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EDITED BY

Jian Wang,
Huazhong University of Science and
Technology, China

REVIEWED BY

Qiang Zhou,
University of Electronic Science and
Technology of China, China
Youbin Yu,
Zhejiang Sci-Tech University, China

*CORRESPONDENCE

Yichen Liu,
✉ yourslyc@163.com
Liangliang Lu,
✉ lianglianglu@nju.edu.cn

[†]These authors have contributed equally
to this work

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Full characterization of spontaneous parametric down conversion in non-ideal quarter-wavelength semiconductor Bragg reflection waveguide

Bin Niu^{1,2†}, Cheng Qian^{3†}, Xu Jing^{1,2†}, Chenquan Wan^{1,2},
Yuechan Kong^{1,2}, Tangsheng Chen^{1,2}, Yichen Liu^{4,5*} and
Liangliang Lu^{1,3,5*}

¹Science and Technology on Monolithic Integrated Circuits and Modules Laboratory, Nanjing Electronic Devices Institute, Nanjing, China, ²Nanjing Chip Valley Industrial Technology Institute, Nanjing, China, ³Key Laboratory of Optoelectronic Technology of Jiangsu Province, School of Physical Science and Technology, Nanjing Normal University, Nanjing, China, ⁴Research Center for Quantum Optics and Quantum Communication, School of Science, Qingdao University of Technology, Nanjing, China, ⁵National Laboratory of Solid State Microstructures, Nanjing University, Nanjing, China

Entangled photons are important for testing foundations of quantum physics and are at the heart of quantum technology. Integrated photonics has overwhelming dominance in terms of density and performance, making it a promise route for scalable quantum information processing. AlGaAs-based materials having large second-order non-linearities, direct bandgap and strong electro-optical effect can offer distinct advantages in quantum light source. Here we report a non-ideal quarter-wavelength Bragg reflection waveguide for generating three types of spontaneous parametric down-conversion processes. A general solution to the dispersion equation is derived and employed for designing high efficiency devices by taking into account the influence of core layer aluminium concentration. We further design and fabricate a Bragg reflection waveguide sample based on the analysis, and experimentally characterize its phase matching types and spectral brightness. Our work paves the path for the development of portable quantum light sources.

KEYWORDS

Bragg reflection waveguide, quantum light source, spontaneous parametric down conversion, entanglement, integrated quantum optics

1 Introduction

To demonstrate the advantage of quantum systems over their classical counter-parts, it is necessary to generate, manipulate and detect various entangled states [1, 2]. Photonics is crucial for the development of quantum technologies [3]. At present, the spontaneous parametric down conversion (SPDC) in non-linear crystals is widely used to generate entangled photons at room temperature. The photon pair can be entangled in various degrees of freedom (DOF), such as polarization [4], frequency [5], path [6] and orbital angular momentum [7]. However, the long-time system stability and manufacturability is a daunting task for conventional bulk-crystal as the system complexity increases. To this end, the generation of non-classical light in monolithically integrated chips is of vital importance for large-scale implementations [8–12].

To date, a mass of components has been integrated onto a single silicon chip, realizing both entangled photons generation and coherent control [13–16]. There has been a growing interest in AlGaAs/GaAs based semiconductor material recently, because its mature fabrication technology for devices, such as lasers and modulators, and very large second order non-linearity [17–27]. Among them, the Bragg reflection waveguide (BRW) structure is appealing for developing turn-key devices for quantum applications. Phase matching (PM) in the waveguide is achieved by using total internal reflection (TIR) modes and quasi-bounded BRW modes, where BRW modes are formed by transverse Bragg reflections at the interface between core and period cladding layers and TIR modes are guided through internal reflection between high- and low-index claddings. The BRW sources have been used for several applications, such as generating different types of photon pair generation [28–30] and distributing entanglement in multiuser quantum network [31, 32]. Traditionally, the perfect transverse quarter-wavelength cladding condition is proposed to simplify the theoretical analysis. In fact, the structure may have higher modal overlap in non-ideal quarter-wavelength (NIQW) cases [33].

Here, we design and fabricate a NIQW BRW sample with high figure-of-merit modal overlap by using high-index core layer, which is different from the usual design, and can provide a way for the research of high efficiency multifunctional semiconductor non-linear devices. The general expressions for modes intensity profiles and dispersion equation in NIQW cases are deduced. According to the analytical results, the influence of core layer aluminium concentration on modes properties and three types of SPDC processes are analyzed. Finally, we experimentally characterize the three PM types and their bright spectral brightness of the real NIQW sample.

