



# New Antenna for Detecting Polarization States of Terahertz

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The polarization measurement of terahertz (THz) waves is indispensable in THz time-domain spectroscopy (THz-TDS) applications to detect material properties. The rapid development of accurate THz wave polarization-sensitive detectors will greatly promote THz-TDS applications. A new type of photoconductive antenna array detector is proposed in this paper. The antenna is composed of two vertical  $1 \times 2$  arrays, which respectively detect the orthogonal component of the terahertz pulse in any direction, while quickly and accurately detecting the polarized THz waves. Rotating the detector to measure the THz electric field at different angles shows the reliability of the detector for THz wave polarization measurement. Its polarization detection accuracy is  $0.2^\circ$ . At the same time, we use the response matrix to analyze the symmetry of the antenna array.

**Keywords:** terahertz wave, antenna array, synthesis, polarization, response matrix

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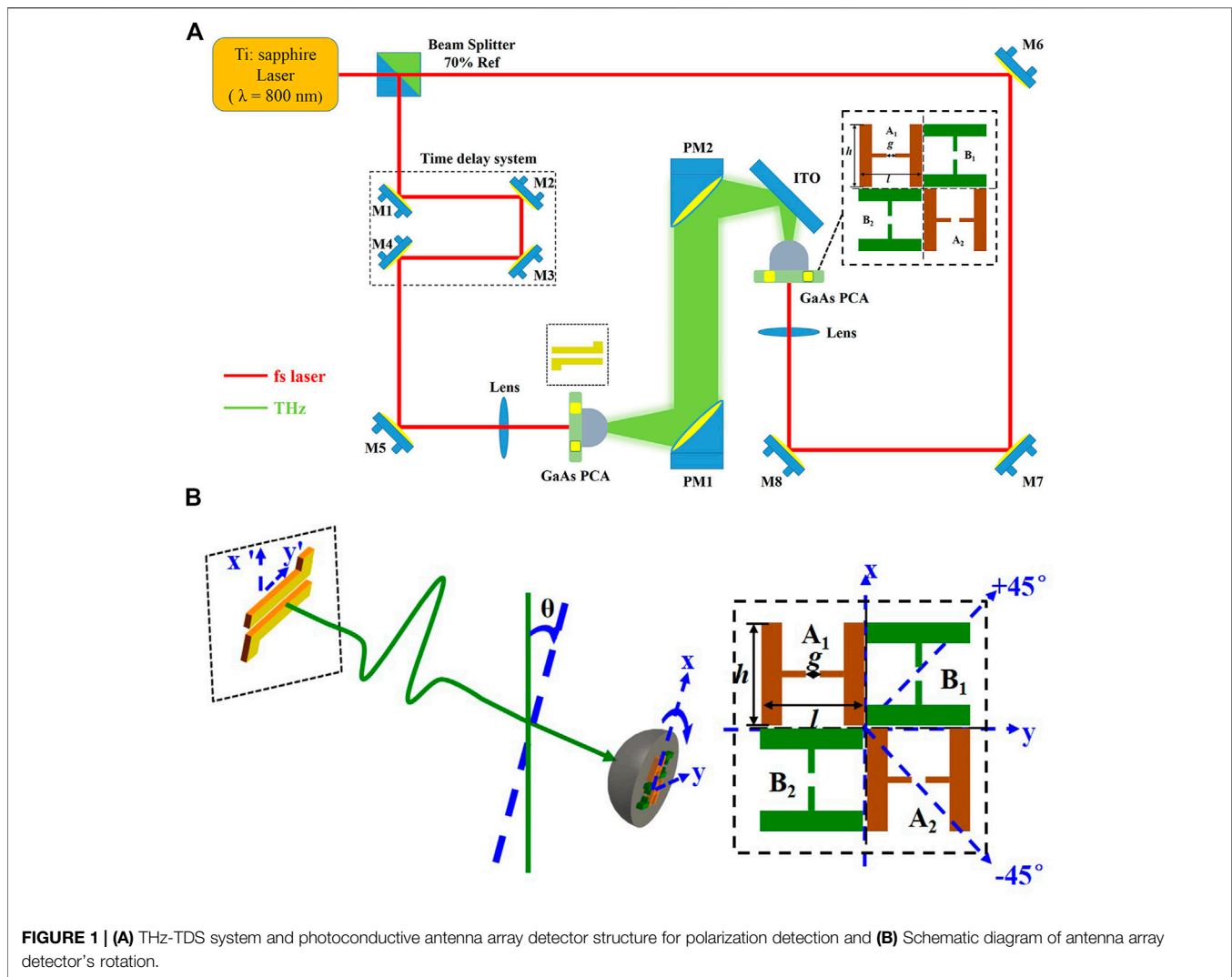
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## INTRODUCTION

