_3}{2}, L'(a_3) = N'(a_3) = 0. \tag{31}$$

The prime here denotes a derivative with respect to χ . For introducing S, Pr , and β in the reduced systems obtained here, we combined (22), (23), (28), and (29) with

$$\chi = \eta\beta\sqrt{\frac{a\mu}{b}}, L = -\frac{b}{a}f'(\eta), M = \beta\sqrt{\frac{b\mu}{a}}f(\eta), N = \vartheta(\eta). \tag{32}$$

This yields

TABLE 2 Lie similarity transformations.

Case	Linear combination and similarity transformation	System of non-linear ODEs
1	$X_4 + X_5$ $\eta = \beta^{-1} \sqrt{\frac{\rho b}{a\mu(1+t)}} y, T = -\frac{\rho x}{\mu} (1+t)\vartheta(\eta) u = -\frac{bx}{a(1+t)} f'(\eta), v = \beta \sqrt{\frac{b\mu}{a\rho(1+t)}} f(\eta)$	$\frac{1+R}{Pr} \vartheta'' + \lambda(S(\frac{1}{2}\vartheta' - \vartheta) - f\vartheta + f'\vartheta) = 0$
2	$X_6 + X_7$ $\eta = \beta^{-1} \sqrt{\frac{\rho b}{a\mu t}} y, T = -\frac{\rho}{\mu} (\vartheta(\eta) + \ln(t(1+x))) u = -\frac{b(1+x)}{at} f'(\eta), v = \beta \sqrt{\frac{b\mu}{a\rho t}} f(\eta)$	$\frac{1+R}{Pr} \vartheta'' + \lambda(S(\frac{1}{2}\vartheta' - 1) - f\vartheta' + f') = 0$
3	$X_5 + X_6$ $\eta = \beta^{-1} \sqrt{\frac{\rho b}{a\mu(1+t)}} y, T = -\frac{\rho t}{\mu} (1+x)\vartheta(\eta) u = -\frac{b(1+x)}{at} f'(\eta), v = \beta \sqrt{\frac{b\mu}{a\rho t}} f(\eta)$	$\frac{1+R}{Pr} \vartheta'' + \lambda(S(\frac{1}{2}\vartheta' - \vartheta) - f\vartheta' + f'\vartheta) = 0$
4	$X_4 + X_6$ $\eta = \beta^{-1} \sqrt{\frac{\rho b}{a\mu t}} y, T = -\frac{\rho}{\mu} (1+\frac{x}{t})\vartheta(\eta) - 1 u = -\frac{b}{a} (1+\frac{x}{t}) f'(\eta) - 1, v = \beta \sqrt{\frac{b\mu}{a\rho t}} f(\eta)$	$\frac{1+R}{Pr} \vartheta'' + \lambda(S(\frac{1}{2}\vartheta' + \vartheta) - f\vartheta + f'\vartheta) = 0$
5	$X_3 + X_6$ $\eta = \beta^{-1} \sqrt{\frac{\rho b}{a\mu t}} y, T = -\frac{\rho}{\mu} (1+x-t)\vartheta(\eta) - 1 u = 1 - \frac{b}{at} (1+x-t) f'(\eta), v = \beta \sqrt{\frac{b\mu}{a\rho t}} f(\eta)$	$\frac{1+R}{Pr} \vartheta'' + \lambda(\frac{S\vartheta}{2} - f\vartheta + f'\vartheta) = 0$

$$\eta = \beta^{-1} \sqrt{\frac{\rho b}{a(1+t)\mu}} y, u = -\frac{bx}{a(1+t)} f'(\eta), v = \beta \sqrt{\frac{b\mu}{a(1+t)\rho}} f(\eta),$$

$$T = -\frac{\rho x}{\mu} (1+t)\vartheta(\eta). \tag{33}$$

Transformations (33) map the first equation of (1) into

$$f''' - \lambda(f f'' - f'^2 - S \frac{\eta}{2} f'' - S f') = 0, \tag{34}$$

and the second transformed equation of (1) under (33) is presented in Table 2.