2 Mode equations of the BRW structure

We first consider a one-dimensional (1D) BRW structure where the core layer is surrounded by periodic claddings. The core layer has refractive index n_c and thickness t_c , while the cladding consists of

index n_1 and n_2 ($n_1 > n_2$) with thickness a and b respectively. The period is $\Lambda = a + b$ and the waveguide is symmetric about the center of the Bragg stack position, i.e., $n(x) = n(-x)$, consequently guiding modes have either even or odd symmetry. For simplicity, we take the lowest-order TE and TM modes as examples and concentrate on the $x \geq 0$ region, the high-order modes can be processed in a similar way. We assume the modes propagate along z direction and $\frac{\partial}{\partial y} = 0$, then the field envelop (without normalization) can be written in the form [34]

$$\begin{aligned}
 E_y(x) &= \begin{cases} \cos(k_c x), & 0 \leq x \leq \frac{t_c}{2}, \\ E_K \left(|x| - \frac{t_c}{2} \right) \exp \left[iK \left(|x| - \frac{t_c}{2} \right) \right], & x > \frac{t_c}{2}, \end{cases} \quad \text{TE} \\
 H_y(x) &= \begin{cases} \cos(k_c x), & 0 \leq x \leq \frac{t_c}{2}, \frac{n_1^2 k_2}{n_2^2 k_1} < 1, \\ \sin(k_c x), & 0 \leq x \leq \frac{t_c}{2}, \frac{n_1^2 k_2}{n_2^2 k_1} > 1, \\ H_K \left(x - \frac{t_c}{2} \right) \exp \left[iK \left(x - \frac{t_c}{2} \right) \right], & x > \frac{t_c}{2}, \end{cases} \quad \text{TM} \quad (1)
 \end{aligned}$$

where K is the Block wave vector, $k_c = k_0 \sqrt{n_q^2 - n_{eff}^2}$ is the transverse wave vector in the core layer, and k_0 and n_{eff} are the free-space wave vector and effective refractive index respectively. The electric field of TM can be solved by Maxwell's curl equations $E_x(x) = \beta/\omega n^2 H_y(x)$. From the Floquet theorem, $E_K(x)$ and $H_K(x)$ are periodic with Λ , and the electric and magnetic fields in the n th unit cell are

$$\begin{aligned}
 E_n(x) &= \begin{cases} a_{En} \cos \left[k_1 \left(x - \frac{t_c}{2} - n\Lambda \right) \right] + b_{En} \sin \left[k_1 \left(x - \frac{t_c}{2} - n\Lambda \right) \right], & n\Lambda \leq x - \frac{t_c}{2} \leq n\Lambda + a, \\ c_{En} \cos \left[k_2 \left(x - \frac{t_c}{2} - n\Lambda - a \right) \right] + d_{En} \sin \left[k_2 \left(x - \frac{t_c}{2} - n\Lambda - a \right) \right], & n\Lambda + a \leq x - \frac{t_c}{2} \leq (n+1)\Lambda, \end{cases} \\
 H_n(x) &= \begin{cases} a_{Hn} \cos \left[k_1 \left(x - \frac{t_c}{2} - n\Lambda \right) \right] + b_{Hn} \sin \left[k_1 \left(x - \frac{t_c}{2} - n\Lambda \right) \right], & n\Lambda \leq x - \frac{t_c}{2} \leq n\Lambda + a, \\ c_{Hn} \cos \left[k_2 \left(x - \frac{t_c}{2} - n\Lambda - a \right) \right] + d_{Hn} \sin \left[k_2 \left(x - \frac{t_c}{2} - n\Lambda - a \right) \right], & n\Lambda + a \leq x - \frac{t_c}{2} \leq (n+1)\Lambda, \end{cases} \quad (2)
 \end{aligned}$$

where $j = E$ or H represent the non-zero field components $E_y(TE)$ and $H_y(TM)$, a_{jn} (b_{jn}) and c_{jn} (d_{jn}) ($j = E/H$), are the incident (reflected) amplitudes in n_1 and n_2 regions respectively. With the transfer matrix method and continuous condition at the boundaries, one can obtain

