



# Insightful Facts on Peristalsis Flow of Water Conveying Multi-Walled Carbon Nanoparticles Through Elliptical Ducts With Ciliated Walls

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In this research, a mathematical model is disclosed that elucidates the peristaltic flow of carbon nanotubes in an elliptic duct with ciliated walls. This novel topic of nanofluid flow is addressed for an elliptic domain for the very first time. The practical applications of current analysis include the customization of the mechanical peristaltic pumps, artificial cilia and their role in flow control, drug delivery and prime biological applications etc. The dimensional mathematical problem is transformed into its non-dimensional form by utilizing appropriate transformations and dimensionless parameters. Exact mathematical solutions are computed over the elliptic domain for the partial differential equations appearing in this convection heat transfer problem. A thorough graphical assessment is performed to discuss the prime results. The graphical visualization of the flow in this elliptic duct is obtained by plotting streamlines. The viscous effects are playing a vital role in the heat enhancement as compared to the molecular conduction. Since the incrementing Brinkman number results in a declined conduction due to viscous dissipation that eventually results in an enhanced temperature profile. This research first time elucidates the impacts of nanofluid flow on the peristaltic pumping through an elliptic domain having ciliated walls. Considering water as base fluid with multi-wall Carbon nanotubes for this ciliated elliptic domain having sinusoidal boundaries.

**Keywords:** peristaltic flow, elliptic duct, nanofluid (CNT), ciliated walls, exact solutions

## INTRODUCTION

Peristalsis is concerned with fluid dynamics problems involving flow inside ducts with wavelike deformable walls. The flexible walls' sinusoidal movement eventually aids in the development of flow along the duct's axis. This fascinating subject has a wide range of functional, engineering, and medical applications, making it a hot research topic. Slurries, various heated mixtures, and chemicals are among its primary industrial applications; see Jaffrin and Shapiro [1]. These are some finest mathematical models furnished by different precise researchers that elucidate the peristaltic flow in distinct geometries like cylinders, Barton [2] had numerically examined the peristaltic flow inside a cylindrical conduit, Siddiqui and Schwarz [3] had conveyed the perturbation solution analysis on

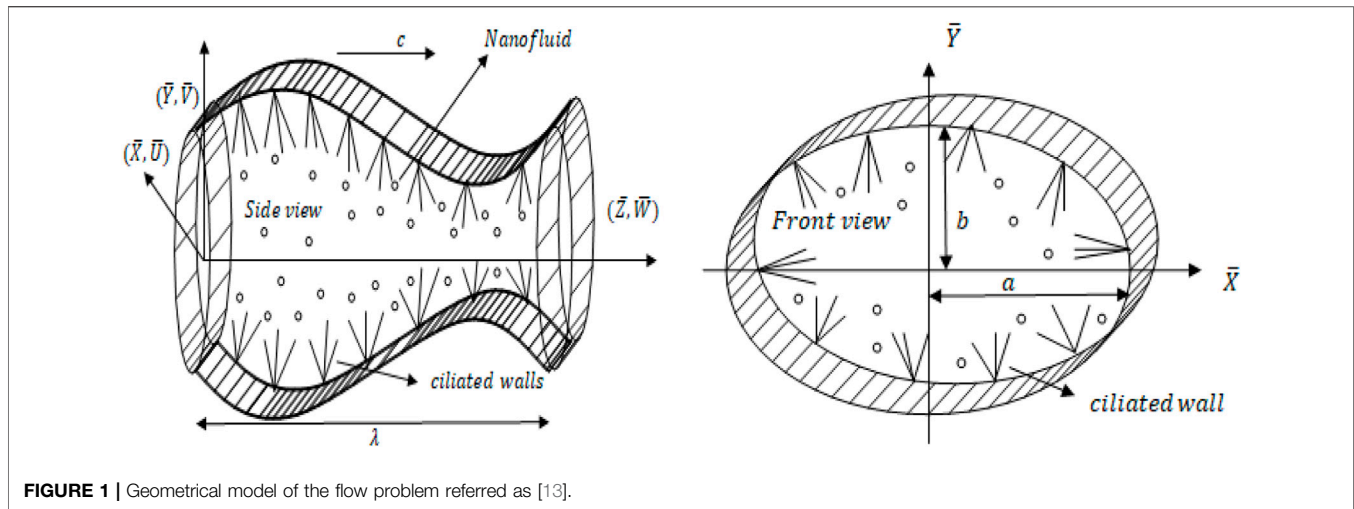


FIGURE 1 | Geometrical model of the flow problem referred as [13].

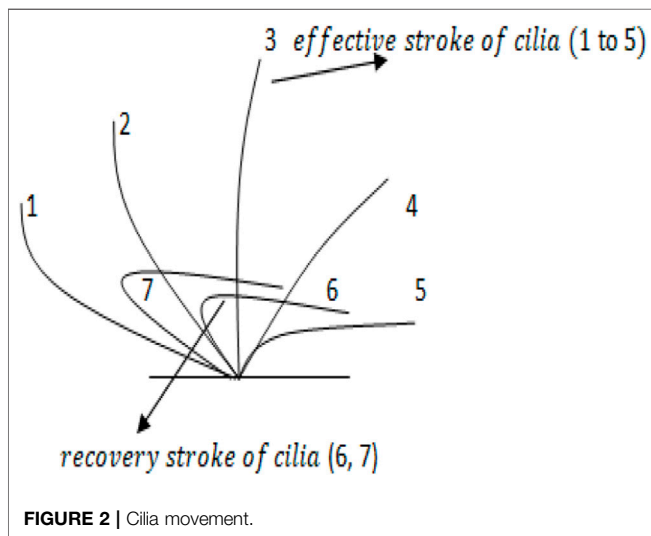


FIGURE 2 | Cilia movement.

Peristaltic pumping of a non-Newtonian fluid, Nadeem et al. [4] had interpreted the Homotopy Analysis solutions on the peristaltic pumping of non-Newtonian Sisko fluid, curved channels, Nadeem and Maraj [5] had disclosed the Homotopy Perturbation solutions on the Peristaltic pumping of Hyperbolic Tangent non-Newtonian fluid through a curved domain, Rashid et al. [6] had also utilized the Homotopy Perturbation analysis to interpret the magnetohydrodynamics effects on the peristaltic pumping of Williamson fluid inside a curved domain, rectangular ducts, Nadeem and Akram [7] had provided exact solutions on Jeffrey fluid flow within a rectangular domain having sinusoidal wall fluctuations, Ellahi et al. [8] provided the Homotopy Perturbation analysis on the three dimensional flow inside a rectangular conduit working as a peristaltic pump, Akram and Saleem [9] had interpreted the Carreau fluid transportation inside a rectangular domain operating as a peristaltic pump, asymmetric geometry, Nadeem and Akram [10] had disclosed the peristaltic

pumping activity for asymmetric domain by using the regular perturbation expansion method, Akbar et al. [11] had highlighted the impact of nanofluids on peristaltic pumping through asymmetric domain, Akbar [12] had also considered the magnetohydrodynamic effects on the peristaltic pumping through asymmetric domain and the peristaltic pumping through an elliptic duct *via* exact solutions was interpreted by Saleem et al. [13].

Nanofluids consist of small-scale (1–100 nm in size) nano particles that are scattered in the base fluid. Scientifically, experts prefer multi-walled carbon nanotubes (MWCNTs) been a special form of carbon nanoparticles because they are nested inside one another and possess elongated hollow cylindrical tiny molecules of  $sp^2$  carbon [14, 15]. These are useful in industrial problems where thermal conductivity is a prime factor [16]. Akbar and Nadeem [17] had reported a mathematical study that elucidates the combine analysis of peristaltic flow and nanofluids. Akbar and Butt [18] had mathematically elucidated the peristaltic flow of water as a base fluid with nano particles having distinct structures. Akbar [19] had numerically examined the nanofluid flow inside asymmetric domain *via* Runge-Kutta technique. Nadeem et al. [20, 21] had evaluated the nanofluids impact on the peristaltic pumping through an annular in addition to rectangular domain. Akbar et al. [22] evaluated the magnetohydrodynamic impacts on the nanofluid pumping through a vertically held asymmetric domain.

