



# Near-Infrared Dual-Gas Sensor System for Methane and Ethane Detection Using a Compact Multipass Cell

Zhenhai Xi<sup>1†</sup>, Kaiyuan Zheng<sup>1†</sup>, Chuantao Zheng<sup>1\*</sup>, Haipeng Zhang<sup>1</sup>, Fang Song<sup>1</sup>, Chunguang Li<sup>2\*</sup>, Weilin Ye<sup>3</sup>, Yu Zhang<sup>3</sup>, Yiding Wang<sup>1</sup> and Frank K. Tittel<sup>4</sup>

<sup>1</sup>State Key Laboratory of Integrated Optoelectronics, College of Electronic Science and Engineering, Jilin University, Changchun, China, <sup>2</sup>College of Biological and Agricultural Engineering, Jilin University, Changchun, China, <sup>3</sup>Key Laboratory of Intelligent Manufacturing Technology of Ministry of Education, College of Engineering, Shantou University, Shantou, China, <sup>4</sup>Department of Electrical and Computer Engineering, Rice University, Houston, TX, United States

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### \*Correspondence:

Chuantao Zheng  
zhengchuantao@jlu.edu.cn  
Chunguang Li  
lichunguang@jlu.edu.cn

<sup>†</sup>These two authors contributed  
equally to this research work

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In this invited paper, a compact dense-pattern multipass cell-based near-infrared sensor system was demonstrated for detection of parts-per-billion in volume (ppbv)-level methane (CH<sub>4</sub>) and ethane (C<sub>2</sub>H<sub>6</sub>). The dimension size of the fabricated gas cell is 18.5 × 8 × 9 cm<sup>3</sup> with an absorption path length of 9.39 m. CH<sub>4</sub> measurement was realized within a spectral range of 6,046–6,048 cm<sup>-1</sup> and an absorption line of 6,046.95 cm<sup>-1</sup>. The spectral range for C<sub>2</sub>H<sub>6</sub> detection is 5,951–5,953 cm<sup>-1</sup> with an absorption line of 5,951.73 cm<sup>-1</sup>. Allan deviation analysis was used for evaluating the dual-gas sensing performance, and a detection limit of 78 ppbv for CH<sub>4</sub> and 190 ppbv for C<sub>2</sub>H<sub>6</sub> were achieved, respectively, with an averaging time of 0.8 s. Furthermore, CH<sub>4</sub> measurement in the indoor and outdoor atmosphere was both performed to verify the field sensing capability of the sensor system. Compared with two separate sensor systems for CH<sub>4</sub>/C<sub>2</sub>H<sub>6</sub> sensing, the proposed dual-gas sensor system using two near-infrared lasers and one multipass cell has the advantages of low-cost, compact-size without decreasing the selectivity and sensitivity.

**Keywords:** infrared absorption, dual-gas detection, laser absorption spectroscopy, multi-pass cell, atmospheric gas monitoring

## INTRODUCTION

Methane (CH<sub>4</sub>) and ethane (C<sub>2</sub>H<sub>6</sub>) are the two most abundant alkanes in the atmosphere [1–3]. CH<sub>4</sub> is widely distributed in nature and is one of the main greenhouse gases. Atmospheric CH<sub>4</sub> concentration detection is of great significance for climate research and atmospheric monitoring. CH<sub>4</sub> is also the main component of natural gas and biogas. CH<sub>4</sub> leakage has become the major safety hazard in the industrial field including coal mines, natural gas transportation and other industries [4–7]. Therefore, it is necessary to monitor the CH<sub>4</sub> concentration in real time, so that people can respond and evacuate when leakage occurs.

C<sub>2</sub>H<sub>6</sub> is the second-largest component of natural gas after CH<sub>4</sub>, which can be treated as a target gas for natural gas leakage monitoring. Also, highly-sensitive C<sub>2</sub>H<sub>6</sub> detection has found applications in human breath analysis as a non-invasive method to identify different diseases [8–10]. CH<sub>4</sub> and C<sub>2</sub>H<sub>6</sub> molecules all have absorption peaks in the near-infrared range. Therefore, compact near-infrared laser source can be used for the two gas species detection. Compared with mass spectrometry and gas chromatography, infrared absorption spectroscopy, including photothermal and

photoacoustic spectroscopy [11–16], provides a less-costly approach for  $\text{CH}_4$  and  $\text{C}_2\text{H}_6$  concentration detection, and enables real-time measurement without the need for pretreatment or accumulation of target gas samples.

Tunable diode laser absorption spectroscopy (TDLAS) is an effective non-contact method for trace gas detection, which uses a single, narrow-band near-/mid-infrared laser to scan gas absorption peaks with to increase sensitivity and selectivity [17–20]. In TDLAS, an optical absorption cell design is generally based on White [21], Herriott [22, 23] or other multipass cell (MPC) [24, 25]. Compared with White cell, Herriott-based MPC has the advantages of simpler structure and more compact size. In recent years, Herriott MPC has been widely used in various applications [26] and the main development is the change of spot distribution, *i.e.* from initial single-ring Herriott to dense spot distribution. Herriott-based MPC is widely used in TDLAS sensor systems due to its improvement in effective path length and therefore in gas absorption ability. A dense-pattern (DP)-MPC with a light absorption path length of 26.4 m was designed by Gao *et al.*, and the  $\text{CH}_4$  measurement accuracy reached 79 parts-per-billion in volume (ppbv) [27]. A mini-MPC with an absorption optical path length of 4.2 m was designed by Dong *et al.* The optical system is highly integrated, and the  $\text{CH}_4$  measurement accuracy reached 117 ppbv [28]. The gas absorption coefficient can also be improved by optimizing the Herriott cell configuration. A double-spot ring Heriot cell (DSR-HC) with an optical path length of 20 and 6 m was designed by Zheng *et al.*, respectively. Two different optical paths provide different detection ranges for  $\text{C}_2\text{H}_2$  detection. The practicability of the sensor is improved by increasing the detection range of  $\text{C}_2\text{H}_2$ . The detection limits under the two absorption path lengths were 7.9 parts-per-million in volume (ppmv) and four ppmv, respectively [29].