$$\begin{aligned}
 \begin{pmatrix} a_{E_{n+1}} \\ b_{E_{n+1}} \end{pmatrix} &= \begin{bmatrix} \cos(k_2 b) & \sin(k_2 b) \\ -\frac{k_2}{k_1} \sin(k_2 b) & \frac{k_2}{k_1} \cos(k_2 b) \end{bmatrix} \begin{pmatrix} c_{E_n} \\ d_{E_n} \end{pmatrix} \\
 &= \begin{bmatrix} A_E & B_E \\ C_E & D_E \end{bmatrix} \begin{pmatrix} a_{E_n} \\ b_{E_n} \end{pmatrix} \quad (3)
 \end{aligned}$$

and

$$\begin{aligned}
 \begin{pmatrix} a_{H_{n+1}} \\ b_{H_{n+1}} \end{pmatrix} &= \begin{bmatrix} \cos(k_2 b) & \sin(k_2 b) \\ -\frac{n_1^2 k_2}{n_2^2 k_1} \sin(k_2 b) & \frac{n_1^2 k_2}{n_2^2 k_1} \cos(k_2 b) \end{bmatrix} \begin{pmatrix} c_{H_n} \\ d_{H_n} \end{pmatrix} \\
 &= \begin{bmatrix} A_H & B_H \\ C_H & D_H \end{bmatrix} \begin{pmatrix} a_{H_n} \\ b_{H_n} \end{pmatrix} \quad (4)
 \end{aligned}$$

where

$$\begin{aligned}
 A_E &= \cos(k_1 a) \cos(k_2 b) - \frac{k_1}{k_2} \sin(k_1 a) \sin(k_2 b) \\
 B_E &= \sin(k_1 a) \cos(k_2 b) + \frac{k_1}{k_2} \cos(k_1 a) \sin(k_2 b) \\
 C_E &= -\sin(k_1 a) \cos(k_2 b) - \frac{k_2}{k_1} \cos(k_1 a) \sin(k_2 b) \\
 D_E &= \cos(k_1 a) \cos(k_2 b) - \frac{k_2}{k_1} \sin(k_1 a) \sin(k_2 b)
 \end{aligned} \tag{5}$$

and

$$\begin{aligned}
 A_H &= \cos(k_1 a) \cos(k_2 b) - \frac{n_2^2 k_1}{n_1^2 k_2} \sin(k_1 a) \sin(k_2 b) \\
 B_H &= \sin(k_1 a) \cos(k_2 b) + \frac{n_2^2 k_1}{n_1^2 k_2} \cos(k_1 a) \sin(k_2 b) \\
 C_H &= -\sin(k_1 a) \cos(k_2 b) - \frac{n_1^2 k_2}{n_2^2 k_1} \cos(k_1 a) \sin(k_2 b) \\
 D_H &= \cos(k_1 a) \cos(k_2 b) - \frac{n_1^2 k_2}{n_2^2 k_1} \sin(k_1 a) \sin(k_2 b)
 \end{aligned} \tag{6}$$

Furthermore, the periodicity of the electric field can be expressed as

$$\begin{pmatrix} a_{jn+1} \\ b_{jn+1} \end{pmatrix} = \exp(iK_j \Lambda) \begin{pmatrix} a_{jn} \\ b_{jn} \end{pmatrix} \tag{7}$$

Combing Eqs 3, 4, 7, we have

$$\exp(iK_j \Lambda) = \frac{A_j + D_j}{2} \pm \sqrt{\left[\frac{A_j + D_j}{2}\right]^2 - 1} \tag{8}$$

and

$$\begin{pmatrix} a_{jn} \\ b_{jn} \end{pmatrix} = \begin{pmatrix} B_j \\ \exp(iK_j \Lambda) - A_j \end{pmatrix} = \exp(-inK_j \Lambda) \begin{pmatrix} a_{j0} \\ b_{j0} \end{pmatrix} \tag{9}$$

The coefficients in the first layer of the periodical structures can be deduced by the continuity of fields at the core-cladding interface,

$$\begin{pmatrix} a_{E0} \\ b_{E0} \end{pmatrix} = \begin{pmatrix} \cos(k_c t_c / 2) \\ -\frac{k_c}{k_1} \sin(k_c t_c / 2) \end{pmatrix} \tag{10}$$

$$\begin{pmatrix} a_{H0} \\ b_{H0} \end{pmatrix} = \begin{cases} \begin{pmatrix} \cos(k_c t_c / 2) \\ -\frac{n_1^2 k_c}{n_2^2 k_1} \sin(k_c t_c / 2) \end{pmatrix}, & \frac{n_1^2 k_2}{n_2^2 k_1} < 1 \\ \begin{pmatrix} \sin(k_c t_c / 2) \\ \frac{n_2^2 k_1}{n_1^2 k_c} \cos(k_c t_c / 2) \end{pmatrix}, & \frac{n_1^2 k_2}{n_2^2 k_1} > 1 \end{cases} \tag{11}$$

