



Topological One-Way Edge States in an Air-Hole Honeycomb Gyromagnetic Photonic Crystal

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Topological one-way edge states have attracted increasing attention because of their intriguing fundamental physics and potential applications, particularly in the realm of photonics. In this paper, we present a theoretical and numerical demonstration of topological one-way edge states in an air-hole honeycomb gyromagnetic photonic crystal biased by an external magnetic field. Localized horizontally to the edge and confined in vertical direction by two parallel metallic plates, these unique states possess robust one-way propagation characteristics. They are strongly robust against various types of defects, imperfections and sharp corners on the path, and even can unidirectionally transport along the irregular edges of arbitrary geometries. We further utilize the one-way property of edge states to overcome entirely the issue of back-reflections and show the design of topological leaky wave antennas. Our results open a new door towards the observation of nontrivial edge states in air-hole topological photonic crystal systems, and offer useful prototype of robust topological photonic devices, such as geometry-independent topological energy flux loops and topological leaky wave antennas.

Keywords: topological one-way edge state, robust one-way propagation, geometry-independent topological energy flux loop, topological leaky wave antenna, gyromagnetic photonic crystal

INTRODUCTION

Topological physics is flourishing as an active field, which has drawn extensive attention in both fundamental research and applied science [1]. Topological insulator commonly features the striking phenomenon of topologically protected one-way transport, exhibiting edge states or surface states that are strongly robust against defects, disorders, obstacles, sharp corners and so on [2, 3]. Inspired from the discovery of condensed quantum Hall effect, many studies have shown that topological states show essentially single-particle behavior of electrons and one can establish an analogy relationship with photon behaviors called topological photonic state (or topological one-way edge state) [4–7]. Topological one-way edge state provides a powerful platform for novel photonic devices with nontrivial functionalities and excellent performances, such as one-way waveguide [8–12], topological laser [13–17], rainbow trapping phenomenon [18–21], dispersionless slow light [22–24], topological fibre [25–27].

One feasible way to produce topological one-way edge states is to immerse a gyromagnetic photonic crystal (GPC) in an external static magnetic field to break the time-reversal symmetry [28–34]. When this symmetry is broken, truly one-wave edge states emerge, allowing the electromagnetic (EM) wave and light propagate forward smoothly when impinging on defects or propagating in disordered media, or even tanking sharp turns at arbitrary angles. To date, plenty of

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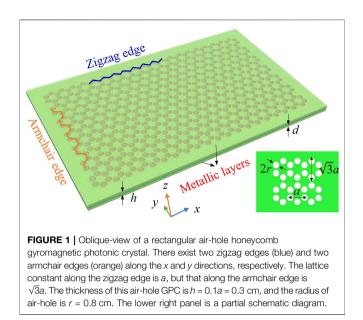
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topological one-way edge states are focused on the twodimensional cylinder-type GPC systems, which are consisted of an array of gyromagnetic cylinders immersed in air [30–34]. In contrast, little of them touch the air-hole-type GPC formed by an array of air holes in a gyromagnetic slab [35]. Yet, previous works in dielectric photonic crystals have shown that usually the transport behaviors of EM wave and light in cylinder-type photonic crystals are very different from that in air-hole-type photonic crystals [36–38]. So, it is interesting to examine the transport property of EM wave and light in an airhole GPC, and it is also very worthwhile to explore the potential applications and devices of air-hole topological photonic system.

In this paper, we investigate, theoretically and numerically, topological one-way edge states in an air-hole GPC of a honeycomb lattice of air holes drilled in a gyromagnetic slab surrounded by two parallel metallic plates in vertical direction. We systematically study the projected band structures of edge states at both zigzag and armchair edges and analyze their eigenmodal fields. We demonstrate the one-way property of these special edge states, and also verify their transport robustness against various types of defects, imperfections, sharp corners, and even the irregular edges of arbitrary geometries. We further utilize the one-way property of edge states to overcome entirely the issue of back-reflections and show the design of topological leaky wave antennas. Our results open a new door towards the observation of nontrivial edge states in air-hole topological photonic systems, and show the prototype of robustly topological photonic devices.

TOPOLOGICAL ONE-WAY EDGE STATES AT ZIGZAG AND ARMCHAIR EDGES

We first design a rectangular air-hole GPC with 140 honeycomb lattices, where the lengths along the x and y directions are seven and twenty lattices respectively, as illustrated in **Figure 1**. The