Most reported MPC-based TDLAS sensor systems were designed for single-gas detection. If they are used to detect multi-gas species, two sets of systems are required, which increases the whole size of the sensor system. Especially in the harsh geographical environment, it is difficult to transport safely and operate normally, which virtually limits the function of the sensor. In order to overcome the above-mentioned issue, a near-infrared dual-gas TDLAS sensor was developed using two distributed feedback (DFB) lasers, *i.e.* 1654 nm for  $\text{CH}_4$  and 1,680 nm for  $\text{C}_2\text{H}_6$  detection, respectively. Compared to a sensor system based on mid-infrared lasers [30], near-infrared lasers are lower in cost and a sensor system based on such sensors is smaller in size, which is conducive to the integration and commercial use of the sensor system. In addition, in order to further reduce the size of the sensor system, a DP-MPC was developed, with an absorption path length of 9.39 m. Furthermore, a LabVIEW based data-processing system, which consists of a scan signal generator and a signal acquisition module was developed. Such a system can perform the normal operation of driving two DFB lasers as well as extracting the ppbv-level  $\text{CH}_4$  and  $\text{C}_2\text{H}_6$  concentration employing a laptop and a data acquisition (DAQ) card. The practicability of the sensor system was verified by continuous monitoring of the indoor and atmospheric  $\text{CH}_4$  concentration levels.

## EXPERIMENTAL SET-UP

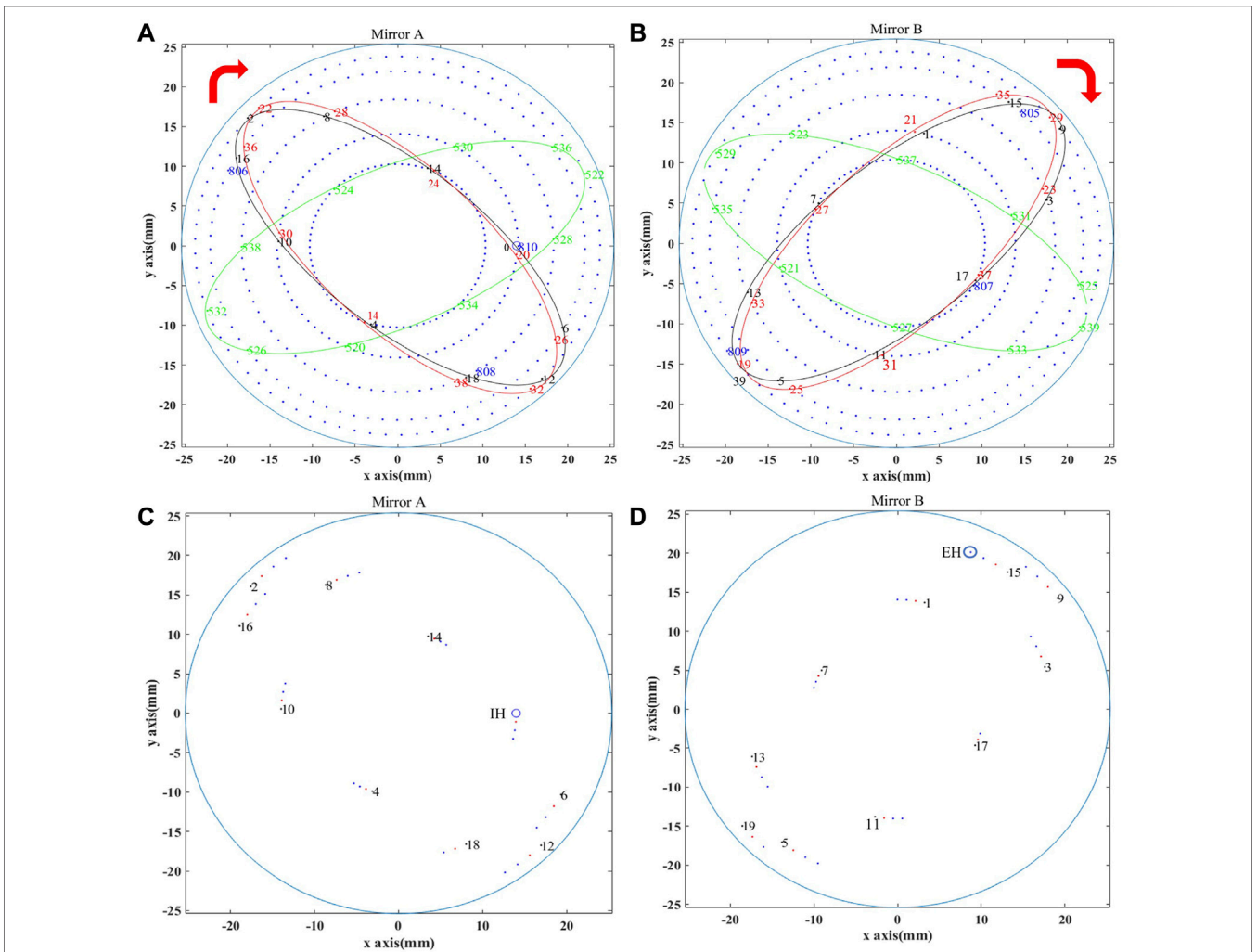
### Simulation and Modelling of the Compact MPC

A model of the compact MPC was designed based on MATLAB, and the reflection of light in the cell was simulated using a similar method with Ref. [31]. The radius of curvature of the used spherical mirror is 150 mm with a diameter of 50.8 mm and a mirror reflectivity of >95%. The obtained spot distribution on the two mirrors is shown in **Figures 1A,B**, where the first 20 reflection points are labeled. On mirror A, the injection hole (IH) shown as a blue circle is labeled as 0, the second reflection point is labeled 2, the third is labeled 4, the fourth is labeled 6, and so on. The connection of the first ten reflection points (numbered as 0, 2, . . . , 18) will form the first ellipse. The next ten reflection points (numbered as 20, 22, . . . 38) will be offset clockwise, and also the connection between them forms the second ellipse. It can be seen that the second ellipse can be treated as the clockwise rotation of the first ellipse. A similar distribution can be found on mirror B. All the reflection points and the formed rings on mirror A and mirror B are found to rotate clockwise to form the spot distribution. When the light is reflected for the 809th on mirror B, it escapes through the injection hole on mirror A. There are 810 reflections between the mirrors, 40 and a half ellipses and five rings are formed on each mirror. **Eq. 1** is used to calculate the total optical path length