The consequence of ciliated walls on the peristalsis driven flow is also a subject of keen interest. Cilia are tiny structures (like human hair) that play a prime role in the flow development. The peristaltic flow mechanism is also studied for distinct geometries having ciliated boundaries like ciliated cylindrical tube, Butt et al. [23] had provided exact solutions on the Phan Thien Tanner non-Newtonian flow inside a ciliated cylindrical domain, Saleem et al. [24] had interpreted the effects of hybrid nanofluid on the peristaltic pumping through a ciliated curved domain, Akbar and Khan [25] highlighted the impacts of MHD on the peristaltic pumping *via* a ciliated asymmetric domain. Sadaf and Nadeem

**TABLE 1 |** Thermophysical properties of nanofluid.

Physical properties	Water (H <sub>2</sub> O)	MWCNT
C <sub>p</sub>	4179	796
k	0.613	3000
ρ	997.1	1600

**TABLE 2 |** Mathematical expressions for nanofluid thermophysical properties.

Density	$\rho_{nf} = (1 - \psi)\rho_f + \psi\rho_{CNT}$
Heat Capacity	$(\rho C_p)_{nf} = (1 - \psi)(\rho C_p)_f + \psi(\rho C_p)_{CNT}$
Viscosity	$\mu_{nf} = \frac{1}{(1 - \psi)^{2.5}}$
Thermal Conductivity	$k_{nf} = \frac{1 - \psi + 2\psi \left( \frac{k_{CNT}}{k_f} \right) \text{Log} \left( \frac{k_{CNT} + k_f}{2k_f} \right)}{1 - \psi + 2\psi \left( \frac{k_f}{k_{CNT} - k_f} \right) \text{Log} \left( \frac{k_{CNT} + k_f}{2k_f} \right)}$
Thermal expansion coefficient and density relation	$(\rho\beta)_{nf} = (1 - \psi)(\rho\beta)_f + \psi(\rho\beta)_{CNT}$

[26] had presented a mathematical model that relates the combine effects of ciliated walls and peristalsis with nanofluid flow. Akbar [27] had reported the mathematical investigation of peristaltic flow of CNT in a symmetric geometry having ciliated boundaries. Akbar and Butt [28] elucidated the impacts of MHD and entropy interpretation on the peristaltic pumping of water based nanofluids through a cylindrical ciliated domain. Nadeem and Sadaf [29] had investigated the trapping phenomenon of nanofluids flow via a ciliated annular domain. Vaidya et al. [30, 31] had highlighted the impacts of chemical reactions on the peristaltic pumping of Ree-Eyring non-Newtonian fluid passing through a permeable domain in addition to an asymmetric domain under MHD effects. Ashraf et al. [32] had examined the MHD impacts on nanofluid flow of Casson fluid through a cylindrical domain with sinusoidal wall fluctuations. Samuel et al. [33–35] had interpreted the effects of MHD, nanofluidic volume fraction with convection analysis through numerical techniques. Saleem et al. [36] highlighted the impacts of activation energy and magnetohydrodynamics on ciliary propelled flow of nanofluid. Ramesh et al. [37] modelled the cilia driven couple stress fluid flow under MHD effects. Farooq et al. [38] had analysed the micro polar flow developed due to cilia propelled rhythmic wave. Akbar et al. [39] modelled the pressure driven flow generated due to rhythmic activity of cilia.

A thorough and careful investigation of the available literature has disclosed that the peristaltic flow of carbon nanotubes in an elliptic duct with ciliated walls is not mathematically reported yet. Thus, the intent of the present mathematical computation is to elucidate this important topic for an elliptic domain for the first time. The base fluid considered in this mathematical study is water and multi-wall carbon nanotubes are taken into account. The viscous dissipation effect is also incorporated for a detailed study of convection heat transfer. Exact mathematical solutions are computed and the results are verified through graphical assessment. Streamlines depict the visualization of flow pattern.

## MATHEMATICAL MODEL

The peristaltic flow of carbon nanotubes in an elliptic duct with ciliated walls is mathematically investigated. A Cartesian coordinate system approach is utilized to interpret this mathematical study. The geometry of the problem is given by **Figure 1** providing the model of elliptic domain having ciliated walls. The sinusoidal wall fluctuations are evident in **Figure 1** and the ciliated wall are also mentioned. **Figure 1** contains the front together with a side view of this geometry, the front view highlights the elliptic domain of this duct.

The envelope model of cilia motion that considers the elliptical shape movements is taken into account. The equations considered for this model incorporates the sinusoidal metachronal wave movements generated due to rhythmic cilia motion. The computational equations that narrate this envelope model of cilia tips are referred as [40].

$$\begin{aligned} \bar{Y} &= b_0 + b_0\phi\text{Cos}\left(\frac{2\pi}{\lambda}(\bar{Z} - c\bar{t})\right) = \bar{f}(\bar{Z}, \bar{t}), \\ \bar{Z} &= \bar{Z}_0 + b_0\phi\alpha\text{Sin}\left(\frac{2\pi}{\lambda}(\bar{Z} - c\bar{t})\right) = \bar{g}(\bar{Z}, \bar{Z}_0, \bar{t}), \end{aligned} \tag{1}$$

The following computational equations are used to express the velocities of cilia tips (i.e. axial and radial velocity respectively).

$$\begin{aligned} \bar{W} &= \frac{\partial \bar{Z}}{\partial \bar{t}} \Big|_{\bar{Z}_0} = \frac{\partial \bar{g}}{\partial \bar{t}} + \frac{\partial \bar{g}}{\partial \bar{Z}} \frac{\partial \bar{Z}}{\partial \bar{t}} = \frac{\partial \bar{g}}{\partial \bar{t}} + \frac{\partial \bar{g}}{\partial \bar{Z}} \bar{W}, \\ \bar{V} &= \frac{\partial \bar{Y}}{\partial \bar{t}} \Big|_{\bar{Z}_0} = \frac{\partial \bar{f}}{\partial \bar{t}} + \frac{\partial \bar{f}}{\partial \bar{Z}} \frac{\partial \bar{Z}}{\partial \bar{t}} = \frac{\partial \bar{f}}{\partial \bar{t}} + \frac{\partial \bar{f}}{\partial \bar{Z}} \bar{W}, \end{aligned} \tag{2}$$