All conditions (2) are transformed to

$$f(0) = 0, f'(0) = \vartheta(0) = 1, f(1) = \frac{S}{2}, f''(1) = \vartheta'(1) = 0. \tag{35}$$

By employing these symmetries or their linear combinations, which are again Lie point symmetries, we reduce system (1) twice, using the invariants of these symmetries and their linear combinations. These reductions are in the independent variables of the system, and such double reductions enable the construction of the Lie similarity transformation, as presented in Table 2. This table presents the second transformed equation of (1) obtained through the Lie similarity transformations mentioned previously. The first transformed equation of (1) under all similarity transformations is (34), which is the same for all the systems in Table 2.

3 Numerical solution

The difference equations for a non-linear coupled system of ODEs in (8) are constructed using forward finite difference schemes. We now solve the resulting non-linear algebraic equations obtained along with (9) using the Newton–Raphson method. The boundary conditions at $\eta = 0$ and $\eta = 1$ are also approximated using forward difference and backward difference finite schemes, respectively. The

first-order accurate $O(h)$ finite-difference approximations for the first-, second-, and third-order derivatives are expressed as follows:

Forward difference:

$$\frac{df}{d\eta} = \frac{f(\eta_{i+1}) - f(\eta_i)}{h}, \frac{d^2f}{d\eta^2} = \frac{f(\eta_{i+2}) - 2f(\eta_{i+1}) + f(\eta_i)}{h^2},$$

$$\frac{d^3f}{d\eta^3} = \frac{f(\eta_{i+3}) - 3f(\eta_{i+2}) + 3f(\eta_{i+1}) - f(\eta_i)}{h^3}. \tag{36}$$

Backward difference:

$$\frac{df}{d\eta} = \frac{f(\eta_i) - f(\eta_{i-1})}{h}, \frac{d^2f}{d\eta^2} = \frac{f(\eta_i) - 2f(\eta_{i-1}) + f(\eta_{i-2})}{h^2},$$

$$\frac{d^3f}{d\eta^3} = \frac{f(\eta_{i+3}) - 3f(\eta_{i+2}) + 3f(\eta_{i+1}) - f(\eta_i)}{h^3}, \tag{37}$$

The resulting non-linear algebraic equations are solved implicitly. If the dimensionless film thickness λ in (8) is known, five boundary conditions are required to obtain the solution. However, as λ is unknown, the system is made consistent using $f(\eta) = \frac{S}{2}$ from (9). The system is observed to be stable while obtaining the solutions of the non-linear algebraic equations.

3.1 Convergence and grid independence

Newton’s method was used because of its quadratic convergence rate; however, its convergence strongly depended on the initial guess. We performed iterations with an initial guess of 0.2 for each term until the error was less than 10^{-10} . For each variable, satisfactory convergence was achieved over approximately 10 iterations, as shown in Figure 2.

In addition, for all finite-difference-based approximation methods, the truncation error decreased with an increase in the number of nodes. The grid independence was assessed, and a comparison was made with the analytical solution, as shown in Table 3. As the number of nodes exceeds 1,500, the $|\% \text{ error in } \beta|$ and $|\% \text{ error in } f''(0)|$ do not vary significantly. Thus, 1,500 nodes were sufficient to approximate the solution of system (8) subject to

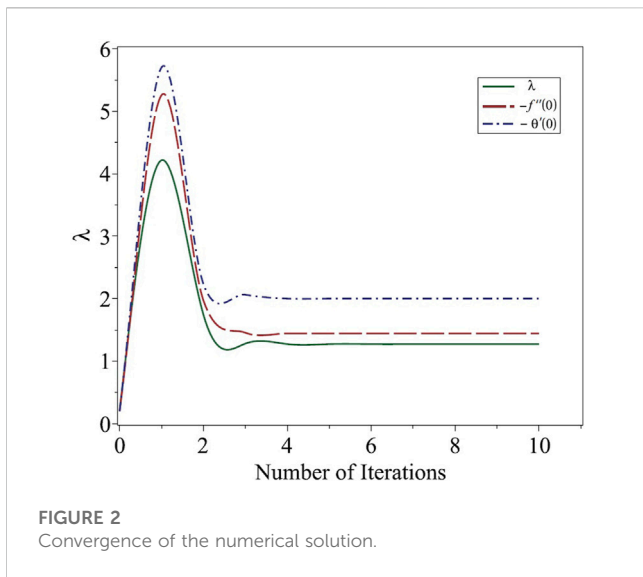


FIGURE 2
Convergence of the numerical solution.

