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Free-electron terahertz radiation based on silicon gratings with in-plane waveguide emission

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We present a method utilizing the coupling between a pre-bunched electron beam and a silicon subwavelength grating to generate coherent terahertz waves. The grating that is connected to two opposite-traveling in-plane waveguides functions as a resonator. An example operating around 2 THz shows that, when the velocity and repetition frequency of the electron bunches respectively match the phase velocity and resonant frequency of the Bragg resonance in the grating, the strong electron-wave coupling leads to coherent radiation through the waveguide. The repetition frequency of the electron bunches can be halved by using its second harmonic to match the resonant frequency. This study might offer a potential approach for on-chip terahertz sources.

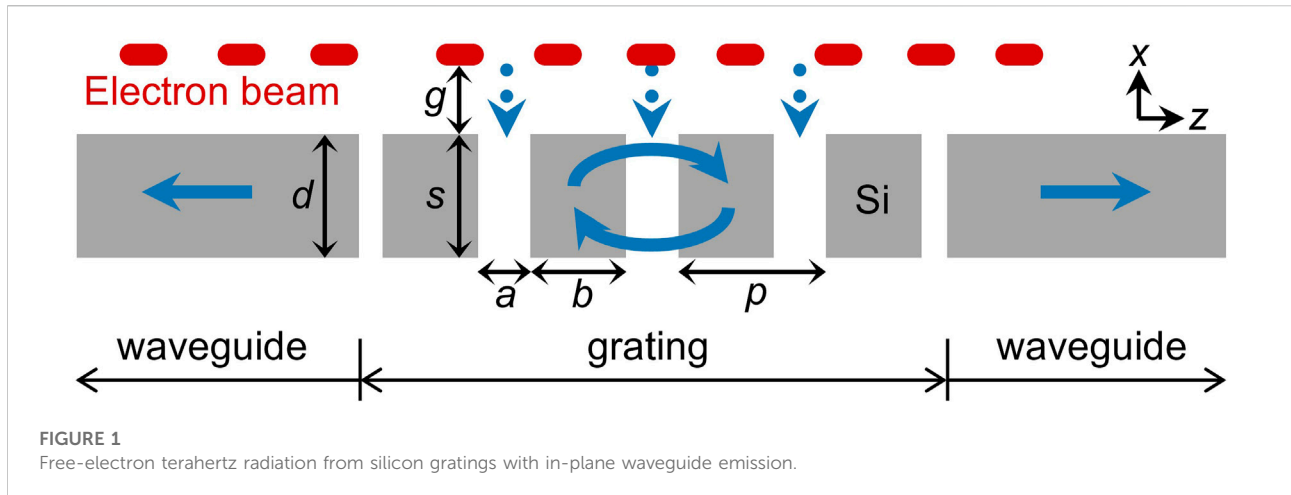
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free-electron radiation, terahertz wave, subwavelength grating, electron bunch, coherent emission

1 Introduction

In the past few decades, substantial progress has been achieved in developing science and technologies based on terahertz radiation (0.1–30 THz) due to its unique physical properties for a variety of applications in communication, imaging, and spectroscopy [1–3]. The performance of terahertz sources, which is traditionally linked to the concept of the terahertz gap, has been significantly improved using electronic and photonic technologies [4–7]. Currently, great attention is paid to the quantum cascade laser (QCL). It can work with an efficiency higher than 1%, but its practical application is severely limited by the low operation temperature [4]. Free-electron radiation sources, e.g., backward wave oscillators (BWOs) and free-electron lasers (FELs), have been shown to be superior at handling high power [8]. BWOs can deliver power in the range of 50 mW at sub-THz to about 2 mW at 2 THz, but it is very difficult to operate at higher frequencies owing to the great challenges in reliable fabrication [9, 10]. On the other hand, FELs, in which radiation is generated as an electron bunch passes through a magnetic structure, can achieve terahertz powers of 100 W, but they suffered from their tremendous cost and large size. Seeking new method to develop terahertz radiation sources has been a pursuit of researchers.