The simplification of **Eqs 1, 2** provides the following equations

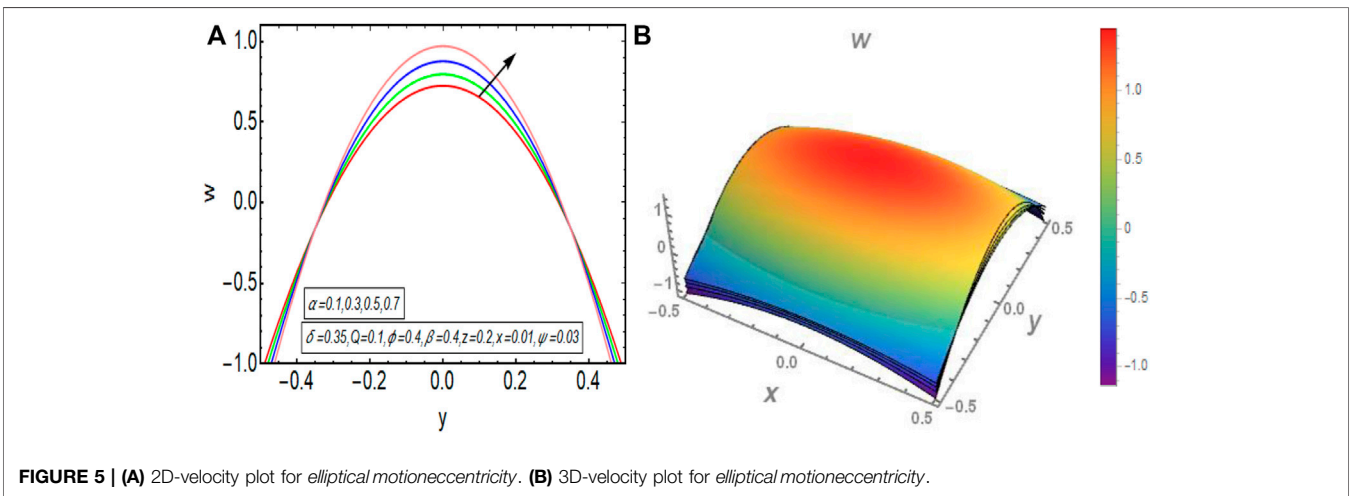
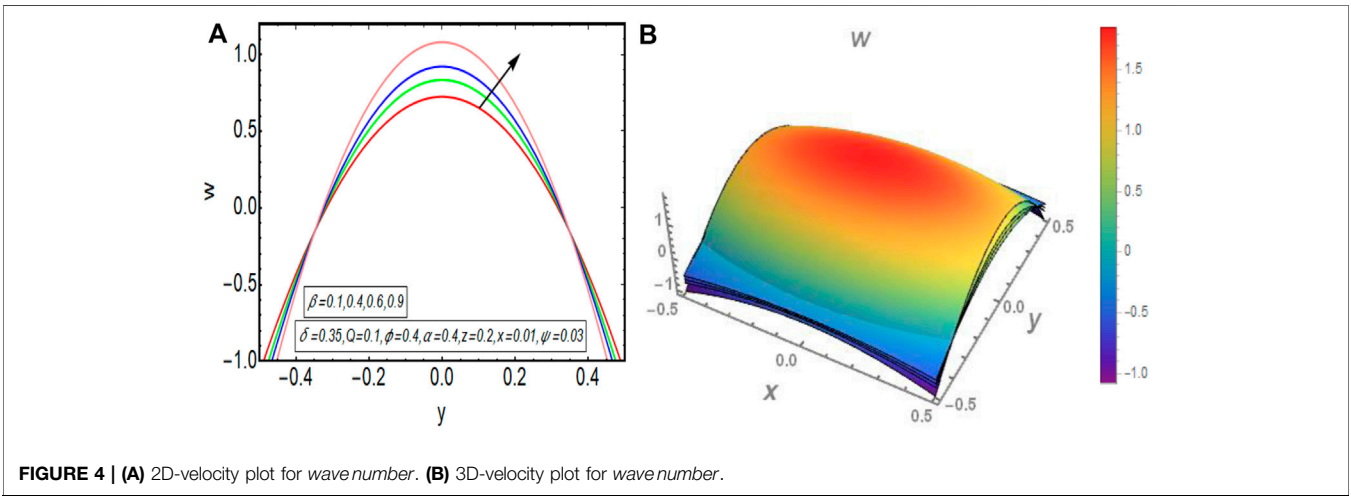
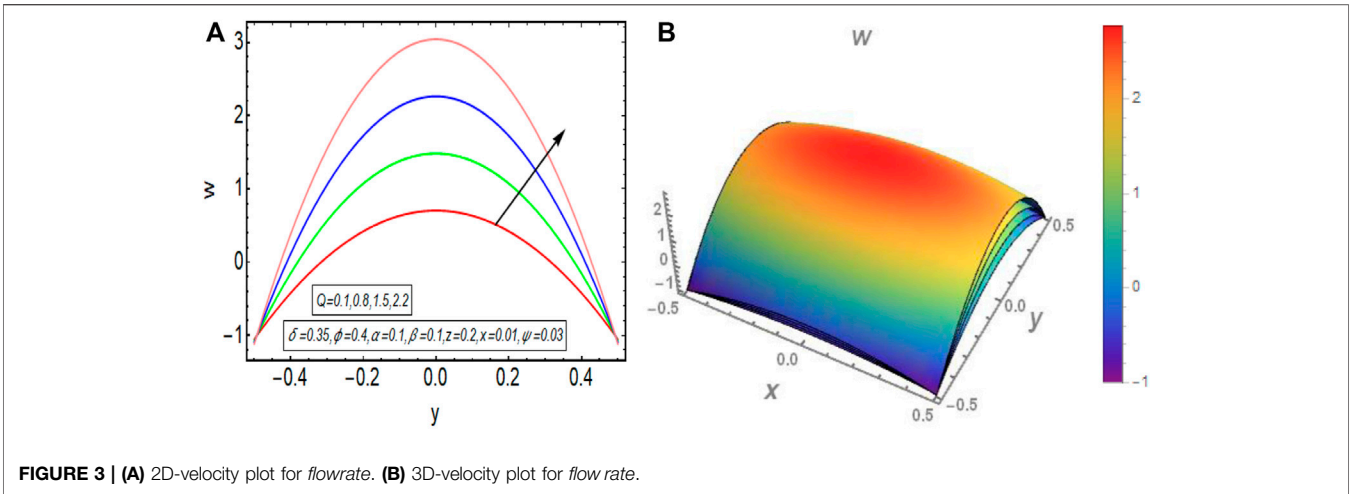
$$\begin{aligned} \bar{W} &= \frac{-\left(\frac{2\pi}{\lambda}\right) \left[ \phi\alpha b_0 c \text{Cos}\left(\frac{2\pi}{\lambda}(\bar{Z} - c\bar{t})\right) \right]}{\left[ 1 - \left(\frac{2\pi}{\lambda}\right) \left\{ \phi\alpha b_0 c \text{Cos}\left(\frac{2\pi}{\lambda}(\bar{Z} - c\bar{t})\right) \right\} \right]}, \\ \bar{V} &= \frac{\left(\frac{2\pi}{\lambda}\right) \left[ \phi b_0 c \text{Sin}\left(\frac{2\pi}{\lambda}(\bar{Z} - c\bar{t})\right) \right]}{\left[ 1 - \left(\frac{2\pi}{\lambda}\right) \left\{ \phi\alpha b_0 c \text{Cos}\left(\frac{2\pi}{\lambda}(\bar{Z} - c\bar{t})\right) \right\} \right]}, \end{aligned} \tag{3}$$

The above mentioned velocities  $\bar{W}$  and  $\bar{V}$  mainly differentiate between the two strokes of cilia motion, (i.e., effective and recovery strokes respectively). The cilia tips are assumed to circulate in an elliptical course, as revealed in **Figure 2**. Cilium remains inflexible and rigid during its effective stroke. On contrary, it shows flexibility during its recovery stroke and retreats loosely.

The mathematical modelling for the incompressible flow with carbon nanotubes and heat convection is provided in dimensional form as follows

$$\frac{\partial \bar{U}}{\partial \bar{X}} + \frac{\partial \bar{V}}{\partial \bar{Y}} + \frac{\partial \bar{W}}{\partial \bar{Z}} = 0, \tag{4}$$

$$\begin{aligned} \rho_{nf} \left( \frac{\partial \bar{U}}{\partial \bar{t}} + \bar{U} \frac{\partial \bar{U}}{\partial \bar{X}} + \bar{V} \frac{\partial \bar{U}}{\partial \bar{Y}} + \bar{W} \frac{\partial \bar{U}}{\partial \bar{Z}} \right) \\ = -\frac{\partial \bar{P}}{\partial \bar{X}} + \mu_{nf} \left( \frac{\partial^2 \bar{U}}{\partial \bar{X}^2} + \frac{\partial^2 \bar{U}}{\partial \bar{Y}^2} + \frac{\partial^2 \bar{U}}{\partial \bar{Z}^2} \right), \end{aligned} \tag{5}$$



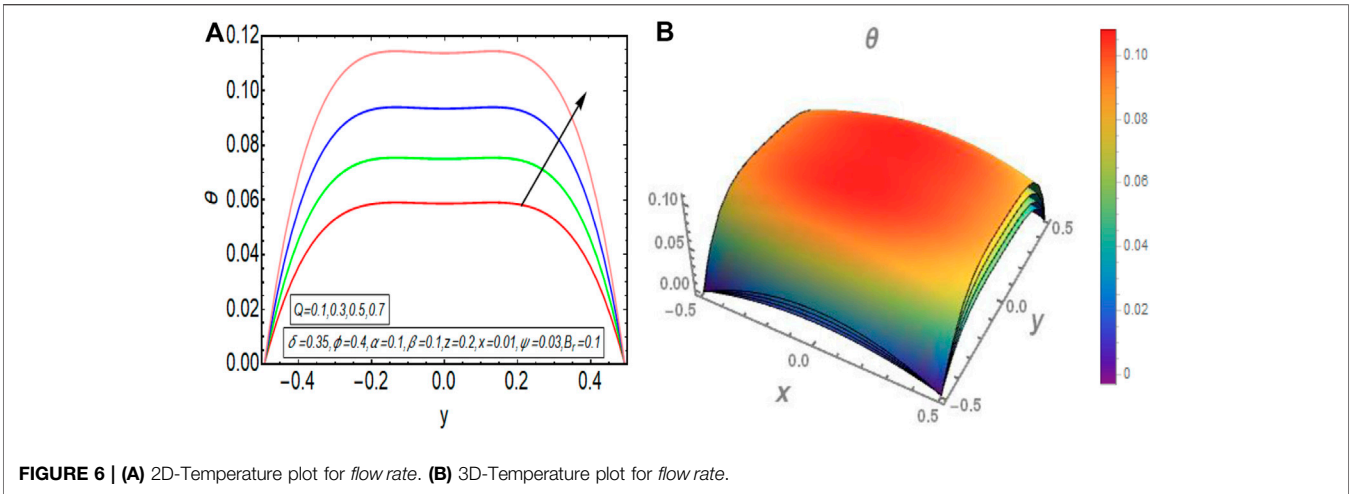


FIGURE 6 | (A) 2D-Temperature plot for flow rate. (B) 3D-Temperature plot for flow rate.