The THz time-domain spectroscopy (THz-TDS) system can be used to detect the spectral characteristics of materials in the range of hundreds of GHz to several THz, and has been widely used in material science [1], chemistry [2], biomolecules [3–5], nerve cells [6], security inspection [7], and other fields. Usually, we use the THz-TDS system to obtain two crucial information about samples: refractive index and absorption coefficient [8]. However, for chiral materials such as birefringent or optically active materials, the polarization measurement of the THz electric field is crucial for the accurate acquisition of the characteristic parameters of the sample. Therefore, a detector capable of simultaneously measuring the polarization state of the THz electric field and the spectral information of the sample is necessary. Since Auston proposed photoconductive dipole antennas [9], dipole antennas have been rapidly developed as THz transmitters and receivers in THz-TDS systems. In the polarization measurement of THz waves using dipole antennas, the photoconductive dipole antennas can only detect the THz electric field amplitude in one direction at a time, that is, the projection of THz electric field amplitude on the direction of dipole antenna electrodes. In fact, the polarization direction of the THz electric field is determined by the direction of the electrostatic field of the transmitting antenna. Similarly, the direction of the antenna electrode also determines the magnitude of the photocurrent caused by polarized THz electric field received by the detection antenna. Among many photoconductive antenna detectors, the geometric structure of the three-contact electrode [10] and the four-contact electrode [11] have proved their ability to detect the polarization direction of THz electric field, however, its effective area for receiving the THz wave is exceedingly small and cannot be expanded. The photoconductive antenna array detector of the interdigital electrode [12] can expand the effective area while measuring the polarization of the THz electric field; however, it still has the shortcoming of the traditional interdigital antenna array: the reverse current between adjacent antenna elements [13]. Therefore, the photoconductive antenna detector used for the THz electric



field polarization measurement still needs to be improved in terms of the effective area, sensitivity, and detection efficiency.

In this paper, a THz polarization detector based on the photoconductive antenna array is designed to eliminate the reverse current between adjacent antenna elements and improve polarization detection sensitivity. By measuring the quadrature components of THz electric field by the detector at different angles, the dependence of the response matrix factor on the frequency is obtained, and the symmetry of the antenna array is analyzed. In addition, the effective area of the detector to receive THz waves is expandable, which is beneficial to improve the detector's performance.

## POLARIZATION DETECTION

There have been many reports on the principle description of the photoconductive antenna for detecting THz waves [14, 15], and the preparation method of the photoconductive antenna designed in this paper has been reported [16], therefore, this part will not be

described here. The THz-TDS system used in the experiments is shown in **Figure 1A**. The laser used in the experiment has a wavelength of 800 nm, a pulse width of 104 fs, and a repetition frequency of 80 MHz. A dipole emitting antenna with a gap of 150  $\mu\text{m}$  is used, a bias voltage of 240 V is applied, and the electrode gap is vertical. The photoconductive antenna array detector designed in this paper is a four-antenna centrally symmetric layout, which is shown in the inset of **Figure 1A**. The adjacent antennas are arranged orthogonally to form a dual signal channel to obtain the orthogonal components of the THz electric field in any direction. The electrode directions of A<sub>1</sub> and A<sub>2</sub> are the same, so are B<sub>1</sub> and B<sub>2</sub>. The A<sub>1</sub>A<sub>2</sub> and B<sub>1</sub>B<sub>2</sub> electrode directions are perpendicular to each other to form a dual signal channel. The photoconductive antenna element gap  $g = 50$   $\mu\text{m}$ , and  $h = l = 990$   $\mu\text{m}$ . The effective area of each antenna element receiving THz wave is 30  $\mu\text{m} \times 50$   $\mu\text{m}$ . The detector is integrated into a silicon lens with a diameter of 1 cm and fixed in a rotation stage, as shown in **Figure 1B**. In this paper, it is specified as follows: the coordinate system of the photoconductive antenna array detector is  $x - y$ ; the emitting antenna coordinate system is  $x' - y'$ , the direction of the electrostatic field of the emitting antenna is along the

$x'$  axis, and the two electrodes are in  $y'$  axis, the rotation axis of the photoconductive antenna array detector overlaps with the propagation direction of the THz wave.

