



Simulations and Experiments Toward Continuous Wave 167 nm Laser Generation for ARPES With High Energy Resolution

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Continuous wave (CW) laser at a vacuum ultraviolet (VUV) range with the narrow-linewidth is an ideal optical source in angle-resolved photoemission spectroscopy (ARPES) for the research of superconductors with a narrow band gap. In this study, we present an eighth-harmonic-generation (EHG) laser scheme for CW laser generation at the VUV range, in particular at 167.75 nm, based on the cascaded power enhancement cavities. An intracavity second-harmonic generation (ICSHG) 671 nm laser with the narrow-linewidth and active frequency stabilization is built as the first stage, delivering the 2.55 W output power. A resonant cavity for fourth-harmonic-generation (FHG) constitutes the second stage, which generates the 335.5 nm laser with the output power of up to 1.25 W. The third stage is designed for the EHG of 167.75 nm based on the KBBF crystal. To realize the efficient CW laser generation at 167.75 nm, a theoretical analysis concerning the enhancement factor and the conversion efficiency of the KBBF-based EHG is carried out. The results show that it is possible for mW-level 167.75 nm generation if the transmittance of the KBBF prism-coupled device is increased to 97%. A 59 W circular intracavity power is observed in the 335.5 nm enhanced cavity experiments, corresponding to the peak power density of up to 20.86 MW/cm². This work paves a solid way for CW VUV laser generation with the narrow-linewidth, which would be an ideal tool for the extremely high resolution ARPES.

Keywords: vacuum ultraviolet, resonant enhancement, second-harmonic generation, narrow-linewidth, KBBF, ARPES

INTRODUCTION

Angle-resolved photoemission spectroscopy (ARPES) is the most direct and powerful method to study the electronic structure of materials and plays an important role in the fields of advanced materials including high temperature superconductors, topological materials, and quantum materials. The higher the photon energy of the drive sources is, the larger the Brillouin zone can be measured, which is preferred for the research of superconductors with a narrow band gap. With the traditional vacuum ultraviolet (VUV) pulsed lasers as the drive sources, the energy resolution of the ARPES is limited to meV and the space charge effect affects the reliability of the

obtained spectroscopy. The narrow-linewidth continuous wave (CW) VUV lasers can be utilized as an alternative drive source to improve the energy resolution to neV and eliminate the space charge effect [1–6]. The narrow-linewidth continuous wave lasers have also revolutionized the fields of precision metrology through atomic and molecular spectroscopy. The 167.079 nm narrow-linewidth CW laser corresponds to the transition from 1S_0 to 3P_0 of $^{27}\text{Al}^+$, used for achieving the Doppler cooling of the aluminum ions optical clocks [7]. So it is important to develop > 7 eV VUV narrow-linewidth CW laser sources.

There are several methods to generate VUV lasers such as free electron lasers, high harmonic generation and synchrotron radiation, and so on, which are all pulsed lasers and very expensive scientific facilities [8–10]. The excimer lasers are the most common deep ultraviolet lasers, which are key elements in the fields of lithography. However, they are mostly pulsed lasers with a single repetition frequency and have a poor beam quality, which brings inconvenience to the scientific application [11]. The VUV generation based on nonlinear frequency conversion has attracted great attention because of the good beam quality, high compactness, high robustness, and the flexible parameter adjustability [12]. Several reports have classified the ultraviolet nonlinear crystals through the generated photon energy limit and absorption edge, showing that the $\text{KBe}_2\text{BO}_3\text{F}_2$ (KBBF) crystal is the only transparent medium supporting the > 7 eV second-harmonic generation (SHG) [13]. A number of ultraviolet laser results based on the KBBF nonlinear crystal have been reported including femtosecond, picosecond to quasi-CW microsecond pulse durations generation, joule to microjoule pulse energies generation, 170–210 nm tuning wavelengths generation, which have also been used to drive the ARPES, photoemission electron microscopy, and revolutionized many frontier research studies [14–18]. In 2015, S. B. Dai et al. demonstrated a 65 μW 167.75 nm picosecond pulse laser generation based on the eighth-harmonic generation (EHG) of the 1,342 nm picosecond fundamental frequency laser [19]. In 2018, J. J. Li et al. present the 1.5 μJ 167.79 nm laser output with the linewidth of 0.025 pm, which was also generated from EHG of a 5 Hz 1,336 nm fundamental frequency quasi-CW laser [20].