(9). However, to verify the convergence of the solution in the present study, we approximated all solutions using 2,000 nodes.

3.2 Validation of the numerical solution method

The numerical results obtained using 2,000 nodes were compared with the analytical solutions provided by [8] for the effects of variation of λ and $f''(0)$ as shown in Table 4.

4 Results and discussion

Five similarity transformations exist for the system of PDEs (1), given in Table 2. The first step is to obtain the approximate solution of the reduced system of ODEs to classify the transformations based on the trends. In this section, we studied the effect of variation of different parameters of flow and heat transfer in the boundary layer. Table 2 indicates that the first equation in all systems (1)–(5) is the same, namely, an uncoupled non-linear ODE with $f(\eta)$ and η as the dependent and independent terms, respectively. Therefore, the variations in film thickness λ and velocity distributions $f'(\eta)$ were the same for all these systems, owing to a change in the unsteadiness

parameter S . In all these systems, the second equation is a coupled non-linear ODE with $f(\eta)$ and $\vartheta(\eta)$ as dependent and η as independent terms. In the remainder of this section, we first discuss similarity transformations. Subsequently, we study the effects of unsteadiness on film thickness and fluid velocity using the first uncoupled equations of systems (1) and (5). Finally, we present the effects of unsteadiness S , Prandtl number Pr , and radiation R on the temperature.

4.1 Similarity transformations

A major limitation of the previous similarity transformations for similar types of systems is that they are only valid when $t = 1/a$. All previously existing similarity solutions in (7) become invalid at $t = 1/a$ because of (3), i.e., $U = bx/(1 - at)$, which dictates the form of these similarity solutions. In a physical sense, these similarity transformations (7) and the resulting system (8) provide a solution in which the velocity of the stretching sheet U is less than the u -velocity of the fluid. This limits their applicability to real-world scenarios; however, they form the basis of many real problems, including those addressed in the present study.

However, the similarity solutions for all the systems in the current study obtained using the Lie symmetry transformation and presented in Table 2 have no such limitations. Mathematically, they are all valid at any time (i.e., $t > 0$). However, in a physical sense, the velocity and temperature profiles in the boundary layer further finalize the valid transformations. Approximate solutions using a well-established robust method can help eliminate invalid reductions.

4.2 Effects of unsteadiness

Table 5 presents the variation in the dimensionless film thickness λ owing to the unsteadiness S . For a fully developed flow, the film thickness λ decreases with an increase in S . Similarly, the velocity of the flow $f'(\eta)$ is directly proportional to S as shown in Figure 3 and Table 5.

Figure 4A; Figure 5A; Figure 6A; Figure 7A show the effects of variation in temperature distribution $\vartheta(\eta)$ with S . For systems (1) and (3), the surface temperature $\vartheta(1)$ is inversely proportional to S , as shown in Table 6. However, the temperatures for systems (4) and (5) increase with S . The trends observed for systems (4) and (5) for the variation in S contradict those of incompressible viscous laminar flows because the temperature of fluid $\vartheta(\eta)$ cannot exceed the temperature of surface $T_s(x, t)$ or temperature of the flowing fluid itself when the S increases in any fluid flow problem.

TABLE 3 Variation of the film thickness and skin friction with the number of nodes for FDM at $S = 1.2$.

Node	Compute time (S)	β	$-f''(0)$	[% error in β]	[% error in $f''(0)$]
10	0.29	1.2396749	1.5639389	9.93	8.41
50	1.17	1.1475035	1.4657885	1.75	1.61
100	3.4	1.1374664	1.4541253	0.86	0.79
500	87.3	1.1296894	1.4449116	0.17	0.16
1,000	325	1.1287335	1.4437681	0.08	0.08
1,500	690	1.1283772	1.4433873	0.05	0.05
2,000	1,251	1.1282594	1.4419199	0.04	0.05

TABLE 4 Validation of the numerical solution using 2,000 nodes with the analytical solution provided by [8].