The response of the photoconductive antenna array detector to the orthogonal components of the THz electric field can be described by the response matrix [17],

$$\begin{pmatrix} \mathbf{S}_{A_1A_2}(\omega) \\ \mathbf{S}_{B_1B_2}(\omega) \end{pmatrix} = \mathbf{M}(\omega) \begin{pmatrix} \mathbf{E}_{x'}(\omega) \\ \mathbf{E}_{y'}(\omega) \end{pmatrix}$$

where  $\omega$  is the frequency of electromagnetic waves in the THz band,  $E_{x'}(\omega)$  and  $E_{y'}(\omega)$  represent the spectral signal components of the incident THz electric field in the  $x'$  and  $y'$  directions, respectively.  $S_{A_1A_2}(\omega)$  and  $S_{B_1B_2}(\omega)$  are the signals after the Fourier transformation of the time-domain signals  $S_{A_1A_2}(\tau)$  and  $S_{B_1B_2}(\tau)$  that the photoconductive antenna array detector responds to.  $M(\omega)$  is the response matrix of the photoconductive antenna array detector. The  $M(\omega)$  can be described as:

$$\mathbf{M}(\omega) = \begin{pmatrix} \mathbf{m}_1 & \mathbf{0} \\ \mathbf{0} & \mathbf{m}_2 \end{pmatrix}$$

Since the long axis and short axis of the THz electric field in the optical path system are constants, the orthogonal projection component of the long axis (short axis) on the photoconductive antenna array detector changes linearly, so the elements of one set of diagonal response matrices are zero. When the photoconductive antenna array detector rotates,

$$\begin{pmatrix} \mathbf{S}_{A_1A_2,\theta}(\omega) \\ \mathbf{S}_{B_1B_2,\theta}(\omega) \end{pmatrix} = \begin{pmatrix} \mathbf{m}_1 & \mathbf{0} \\ \mathbf{0} & \mathbf{m}_2 \end{pmatrix} \begin{pmatrix} \cos \theta & \sin \theta \\ -\sin \theta & \cos \theta \end{pmatrix} \begin{pmatrix} \mathbf{E}_{0x}(\omega) \\ \mathbf{E}_{0y}(\omega) \end{pmatrix}$$

where  $\theta$  is the angle between the  $x'$ -axis (or  $y'$ -axis) and the  $x$ -axis (or  $y$ -axis).  $A_1A_2$  is initially placed vertically ( $\theta = 0^\circ$ ), and  $E_{0x}$  and  $E_{0y}$  are the initial electric field components with constant values. For the convenience of discussion, the dependence on frequency  $\omega$  is omitted. According to the detection data of the photoconductive antenna array detector at  $\theta = \pm 45^\circ$ , the response matrix can be calculated as:

$$\mathbf{M} = \frac{\mathbf{1}}{\sqrt{2}E_{0x}} \begin{pmatrix} \mathbf{S}_{A_1A_2,45} + \mathbf{S}_{A_1A_2,-45} & \mathbf{0} \\ \mathbf{0} & \mathbf{S}_{B_1B_2,-45} - \mathbf{S}_{B_1B_2,45} \end{pmatrix}$$

in which,

$$\begin{aligned} \mathbf{S}_{A_1A_2,\theta} &= \mathbf{S}_{A_1,\theta} + \mathbf{S}_{A_2,\theta} \\ \mathbf{S}_{B_1B_2,\theta} &= \mathbf{S}_{B_1,\theta} + \mathbf{S}_{B_2,\theta} \end{aligned}$$

At the same time, the angle of the polarization direction of the THz electric field can be calculated:

$$\tan(\theta) = \frac{E_y}{E_x} = \frac{E_y/E_{0x}}{E_x/E_{0x}}$$

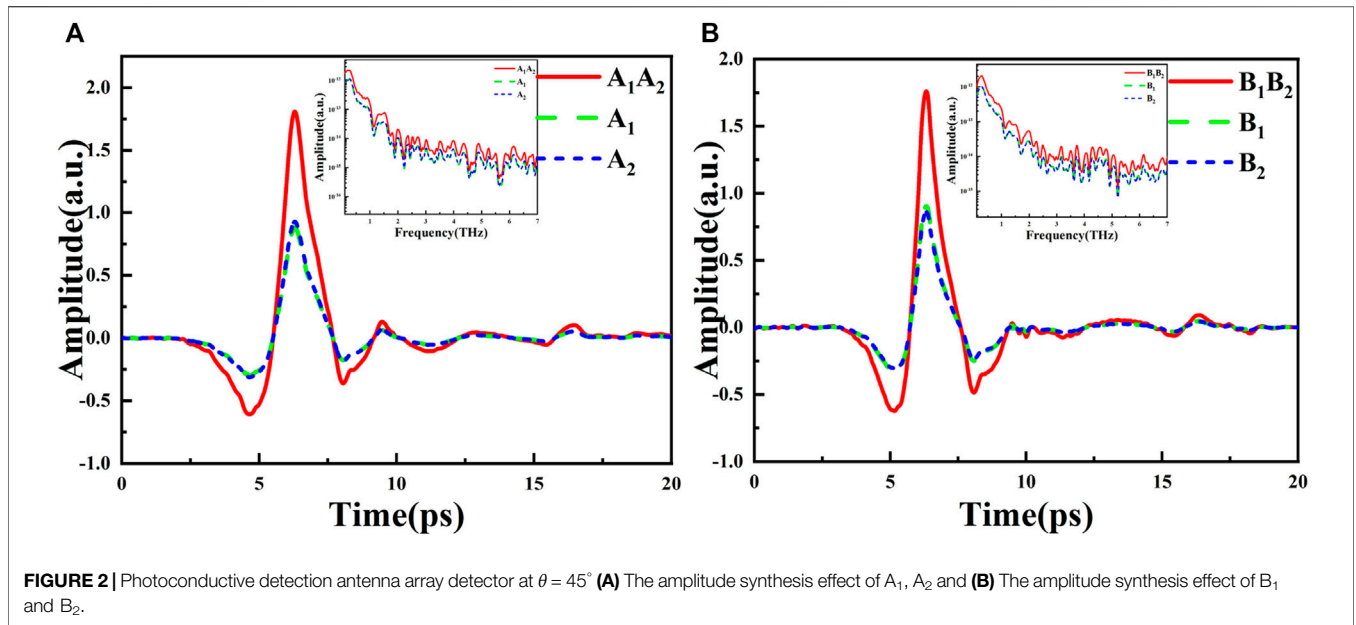
## EXPERIMENTAL RESULTS AND ANALYSIS

Before polarization measurement, we need to make sure that there is no reverse current between adjacent antenna elements,

because the interference of reverse current will reduce the signal-to-noise ratio and measurement accuracy of polarization detection. According to the layout characteristics of the photoconductive antenna array detector, the experiments have tested the synthesis efficiency of the  $A_1A_2$  and  $B_1B_2$ , as shown in **Figure 2A,B**. Taking  $A_1A_2$  as an example, the algebra sum of the peak-to-peak amplitude of the THz signal received by them is used as the peak-to-peak amplitude of the reference signal, and the synthesis efficiency can be calculated according to the amplitude of the actual output signal of the array  $A_1A_2$  and  $B_1B_2$ . The experimental results show that the synthesis efficiency of the array  $A_1A_2$  is 98.1%, and that of  $B_1B_2$  is 99.9%. In addition, the largest difference in signal amplitudes appears between  $A_1$  and  $B_2$ , and the amplitude difference is only 2.98%, which shows that the THz and laser energy received by each antenna element gap can be considered to be the same. The signal amplitude data of the antenna elements and the array are shown in **Table 1**.