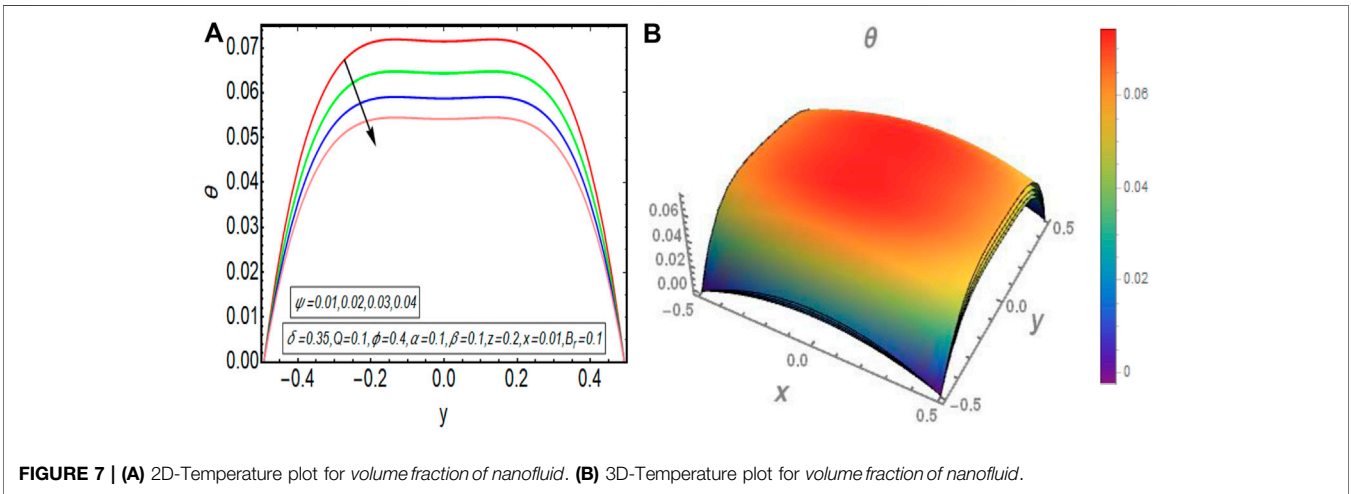


FIGURE 7 | (A) 2D-Temperature plot for volume fraction of nanofluid. (B) 3D-Temperature plot for volume fraction of nanofluid.

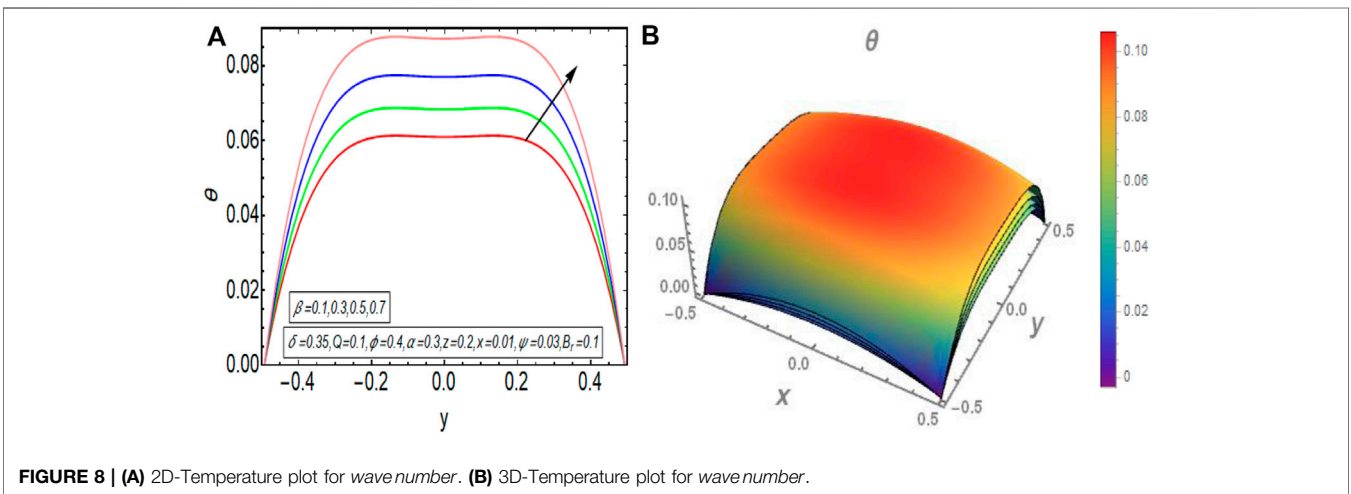
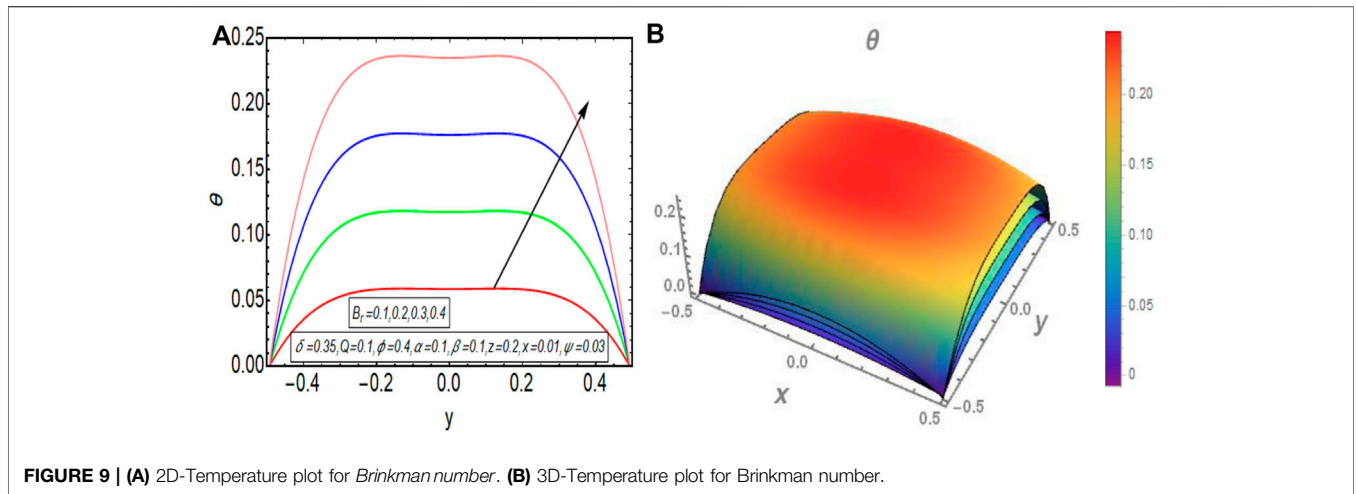


FIGURE 8 | (A) 2D-Temperature plot for wave number. (B) 3D-Temperature plot for wave number.





$$\begin{aligned} &\rho_{nf} \left( \frac{\partial \bar{V}}{\partial t} + \bar{U} \frac{\partial \bar{V}}{\partial \bar{X}} + \bar{V} \frac{\partial \bar{V}}{\partial \bar{Y}} + \bar{W} \frac{\partial \bar{V}}{\partial \bar{Z}} \right) \\ &= -\frac{\partial \bar{P}}{\partial \bar{Y}} + \mu_{nf} \left( \frac{\partial^2 \bar{V}}{\partial \bar{X}^2} + \frac{\partial^2 \bar{V}}{\partial \bar{Y}^2} + \frac{\partial^2 \bar{V}}{\partial \bar{Z}^2} \right), \end{aligned} \quad (6)$$

$$\begin{aligned} &\rho_{nf} \left( \frac{\partial \bar{W}}{\partial t} + \bar{U} \frac{\partial \bar{W}}{\partial \bar{X}} + \bar{V} \frac{\partial \bar{W}}{\partial \bar{Y}} + \bar{W} \frac{\partial \bar{W}}{\partial \bar{Z}} \right) \\ &= -\frac{\partial \bar{P}}{\partial \bar{Z}} + \mu_{nf} \left( \frac{\partial^2 \bar{W}}{\partial \bar{X}^2} + \frac{\partial^2 \bar{W}}{\partial \bar{Y}^2} + \frac{\partial^2 \bar{W}}{\partial \bar{Z}^2} \right), \end{aligned} \quad (7)$$

$$\begin{aligned} &(\rho C_p)_{nf} \left( \frac{\partial \bar{T}}{\partial t} + \bar{U} \frac{\partial \bar{T}}{\partial \bar{X}} + \bar{V} \frac{\partial \bar{T}}{\partial \bar{Y}} + \bar{W} \frac{\partial \bar{T}}{\partial \bar{Z}} \right) \\ &= k_{nf} \left( \frac{\partial^2 \bar{T}}{\partial \bar{X}^2} + \frac{\partial^2 \bar{T}}{\partial \bar{Y}^2} + \frac{\partial^2 \bar{T}}{\partial \bar{Z}^2} \right) + \mu_{nf} \left[ 2 \left\{ \left( \frac{\partial \bar{U}}{\partial \bar{X}} \right)^2 + \left( \frac{\partial \bar{V}}{\partial \bar{Y}} \right)^2 \right. \right. \\ &\quad \left. \left. + \left( \frac{\partial \bar{W}}{\partial \bar{Z}} \right)^2 \right\} + \left( \frac{\partial \bar{U}}{\partial \bar{Y}} + \frac{\partial \bar{V}}{\partial \bar{X}} \right)^2 + \left( \frac{\partial \bar{V}}{\partial \bar{Z}} + \frac{\partial \bar{W}}{\partial \bar{Y}} \right)^2 \right. \\ &\quad \left. + \left( \frac{\partial \bar{W}}{\partial \bar{X}} + \frac{\partial \bar{U}}{\partial \bar{Z}} \right)^2 \right], \end{aligned} \quad (8)$$