When it comes to VUV narrow-linewidth CW laser generation, the conversion efficiency of the single-pass nonlinear process such as SHG and sum-frequency generation is extremely low as the focused power density hardly reaches MW/cm^2 . The resonant enhanced cavity is generally used to improve the SHG efficiency of the CW lasers. However, it is still difficult to generate VUV through cavity-enhanced SHG based on the KBBF nonlinear medium. There are three main obstacles: first, the loss of the ultraviolet resonant cavity is hard to control, which mainly comes from the un mature ultraviolet coating technology and the complex structure of the KBBF prism-coupled device (KBBF-PCD) [21]. The former limits the reflectivity and adds the transmission loss of the cavity mirrors. Every time passing through the KBBF-PCD, the laser beam suffers the Fresnel reflection loss, unpredictable scattering, and absorption losses due to the uneven optical-contact interface, making it difficult to enhance the fundamental laser. Second, the fundamental ultraviolet output power is also much lower than the

common visible and near-infrared wavelength and there are few commercial products. Third, cascading resonant cavities with the Pound–Drever–Hall (PDH) techniques make it challenging to keep the compactness and long-term operation [22]. In 2012, M. Scholz et al. reported a 1.3 mW 191 nm VUV laser generated from the fourth-harmonic generation (FHG) of a commercial 764 nm semiconductor laser with the power of 1.6 W and the line width of 50 kHz [23]. In 2013, they utilized 3 W 772 nm semiconductor lasers as the fundamental source and generated the 193 nm CW VUV laser with the stable output power of 4 mW [24].

In this report, we present the theoretical and experimental results ready for the 167.75 nm VUV CW laser generation. A narrow-linewidth Nd: YVO_4 single-frequency CW laser based on the intracavity second-harmonic generation (ICSHG) is utilized as the fundamental source with the output power of 2.55 W at 671 nm. The active frequency stabilization is built to suppress the frequency jitter. The second cavity-enhanced FHG stage is based on a BBO crystal, delivering a 1.25 W 335.5 nm laser. The third SHG stage is designed to employ the KBBF crystal. A theoretical analysis is carried out, showing that the prerequisite of the mW-level 167.75 nm VUV CW laser generation is the transmittance of the KBBF-PCD increased to more than 97%. A 59 W circular intracavity power of the 335.5 nm is experimentally observed in the resonant EHG cavity, laying a good foundation for the 167.75 nm VUV CW laser generation.

LASER SYSTEMS FOR 335.5 NM GENERATION

A high power all-solid-state single-frequency CW laser with the active frequency stabilization system is used as the fundamental source, as shown in **Figure 1**. An 880 nm laser diode is used to pump the Nd: YVO_4 gain medium, and a TGG device is inserted to keep the direction of optical beam. An LBO nonlinear crystal is placed between the concave mirrors to convert the 1,342 nm radiation to the 671 nm laser, synchronously choosing the resonant wavelength and maintaining the single-frequency operation [25]. The output power of the 671 nm laser is 2.55 W with a peak-to-peak variation of 0.69%, as shown in **Figure 2A**. The M^2 factor is measured to be 1.14 in the x direction and 1.09 in the y direction respectively, exhibiting a good beam quality.

To further suppress the short-term and long-term frequency drift, an active frequency stabilization system based on the Pound–Drever–Hall (PDH) method is built as shown in **Figure 1**. A 10 cm-long Fabry–Perot cavity made of indium steel material is chosen as the reference for the pre-stabilization stage. The leakage of the 1,342 nm single-frequency laser, the line width of which is measured to be 115 kHz, is led to the Fabry–Perot cavity after frequency was modulated using an electro-optic modulator (EOM). A photodetector is placed at the end of the Fabry–Perot cavity to get the transmitted signal, which is then demodulated in the phase detector and processed using a PID controller. The control