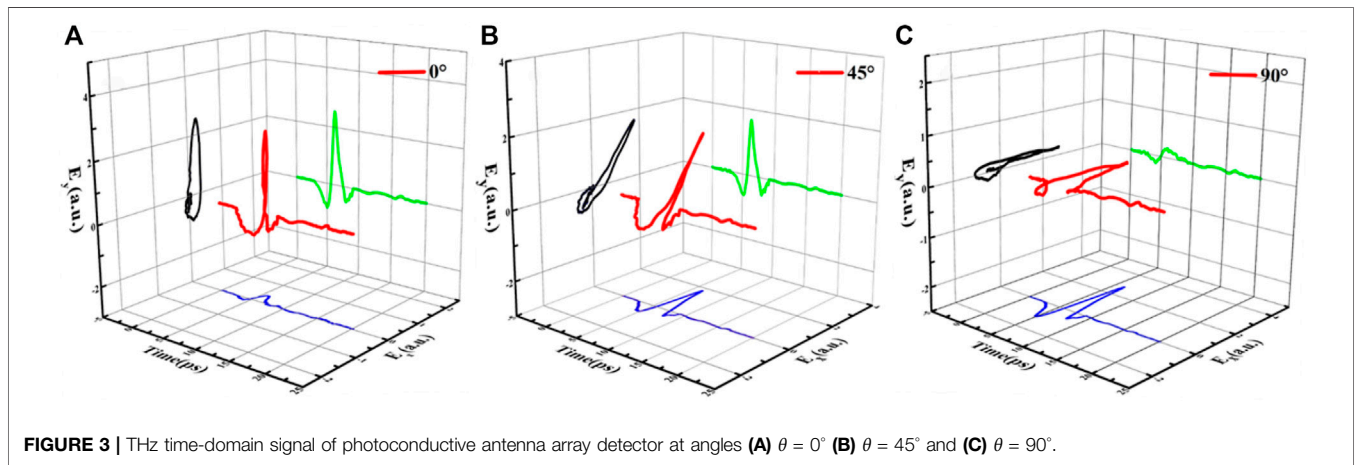
In order to preliminarily verify the expected operation of the detector, three cases of orthogonal polarizations were tested. Firstly,  $\theta = 0^\circ$ ,  $A_1$  and  $A_2$  detect the horizontally polarized THz electric field,  $B_1$  and  $B_2$  detect the vertically polarized THz electric field. Secondly,  $\theta = 45^\circ$ ,  $A_1$ ,  $A_2$ , and  $B_1$ ,  $B_2$  detect the same magnitude projection components of the THz electric field in the  $x$  and  $y$  directions, respectively. Thirdly,  $\theta = 90^\circ$ ,  $B_1$  and  $B_2$  detect the horizontally polarized THz electric field,  $A_1$  and  $A_2$  detect the vertically polarized THz electric field. The polarization-resolved time-domain trace are shown in **Figure 3A–C**. By rotating the detector, the antennas array detected the polarization state of the THz electric field as expected. The THz electric field in the figures show a certain degree of elliptical polarization. The reasons for this phenomenon can be explained as follows: firstly, the dipole photoconductive antenna emitter will generate a small quadrupole field; secondly, the low-f acquisition system make the linear polarization amplitude slightly elliptical [18, 19]; finally, the frequency-dependent cross polarization of the dipole radiation field [20].

The polarization state of the THz pulse is constant during the rotation of the photoconductive antenna array detector. By rotating the photoconductive antenna array detector in the range of  $360^\circ$ , the peak-to-peak amplitude of the time-domain signal of antennas  $A_1$ ,  $A_2$ , and  $B_1$ ,  $B_2$  distributed in the polar coordinates is shown in **Figure 4A,B**. Angle change step size is  $10^\circ$ , and the red curve is the sine curve fitted to the scatter diagram. The distribution law of the scattered points is consistent with the fitted curve and has good symmetry. The peak-to-peak amplitude of the signals at all angles have been taken as a positive value, the amplitude peak-to-peak value of  $A_1A_2$  and  $B_1B_2$  varies with angle are in accordance with Malus's Law. The signal amplitudes of the antennas in groups  $A_1$  and  $A_2$  are not zero at  $0^\circ$  and  $180^\circ$ , so are  $B_1$  and  $B_2$  at  $90^\circ$  and  $270^\circ$ , indicating that the THz pulse does have a certain degree of elliptic polarization. Since the total energy of the radiated THz pulse is constant and the amplitude of the THz electric field can be expressed as  $E = \sqrt{E_x^2 + E_y^2}$ , the magnitude of the THz electric field can be calculated, as shown in **Figure 4C**, where the red curve is the fitted curve. A good matching relationship between the measured



**TABLE 1** | Signal amplitudes of photoconductive antenna elements and arrays.

	Unit $A_1$	Unit $A_2$	Unit $B_1$	Unit $B_2$	Array $A_1A_2$	Array $B_1B_2$
Amplitude (A)	$1.20 \times 10^{-11}$	$1.21 \times 10^{-11}$	$1.23 \times 10^{-11}$	$1.24 \times 10^{-11}$	$2.37 \times 10^{-11}$	$2.47 \times 10^{-11}$