The respective dimensional form of boundary conditions for ciliated walls and elliptic domain are given as

$$\bar{W} = \frac{-(\frac{2\pi}{\lambda})[\phi \alpha b_0 c \text{Cos}(\frac{2\pi}{\lambda}(\bar{Z} - c\bar{t}))]}{[1 - (\frac{2\pi}{\lambda})\{\phi \alpha b_0 \text{Cos}(\frac{2\pi}{\lambda}(\bar{Z} - c\bar{t}))\}]}, \text{ for } \frac{\bar{x}^2}{a^2} + \frac{\bar{y}^2}{b^2} = 1. \quad (9)$$

$$\bar{T} = \bar{T}_w \text{ for } \frac{\bar{x}^2}{a^2} + \frac{\bar{y}^2}{b^2} = 1.$$

The unsteady and steady frames of reference are related by using the following equations

$$\bar{x} = \bar{X}, \bar{y} = \bar{Y}, \bar{z} = \bar{Z} - c\bar{t}, \bar{p} = \bar{P}, \bar{u} = \bar{U}, \bar{v} = \bar{V}, \bar{w} = \bar{W} - c, \quad (10)$$

The non-dimensional variables that are incorporated in present analysis are given as

$$\begin{aligned} x &= \frac{\bar{x}}{D_h}, y = \frac{\bar{y}}{D_h}, z = \frac{\bar{z}}{\lambda}, t = \frac{c\bar{t}}{\lambda}, w = \frac{\bar{w}}{c}, p = \frac{D_h^2 \bar{p}}{\mu_f \lambda c}, \\ \theta &= \frac{\bar{T} - \bar{T}_w}{\bar{T}_b - \bar{T}_w}, \delta = \frac{b_0}{a_0}, \phi = \frac{d}{b_0}, u = \frac{\lambda \bar{u}}{D_h c}, v = \frac{\lambda \bar{v}}{D_h c}, \\ a &= \frac{\bar{a}}{D_h}, b = \frac{\bar{b}}{D_h}, Br = \frac{\mu_f c^2}{k_f (\bar{T}_b - \bar{T}_w)}, \beta = \frac{b_0}{\lambda}, \end{aligned} \quad (11)$$

Whenever we deal with a non-circular domain then the concept of hydraulic diameter needs to be considered. It is considered as four times the cross-sectional area divided by the wetted perimeter of cross-section. The mathematical expression for the hydraulic diameter of elliptic duct is narrated as

$$D_h = \frac{\pi b_0}{E(e)}, \quad (12)$$

The computational equation that narrates the eccentricity of ellipse is  $e = \sqrt{1 - \delta^2}$ , where  $\delta$  is the aspect ratio and the second kind elliptical integral  $E(e)$  is referred as Yang et al. [41].

$$E(e) = \int_0^{\frac{\pi}{2}} \sqrt{1 - e^2 \text{Sin}^2 \alpha_1} d\alpha_1, \quad (13)$$

The useful transformations provided in Eq. 10, the dimensionless variables given in Eq. 11 are used in Eqs 5–9 and the approximation ( $\lambda \rightarrow \infty$ ) is used to avail the following set of dimensionless equations

$$\frac{\partial p}{\partial x} = 0, \quad (14)$$

$$\frac{\partial p}{\partial y} = 0, \quad (15)$$

$$\frac{dp}{dz} = \left( \frac{\mu_{nf}}{\mu_f} \right) \left( \frac{\partial^2 w}{\partial x^2} + \frac{\partial^2 w}{\partial y^2} \right), \quad (16)$$

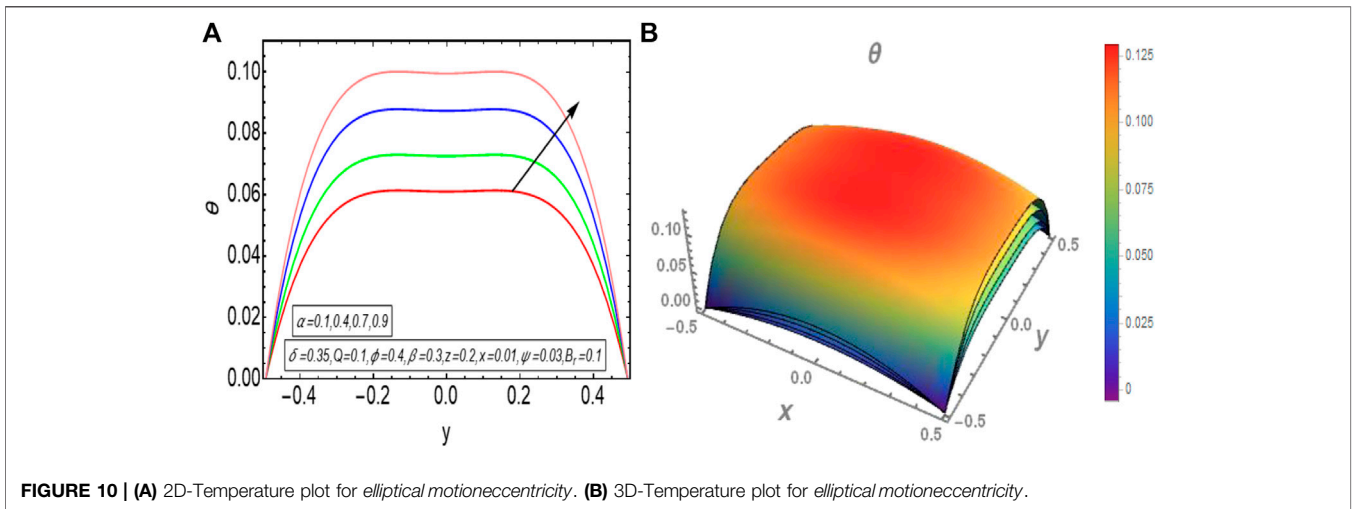


FIGURE 10 | (A) 2D-Temperature plot for elliptical motion eccentricity. (B) 3D-Temperature plot for elliptical motion eccentricity.

$$\left(\frac{k_{nf}}{k_f}\right)\left(\frac{\partial^2 \theta}{\partial x^2} + \frac{\partial^2 \theta}{\partial y^2}\right) + Br_r \left(\frac{\mu_{nf}}{\mu_f}\right) \left[\left(\frac{\partial w}{\partial x}\right)^2 + \left(\frac{\partial w}{\partial y}\right)^2\right] = 0, \quad (17)$$

$$2C_4 + 2C_5 = \frac{dP/dz}{\mu_{nf}/\mu_f}, \quad (iii)$$

Eq. 17 contains the dimensionless brinkman number  $Br_r$  that is the product of two dimensionless numbers Prandtl ( $P_r$ ) and Eckert ( $E_r$ ), i.e.,  $Br_r = P_r E_r$ .

The dimensionless boundary conditions over the elliptic domain are

$$w = -1 - \frac{2\pi\phi\alpha\beta\cos(2\pi z)}{1 - 2\pi\phi\alpha\beta\cos(2\pi z)}, \text{ for } \frac{x^2}{a^2} + \frac{y^2}{b^2} = 1. \quad (18)$$

$$\theta = 0, \text{ for } \frac{x^2}{a^2} + \frac{y^2}{b^2} = 1, \quad (19)$$

Where  $a = \frac{E(\epsilon)}{\pi} [1 + \phi \sin(2\pi z)]$ ,  $b = \frac{E(\epsilon)}{\pi} [1 - \phi \sin(2\pi z)]$ . Where  $a$  and  $b$  provide the dimensionless form of wall functions that tackle the sinusoidal movement of travelling boundaries.

Table 1 Akbar [42], provides the thermophysical properties of base fluid water and nanofluid. Table 2 Akbar [27], shows the mathematical properties of nanofluid.