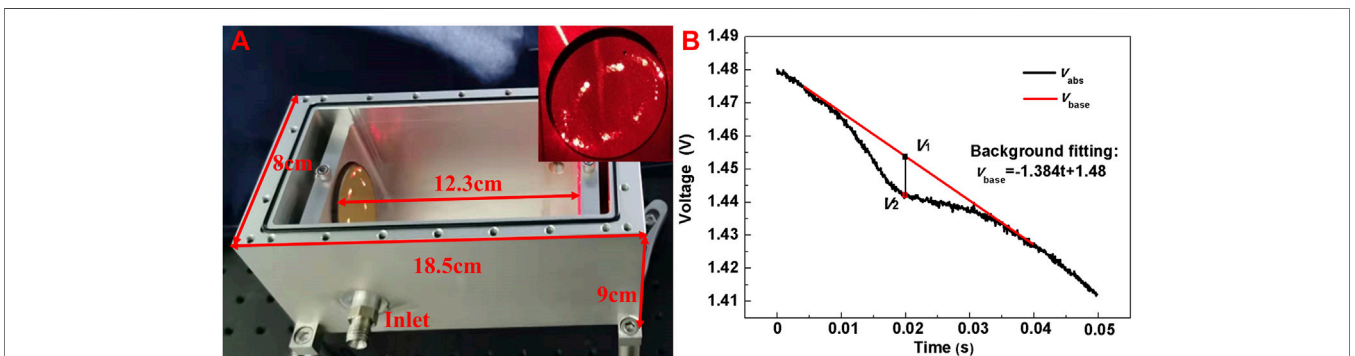
$$L = \sum_{i=1}^N \sqrt{[(x_i - x_{i-1})^2 + (y_i - y_{i-1})^2 + (z_i - z_{i-1})^2]} \quad (1)$$

where  $(x_i, y_i, z_i)$  is the coordinates of the *i*th reflection point, and  $N = 810$  is the total reflection number. Due to the limitation in laser power and the mirror reflection loss, the signal derived by output from the detector cannot be large with too many reflections. Therefore, the laser beam was designed to exit in advance with 76 reflections. As shown in the model in **Figures 1C,D**, when the light is reflected for the 76th time, it escapes through the designed ejection hole (EH) on mirror B, reaches the detector for optoelectrical conversion, and the derived electrical signal enters a data acquisition (DAQ) card for data processing. The total optical path length with 76 reflections was calculated to be 9.36 m through simulation.

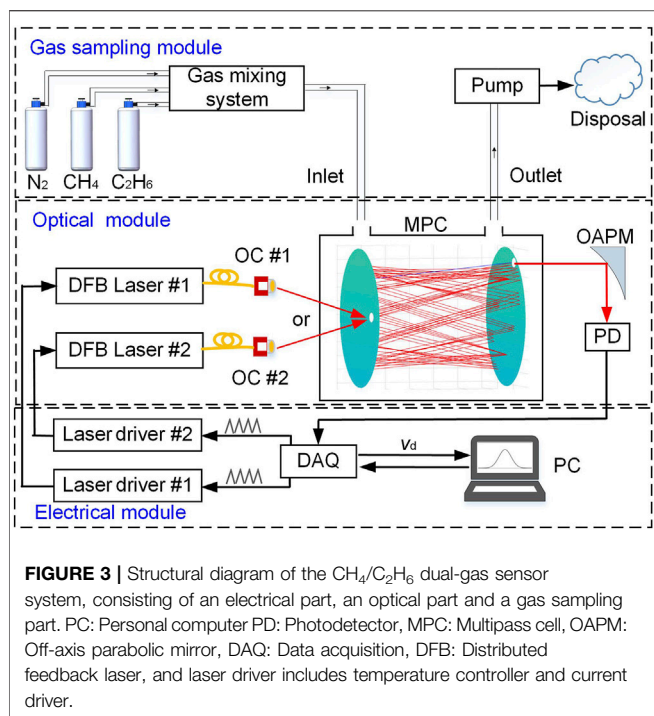
According to the designed model and optimized parameters, a compact MPC with 76 reflections was fabricated, whose photo is shown in **Figure 2A**. The spot distribution of the mirror shown in the inset was obtained using a He-Ne laser as a trace laser, which basically coincides with the simulated spot distribution in **Figure 1D**. The external dimension size of the fabricated gas cell is  $18.5 \times 8 \times 9 \text{ cm}^3$  with an internal volume of 683.9 mL. Two optical windows (*i.e.*  $\text{CaF}_2$  lens) were placed at both sides with the same aperture as the reflection mirror, and the groove where the window is placed was designed to tilt  $15^\circ$  to prevent the infrared light from directly reflecting into the laser collimator resulting in laser damage. An air inlet and outlet were equipped on the gas cell, separately for gas injection and ejection, and the whole gas chamber was sealed for a good gas tightness. Glass glue was used to fix the optical window at both ends of the MPC, and the upper opening was sealed with a sealing ring to ensure air tightness.



**FIGURE 1 |** Complete spot distribution of (A) Mirror A and (B) Mirror B in simulation. Spot distribution of (C) Mirror A and (D) Mirror B in simulation with mirror refraction.



**FIGURE 2 |** (A) Photograph of the fabricated multi-pass cell design with an external size of  $18.5 \times 8 \times 9 \text{ cm}^3$  and a physical spot distribution of Mirror B in the inset (B) Measured  $\text{CH}_4$  absorption signal (black curve) with the compact MPC at a concentration level of 20 ppmv. The red curve shows the background fitting signal.



With a sealing detection, the air leakage rate was measured to be  $2.4 \times 10^{-3}$  TorrL/s.