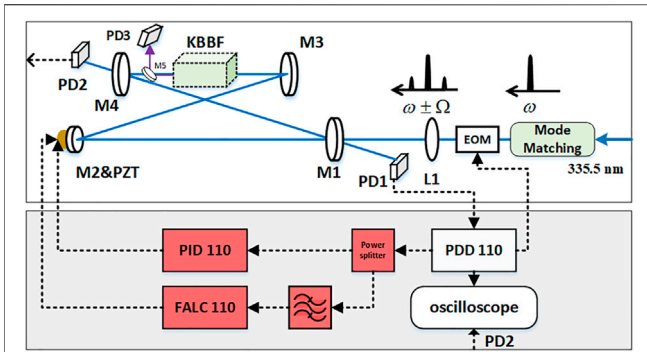


FIGURE 3 | Experimental setup of the resonant cavity based on the KBBF crystal. M1–M5: cavity mirror, PD: Photodetector, PZT: Piezo electric transducer, EOM: electronic-optical modulator.

$$h = \frac{\pi^2}{\xi_x} \exp(\mu a l) \left[\frac{2}{\sqrt{\pi}} e \int_{-\infty}^{\infty} \exp(-4s^2) |H|^2 ds \right]. \quad (3)$$

According to Ref. [28], where $\xi_x = \frac{l}{b_x} = \frac{l}{k_1 \omega_x^2}$ is the focusing parameter and

$$H = \frac{1}{2\pi} \int_{-\xi_x(1-\mu)}^{\xi_x(1+\mu)} \frac{\exp(-\kappa \tau'_x) \exp(i\sigma' \tau'_x)}{(1 + i\tau'_x)^{\frac{1}{2}} [1 + i(e^2 \tau'_x + \Delta)]^{\frac{1}{2}}} d\tau'_x. \quad (4)$$

The focus position is $\mu = \frac{l-2f_x}{l}$, and the astigmatic distance beam waists are $\Delta = \frac{2(f_x - f_y)}{k_1 \omega_y^2}$. The ellipticity of the Gaussian beam is $e = \frac{\omega_x}{\omega_y}$, and the phase mismatch is $\sigma' = 1/2 k_1 \omega_y^2 \Delta k + 4sp\omega_x k_1/2$. $\kappa = 1/2(\alpha^2 - 1/2\alpha^2)k_1 \omega_x^2$.

Since the nonlinear efficiency of a type-I phase-matched crystal is low and the fundamental power of a CW laser is not comparable with high-peak-power narrow-duration pulsed lasers, the output power of the single-pass nonlinear process is usually at less than μW -level. A bow-tie resonant cavity is designed to enhance the fundamental power and improve the SHG conversion efficiency, as shown in **Figure 3**. Mirror M1 and M2 are plane. The former is the input coupler with the reflectivity of r_1 and the transmission of t_1 corresponding to the fundamental frequency, and the latter is mounted on two PZTs to stabilize the cavity length to the resonant wavelength. The mirror M3 and M4 are concave and the nonlinear crystal is placed at the focus between them. The reflectivity of the mirror M2–M4 is assumed as r_2 , r_3 , and r_4 . The mirror M4 is usually chosen as the output coupler of the second harmonic, but for the $> 7 \text{ eV}$ VUV lasers present coating technology can hardly maintain the high reflectivity of the fundamental frequency and high transmission of the second harmonic synchronously. As a result, a reflective output coupler is inserted with high transmission of fundamental laser and high reflection for the harmonic generation with a transmission of t_5 . The KBBF-PCD is the nonlinear medium as mentioned before with a transmission of t_{PCD} .

When the fundamental laser is coupled into the cavity and circling around, the main losses it suffered are the transmission

TABLE 1 | Parameters related to the KBBF crystal.

Crystal length	1 mm
Phase-matching angle (335.5–167.75 nm)	73.2°
n_1 (335.5 nm in the KBBF)	1.5007
n_2 (167.75 nm in the KBBF)	1.4993
d_{eff} (335.5 nm in the KBBF)	0.14 pm/V
α_1	0.1 cm^{-1}
α_2	10 cm^{-1}
Walk-off angle	38.83 mrad

and scattering loss of cavity mirrors r_i , the transmission loss of the KBBF-PCD ($1-t_{PCD}$), and the nonlinear conversion loss ($1-t_{SHG}$). Therefore, the equivalent reflectivity of resonator cavity can be expressed as $r = r_2 r_3 r_4 t_5 \cdot t_{PCD} \cdot t_{SHG}$, and $t_{SHG} = 1 - E_{SHG} \cdot P_c$. As the resonant cavity enters a steady state, the incident fundamental power P_1 , the reflected power of the input coupler P_r , and the total circulating power P_c in the cavity have the following relationship