Recently, the development of dielectric laser accelerators has attracted increasing interest and inspired new opportunities for applications using compact particle



accelerators [11–13]. Using dielectrics with a high breakdown threshold instead of metals to enable a higher accelerating gradient for particle acceleration, the cost and size of accelerators can be reduced by orders of magnitude [14]. Besides electron acceleration, this method has been demonstrated the capability of electron bunching and focusing [12, 15–17]. Such concept has been extended to terahertz, promising an attractive particle accelerator on chip that can generate a train of electron bunches with terahertz repetition rate [18–21]. It is interesting to see if it is possible to realize a coherent terahertz radiation source on chip by using such an electron beam.

Cherenkov radiation and Smith-Purcell radiation are two mechanisms that can generate electromagnetic waves without destroying the electron beam and manipulate the radiation characteristics by designing the structures, making them rather attractive for many applications [17, 22–24]. In order to facilitate the integration of radiators and dielectric accelerators on chip, it is desirable that they have similar structures. So far, gratings and photonic crystals, which are extensively used in dielectric accelerators [14], have also been studied for radiation generation, e.g., 1D subwavelength gratings (SWG) for Smith-Purcell radiation [25], and 2D photonic crystals for Cherenkov radiation [26, 27]. In those radiators, the formation of the radiation that normally spreads out at a certain angle is well understood [28]. However, for downstream applications of such radiators, in order to improve the utilization efficiency, a more directional wave confined in a waveguide might be preferable [29]. It is well known that the SWG itself can serve as a waveguide or resonator for confinement of electromagnetic waves, but the coupling between the electron and the SWG waveguide or resonator is less clear [30–34]. If electrons can directly couple energy into the guided mode in a grating, an on-chip terahertz source could become possible by outputting the energy through the slab waveguides attached to the grating ends.

Here, we present a method in which the coupling between a pre-bunched electron beam and a silicon SWG is utilized to generate terahertz wave. We first introduce the guideline for designing the SWG for such purpose. Then, we perform particle-in-cell (PIC) simulation to understand the characteristics of the radiator driven by a pre-bunched electron beam. We show that the electron-wave coupling leads to coherent terahertz radiation through the waveguides connected to the SWG. Such dielectric radiator is ready to be integrated with the terahertz dielectric accelerator. Besides, the output wave confined by the slab waveguide has the advantage of facilitating integration with down-stream terahertz components.

2 Model description

Figure 1 schematically illustrates our method of employing silicon SWGs driven by a pre-bunched electron beam to generate terahertz waves. The two-dimensional model is adopted in the analysis for simplicity. The dielectric grating comprises of a series of silicon bars, separated by vacuum gaps. The thickness and width of the bar, the width of the air gap, the SWG period the period number and the beam-grating distance are s , b , a , p , N and g , respectively. $x = 0$ is located at the upper surface of the SWG. There is a slab waveguide of thickness d on either side of the SWG. The SWG is designed to operate with a Bragg resonance, which is essentially a stationary non-propagating mode with a vanishing group velocity. When an electron moves over the grating with a velocity that matches the phase velocity of the Bragg resonance, strong coupling occurs. When a pre-bunched electron beam, in which each bunch is shorter than the emitted radiation period, moves over the grating, the radiation fields of the different electrons in one bunch can add coherently in phase [28]. If the repetition frequency of the electron bunches f_b or its higher harmonics match the resonant frequency f_0 of the Bragg resonance, coherent radiation can be emitted at f_0 due to the

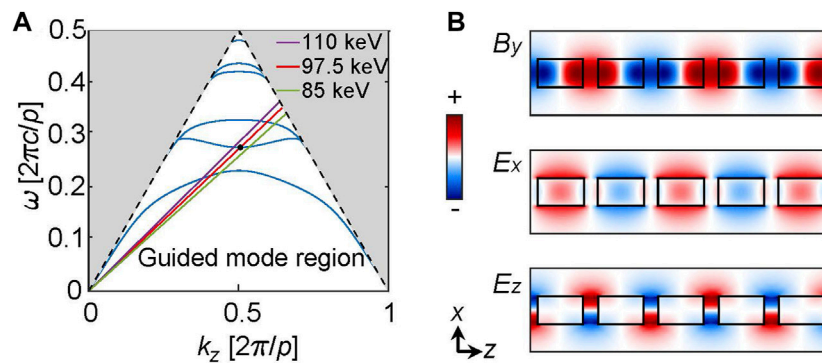


FIGURE 2

(A) Dispersion diagram of the SWG calculated by CST. The gray area above the black dashed lines are the radiation continuum. The 85, 97.5, 110 keV electron lines are indicated by the green, red, and purple solid lines, respectively. (B) The B_y , E_x and E_z field profiles of the Bragg resonance at the black dot in (A). The silicon bars are depicted by the rectangles with solid black borders.