To determine the actual effective optical path length, a sawtooth scan signal with a frequency of 50 Hz was used to change the current of the DFB laser and a CH<sub>4</sub> sample with a concentration level of 20 ppmv was injected into the compact MPC. The output signal from the detector with CH<sub>4</sub> absorption, defined as  $v_{\text{abs}}(t)$ , is shown in **Figure 2B**. The red line is the background fitting signal, expressed as  $v_{\text{base}}(t)$ . A differential signal can be obtained by subtracting  $v_{\text{abs}}$  from  $v_{\text{base}}$ , which represents gas absorption. The maximum absorption (i.e.  $v_{\text{base}} - v_{\text{abs}}$ ) occurred at  $t = 0.1986$  s and the corresponding voltage ( $V_2 = v_{\text{abs}}(t = 0.1986 \text{ s})$ ) is 1.443 V. The non-absorption voltage ( $V_1 = v_{\text{base}}(t = 0.1986 \text{ s})$ ) is 1.453 V. Then the absorbance ( $\alpha$ ) can be calculated from **Eq. 2**, as

$$\alpha = -\ln(V_2/V_1) \quad (2)$$

According to **Eq. 2**, the absorbance is 0.0069, and the actual total optical path is determined to be 9.39 m by referring to the high-transmission (HITRAN) molecular absorption database, which are highly consistent with the simulation result of 9.36 m.

## Sensor Structure Design

An overall sensor system structure is shown in **Figure 3**, which is divided into three parts, including an optical part, an electrical part and a gas sampling part. In the optical part, two near-infrared DFB lasers were used as the excitation source for the detection of CH<sub>4</sub> and C<sub>2</sub>H<sub>6</sub>. In order to facilitate the optical path establishment, the two lasers followed the same light propagation path. For CH<sub>4</sub> detection, the laser operating temperature was set to 20°C, and the center current was set to 84 mA for targeting the

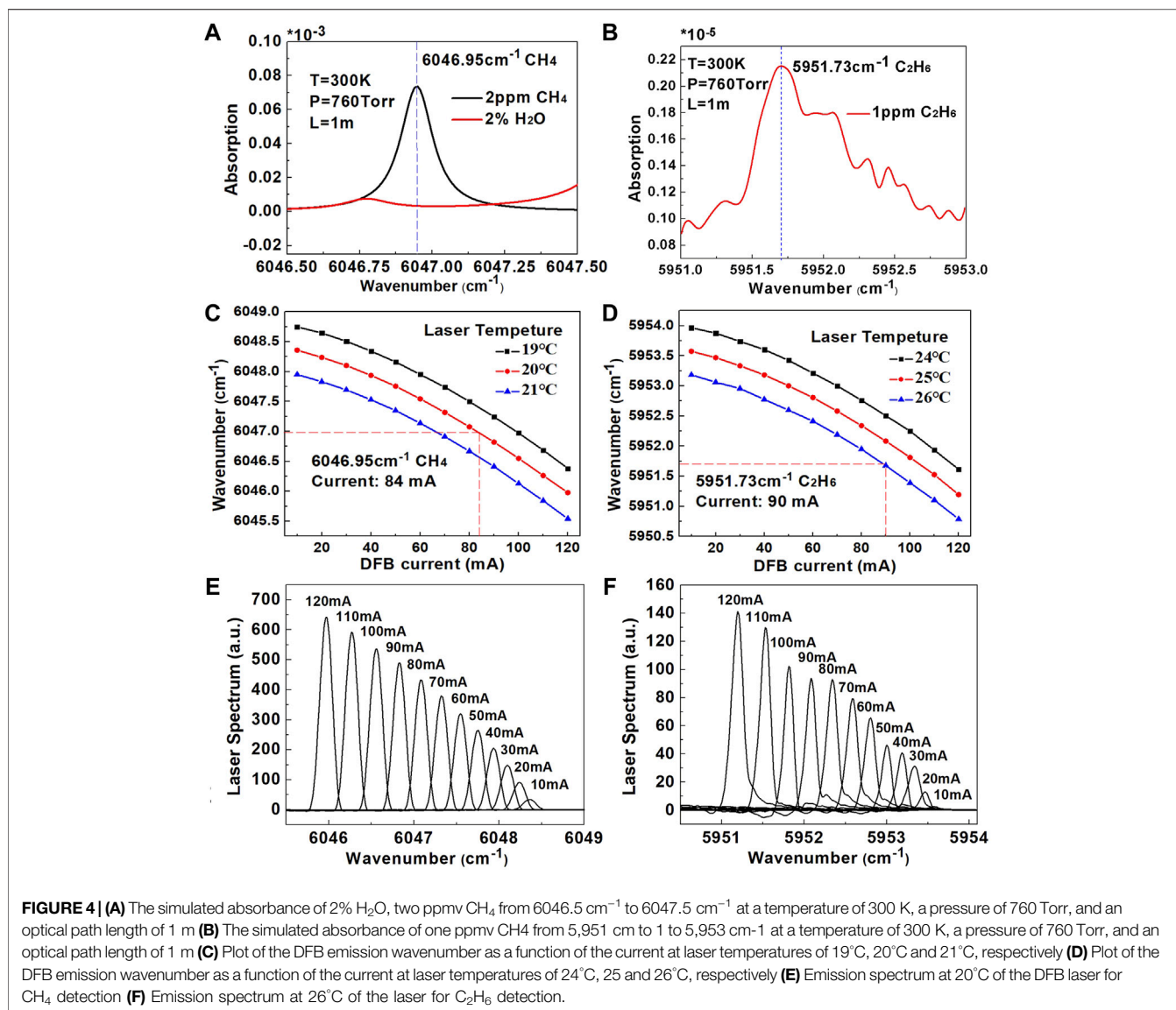
absorption line at  $6046.95 \text{ cm}^{-1}$ . For C<sub>2</sub>H<sub>6</sub> detection, the laser was operated at 26°C with a center current of 90 mA for targeting the absorption line at  $5951.73 \text{ cm}^{-1}$ . The emitted infrared laser beams were combined and the collimated laser beam enters the MPC through an optical fiber collimator. A fiber adapter as well as an optical switch can be used to automatically exchange the 1,654 nm and 1,680 nm laser for different gas detection. Because of the loss resulting from light reflection, the light power will be reduced after multiple reflections. An off-axis parabolic lens was therefore added at the exit to focus the light intensity, and then the signal amplitude output from a Ge transimpedance photodetector was increased. The electrical part included a laptop (HP model BH872PHB), a DAQ card (Model USB-6211, National Instrument, United States), two current and temperature integrated drive modules (LDTC0520, Wavelength, United States). Laser direct absorption spectroscopy (LDAS) technique was used for CH<sub>4</sub> and C<sub>2</sub>H<sub>6</sub> dual-gas detection, which is easy to realize and suitable for portable applications, compared to wavelength modulation spectroscopy (WMS). A scan signal was generated by the DAQ card controlled by the LabVIEW platform to drive the DFB laser. The output signal from the detector was sampled by the DAQ card, and synchronous sampling was realized triggered by the signal generation module. With respect to the gas sampling module, the MPC was equipped with an inlet and an outlet, allowing gas flow during measurements. CH<sub>4</sub>/C<sub>2</sub>H<sub>6</sub>:N<sub>2</sub> mixtures were diluted from a standard 50 ppmv CH<sub>4</sub> sample and a 100 ppmv C<sub>2</sub>H<sub>6</sub> sample in N<sub>2</sub> using a commercial gas mixing system (Series 4,000, Environics).