$$\frac{P_r}{P_1} = \frac{(\sqrt{r_1} - \sqrt{r})^2}{(1 - \sqrt{r_1 r})^2}, \quad (5)$$

$$\frac{P_c}{P_1} = \frac{t_1}{[1 - \sqrt{r_1 r}]^2} = \frac{t_1}{[1 - \sqrt{r_1 \cdot r_2 r_3 r_4 t_5 \cdot t_{PCD} \cdot (1 - E_{nl} \cdot P_c)}]^2}, \quad (6)$$

when the reflectivity of the input coupler is consistent with the equivalent reflectivity of the cavity, $r_1 = r$, the impedance matching is fulfilled, which means the most efficient input coupling of the fundamental laser.

Simulation Results

The cavity is designed as shown in **Figure 3**. The reflectivity of the cavity mirrors M2–M4 is designed as $r_2 = r_3 = r_4 > 99.8\%$ at 335.5 nm, which is the highest reflectivity present coating technology can get. The output coupler M5 is designed as $t_5 > 99.5\%$ at 335.5 nm and $r_5 > 94\%$ at 167.75 nm. The parameters related to the KBBF device are listed in **Table 1**. The conversion efficiency is E_{SHG} calculated to be $1.41 \times 10^{-6}/\text{W}$.

Assuming that the mirrors are ideal and the input beam of the fundamental laser is circular and optimal mode matching, the input power of the fundamental laser is about 1.1 W. According to **Eqs 1–6**, simulations of the resonant cavity is carried out and the results are shown in **Figure 4**.

First, when the transmittance of the KBBF device is determined, the intracavity circulating power varies with the reflectivity of the input coupler and there is an optimum corresponding to the impedance matching state. For instance, when $t_{PCD} = 99\%$, the impedance matching appears at $r_1 = 97.9\%$. In this condition, the intracavity power P_c of the fundamental 335.5 nm laser is 52.58 W and the generated harmonic 167.75 nm is 3.89 mW theoretically, the nonlinear efficiency of which is only 0.35%.

Second, as the transmittance of the KBBF-PCD decreases from 99% to 97%, the optimal intracavity circulating power also decreases significantly from 52.58 W to 25.06 W and the impedance matching reflectance of the input coupler drops from 97.9% to 95.9%. The theoretically generated harmonic laser drops from 3.89 mW to 1.03 mW and the nonlinear