S	[8]		Present study	
	β	$-f''(0)$	β	$-f''(0)$
1.0	1.54362	1.97238	1.5443142	1.9715454
1.2	1.127780	1.442631	1.1282594	1.4419199
1.4	0.821032	1.012784	0.8230063	1.0122552
1.6	0.576173	0.642397	0.5743254	0.6425275

TABLE 5 Variation of the surface velocity and dimensionless film thickness with the unsteadiness parameter.

S	λ	$f'(1)$
4.0	0.2140562	2.534312
6.0	0.1791313	4.113212
8.0	0.1460321	5.688561
10.0	0.1225231	7.262964

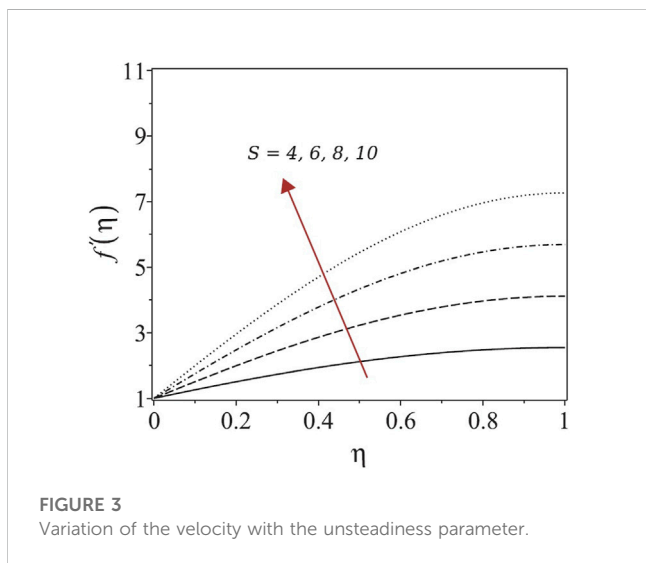


FIGURE 3 Variation of the velocity with the unsteadiness parameter.

distribution $\vartheta(\eta)$ in the boundary layer. For systems (1) and (3), the surface temperature $\vartheta(1)$ decreases with increasing Prandtl number Pr , as shown in Table 7. Similar results have been reported by [16]. However, a decrease in the temperature $\vartheta(1)$ is observed for systems (4) and (5). The temperature profiles for systems (4) and (5) contradict the trends followed by the incompressible viscous laminar flows obtained for such variations in the Prandtl numbers.

4.4 Effects of radiation

The effects of the radiation R on the temperature distribution $\vartheta(\eta)$ in the boundary layer are shown in Figure 4C; Figure 5C; Figure 6C; Figure 7C. As observed before, systems (1) and (3) exhibit trends that are different from the rest of systems (4) and (5); in other words, the surface temperature $\vartheta(1)$ increases with the R for the first three systems while for systems (4) and (5), it decreases with increasing R . In addition, we present the results in Table 8. Liu and Megahed [16] generated temperature profiles by varying R and reported profiles of the type observed for systems (1) and (3). The temperature profiles for systems (4) and (5) contradicted the trends exhibited by the incompressible viscous laminar flows obtained under such variations in radiation. The surface temperature $\vartheta(1)$ is expected to increase with the radiation in the fluid.

4.3 Effects of the Prandtl number

Figure 4B; Figure 5B; Figure 6B; Figure 7B show the effects of the variation of the Prandtl number Pr on the temperature