superradiant effect [35]. The radiation power increases with the number of electron bunches until steady states. Meanwhile, part of the energy is bidirectionally coupled into the slab waveguides connected to the grating as output.

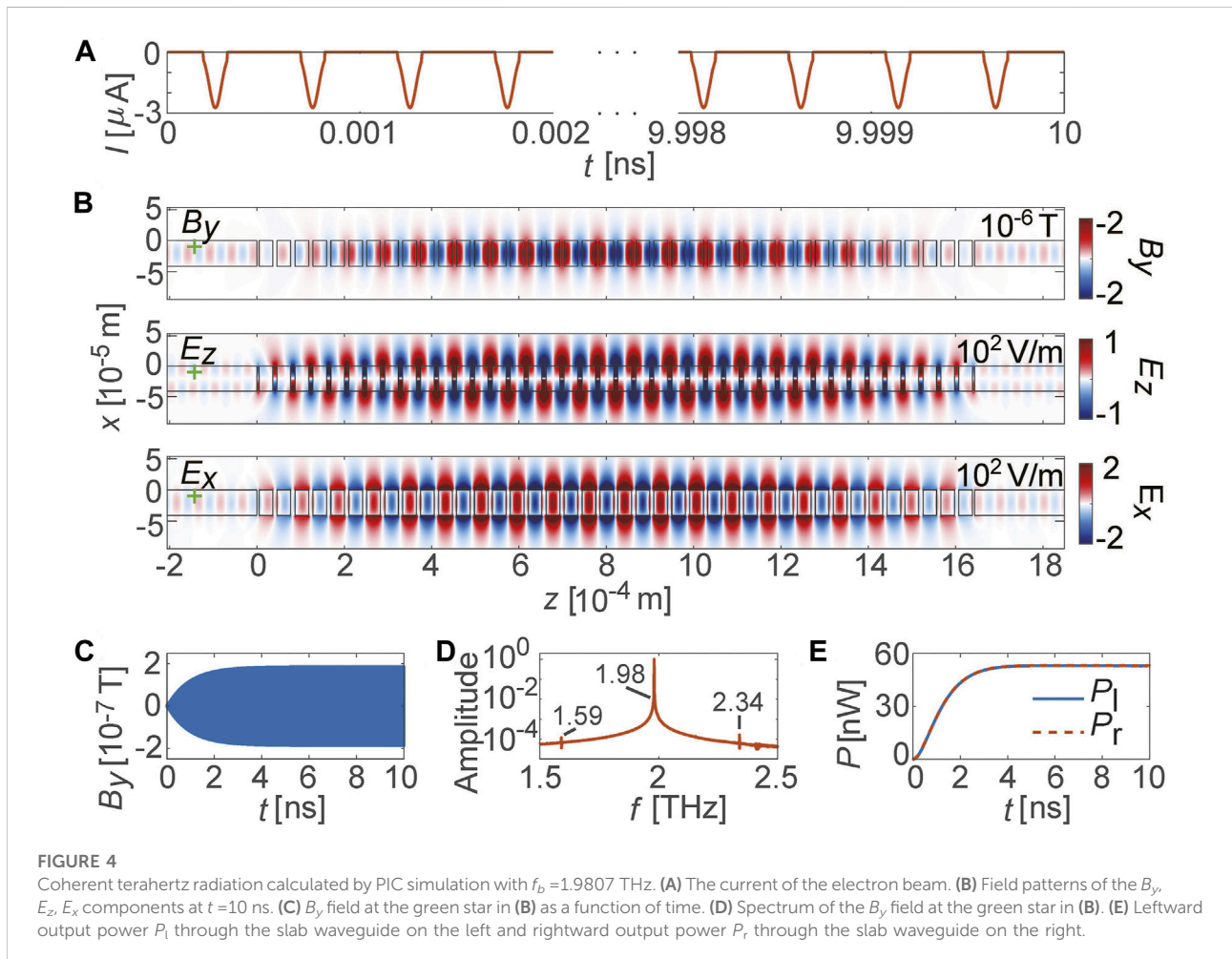
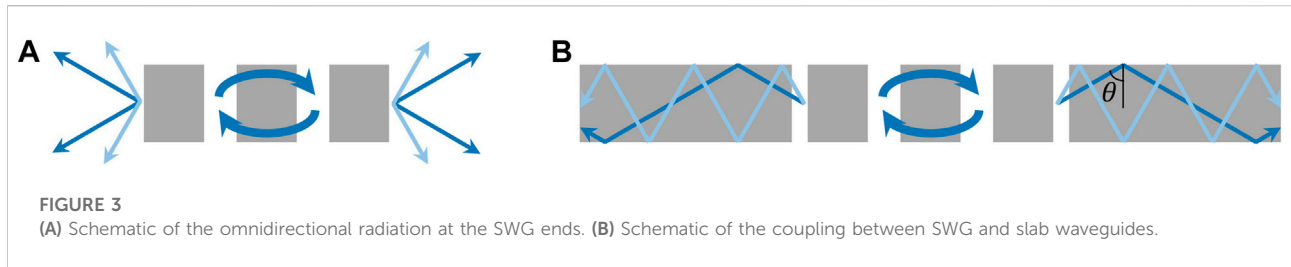
The dispersion diagram is a key property to calculate when studying the electron-wave coupling. As an example, we first consider an infinitely long SWG with thickness being $s = p$ and dutycycle $b/p = 0.76$. By finding the eigenmodes with different Bloch phase shift for the periodic boundary conditions in the z direction, we can obtain the dispersion diagram with the CST software, as shown in Figure 2A. The diagram can be divided into two operation regions [36, 37]: the radiating continuum above the dashed lines, where the fields are extended in the region above or below the grating [38]; the guided mode region, where the fields above or below the grating are evanescent [33, 34, 39]. For the Smith-Purcell radiation, the operation point is located in the radiation continuum. In this article, we utilize the resonance in the guided mode region to generate Cherenkov radiation.