## DUAL-GAS SENSOR PERFORMANCE

### Absorption Lines Selection for CH<sub>4</sub> and C<sub>2</sub>H<sub>6</sub>

The selected absorption line of CH<sub>4</sub> is shown in **Figure 4A**. According to the simulation results of HITRAN, under the conditions of temperature of 300 K, pressure of 760 Torr and optical path length of 1 m, the absorbance of CH<sub>4</sub> at a concentration level of two ppmv and H<sub>2</sub>O at a concentration level of 2% were obtained. It can be seen that when the H<sub>2</sub>O concentration is high, it will have a certain influence on the detection of CH<sub>4</sub>. Therefore, a dehumidification treatment was performed in the gas inlet to reduce the interference of H<sub>2</sub>O. CH<sub>4</sub> has a strong absorption line located at  $6046.95 \text{ cm}^{-1}$ . Accordingly, we chose the laser emission wavelength range of  $6046\text{--}6048 \text{ cm}^{-1}$  for CH<sub>4</sub> detection. **Figure 4C** shows the current variation within the selected wavenumber range when the temperature of the DFB laser is 19°C, 20 and 21°C. In **Figure 4E**, the emission spectrum under a laser driving current of 10–120 mA was measured at 20°C. In order to cover the CH<sub>4</sub> absorption line, the laser temperature was set at 20°C and the central current at 84 mA.

The selected C<sub>2</sub>H<sub>6</sub> absorption line is shown in **Figure 4B**. According to the simulation results of HITRAN, under the condition of temperature of 300 K, pressure of 760 Torr and optical path length of 1 m, the C<sub>2</sub>H<sub>6</sub> absorption line with one ppmv concentration was obtained. C<sub>2</sub>H<sub>6</sub> has a strong absorption



line at 5,951.73 cm<sup>-1</sup>, and the selected wavenumber range is 5,951–5,953 cm<sup>-1</sup> for C<sub>2</sub>H<sub>6</sub> detection. **Figure 4D** shows the current variation in the selected wavenumber range at a laser temperature of 24°C, 25 and 26°C. The laser drive temperature was set at 26°C, and the central current was 90 mA for C<sub>2</sub>H<sub>6</sub> detection. In **Figure 4F**, the emission spectrum of the laser under a current of 10–120 mA was measured at a temperature of 26°C.

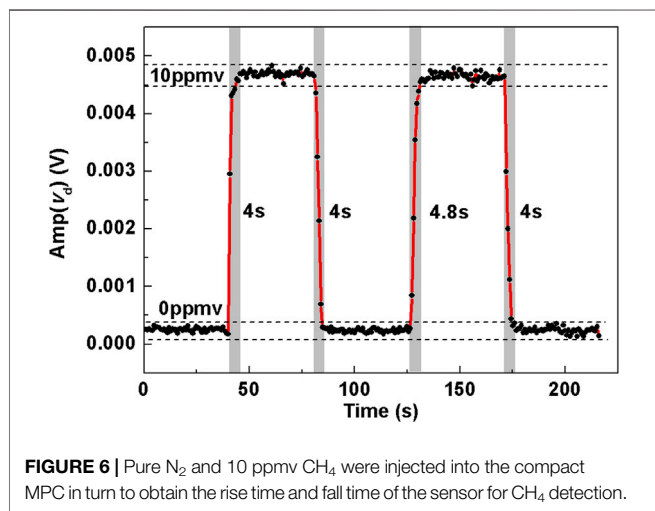
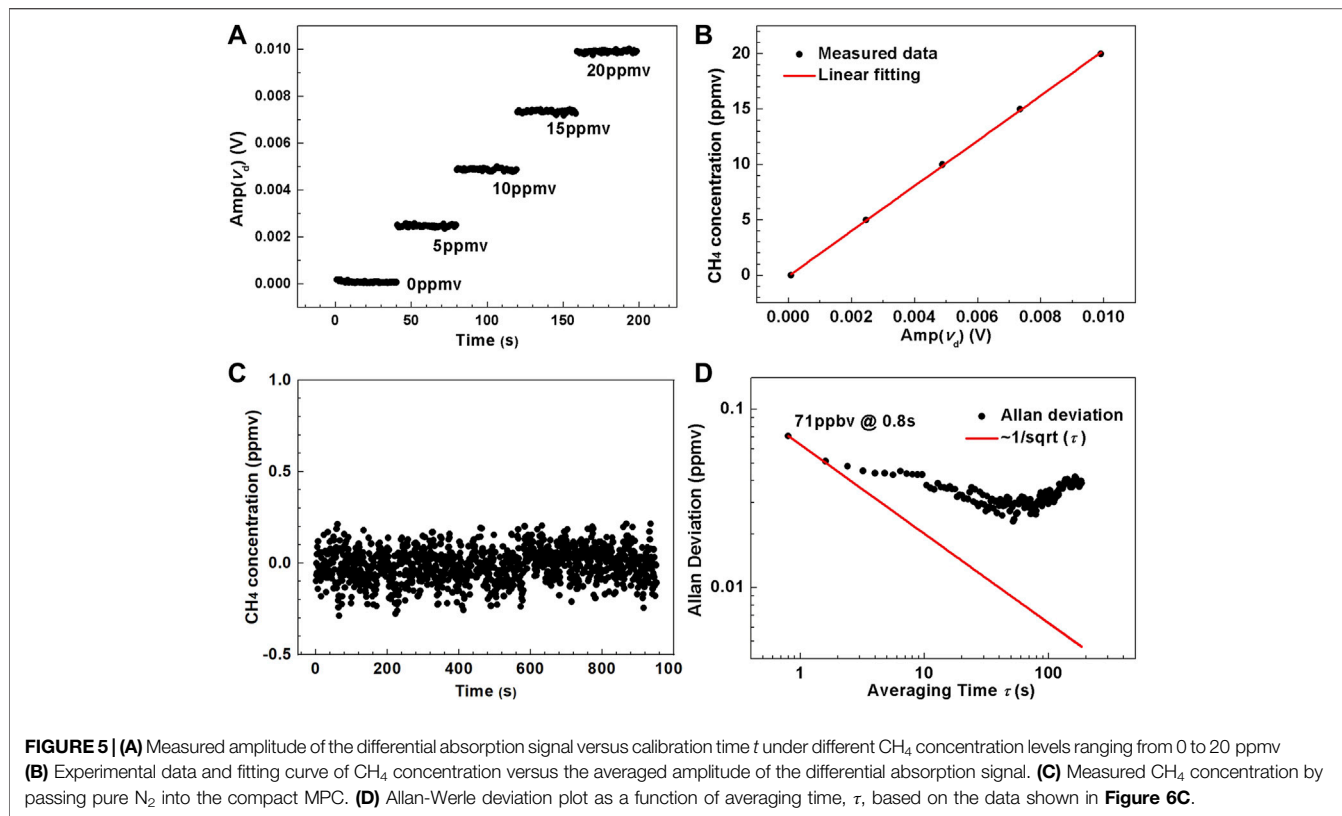
## CH<sub>4</sub> Sensor Performance