Finally, the mode dispersion equation can be obtained by the ratio between the coefficients. Although the guiding mechanisms are distinct, the TIR modes can be regarded as special modes confined by the Bragg reflection at the interfaces,

i.e., $n_{eff} > n_2$, so the waveguide can still be modeled using the above derivations by substituting down converted frequencies [18]. In order to tailor BRW samples toward high conversion efficiencies, we perform numerical optimization on the thickness of each layer and its aluminium concentration in the BRW slab structures based on the 1D general eigen equation deduced, independent of whether the Bragg layers are perfect quarter-wavelength thick or not. The high modal overlap with degenerate type-II phase-matching process around 1,550 nm is set as the optimization goal. After that, the optimized structure contains a core $\text{Al}_{x_c}\text{Ga}_{1-x_c}\text{As}$ layer with $x_c = 0.13$ and thickness of 230 nm, sandwiched in a Bragg stack made of alternative 127 nm high ($x_a = 0.33$) and 622 nm low ($x_b = 0.76$) index layers [35]. The corresponding refractive indices are extrapolated from Ref. [36]. However, optimizing the modes of BRWs to remain phase matched with TIR modes is not straightforward, as an imperfection of the fabrication process may increase the absorption of the BRW modes when it approaches the core bandgap. Therefore, the effects of refractive index (aluminium concentration) change to the core layer need to be quantified. The influence of core layer aluminium concentration on the absorption wavelength of core layer and phase matching processes as well as modal overlap in type-II process is shown in Figure 1A. It shows that with the increase of x_c , the absorption wavelength and modal overlap decrease. The PM wavelength decreases slightly at first and then increases. When the absorption wavelength is close to the PM wavelength, the overlap is maximum. This is associated with bringing the operating point of the device closer to the band gap in $\text{Al}_{x_c}\text{Ga}_{1-x_c}\text{As}$, which increases the confinement of the BRW modes. To avoid the photon-absorption may be incurred by the uncertainty of molecular beam epitaxy (MBE) process while maintaining a large modal overlap, we respectively choose $x_c = 0.17$, $x_a = 0.28$ and $x_b = 0.72$ in fabricating our real sample. The sample is grown along the [001] crystal axis with a width of 5.3 μm and an etching deep of 4.17 μm . The cross-sections of the proposed structure are shown in Figures 1B,C, with the loss contours are distributions of the TE (B) and TM (C) BRW modes which are calculated by using the finite-element method (commercial software COMSOL simulation). By using the analytical equation deduced above, the dispersion diagrams of the three parametric processes for interacting modes are shown in Figure 2. The designed PM wavelengths are between 1,540 nm and 1,570 nm, and the type-II operating point is around 1,550 nm which can be used for generating polarization entanglement directly due to the little material birefringence [28].

3 Experiment

In experiments, we fabricate a 2 mm-long AlGaAs BRW ridge waveguide with six periods upper (low) mirrors