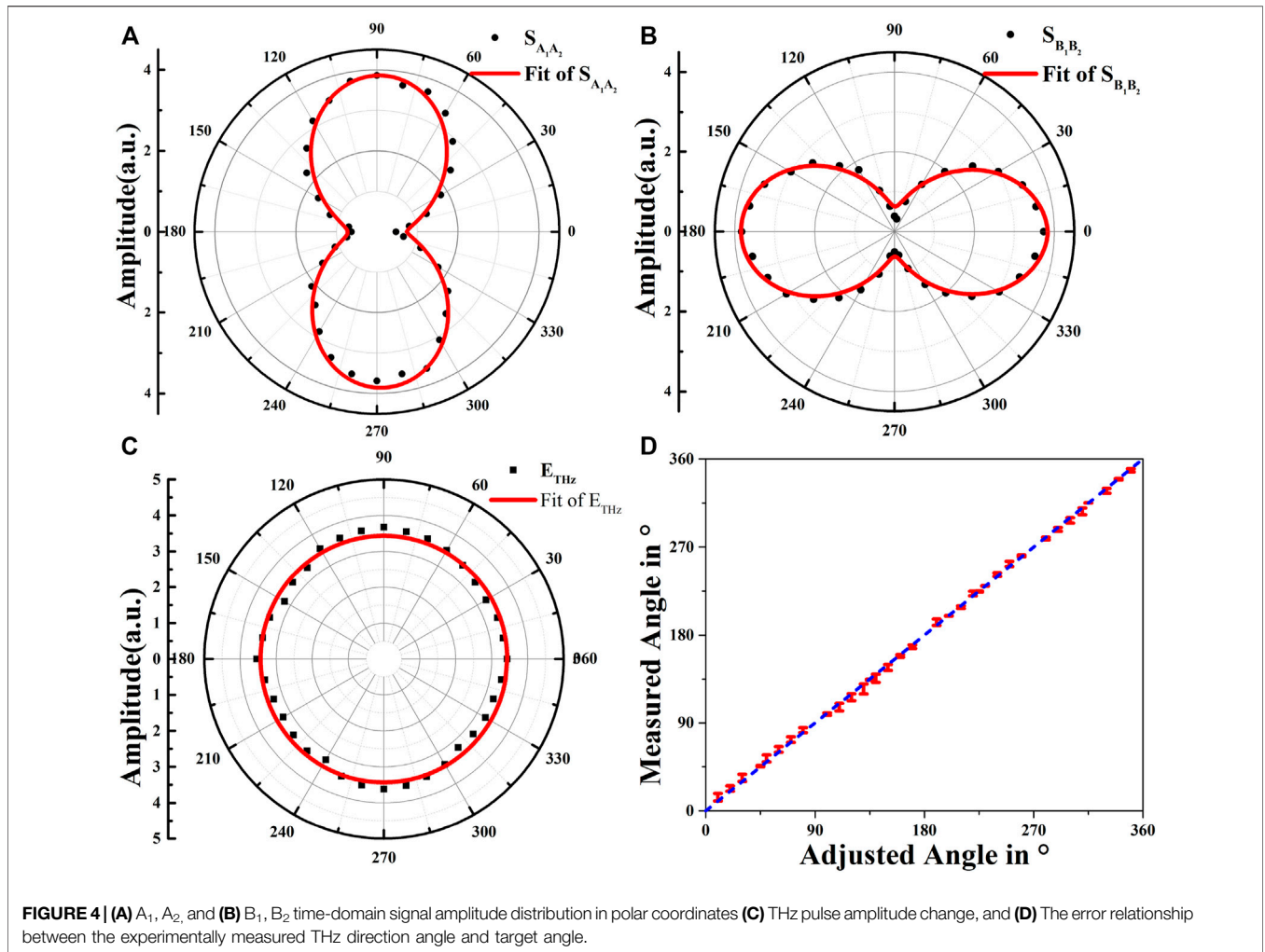
data points and the fitted curve can be observed. **Figure 4D** shows the error relationship between the experimentally measured direction angle of the THz pulse and the target angle. The measured angle is close to the target angle within the measurement range. The blue dashed line is the ideal relationship between the measured angle and the target angle, revealing the reliability of the photoconductive antenna array detector in measuring the polarization angle of the THz pulse.