The measured amplitude of the differential signal of CH<sub>4</sub> (i.e.  $v_d = v_{\text{base}} - v_{\text{abs}}$ ) at different concentration levels of 0, 5, 10, 15 and 20 ppmv is shown in **Figure 5A**. In order to speeding the response of the sensor, a high sampling frequency was adopted, and one data point was acquired per 0.8 s. The amplitude (defined as  $\text{Amp}(v_d)$ , in V) at each concentration was recorded for 40 s, leading to 50 points. The average value of these 50 data was used to obtain the linear relationship between CH<sub>4</sub> concentration and the

amplitude, as shown in **Figure 5B**. The linear relationship is expressed by **Eq. 3** with a good linear fitting degree of 99.97%, as

$$C_{\text{CH}_4} = 2037.42458 \times \text{Amp}(v_d) - 0.05898 \quad (3)$$

where  $C_{\text{CH}_4}$  (in ppmv) is the concentration of CH<sub>4</sub>. Then, the CH<sub>4</sub> sample with a concentration of 0 ppmv was injected into the MPC to observe the stability of the whole system, and the overall observation time was ~16 min. The sampled signal amplitude was substituted in **Eq. 3** to calculate the corresponding CH<sub>4</sub> concentration levels. Curve of CH<sub>4</sub> concentration level changing with measurement time is shown in **Figure 5C**, which is relatively stable overall and verifies the reliability of the whole sensor system. The measured concentration was then used for Allan variance analysis to obtain the detection limit of the CH<sub>4</sub> sensor, as shown in **Figure 5D**. The first data point is the minimum concentration that can be detectable, which indicates that the 1 $\sigma$  detection limit of CH<sub>4</sub> is 71 ppbv at an averaging time



of 0.8 s. As integration time increases, system noise occurs leading to the decrease of sensor stability. This type of noise is the sensor system drift, mainly originating from the drift of the near-infrared detector, the laser power and wavelength as well as the electrical circuits for signal processing.

The response time of the sensor system for  $\text{CH}_4$  detection was determined by the measured time that was needed for the  $\text{CH}_4$  concentration exchange between 0 ppmv and 10 ppmv. The sampling time for each data point was 0.8 s, as shown in Figure 6. Several