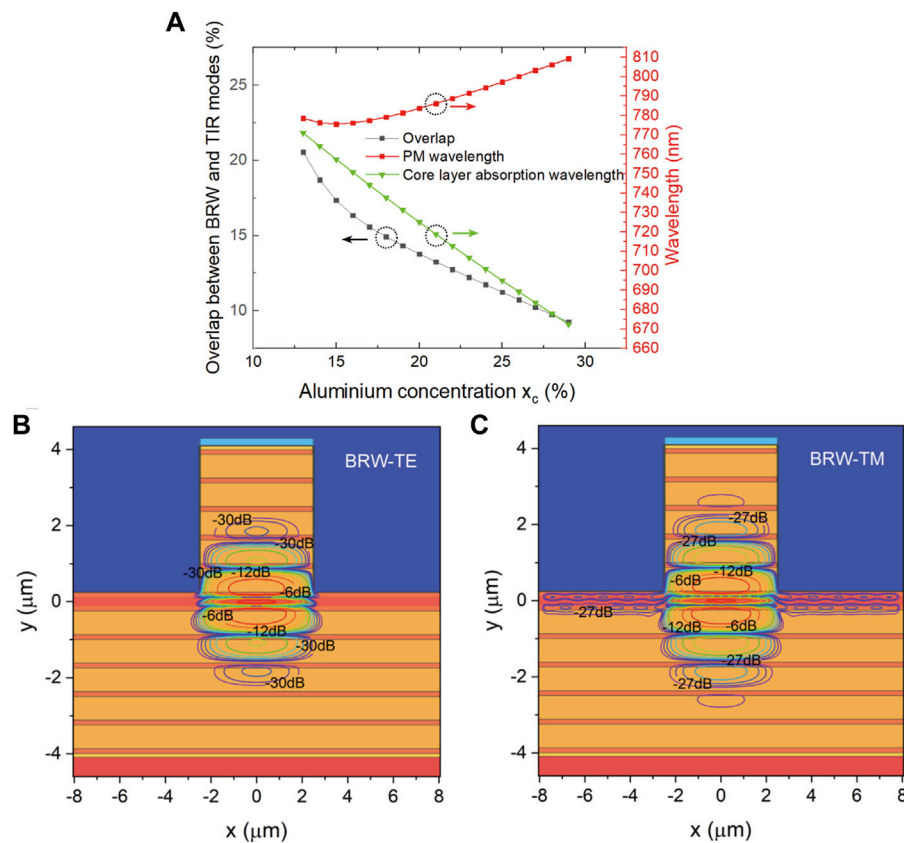


FIGURE 1 (A) The dependence of overlap factor and PM wavelength between pump and down converted fields on core layer aluminium concentration. The contours are the calculated TE (B) and TM (C) BRW modes.

through MBE and wet chemical etching. The temperature of the waveguide can be stabilized by a temperature controller. To find the PM wavelengths, we first test the three PM processes of the sample by means of the second harmonic generation (SHG). A 0.1 mW tunable continuous semiconductor laser with a linewidth of 10 kHz is used as the fundamental light (FL). The FL is connected to a fiber optic beam splitter, one of which (1% power) goes to the optical spectrum analyzer (OSA) for wavelength detection and another port (99% power) is connected to the optical fiber polarization controller (FPC) and enters the waveguide through port a. The SHG light is collected at port b and entered into a single-photon detector with about 70% detection efficiency. The total fiber-chip-fiber loss is 8 dB. In our experiment, the highly versatile modal birefringence in BRW enabled the phase-matching of the three modalities [20, 24, 37] namely type-0: $\text{TM}_\omega + \text{TM}_\omega \rightarrow \text{TM}_{2\omega}$, type-I: $\text{TE}_\omega + \text{TE}_\omega \rightarrow \text{TM}_{2\omega}$ and type-II: $\text{TE}_\omega + \text{TM}_\omega \rightarrow \text{TE}_{2\omega}$. By varying the wavelength and polarization of FL, we record the SHG output

power as a function of FL wavelength. As the results shown in Figure 3A, when the FL wavelength is tuned to 1,580.6 nm, a maximum SHG output power of 4.029 pW is obtained. Three resonance features at 1,551.7 nm, 1,559.2 nm and 1,580.6 nm, denote the pump wavelengths at which type-I, type-II and type-0 PM conditions are satisfied, respectively [24]. The discrepancy between theoretical and experimental results are mainly because the lateral confinement and fabrication errors. In addition, we measure the dependence of PM wavelength on temperature by varying the sample temperature from 17.5°C to 28°C for type-II process as an example. The operating wavelength is almost linearly increased from 1,558.5 nm to 1,560.75 nm, as shown by the black squares in Figure 3B. The line is a guide to the eye.

Following the SHG results, we demonstrate different types of SPDC processes utilizing a wavelength-tunable laser around 775 nm. As shown in Figure 4, the pump light is coupled into the waveguide at port c after passing through