In Figures 2A, A Bragg resonance can be found at $k_z = \pi/p$ for each dispersion curve [29]. For instance, we choose the second guided mode as the operation mode. The Bragg resonance of the second guided mode is located at the intersection point of the 97.5 keV electron line and the second dispersion curve, which is marked by the black dot in Figure 2A. On its left side, the mode works as a backward wave (e.g., the intersection point of the 110 keV electron line and the second dispersion curve). While on its right side, the mode works as a forward wave (e.g., the intersection point of the 85 keV electron line and the second dispersion curve). Figure 2B further illustrates the field profiles of the Bragg resonance, indicating that a TM_0 mode is excited in the SWG, with the B_y component being symmetric about the $x = -s/2$ plane. In the z direction, the half spatial period of the fields is equal to the grating period p .

The above simulation shows that a Bragg resonance can be obtained with an infinite SWG. In practice, we can only use an SWG with a finite period number N . In this case, the side-leakage loss at the SWG ends in the z direction is inevitable, which manifests as omnidirectional radiation, as shown in Figure 3A. With a slab waveguide connected to each SWG end, a majority of the radiation could propagate into the slab. Among them, if the incident angle (θ) of the radiation at the slab-air boundary is larger than the critical angle for total internal reflection, it will be confined in the slab waveguide and transmitted downstream, as shown in Figure 3B. Such bi-directional coupling into those in-plane waveguides can be leveraged as output [40–43]. In the following, the grating period is set to be $p = 41 \mu\text{m}$, so that the resonant frequency of the Bragg resonance f_0 is about 1.98 THz. The period number is set to be $N = 40$. In this case, the finite SWG serves as a cavity and the external quality factor is calculated to be 7917 by using CST Microwave Studio. Below we will show that the electron-wave coupling can generate coherent terahertz waves output through the slab waveguides.