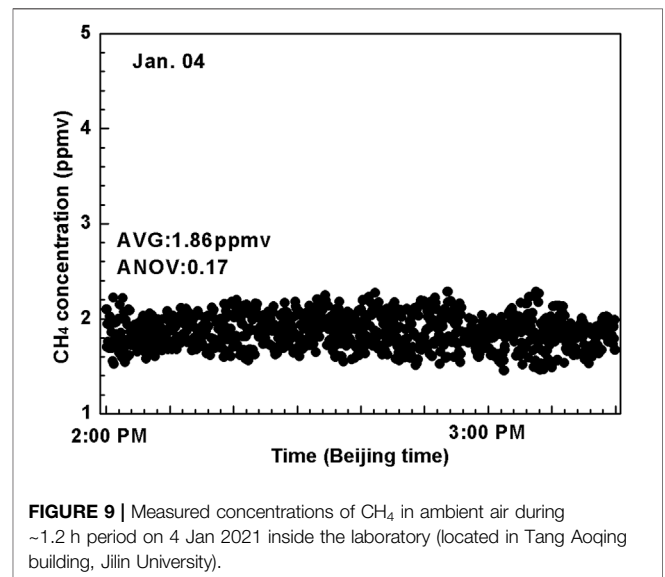
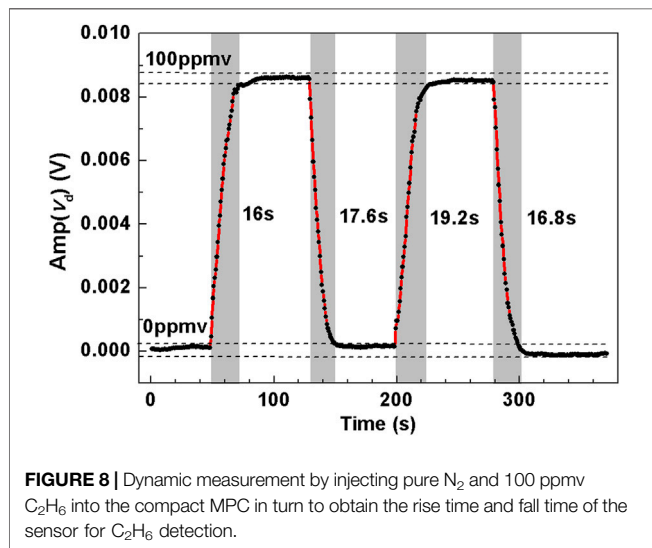
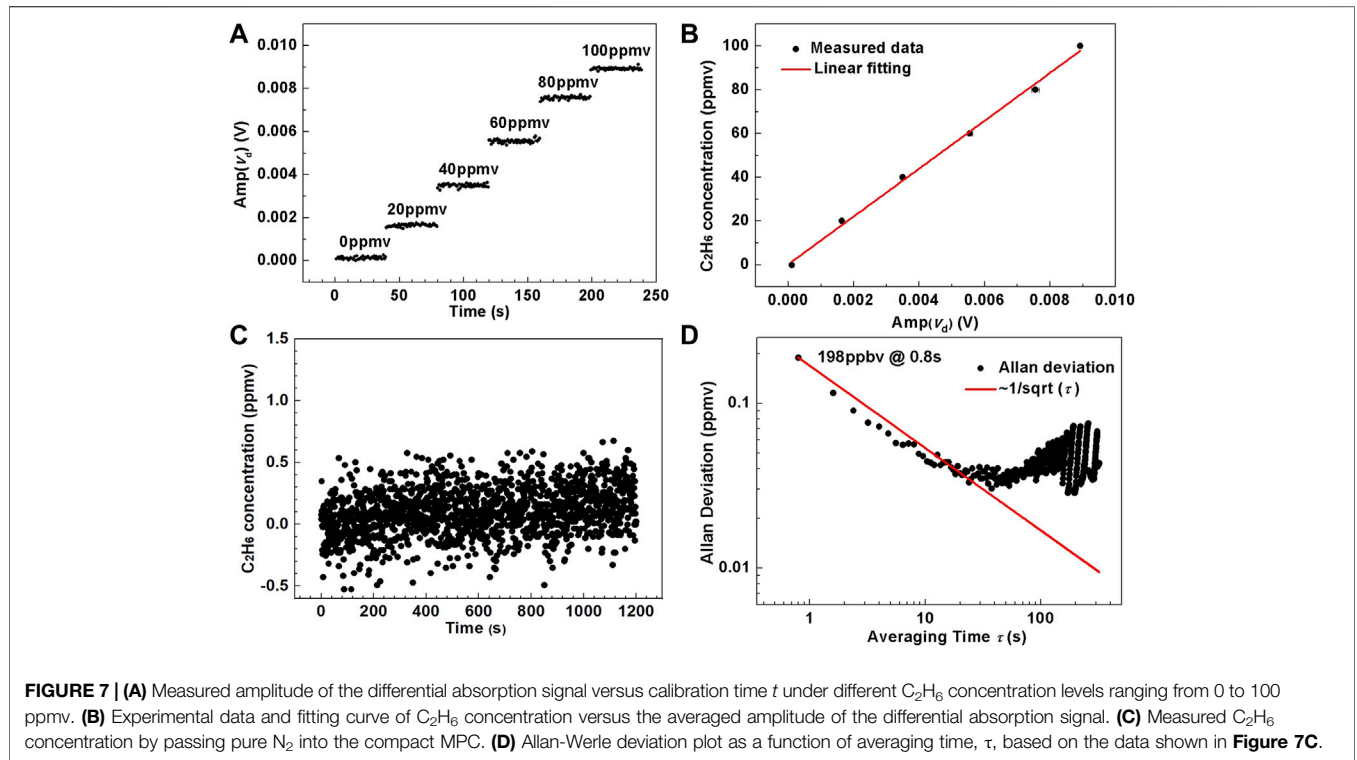
repeated experiments were done to change the concentration level either from 0 ppmv to 10 ppmv or from 10 ppmv to 0 ppmv for multiple times. At each time the concentration became stable, 40 points were recorded. The response time was measured to be 4 s.

### $\text{C}_2\text{H}_6$ Sensor Performance

As shown in Figure 7A, the measured amplitude ( $\text{Amp}(v_d)$ ) of  $\text{C}_2\text{H}_6$  at six different concentration levels of 0, 2, 4, 6, 8, and 10 ppmv were obtained. A data point was derived per 0.8 s, and the total time for recording the amplitude at each concentration was 40 s. The linear relationship between  $\text{C}_2\text{H}_6$  concentration  $C_{\text{C}_2\text{H}_6}$  (in ppmv) and  $\text{Amp}(v_d)$  (in V) was obtained as shown in Figure 7B, expressed as

$$C_{\text{C}_2\text{H}_6} = 10929.09126 \times \text{Amp}(v_d) + 0.29314 \quad (4)$$

Then the  $\text{C}_2\text{H}_6$  concentration was set to 0 ppmv to observe the stability of the whole system, and the overall observation time was 18 min. The real-time  $\text{C}_2\text{H}_6$  amplitude was substituted into Eq. 4 to calculate the corresponding concentration. The variation of  $\text{C}_2\text{H}_6$  concentration with time is shown in Figure 7C, which proved the overall stability and verified the reliability of the whole sensor system. The obtained concentration was used for Allan variance analysis, and the  $\text{C}_2\text{H}_6$  detection limit of the sensor system was achieved, as shown in Figure 7D. The first point is the minimum concentration detected, and the subsequent data is the deviation value, which indicates that the limit of detection of  $\text{C}_2\text{H}_6$  is 189 ppbv at an averaging time of 0.8 s.