### EXACT SOLUTION

The dimensionless form of momentum equation is a non-homogeneous partial differential Eq. 16 subject to non-homogeneous boundary conditions (18). In order to solve this PDE, a polynomial solution method to solve PDE's over elliptic domain is taken into account. Consider the solution in a six constants polynomial form for velocity profile as narrated below

$$w(x, y) = C_1 x^4 + C_2 y^4 + C_3 x^2 y^2 + C_4 x^2 + C_5 y^2 + C_6, \quad (20)$$

Substituting Eq. 20 into Eq. 16 and equating the coefficients of  $x^2$ ,  $y^2$ ,  $x^0$ ,  $y^0$  on both sides of equation, we get

$$12C_1 + 2C_3 = 0, \quad (i)$$

$$2C_3 + 12C_2 = 0, \quad (ii)$$

Now using Eq. 20 in boundary condition (18) and equating the coefficients of  $x^4$ ,  $x^2$ ,  $x^0$ , we have following equations

$$C_1 a^4 + C_2 b^4 - C_3 a^2 b^2 = 0, \quad (iv)$$

$$-2C_2 b^4 + C_3 a^2 b^2 + C_4 a^2 - C_5 b^2 = 0, \quad (v)$$

$$C_2 b^4 + C_5 b^2 + C_6 = -1 - \frac{2\pi\phi\alpha\beta\cos(2\pi z)}{1 - 2\pi\phi\alpha\beta\cos(2\pi z)}, \quad (vi)$$

The simultaneous solution of above equations gives the following values of constants

$$C_1 = 0, C_2 = 0, C_3 = 0, C_4 = \frac{b^2 \frac{dP}{dz}}{2(a^2 + b^2) \left(\frac{\mu_{nf}}{\mu_f}\right)}, C_5 = \frac{a^2 \frac{dP}{dz}}{2(a^2 + b^2) \left(\frac{\mu_{nf}}{\mu_f}\right)},$$

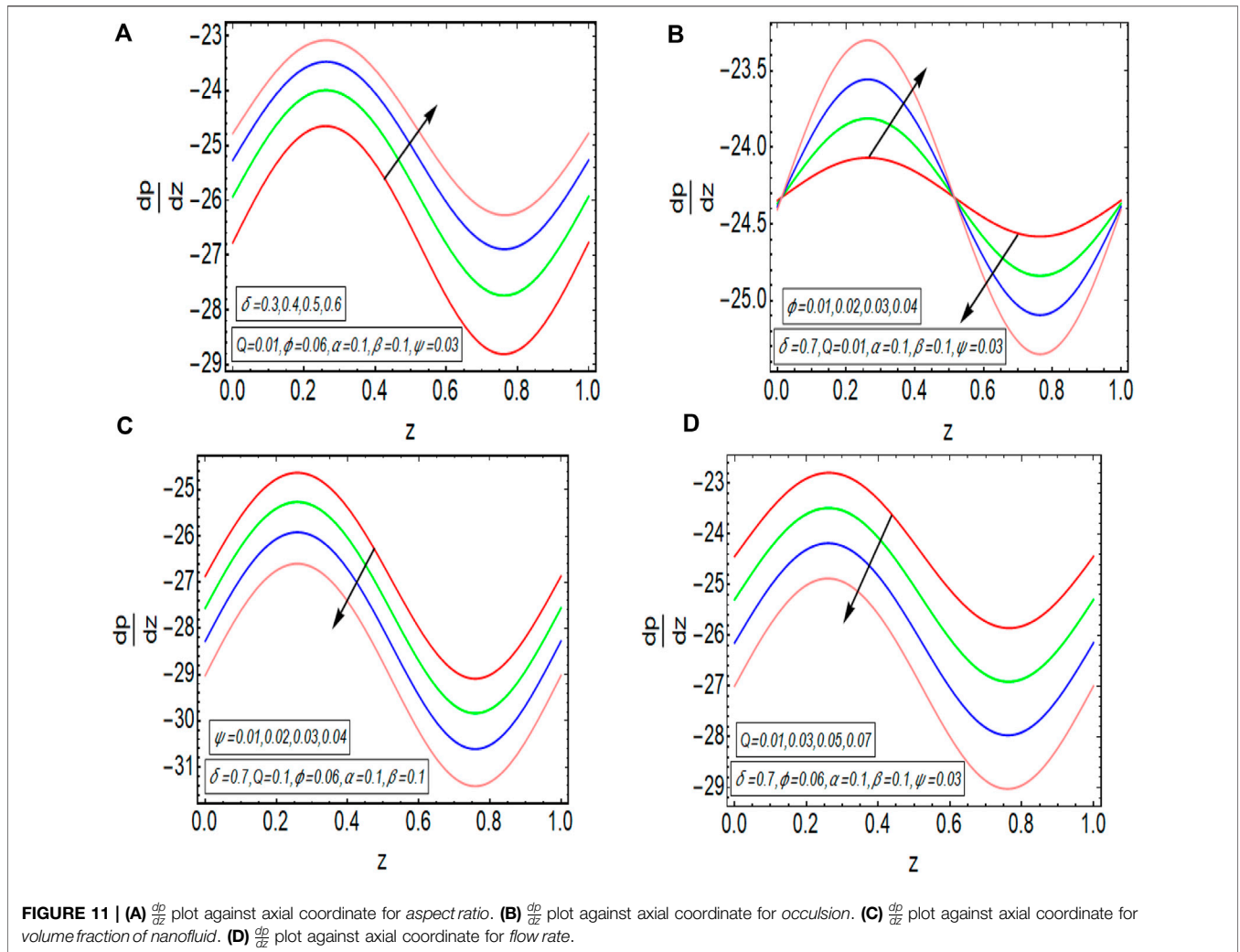
$$C_6 = \frac{-a^2 b^2 \frac{dP}{dz} - 2a^2 \left(\frac{\mu_{nf}}{\mu_f}\right) - 2b^2 \left(\frac{\mu_{nf}}{\mu_f}\right) + 2a^2 b^2 \frac{dP}{dz} \pi \alpha \beta \phi \cos(2\pi z)}{2(a^2 + b^2) \left(\frac{\mu_{nf}}{\mu_f}\right) (-1 + 2\pi\phi\alpha\beta\cos(2\pi z))}$$

The values of these constants is inserted in Eq. 20 and exact mathematical solution is obtained for velocity as follows

$$w(x, y) = \frac{(dP/dz) a^2 b^2 \left(\frac{x^2}{a^2} + \frac{y^2}{b^2} - 1\right)}{2(a^2 + b^2) \left(\frac{\mu_{nf}}{\mu_f}\right)} + \frac{1}{-1 + 2\pi\phi\alpha\beta\cos(2\pi z)}, \quad (21)$$

The non-dimensional mathematical expression for flow rate  $q(z)$  is availed by integrating Eq. 21 over the elliptic domain.

$$q(z) = -\frac{a^3 b^3 \frac{dP}{dz} \pi}{4(a^2 + b^2) \left(\frac{\mu_{nf}}{\mu_f}\right)} + \frac{ab\pi}{-1 + 2\pi\phi\alpha\beta\cos(2\pi z)}, \quad (22)$$



**FIGURE 11 | (A)**  $\frac{dp}{dz}$  plot against axial coordinate for aspect ratio. **(B)**  $\frac{dp}{dz}$  plot against axial coordinate for occlusion. **(C)**  $\frac{dp}{dz}$  plot against axial coordinate for volume fraction of nanofluid. **(D)**  $\frac{dp}{dz}$  plot against axial coordinate for flow rate.