3 Results

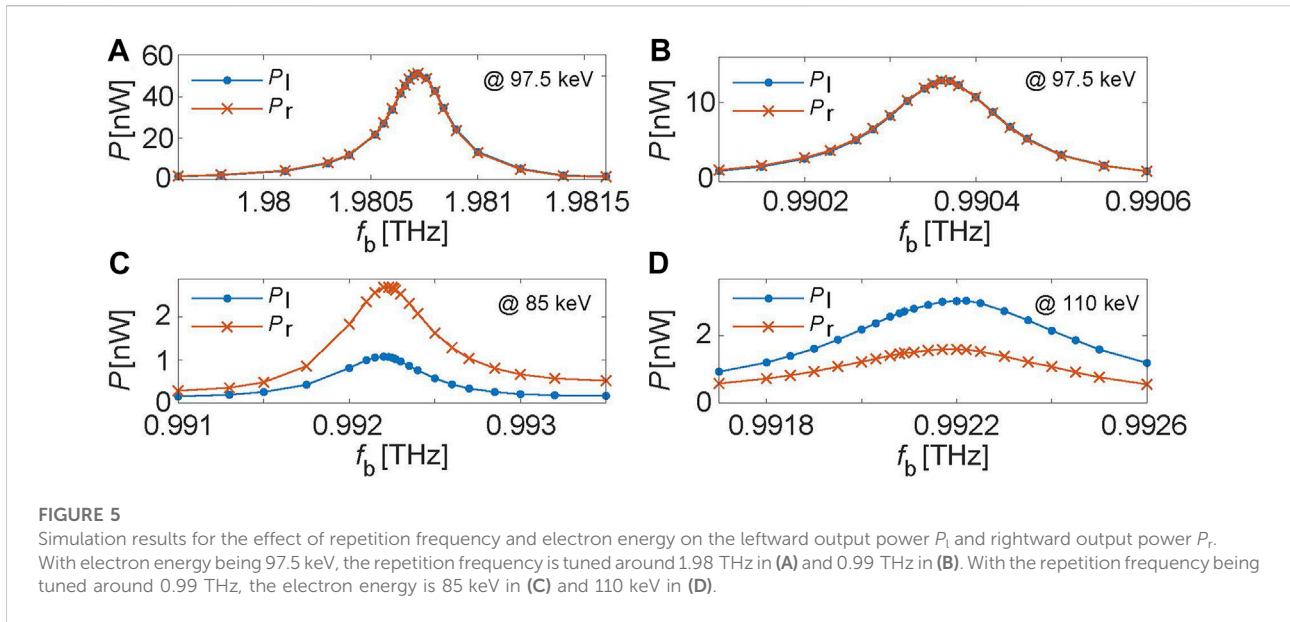
For PIC simulations, a two-dimensional finite-difference-time-domain code CHIPIC-2D is used [44]. The grating dutycycle, thickness, and period remain the same as that in Section 2. The pre-bunched beam is set to be uniform in the x direction, with beam thickness $d = 5.5 \mu\text{m}$. The beam-grating distance is set to be $g = 2.7 \mu\text{m}$. Assuming the width of the system is 1 mm in the y direction, the current of the pre-bunched electron beam is shown in Figure 4A, in which all electron bunches follow the same truncated Gaussian distribution. The peak current density of the beam is 0.05 A/cm^2 . The repetition frequency of electron bunches is set to be f_b , which is a key



parameter that can be tuned in the simulation. To avoid electron bombardment on grating, an external longitudinal magnetic field of 0.1 T is used to confine the beam. In practice, to further reduce surface charging, the dielectric grating can be coated with a thin metallic layer.