At  $\theta = 0^\circ$ , the frequency-dependent degree of polarization (DOP) is calculated. The two  $1 \times 2$  antenna arrays detect the long-axis and short-axis components of the THz electric field

respectively, as shown in **Figure 5A**. In order to characterize the polarization state of the THz electric field, we use DOP to describe the degree of linear polarization in terahertz:

$$DOP(f) = \frac{I_{\parallel}(f) - I_{\perp}(f)}{I_{\parallel}(f) + I_{\perp}(f)}$$

Where  $I_{\parallel}(f)$  and  $I_{\perp}(f)$  are the spectral intensity of the antenna's response to the long-axis and short-axis components of the THz electric field, respectively.  $I_{\parallel}(f) = |S_{B_1B_2,0}(\omega)|^2$ ,  $I_{\perp}(f) = |S_{A_1A_2,0}(\omega)|^2$ , the spectral DOP(f) is shown in



**Figure 5B.** The spectral DOP( $f$ ) is greater than 99% in the 0.1THz-1.5 THz spectral bandwidth.

At  $\theta = 13^\circ$ , we characterize the accuracy of the detector’s response to polarized terahertz electric fields. The rotation stage used in the experiment is PR50CC, and the minimum incremental motion is  $0.02^\circ$ . As shown in **Figure 5C**, where a local enlargement of the peak amplitude is shown in the green box. The detector has distinguishable signal amplitude changes at  $\theta = 13^\circ$  and  $\theta = 13.2^\circ$ , indicating that the detector’s detection accuracy of the polarized THz electric field is  $0.2^\circ$ .

At  $\theta = +/-45^\circ$ , the time domain signals of arrays  $A_1A_2$  and  $B_1B_2$  are Fourier transformed, as shown in **Figure 5D**, the spectral amplitudes of the two  $1 \times 2$  arrays are not strictly equal. This is the actual working state of the antenna, which deviates from the ideal state. According to the spectrum, we can calculate the response matrix factors  $m_1$  and  $m_2$ , and  $m_1 \neq m_2$ , the deviation between  $m_1$  and  $m_2$  can be explained from the following aspects: 1) the signal-to-noise ratio will affect the accuracy of the matrix calculation; 2) the deviation between  $m_1$  and  $m_2$  is frequency dependent, as shown in **Figure 5E,F**, the amplitude difference between the real and imaginary parts of  $m_1$  and  $m_2$  gradually decreases with the increase of frequency, this is due to the effect of the lead wire on

the electrode surface, and the influence of the lead wire on the surface of the antenna electrode is weaker at higher frequencies [11]; 3) the rotating frame of the detector is not accurate enough, resulting in a systematic error in the axial offset during the rotation of the frame. Therefore, the response matrix can be simplified as:

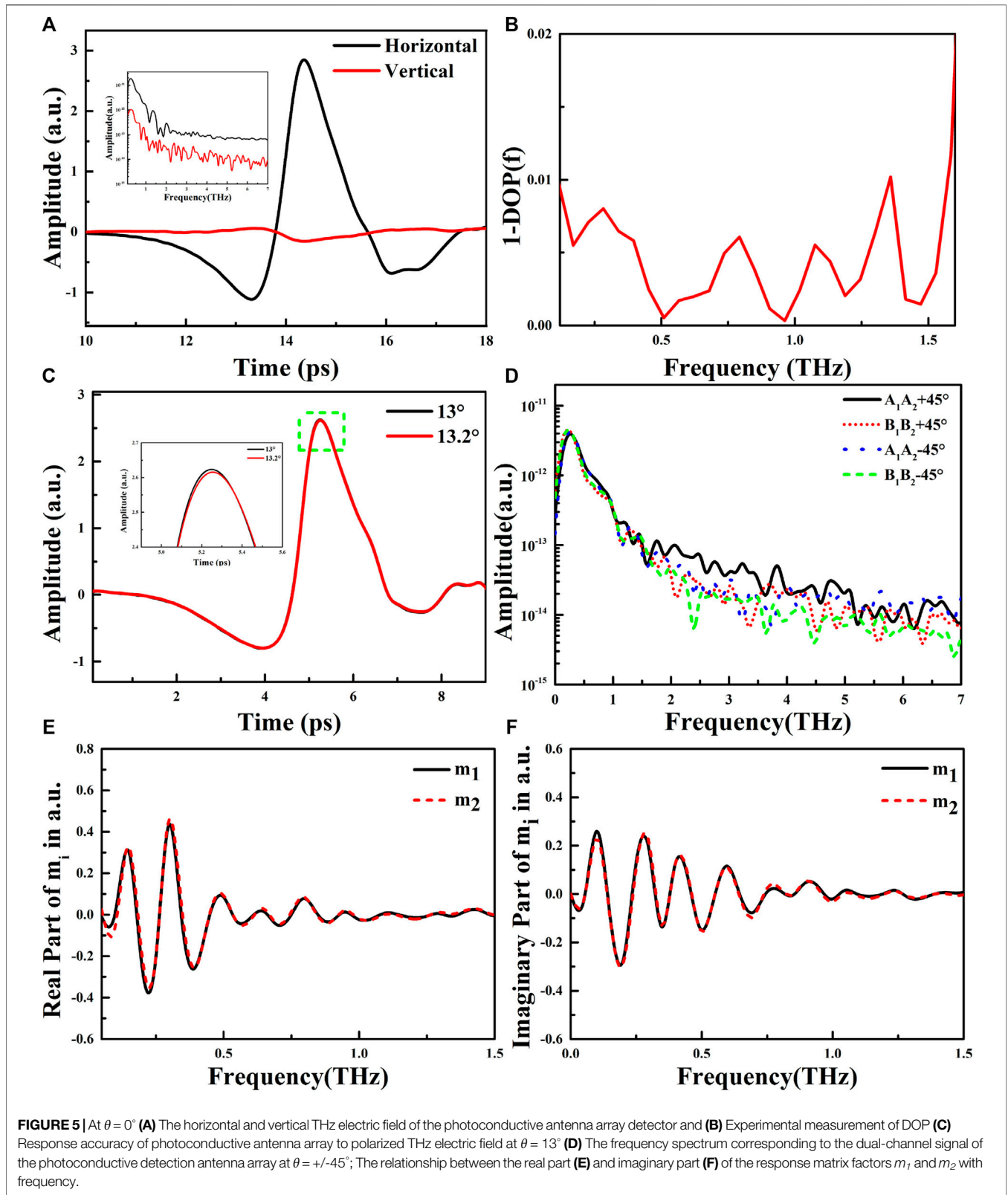
$$M = \begin{pmatrix} 1 & 0 \\ 0 & k \end{pmatrix}$$

where  $l$  and  $k$  are both constant and complex value. Therefore, the expression of the detector for THz polarization measurement can be changed to:

$$\begin{pmatrix} S_{A_1 A_2, \theta} \\ S_{B_1 B_2, \theta} \end{pmatrix} = \begin{pmatrix} 1 & 0 \\ 0 & k \end{pmatrix} \begin{pmatrix} \cos \theta & \sin \theta \\ -\sin \theta & \cos \theta \end{pmatrix} \begin{pmatrix} E_{0x} \\ E_{0y} \end{pmatrix}$$

It should be emphasized that the deviation between  $l$  and  $k$  is almost only in the low-frequency range, and  $l$  and  $k$  are almost equal in the range of 0.3–1.5 THz, therefore, the photoconductive antenna array detector has good symmetry, which is important for polarization detection of THz electric field.





## CONCLUSION

This paper presents the design of a highly efficient photoconductive antenna array detector for THz electric field polarization detection. The detector consists of two perpendicular  $1 \times 2$  arrays, which detect the horizontal and vertical components of the terahertz pulse respectively. The synthesis degree of two perpendicular  $1 \times 2$  array are 98.1 and 99.9%. The detector has a dual signal channel, which can simultaneously obtain the amplitude and phase of the terahertz pulse electric field component received by two vertical  $1 \times 2$  arrays, and give the direction of polarization. The measurement results at different angles are consistent with Malus' law, which shows the reliability of the detector for polarization THz measurement. The polarization detection accuracy of this detector is  $0.2^\circ$ , and the spectrum  $DOP(f)$  is greater than 99% in the 0.1THz-1.5 THz spectrum range. At the same time, we also calculated the expression of the response matrix. The slight difference in the matrix factor indicates that the detector has good symmetry. The new terahertz detection antenna can measure the amplitude, phase and polarization state of the incident terahertz pulse at one time.

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## DATA AVAILABILITY STATEMENT

The original contributions presented in the study are included in the article/Supplementary Material, further inquiries can be directed to the corresponding author.

## AUTHOR CONTRIBUTIONS

Academic thought and preparation of new detection antenna, WS; methodology, LH.; data curation, CF.L. and YP; writing—original draft preparation, ZQ.W.; writing—review and editing, W.S. All authors have read and agreed to the published version of the manuscript.

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