The pressure gradient is calculated by using Eq. 22 and given as

$$\frac{dp}{dz} = \frac{4(a^2 + b^2) \left( \mu_{nf} / \mu_f \right) \left[ \frac{\int_0^1 abdz - Q}{\pi} + \frac{ab}{-1 + 2\pi\phi\alpha\beta\cos(2\pi z)} \right]}{a^3 b^3}, \quad (23)$$

The pressure rise for a single wave-length is computed by using

$$\Delta P = \int_0^1 \frac{\partial p}{\partial z} dz, \quad (24)$$

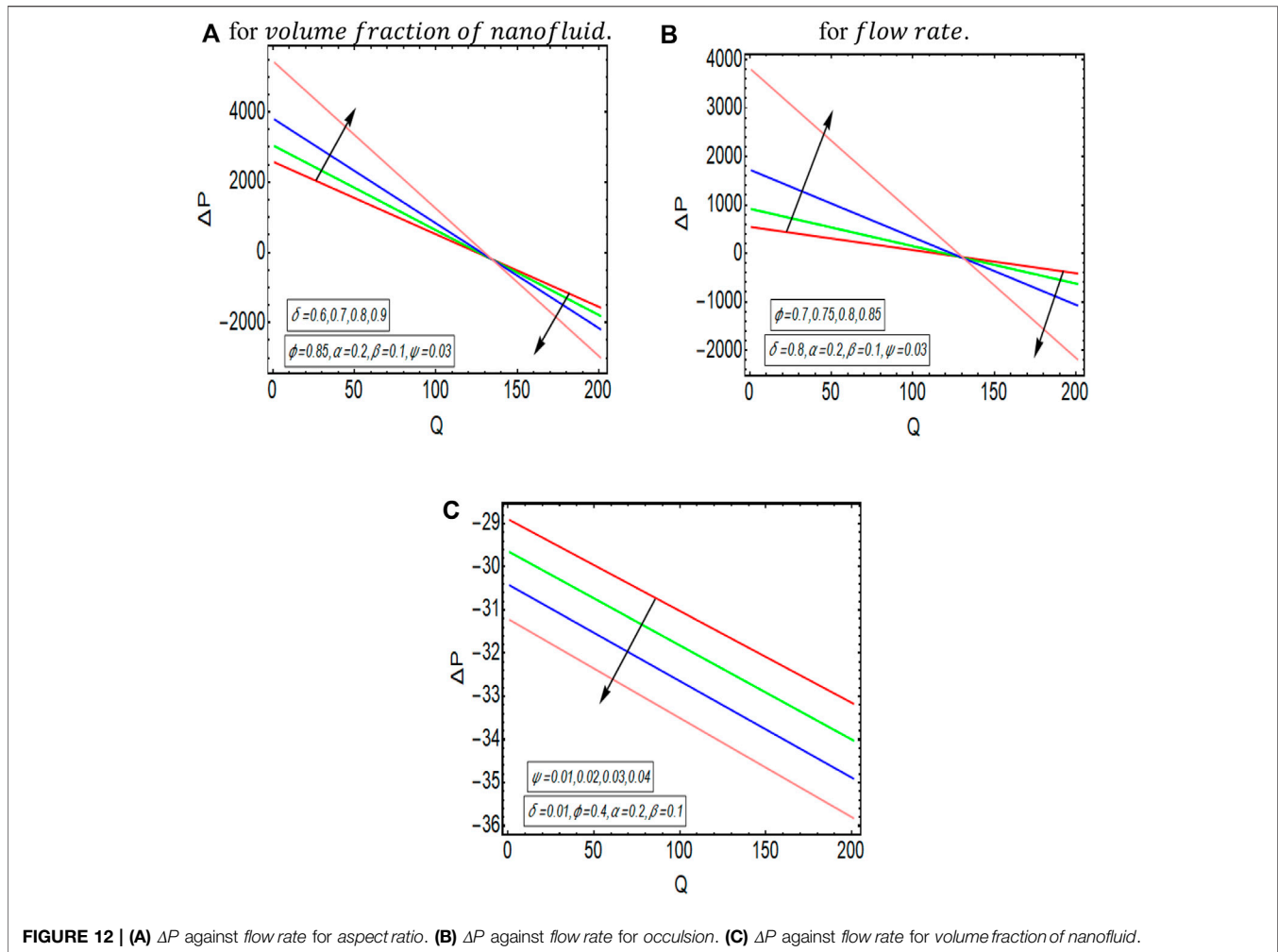
The technique that was utilized to get an exact velocity solution is employed again to get an exact temperature function given as

$$\theta(x, y) = \frac{-B_r \left( \frac{dp}{dz} \right)^2 a^2 b^2 \left( \frac{x^2}{a^2} + \frac{y^2}{b^2} - 1 \right) [b^6 x^2 + a^2 b^4 (b^2 + 6x^2 - y^2) + a^6 (b^2 + y^2) + a^4 b^2 (4b^2 - x^2 + 6y^2)]}{12(a^2 + b^2)^2 (a^4 + 6a^2 b^2 + b^4) \left( \frac{k_{nf}}{k_f} \right) \left( \frac{\mu_{nf}}{\mu_f} \right)} \quad (25)$$

## ANALYSIS OF RESULTS

The results obtained in the exact solution section, that is exact solution of momentum equation given by Eq. 21 exactly satisfies the corresponding momentum Eq. 16 and boundary condition (18). Further, the exact solution of temperature profile given by Eq. 25 also satisfies the corresponding energy Eq. 17 with boundary condition (19). The validation of these solutions is also confirmed by using Mathematica software. According to the modelled problem and relevant boundary conditions, the flow profile in addition to the temperature profile should have a maximum value in the centre of elliptic domain and both the profiles should decline towards the walls of channel. Thus, it is evident from the graphical results that flow and temperature are maximum in the centre and reduces towards the boundaries. The temperature graphs show that temperature profile declines toward the boundaries and becomes zero as it was considered in the boundary condition (19). If  $\frac{x^2}{a^2} + \frac{y^2}{b^2} = 1$  is inserted in Eq. 21 then the reduced form gives the boundary condition (18). Further, if  $\frac{x^2}{a^2} + \frac{y^2}{b^2} = 1$  is inserted in Eq. 25 then the reduced form provides the boundary condition (19). This also validates the considered boundary conditions.

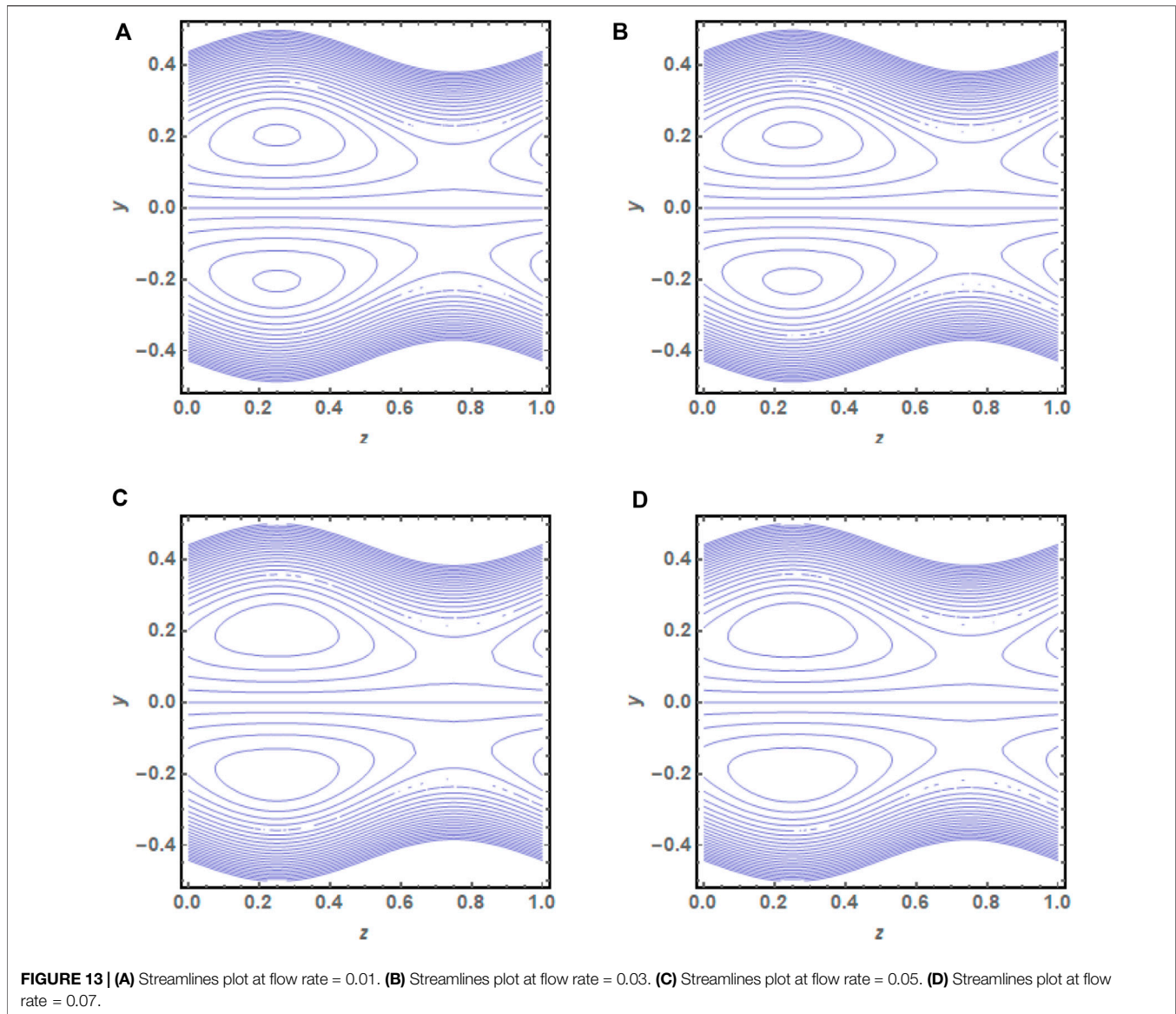




## DISCUSSION OF RESULTS

The graphical results that are incorporated in this section provide a comprehensive evaluation of the mathematical computations given in the exact solution segment. A thorough graphical evaluation is considered for velocity, temperature and various physical characteristics of peristalsis. Figures 3–5 unfold the effect of some important physical parameters on the velocity profile. Figure 3 (i.e., Figures 3A,B) provides the graphical outcome of velocity profile for increasing flow rate  $Q$ . Figure 3A reveals that velocity depicts an increasing behaviour for the escalating numerical values of parameter  $Q$ . Figure 3B shows the dependence of velocity on both the independent variables  $x$  and  $y$  and it is 3D-graphical plot of velocity for the escalating flow rate. An axial symmetry flow profile is noted here in this graph and maximum flow velocity is observed in the centre while it is diminishing towards duct walls. Figure 4 (i.e., Figures 4A,B) depicts the graphical result of velocity for the distinct escalating numerical values of wave number. Figure 4A unfolds that velocity shows an escalating behaviour for the distinct increasing numerical values of  $\beta$  in the centre of