Firstly, we set the electron energy to be 97.5 keV. The repetition frequency of the electron bunches f_b is fine-tuned around 1.98 THz, while the truncated Gaussian distribution of each electron bunch remains unchanged. The output power is

found to reach maximum at 1.9807 THz, in agreement with the resonant frequency calculated in Section 2. Figure 4B shows the calculated B_y , E_z and E_x components at $f_b = 1.9807$ THz, where the field patterns in the SWG are consistent with that calculated by CST in Figure 2. Figures 4C,D show the B_y field at the green star in Figure 4B as a function of time and its spectra, respectively. The output fields saturate at $t = 4$ ns, and its frequency is exactly the same as the repetition frequency of the electron bunches. It is noticeable that there are another two peaks at about 1.59 THz



and 2.34 THz. This is because the 97.5 keV electron line intersects with not only the second guided mode, but also the first and the third. These two peaks are much lower since they are far from the repetition frequency of the electron bunches f_b . Assuming the system's thickness is 1 mm in the y direction, the leftward output power P_l through the slab waveguide on the left and the rightward output power P_r through the slab waveguide on the right are shown in Figure 4E. Here, P_l is found to be approximately the same as P_r . The total power through two slab waveguides is 102.36 nW (per millimeter in the y direction) and the corresponding beam-to-wave power conversion efficiency is 2.59×10^{-6} . Thanks to the superradiant effect, the radiation is coherent and is much stronger than the fields induced by a direct-current electron beam (See Supplementary Material for more information).

We then change the repetition frequency of the electron bunches. With a repetition frequency of f_b , the electron beam's spectrum includes not only the fundamental repetition frequency but also its higher harmonics. Consequently, it is interesting to know whether the repetition frequency can be halved by using its second harmonic to match the resonant frequency, with the output frequency remaining unchanged. When the truncated Gaussian distribution of each electron bunch remains unchanged, we fine-tune the repetition frequency of the electron bunches f_b around 0.99 THz. The output power is found to reach maximum when the repetition frequency equals half the resonant frequency, i.e., $f_b = f_0/2$. Such results clearly show that coherent wave can be generated even when the repetition frequency is halved. For clarity, Figures 5A,B compare the output power P_l and P_r when the repetition frequency f_b is tuned around 1.98 THz and 0.99 THz. The maximum output power around 1.98 THz is higher than that around 0.99 THz.

This is caused by the fact that the fundamental-harmonic component of the pre-bunched beam at f_b is stronger than the second-harmonic component at $2f_b$.

The effect of electron energy is then investigated. Figures 5C,D show the output power as a function of repetition frequency that is tuned around 0.99 THz when the electron energy is changed to 85 keV and 110 keV, respectively. In both cases, the output power reaches its maximum at around 0.9922 THz, which is higher than that for 97.5 keV electrons. This is in agreement with the fact that the frequencies at the intersections of the 85 and 110 keV electron lines with the second dispersion curve are higher than the resonant frequency of the Bragg resonance in Figure 2. The maximum output power is lower than that obtained by 97.5 keV electrons, indicating that the Bragg resonance can enable stronger beam-wave coupling. Notably, when the electron energy is 85 keV, the leftward power is smaller than the rightward power. When the electron energy is 110 keV, on the other hand, the leftward power becomes higher than the rightward power. This is caused by the difference in the mode nature: 85 keV electrons use a forward mode, while 110 keV electrons use a backward mode.

Next, the beam-grating distance g is varied in the simulation, with the other parameters being the same as in Figure 4. Figure 6A show that the leftward output power P_l decreases as the distance g increases. Such phenomena can be explained by considering the effect of incident fields from electrons. For a 2D model, the current density of a single charge q moving with velocity v_0 can be given by $J_z(x, z, t) = qv_0\delta(x-g)\delta(z-v_0t)$ [45]. Using Fourier transform, we can obtain the current density in the frequency domain, i.e., $J_z(x, z, \omega) = q\delta(x-g)\exp(-ik_{z0}z)$, with $k_{z0} = \omega/v_0$. The incident magnetic field can be written as $H_y = -\text{sign}(x-g)q/2 \cdot \exp[-\alpha \cdot \text{sign}(x-g)(x-g) - ik_{z0}z]$,