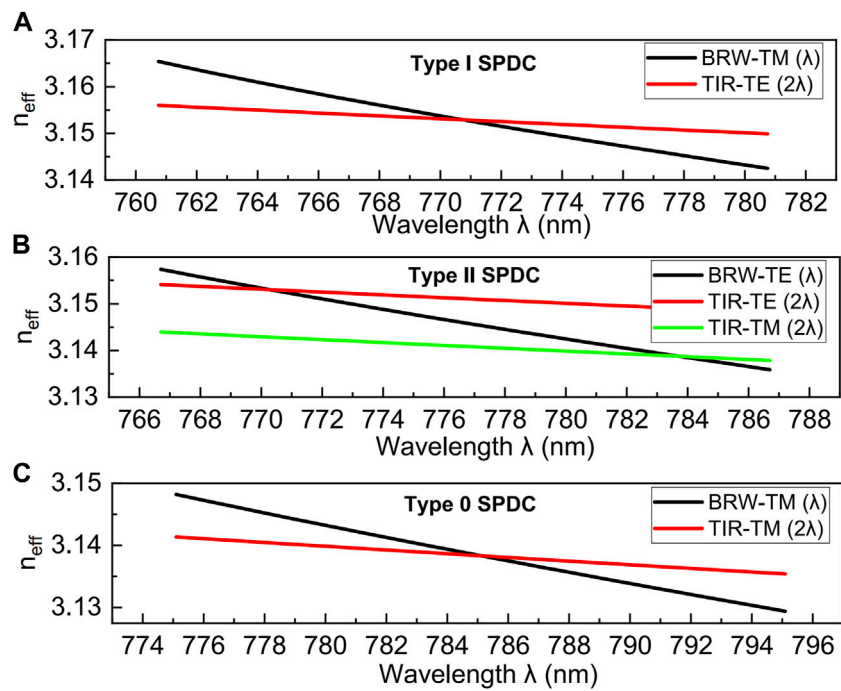


FIGURE 2 Dispersion curves of BRW and TIR modes for three parametric processes: Type-I (A), Type-II (B) and Type-0 (C).

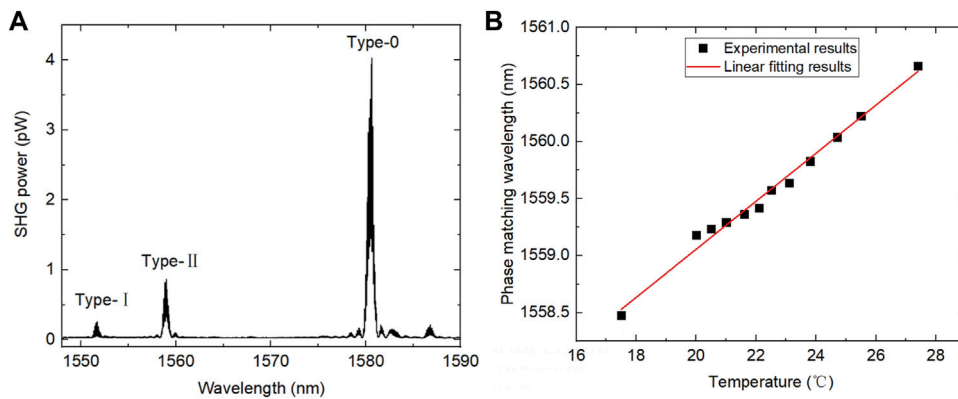


FIGURE 3 (A) The SHG tuning curves of the three PM schemes as a function of the FL wavelength. (B) The dependence of type-II PM wavelength on sample temperature. The line is a guide to the eye.

FPC2 to optimize the pump polarization. Fixing the temperature of waveguide at 20.08 $^{\circ}\text{C}$, we expect to obtain the required three kinds of frequency degenerate SPDC processes under different pump wavelengths. The signal and idler photons will be collected by port d, filtered by off-chip long wavelength pass filters to remove the pump, and

then enter a coarse wavelength division multiplexing (CWDM) with an extinction ratio of ~ 40 dB and a bandwidth of 18 nm for separation. Finally, the photons are detected by two InGaAs semiconductor single photon detectors with 10% detection efficiency, 1.2 kHz dark count rates, and a 5.2 μs dead time. The detector electrical signals