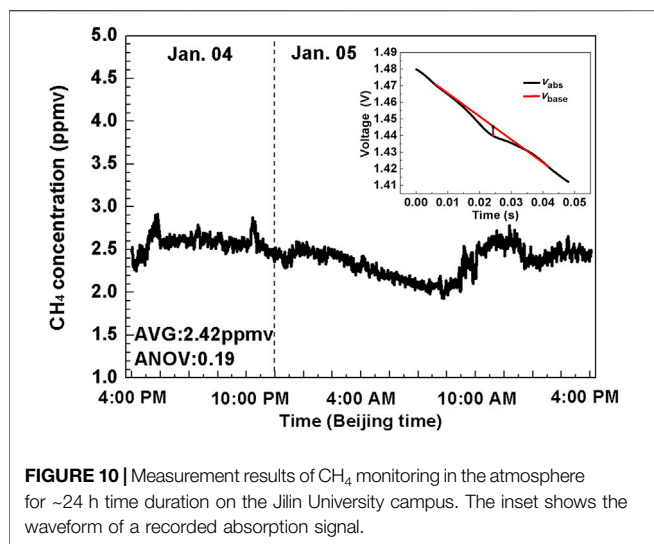


Then, the response characteristics of the dual-gas sensor system for  $C_2H_6$  detection was determined by measuring the response time by switching the  $C_2H_6$  concentration level between 0 ppmv and 100 ppmv. The sampling time for each data point was 0.8 s. The response time from 0 ppm to 100 ppmv for the first concentration exchange was about 16 s. Then several repeated experiments were done, that is, either from 0 ppmv to 100 ppmv or from 100 ppmv to 0 ppmv. 40 data points were recorded each time when the measured concentration was stabilized. As shown

in **Figure 8**, The measured response time was maintained at 16–20 s.

### FIELD SENSING APPLICATION

In order to verify the performance and practicability of the sensor, the demonstrated dual-gas sensor system was used to monitor the



**FIGURE 10** | Measurement results of CH<sub>4</sub> monitoring in the atmosphere for ~24 h time duration on the Jilin University campus. The inset shows the waveform of a recorded absorption signal.

CH<sub>4</sub> concentration levels in the laboratory and the CH<sub>4</sub> concentration levels in the outdoor atmosphere.

### Indoor CH<sub>4</sub> Monitoring

The sensor system was evaluated by measuring the indoor CH<sub>4</sub> concentration levels in a laboratory environment on 4 January 2021 between 2:00 p.m. and 3:20 p.m. The laboratory is located at Tang Aoqing building (GPS position, 125.291,448° E, 43.831,747° N) of Jilin University, Changchun, Jilin Province, China. The total measurement duration was 1.2 h with a sampling interval of 0.8 s (i.e. no averaging on the sampling data). As shown in **Figure 9**, fluctuations in CH<sub>4</sub> concentration levels were observed during the measurement from 1.5 ppmv to 2.2 ppmv, and the concentration of CH<sub>4</sub> showed an average of  $\sim 1.86 \pm 0.17$  ppmv ( $1\sigma$ ). Since the air circulation in the laboratory was relatively slow, the change of CH<sub>4</sub> concentration was not obvious. It thus can be observed that the CH<sub>4</sub> concentration level in the laboratory was relatively stable during this period.

### Outdoor Atmospheric CH<sub>4</sub> Monitoring

The sensor system was re-evaluated by measuring the outdoor CH<sub>4</sub> concentration levels in the atmosphere. The outside air was pumped into the gas cell via a Poly Tetra Fluoroethylene (PTFE) for outdoor atmospheric CH<sub>4</sub> testing. Pre-treatment was carried out before the atmosphere enters the gas cell to remove ambient impurities, aerosols and water vapor. The outside air was pumped into the gas cell via a PTFE filtered tube to detect the outdoor CH<sub>4</sub> concentration levels for 1 day. The measurement was conducted in zone D, Tang Aoqing building, Jilin University, Changchun, and the measurement time was from 4:40 p.m. on 4 January 2021 to 4:40 p.m. on 5 January 2021. The sampling data was averaged per 40 s (i.e. 50 data points were averaged as one data point). As shown in **Figure 10**, it can be concluded from the variation trend that the CH<sub>4</sub> concentration decreased at night and was eventually down to 2.2 ppmv–2.3 ppmv. The CH<sub>4</sub> concentration level

suddenly increased at 10:00 a.m. with a peak up to 2.7 ppmv and was eventually around 2.6 ppmv at 4:00 p.m. in the next day. Over the 1 day, the measured CH<sub>4</sub> concentration ranged between 2.2 and 2.8 ppmv, with an average value of  $2.42 \pm 0.19$  ppmv.

## CONCLUSION

A dense-pattern MPC-based near-infrared sensor system was demonstrated for CH<sub>4</sub>/C<sub>2</sub>H<sub>6</sub> dual-gas detection. Two laser beams were injected into the MPC with an effective path length of 9.39 m. Both indoor and outdoor CH<sub>4</sub> concentration levels were measured to verify the performance of the sensor system. Compared with the traditional single-ring Herriott cell, the volume of the DP-based gas cell is obviously reduced and the optical path becomes longer by increasing the reflection number, and the reduced size leads to an enhanced stability and high sensitivity. Compared with a single-gas sensor, the size of the developed dual-gas sensor system becomes smaller and more convenient for field detection. The dual-gas sensor system extends the application of MPC in the field of infrared absorption spectroscopic gas sensing. Further optimization of optical path will be carried out to improve the sensitivity of C<sub>2</sub>H<sub>6</sub> detection, so as to monitor the ppb-level C<sub>2</sub>H<sub>6</sub> in the atmosphere.

## DATA AVAILABILITY STATEMENT

The original contributions presented in the study are included in the article/supplementary material further inquiries can be directed to the corresponding authors.

## AUTHOR CONTRIBUTIONS

ZX and KZ performed the experiments and wrote the manuscript. CZ and YW supported the experiments and revised the manuscript. HZ. analyzed and verified the experimental results. FS, CL, WY, YZ, YW, and FT provided technical guidance and helped to revise the paper. The manuscript was written through contributions of all authors. All authors have given approval to the final version of the manuscript.

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