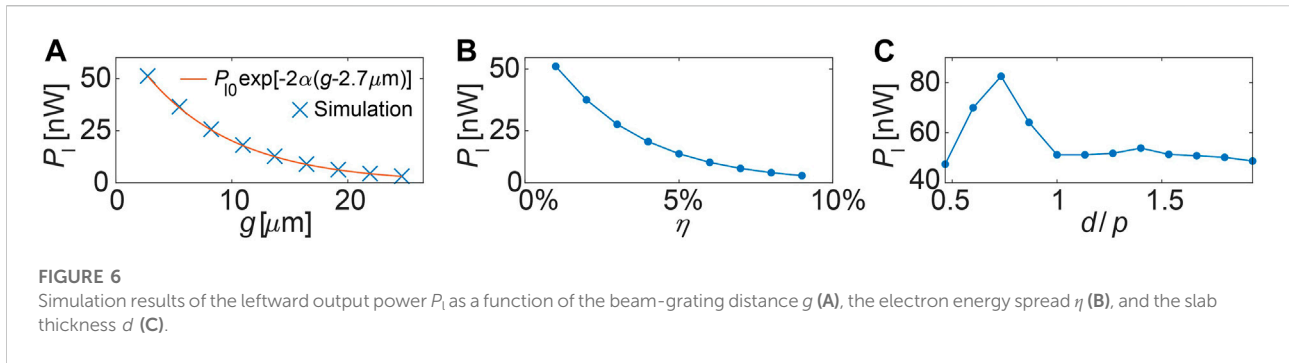


FIGURE 6 Simulation results of the leftward output power P_l as a function of the beam-grating distance g (A), the electron energy spread η (B), and the slab thickness d (C).

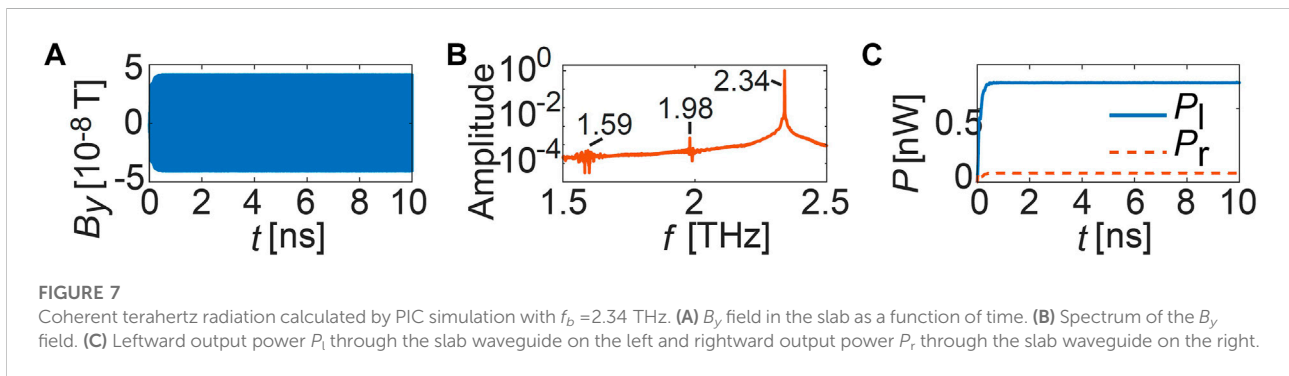


FIGURE 7 Coherent terahertz radiation calculated by PIC simulation with $f_b = 2.34$ THz. (A) B_y field in the slab as a function of time. (B) Spectrum of the B_y field. (C) Leftward output power P_l through the slab waveguide on the left and rightward output power P_r through the slab waveguide on the right.

where $\alpha = (k_{z0}^2 - \omega^2 \mu_0 \epsilon_0)^{0.5}$, ϵ_0 and μ_0 are the permittivity and permeability in vacuum. Such incident fields are bound at the electrons and decay exponentially in the x direction. Thus, when the distance g increases, the amplitude of the incident field at the grating surface decreases, leading to a decline in output power. This can be verified by the agreement between the simulated power P_l and the value of $P_{l0} \exp[-2\alpha(g - 2.7 \mu\text{m})]$, with P_{l0} being the simulated power for $g = 2.7 \mu\text{m}$ as shown in Figure 4E. Such results are also helpful when we consider a three-dimensional model that has an electron pencil-beam moving above a planar grating with a finite width in the y direction. Based on the dependence of output power on g as shown in Figure 6A, one can infer that the radiation in the grating are the strongest just beneath the beam. In the y direction, as the distance from the beam increases, the radiation will become weaker.