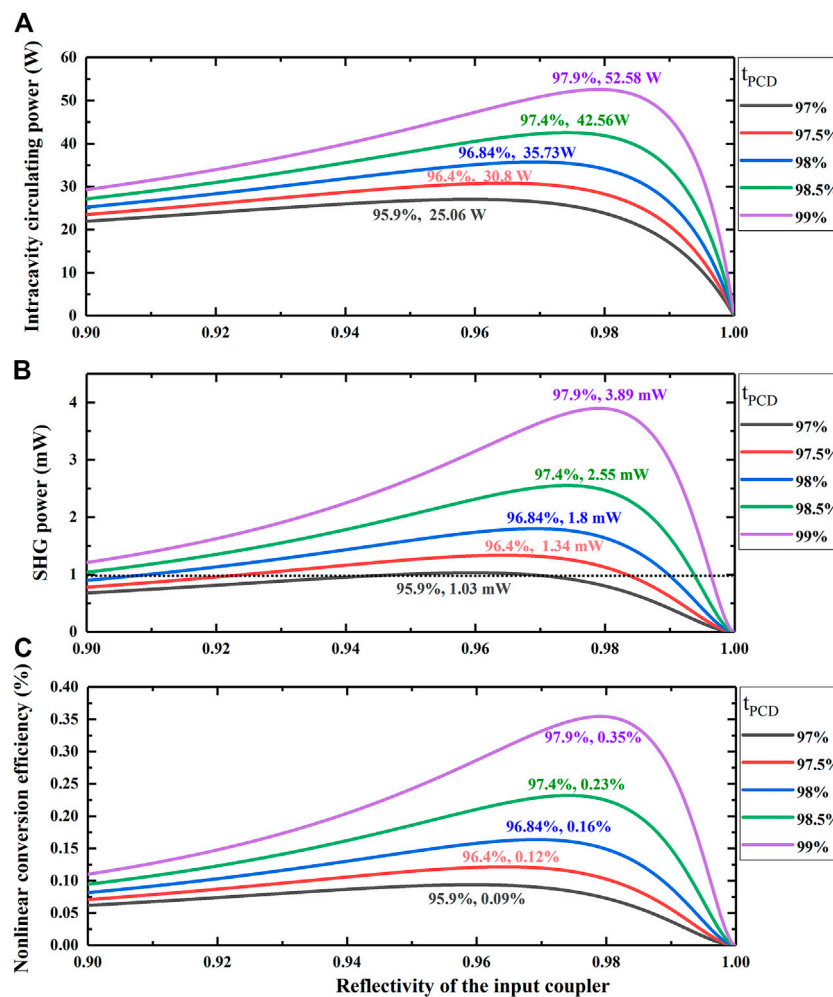


FIGURE 4 | (A) Intracavity circular power, **(B)** second-harmonic generation output power, and **(C)** nonlinear conversion efficiency versus input coupler.

conversion efficiency reduces from 0.35% to less than 0.09%, indicating that the transmittance of the KBBF-PCD is the key factor for the generation of the 167.75 nm harmonic laser. As the KBBF crystal is difficult to grow in the z-direction and cannot be cut along the phase-matching angle, a PCD structure was invented by C. T. Chen et al. to fix the crystal between prisms. The inhomogeneous optical contact introduces scattering loss at the interfaces of the KBBF medium and prisms. The large phase-matched angle 73.2° makes the Fresnel reflection loss larger than 12%. These technical problems make it very challenging to control the transmission loss of 335.5 nm fundamental laser passing through a phase-matched KBBF-PCD less than 3%, which is predicted as the prerequisite for the generation of mW-level of the 167.75 nm VUV CW single-frequency laser.

Experimental Results

A bow-tie resonant EHG cavity is built according to the previous calculations and designs as shown in **Figure 3**. Since the VUV laser is absorbed seriously by the oxygen in the air, the whole cavity is built in a large vacuum chamber.

The distance S1 between plane mirror M1 and M2 is about 120 mm, and the beam waist between the plane mirror M1 and M2 is calculated to be $185 \mu\text{m}$. The radius of the concave mirrors is 100 mm and the distance between them is adjusted to be 115 mm. The total length of the cavity is 493 mm. The reflectivity of the input coupler is designed to be 97%, and the others are 99.8% reflective. In order to efficiently couple the fundamental laser into the EHG resonant cavity, mode matching of the fundamental laser with the resonant mode is of great importance. As a result, after changing different groups of lenses, we chose a lens with the focal length of 1-m to shape the fundamental laser to $173 \times 207 \mu\text{m}^2$, which is the optimal mode-matching conditions as the walk-off effect leading to an elliptical beam spot.

In order to achieve the PDH stabilization, two PZTs with the displacement of $2 \mu\text{m}$ and $10 \mu\text{m}$ were used for the fast-loop and slow-loop stabilization respectively. The size of the plane mirror M2 is $\phi 6 \times 2 \text{ mm}^2$ to reduce the load of the PZTs. A photodetector PD1 is placed behind the input coupler M1 to detect the reflective signal. Another photodetector PD2 is placed