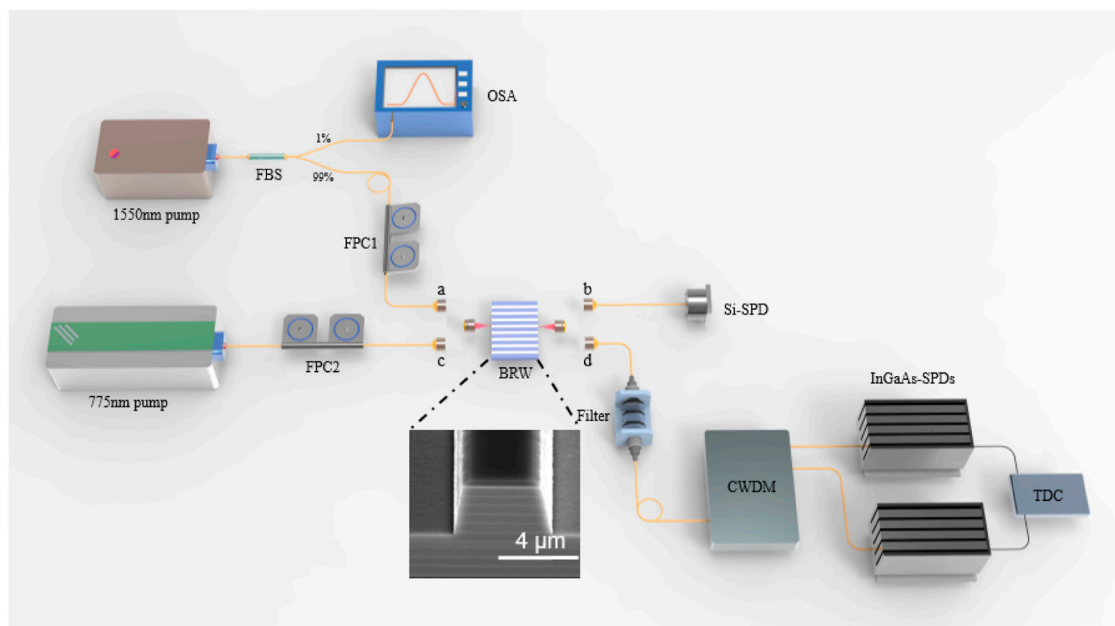


FIGURE 4

Schematic of the experiment setup for SHG and SPDC. Inset shows the scanning electron microscope image of the fabricated BRW sample. Abbreviations of components: BRW, Bragg reflection waveguide; FBS, fiber optic beam-splitter; FPC, fiber polarization controller; OSA, Optical Spectrum Analyzer; CWDM, Coarse wavelength division multiplexing; SPD, single photon detector; TDC, time-to-digital converter.

are collected by a time-to-digital converter (TDC). The correlation is measured as the coincidence counts (C.Cs) between entangled photons as a function of the arrival time difference with 2 minutes integration time and a coincidence window of 1 ns? In the diagram of Figures 5A–C, the three types SPDC results are shown. The pump power is set to be 0.57 mW before coupling into the chip. The generation rate of type-0 and II processes are about 101 Hz and 62 Hz, leading to a brightness of 4.35×10^7 pairs/s and 1.108×10^7 pairs/s, respectively, which are higher than those reported in Refs. [28, 29]. The uncorrelated background is due to the high noise generation rate. Potential noise sources in our system include the dark counts of the detectors and broadband photoluminescence [38]. Figure 5D illustrates the C.Cs and coincidences-to-accidentals ratio (CAR) as a function of the input pump power for type-0 process. The counts constantly increase when the input power is low, because the efficiency of SPDC scales linearly with the pump power. As the power increases, the C.Cs are saturated and the CAR decreases which results from the influence of increasing accidental C.Cs. The CAR is limited by the dark counts of the detectors at low power, and by the detrimental photoluminescence at high power. The SHG and

SPDC results imply that this BRW is potential for cascaded up- and down-conversion processes by virtue of off-the-shelf telecom optical components [39–41].

To illustrate the broadband SPDC in the sample, we measure the continuous emission spectra of type-II (Figure 6A) and type-0 (Figure 6B) processes for the signal and idler photons by using a multi-channel 100 GHz WDM (black points in 6A and 6B) or a tunable filter (red points in 6A). Since the insertion losses are different for each channel, we measure them independently and infer counts obtained with the tunable filter by referring to the WDM's loss. We only record a subset of the data due to the limited filters within the transmission window. However, the energy conservation constraint of the SPDC process implies that the spectral extent should be symmetric around its degenerate wavelength, which implies a 3-dB spectral bandwidth of 105 nm and 67 nm for type-II and type-0 processes respectively. The solid lines are simulated results and the uncertainties denote the standard deviations from the Poisson distribution of the raw photon counts. This broadband source can be used for multiuser quantum network by carving the spectrum into a series of slices and multiplexing them [42–45].