Notably, the above simulations use a mono-energetic electron beam. In order to study the effect of the initial energy spread (denoted by η) of the electron beam, which is inevitable in practice, we set the initial electron velocities to have a Maxwellian distribution, which is in agreement with the typical velocity distribution of electrons emitted from thermionic cathodes [46]. Figure 6B shows the leftward output power P_l as a function of the initial energy spread (η) of the electron beam, with the other parameters being the same as in Figure 4. One can see that the leftward output power P_l decreases as the initial

energy spread of the electron beam η increases. In order that the output power declines no more than 50%, the initial energy spread should not exceed 3%.

Then, the effect of the thickness (d) of slab waveguide is studied in the simulation, with the other parameters being the same as in Figure 4. When changing the slab thickness d , the slab center in the x direction is aligned with the grating center. Figure 6C shows the leftward output power P_l as a function of d . When d increases beyond the grating thickness s that is equal to the grating period p , the output power remains almost unchanged. When it decreases, the output power reaches its maximum at $d = 0.73p$. In this case, however, the different values of slab thickness d and grating thickness s may increase the difficulty in fabrication.

Although we focus on the second guided mode in the above simulations, the other guided modes can also be utilized. As an example, with the other parameters being the same as in Figure 4, the repetition frequency of the electron bunches is changed to 2.34 THz, which corresponds to the intersection point of the 97.5 keV electron line and the third dispersion curve. Figure 7 shows the B_y field at the green star in Figure 4B as a function of time and its spectra, and also the output power P_l and P_r as a function time. The output field saturates at $t = 0.5$ ns and its frequency is 2.34 THz. Here, the other two peaks are located at about 1.98 THz and 1.59 THz, corresponding to the second and

first guided mode, respectively. These two peaks are much lower than the highest one at 2.34 THz, indicating that unwanted mode can be suppressed by mismatching the repetition frequency of the electron bunches with the mode frequency.

4 Discussion

In conclusion, we have described a method to generate terahertz waves based on silicon SWGs with bi-directional emission into in-plane waveguides. We have shown that the coupling between a pre-bunched electron beam and the SWGs' Bragg resonance can generate coherent terahertz waves by matching the velocity and repetition frequency of the electron bunches respectively with the phase velocity and resonant frequency of the Bragg resonance. When the radiation frequency keeps unchanged, we also found that it is possible to reduce the repetition frequency of the electron bunches by using its higher harmonics to match the resonant frequency of the Bragg resonance.

The method investigated in this paper may be useful in future terahertz applications. The usage of silicon gratings in terahertz regime shows that the fabrication of the proposed structure is within reach of established fabrication techniques[47]. With the rapid development of structure-based dielectric accelerators [11–13, 18–20], the pre-bunched beam used to drive the dielectric SWG might be available in the near future. The integration of the dielectric accelerator and the radiator may enable an on-chip terahertz radiation source. The power produced by this method may be further improved increasing the peak current. It can operate at room temperature from sub-terahertz to terahertz by changing the working harmonics. Thus, it is a potential supplement to those existing sources that are widely used for terahertz spectroscopy and imaging [10, 48]. Compared with some other terahertz sources such as BWOs and QCLs, the efficiency of this method is relatively low due to the spontaneous nature of the emission. However, the fact that the electron beam is not destroyed in the process implies that those electrons can still be utilized for other purposes. Thus, such radiation source can be developed as a byproduct of dielectric acceleration. For example, the terahertz radiation can be used to assist early detection of skin cancer, and the electron beam can be used as a non-invasive treatment of skin cancer [4].

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Data availability statement

The raw data supporting the conclusion of this article will be made available by the authors, without undue reservation.

Author contributions

ZC, LM, and MJ contributed to the writing of the manuscript and to the interpretation of results. ZC: Conceptualization, Writing-Original draft preparation. LM and MJ: Writing-Reviewing.

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Conflict of interest

The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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Supplementary material

The Supplementary Material for this article can be found online at: <https://www.frontiersin.org/articles/10.3389/fphy.2022.1061172/full#supplementary-material>

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