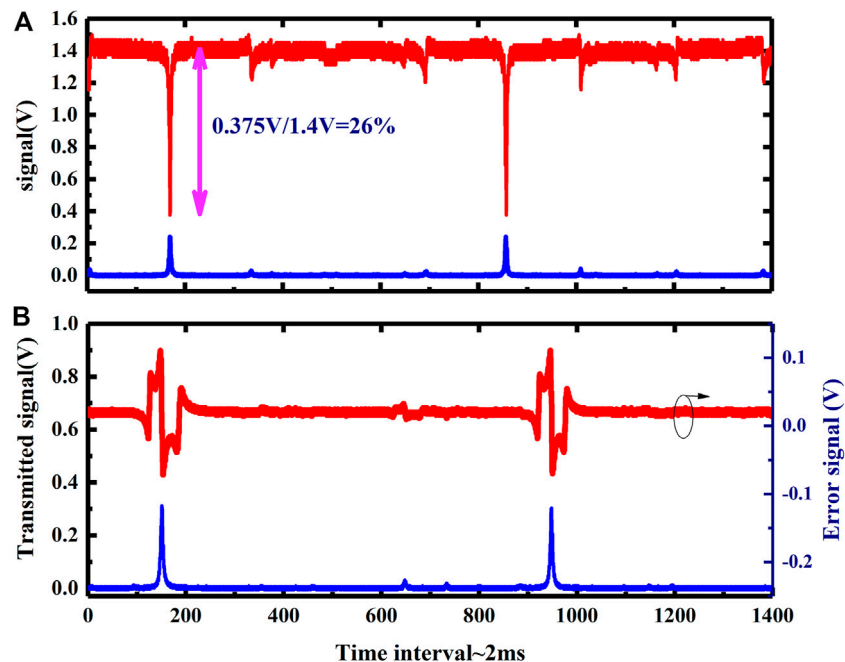


FIGURE 5 | (A) Reflection peaks (red) and transmission peaks (blue) of the 335.5 nm resonant cavity; **(B)** error signals (red).

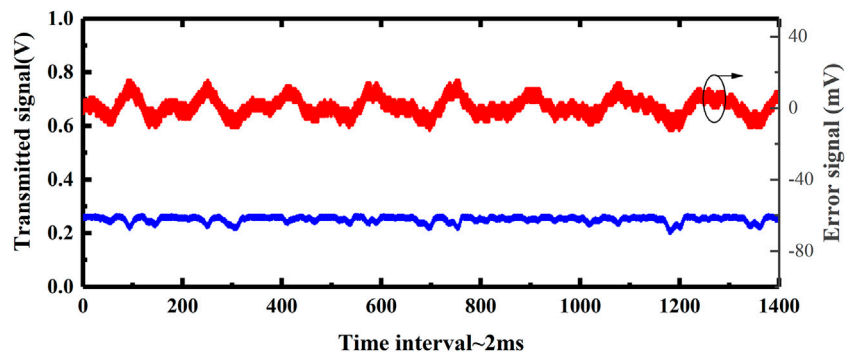


FIGURE 6 | Transmitted signal (blue) and error signal (red) of the PDH locked resonant cavity.

behind the concave mirror to detect the leakage. The locking electronics are from Toptica electronics.

The laser is first phase modulated using an EOM with the modulation frequency of 20 MHz, the detected reflected signal and transmitted signal are shown in **Figure 5A**. The positions of the focusing lens and the cavity mirrors are carefully adjusted according to the detected signals to suppress the high-order modes and improve the amplitude of the circulating power. The reflected signal is optimized as shown in **Figure 5A**, about 26% power was reflected at the resonant position, which is attributed to the mode mismatching and the impedance mismatching.

The reflected signal is then demodulated by the phase detector and the error signal is shown in **Figure 5B**. Two PID modules also from Toptica electronics are used to stabilize the cavity to the

resonant wavelength. Once the locking state is activated, the error signal becomes zero and the transmitted signal stays at the high level, as shown in **Figure 6**. The leakage power of the concave mirror with a transmittance of 0.206% is measured to be 121 mW, and the circulating intracavity power is inferred to be 59 W. According to **Eq. 6**, under certain conditions the reflectivity of the input coupling is 97%, then the enhanced factor would be 90. The difference is attributed to the imperfect mode mismatching and the other scattering losses.

CONCLUSION

We have demonstrated the generation of the 335.5 nm laser with a high-peak-power density ready for the generation of the

narrow-linewidth 167.75 nm VUV single-frequency CW laser, based on a home-built resonant cavity. The cascading resonant harmonic generation systems are designed, delivering the 671 nm single-frequency CW laser with the output power of the 2.55 W and the 335.5 nm single-frequency of 1.25 W. The EHG resonant cavity is preliminarily verified with the circulating power of 59 W and the peak power density of 20.86 MW/cm². A theoretical analysis is carried out, indicating that improving the transmittance of the KBBF-PCD to larger than 97% is the prerequisite for the mW-level generation of the 167.75 nm VUV narrow-line width single-frequency CW laser.

DATA AVAILABILITY STATEMENT

The raw data supporting the conclusion of this article will be made available by the authors, without undue reservation.

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AUTHOR CONTRIBUTIONS

GL and XZ contributed to the ARPES application requirements. ZZ, HH and ZW contributed to the design and experimental schemes. ZZ and HH performed the experiments and are responsible for the data processing. ZZ, GZ, HH, and ZW contributed to write and edit the manuscript.

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