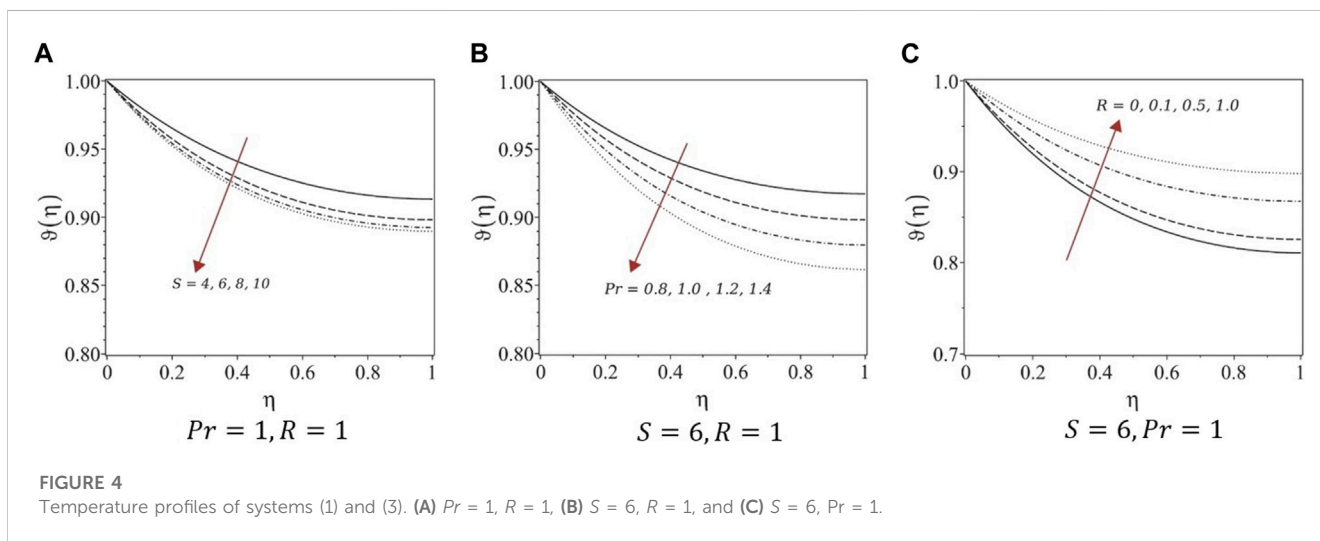


FIGURE 4 Temperature profiles of systems (1) and (3). (A) $Pr = 1, R = 1$, (B) $S = 6, R = 1$, and (C) $S = 6, Pr = 1$.