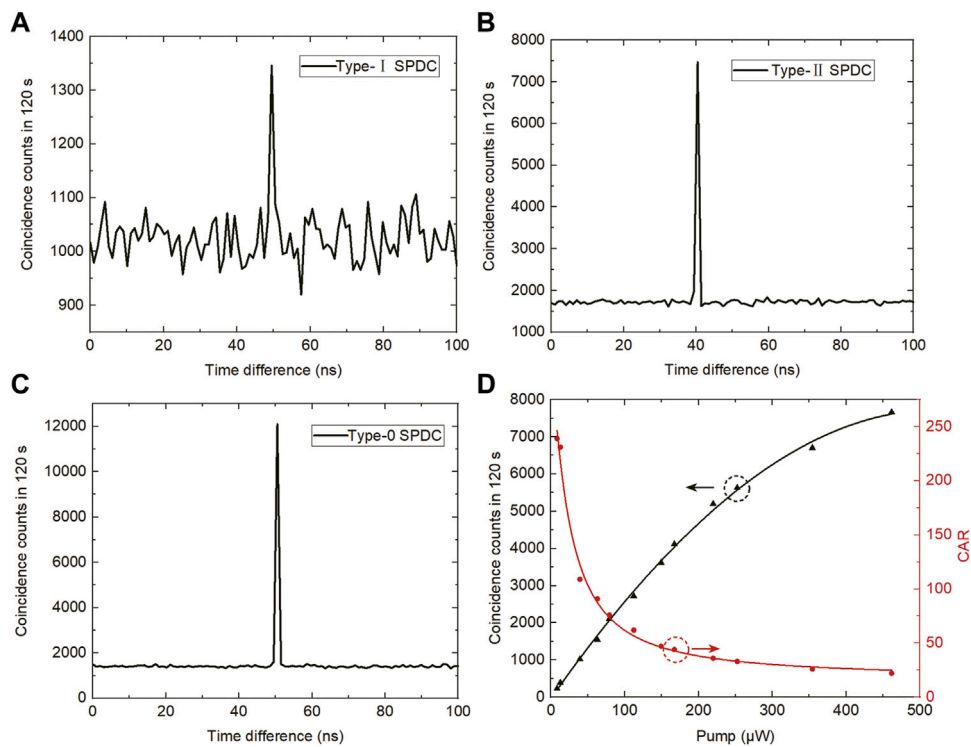


FIGURE 5 Histograms of the coincidence measurements for type-I (A), type-II (B) and type-0 (C) (D) Coincidence counts of type 0 as a function of the average input pump power. The points are experimental data, and the curves are fits. All the data are raw counts and no background counts subtracted.

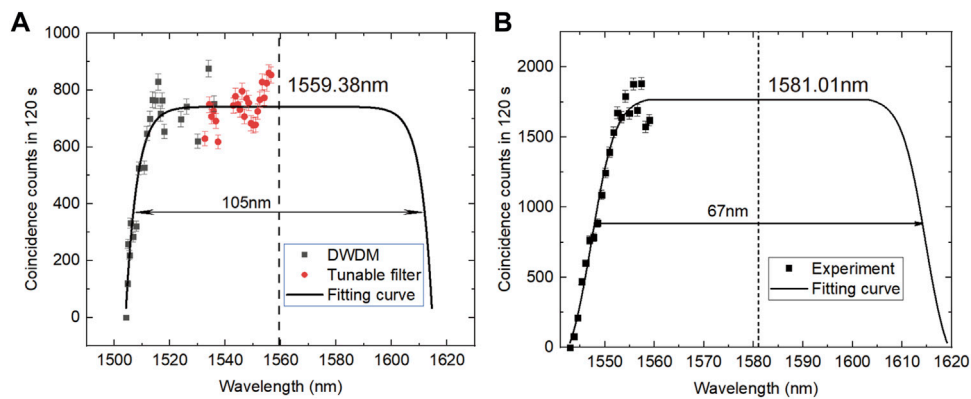


FIGURE 6 Experimental and simulated spectral brightness of the broadband type-II (A) and type-0 (B) SPDC.

4 Conclusion

In conclusion, we have derived general expressions for eigen equation in a one-dimensional BRW independent of

whether each cladding layer has an ideal quarter-wavelength thickness or not. The analytical results are used to simulate three types of SPDC processes with high modal overlap. Experimentally, we fully characterize the light

source and demonstrate broad bandwidth entangled photons over more than 65 nm (100 nm) for type-0 (II) processes. With the advancements of fabrication technology, it is possible to integrate laser and wavelength demultiplexing/multiplexing module onto a single chip, providing a turn-key solution for the large-scale quantum communication network.

Data availability statement

The raw data supporting the conclusions of this article will be made available by the authors, without undue reservation.

Author contributions

BN and LL proposed this idea. LL and YL wrote the original manuscript. BN, CQ, XJ, and LL performed the experiment. CW and YL provided experimental assistance and suggestions. YK, TC and LL supervised the project.

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