elliptic duct while a converse behaviour is observed near walls. Figure 4B gives a 3D-graphical plot of velocity for distinct escalating values of  $\beta$ . Figure 5 (i.e., Figures 5A,B) gives the graphical assessment of velocity for the escalating numerical values of  $\alpha$ . Figure 5A discloses that velocity increases with the escalating numerical values of  $\alpha$  in the centre of duct while a converse behaviour near the walls is noted also for escalating numerical values of  $\alpha$ . This converse behaviour of velocity at the ciliated walls is due to increasing eccentricity of elliptical motion of cilia movement. Figure 5B discloses the 3D-graphical result of velocity for distinct escalating values of  $\alpha$ . All these graphical outcomes of velocity reveal an axially symmetry flow that is a fully developed flow and velocity is diminishing towards walls of duct. Figures 6–10 unfold the graphical outcomes of temperature profile for distinct parameters of physical importance. Figure 6 (i.e., Figures 6A,B) reveals the graphical assessment of temperature for distinct escalating numerical values of  $Q$ . Figure 6A unfolds that the temperature depicts an escalating behaviour for distinct incrementing numerical values of  $Q$ . Figure 6B depicts the 3D-graphical plot of temperature for different escalating



numerical values of  $Q$ . An axially symmetric behaviour is observed for temperature profile. **Figure 7** (i.e., **Figures 7A,B**) reveals the graphical result of temperature profile for various escalating numerical values of  $\psi$ . The parameter  $\psi$  is representing the concentration of carbon nanotubes in the base fluid. **Figure 7A** depicts a diminishing temperature profile with escalating concentration of carbon nanotubes in the base fluid (i.e., water). Since the increasing concentration of carbon nanotubes in the base fluid escalates the thermal conductivity of fluid and this eventually results in decline of temperature of base fluid. Further, it also verifies the inverse relation between the thermal conductivity of fluid and the temperature of fluid. **Figure 7B** is the 3D-graphical plot of temperature profile for escalating numerical values of  $\psi$ . **Figure 8** (i.e., **Figures 8A,B**) is plotted to represent the effect of  $\beta$  on temperature. **Figure 8A** discloses that the increment in the numerical value of wave

number results in the escalation of temperature. **Figure 8B** is the 3D-graphical plot of temperature for distinct escalating numerical values of  $\beta$ . **Figure 9** (i.e., **Figures 9A,9B**) is the graphical assessment of temperature profile for distinct escalating numerical values of  $B_r$ . **Figure 9A** unfolds that the temperature escalates rapidly with even a small increase in the numerical value of  $B_r$ . It reveals that the viscous effects are playing a vital role in the heat enhancement as compared to the molecular conduction. **Figure 9B** unfolds the 3D-graphical plot of temperature profile for escalating numerical values of  $B_r$ . This graph beautifully shows the dependence of temperature profile on the independent variables  $x$  and  $y$ . **Figure 10** (i.e., **Figures 10A,B**) is the graphical representation of temperature for escalating numerical values of  $\alpha$ . **Figure 10A** discloses an escalation in the temperature profile for distinct incrementing numerical values of  $\alpha$ . **Figure 10B** provides a 3D-graphical plot of

temperature for enhancing numerical values of  $\alpha$ . All these temperature graphs reveal an axial symmetry profile of temperature. Further, temperature gains maximum escalation in the centre of duct and drops to zero at the duct walls. **Figures 11A–D** provide a graphical assessment of  $\frac{dp}{dz}$  for different escalating numerical values of distinct parameters. **Figure 11A** reveals an escalation in the value of  $\frac{dp}{dz}$  for different enhancing numerical values of  $\delta$ . **Figure 11B** depicts an escalation in the value of  $\frac{dp}{dz}$  in the first half length of axial coordinate while a drop in the value of  $\frac{dp}{dz}$  is noted in the next half length of axial coordinate for escalating numerical values of  $\phi$ . Basically, the escalation is noted here for crest of peristaltic wave while the drop is noted for the trough. This drop in the pressure gradient for the trough of peristaltic wave eventually accelerates the flow in the axial direction. **Figure 11C** depicts a drop in the value of  $\frac{dp}{dz}$  for distinct accelerating numerical values of  $\psi$ . **Figure 11D** reveals that the value of  $\frac{dp}{dz}$  diminishes for the escalating numerical values of  $Q$ . **Figures 12A–C** provide the graphical results of  $\Delta P$  plotted against the dimensionless flow rate  $Q$ . **Figure 12A** unfolds an escalation in the value of  $\Delta P$  in the region  $\Delta P > 0$  while a converse behaviour is observed for the region  $\Delta P < 0$  with enhancing numerical values of  $\delta$ . **Figure 12B** reveals that  $\Delta P$  escalates in the region  $\Delta P > 0$  and drops in the region  $\Delta P < 0$  with enhancing numerical values of  $\phi$ . **Figure 12C** unfolds a decline in the value of  $\Delta P$  with escalating concentration of carbon nanotubes  $\psi$ . **Figures 13A–D** provide the graphical visualization of flow in the elliptic duct. These graphical results are obtained for distinct escalating numerical values of flow rate. The escalation in the trapping size can be clearly seen in these graphs for incrementing  $Q$ . Streamlines disclose the behaviour of flow regime inside this ciliated elliptic duct.

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## CONCLUSIONS

The peristaltic flow of carbon nanotubes in an elliptic duct with ciliated walls is mathematically investigated. A Cartesian coordinate system approach is utilized to interpret this mathematical study. The prime outcomes are given below.

- All the graphical outcomes of velocity reveal an axially symmetry flow that is a fully developed flow and velocity is diminishing towards walls of duct.
- The increasing concentration of carbon nanotubes in the base fluid escalates the thermal conductivity of fluid and this eventually results in decline of temperature of base fluid.
- The inverse relation between the thermal conductivity of fluid and the temperature of fluid is noted.
- All the temperature graphs reveal an axial symmetry profile of temperature. Further, temperature gains maximum escalation in the centre of duct and drops to zero at the duct walls.
- The escalation in the trapping size can be clearly seen in these graphs for incrementing  $Q$ .

## DATA AVAILABILITY STATEMENT

The raw data supporting the conclusions of this article will be made available by the authors, without undue reservation.

## AUTHOR CONTRIBUTIONS

SN and AS are group Heads and suggest the initial theme. SaA has done the mathematical and numerical part where as OM has done the drafting and proof reading.

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## NOMENCLATURE

$(\bar{U}, \bar{V}, \bar{W})$  Velocity components

$d$  Wave amplitude

$\bar{T}_w$  Duct's wall temperature

$D_h$  Hydraulic diameter of ellipse

$C_p$  Heat capacity

$\mu$  viscosity

$\phi$  Occlusion (amplitude to radius ratio)

$e$  Eccentricity of ellipse

$\alpha$  Eccentricity of elliptical motion of cilia

$B_r$  Brinkman number

$\psi$  Volume fraction of MWCNT (3%)

$nf$  Nanofluid

$(\bar{X}, \bar{Y}, \bar{Z})$  Cartesian coordinate system

$a_0, b_0$  Ellipse half axes ( $b_0 < a_0$ )

$\lambda$  wavelength

$c$  Velocity of propagation

$\bar{T}_b$  Bulk temperature

$k$  Thermal conductivity

$\rho$  Density

$\delta$  Aspect ratio

$\beta$  Wave number for metachronal wave

$t$  time

**MWCNT** Multi wall carbon nanotubes

$p$  pressure