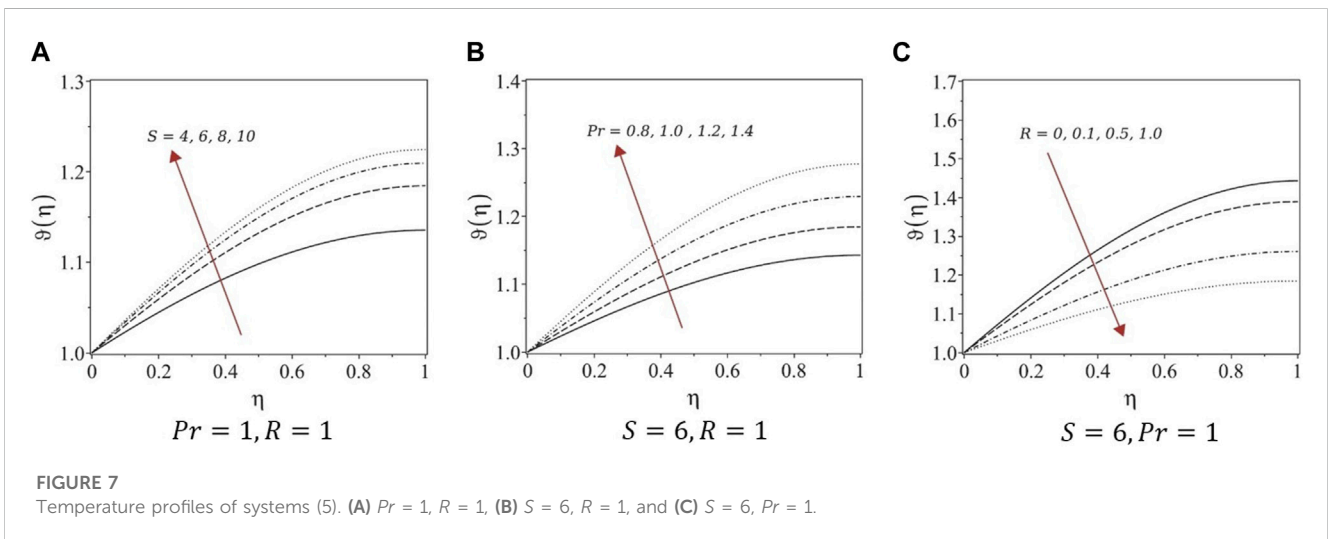
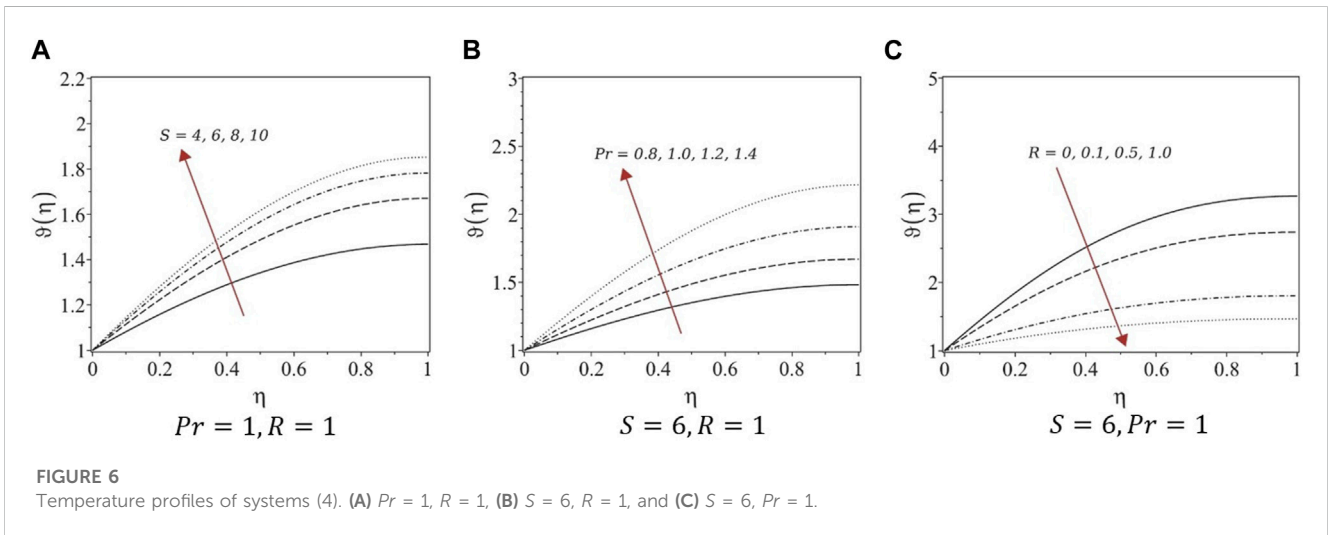
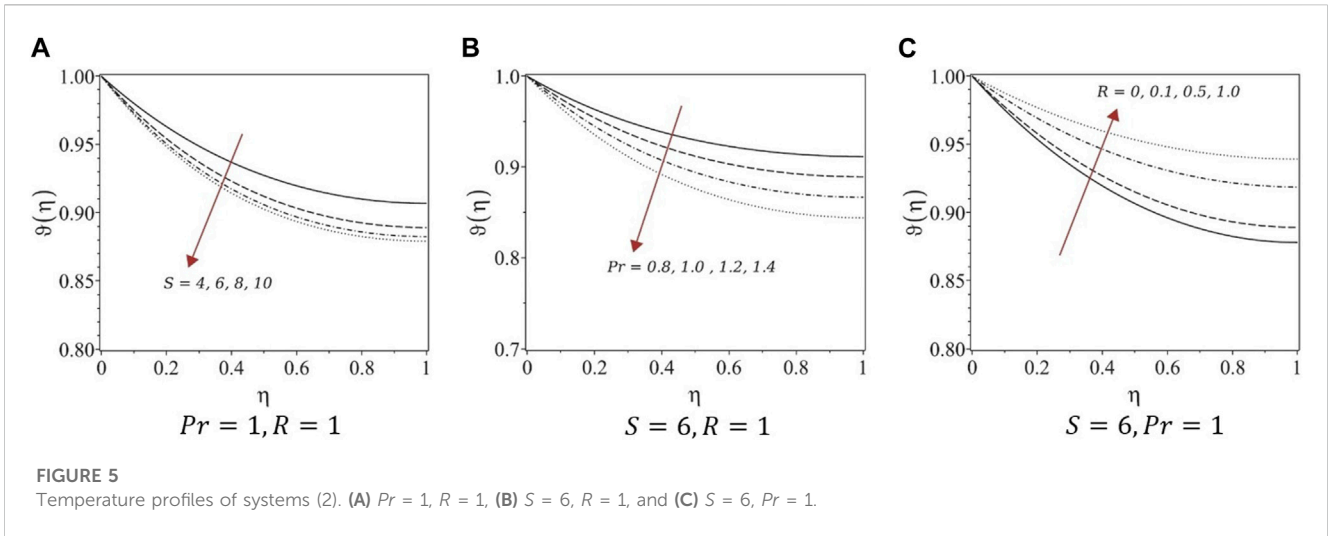


TABLE 6 Variation of the surface temperature with the unsteadiness parameter at $Pr = 1$ and $R = 1$.

S	Systems 1 and 3	System 2	System 3	System 4
4.0	0.91342208	0.90682704	1.46804559	1.13572439
6.0	0.89826710	0.88910677	1.67129567	1.18476313
8.0	0.89266801	0.88245929	1.78297689	1.20975756
10.0	0.88987833	0.87912922	1.85335392	1.22487492

TABLE 7 Variation of the surface temperature with the Prandtl number at $S = 6$ and $R = 1$.

Pr	Systems 1 and 3	System 2	System 3	System 4
0.8	0.91737755	0.91144649	1.48278406	1.1425387
1.0	0.89826708	0.88910680	1.67129454	1.18476307
1.2	0.87972372	0.86669294	1.90964758	1.22950774
1.4	0.86172468	0.84419995	2.21767291	1.27750525

TABLE 8 Variation of the surface temperature with the radiation parameter at $S = 6$ and $Pr = 1$.

R	Systems 1 and 3	System 2	System 3	System 4
0.0	0.81088221	0.87797861	3.26755159	1.44329681
0.1	0.82578737	0.88908093	2.73931277	1.38958115
0.5	0.86766515	0.91872590	1.80650007	1.26112404
1.0	0.89826708	0.93908276	1.46811762	1.18476309

5 Conclusion

We transformed the system of PDEs representing the flow and heat transfer in the boundary layer in the presence of radiation into a system of ODEs using Lie similarity transformations. The Lie similarity transformations presented in this study are different from the existing ones in terms of validity and applicability. These similarity transformations were obtained through invariants associated with linear combinations of Lie symmetry generators, which were used to perform double reductions of the flow model. Four distinct classes of systems of ODEs were revealed with five deduced Lie similarity transformations.

Numerical solutions for the obtained systems of ODEs were determined using finite-difference approximations to eliminate unphysical cases. The first equations in all five systems are the same; hence, the velocity profiles are similar under variations in the unsteadiness parameter. For fully developed flows, the film thickness decreased, whereas the velocity increased with growing unsteadiness. Similar trends were observed for the velocity profiles constructed in this study. For systems (1) and (3), the temperature decreased with increasing unsteadiness and Prandtl number, whereas the temperature increased with increasing radiation parameters. However, for systems (4) and (5), the

temperature increased with the unsteadiness parameter and Prandtl number and decreased with increasing the radiation, which is not the case with real fluids. Therefore, we suggest avoiding the similarity transformation of systems (4) and (5) to study similar types of problems.

Overall, the valid similarity solutions determined using an extensive mathematical procedure allowed us to obtain solutions for unsteady fluid flow and heat transfer in the boundary layer. The HAM or homotopy perturbation method can be used to obtain the analytic solutions for the transformed system, providing valid results. The analytic solutions for fully resolved laminar boundary layer flow and heat transfer at any given time can be obtained by inserting the values for appropriate boundary conditions.

Data availability statement

The original contributions presented in the study are included in the article/Supplementary material. Further inquiries can be directed to the corresponding authors.

Author contributions

Conceptualization: MS; data curation: MB; formal analysis: MB, SA, MS, MA, and AZ; software: MB and MS; validation: MB, SA, MS, MA, and AZ; visualization: MB, MS, KK, KK, and JH; writing—original draft preparation: MS and MB; writing—review and editing: SA, KK, MA, AZ, KK, and JH; funding: KK and JH. All authors contributed to the article and approved the submitted version.

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Conflict of interest

The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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