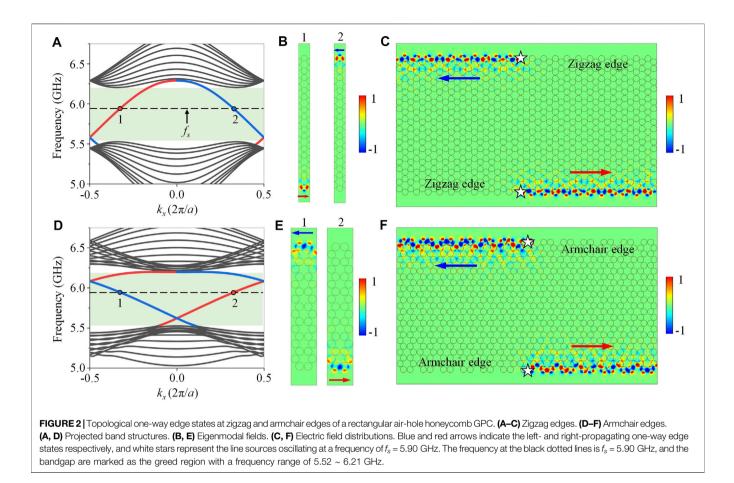
lattice constants of honeycomb lattice along the zigzag edge (*x* direction) and armchair edge (*y* direction) are a = 3.0 cm and $\sqrt{3}a$ respectively. Each air hole has a radius r = 0.8 cm and a height of h = 0.1a. In our simulations, this air-hole GPC is sandwiched between two parallel metallic layers with a thickness of d = 0.15 cm in vertical direction (*z* direction), as illustrated in **Figure 1**. The relative permittivity and permeability of the air are $\varepsilon_1 = 1$ and $\mu_1 = 1$ respectively. The gyromagnetic slab is composed of the commercial available yttrium-iron-garnet (YIG). In the absence of external static magnetic field, the relative permittivity and permeability of YIG is $\varepsilon_2 = 15.26$ and $\mu_2 = 1$ respectively. When an external static magnetic field is applied along + *z* direction, strong gyromagnetic anisotropy will be induced in YIG material, and its permeability can be given by [39–41].

$$\hat{\mu}_2 = \begin{pmatrix} 0.78 & -0.93i & 0\\ 0.93i & 0.78 & 0\\ 0 & 0 & 1 \end{pmatrix}.$$
(1)

These constitutive parameters correspond to those of YIG at 6.0 GHz with an external magnetic field of 500 Oe and a saturation magnetization of 1884 Gauss [39–41]. All the simulations are calculated by using the commercial software COMSOL MULTIPHYSICS with RF module in frequency domain, and only E polarization (where the electric field E is parallel to *z*-axis direction) is considered.

Next, we calculate the projected band structure of air-hole GPC along the zigzag edge, by adopting a supercell consisting of seven honeycomb lattices in one column, and the lattice constant is a = 3.0 cm. The projected band structures of the zigzag edges displayed in Figure 2A show that two dispersion curves (colored in red and blue respectively) appear inside the bandgap (green region) ranging from 5.52 to 6.21 GHz. The eigenmodal fields of points 1 and 2 at a frequency of $f_s = 5.90 \text{ GHz}$ depicted in Figure 2B reveal that there exist two edge states at two parallel zigzag edges. This phenomenon indicates that the YIG material shows the bandgap property that forbids the transport of EM waves in the YIG material, as a result, the one-way energy fluxes can be strongly localized at the zigzag interfaces between the air-hole GPC and the YIG material. As the slope signs of the red and blue dispersion curves are positive and negative respectively, the lower and upper zigzag edges will support right-propagating (red arrow) and left-propagating (blue arrow) one-way edge states respectively, as shown in Figure 2B. To exhibit the transport behaviors of one-way edge states, we use a configuration illustrated in Figure 2C. Two line sources (white stars) oscillating at a frequency of $f_s = 5.90$ GHz are placed at the center of upper and lower zigzag edges. The energy of line sources are confined at the upper and lower zigzag edges and unidirectionally propagate leftwards and rightwards respectively, in exactly agreement with the calculated results of Figures 2A,B.

Then, we calculate the projected band structure of air-hole GPC along the armchair edges, whose lattice constant is $\sqrt{3}a$. Their dispersions are calculated by adopting a supercell consisting of eight honeycomb lattices in one column, as plotted in **Figure 2E**. On the one hand, the calculated results illustrated in **Figure 2D** show that there exist two red and blue



dispersion curves dwelling the bandgap (green region) with a frequency range of 5.52~6.21 GHz, and their slopes are opposite. On the other hand, **Figure 2E** exhibits that the electric fields of eigenmodes 1 and 2 are concentrated at the armchair edges. Thus, there also exist two counter-propagating one-way edge states at the two parallel armchair edges. When two line sources oscillating at $f_s = 5.90$ GHz are placed at the upper and lower armchair interfaces, the left- and right-propagating one-way edge states can be excited respectively, as seen in **Figure 2F**. Consequently, these numerical simulations exhibit that both zigzag and armchair edges of air-hole honeycomb GPC support the one-way edge states in the green region with a frequency range of 5.52 ~ 6.21 GHz (their bandwidth is about 11.8%).

TOPOLOGICAL ENERGY FLUX LOOPS OF ARBITRARY GEOMETRIES

We have demonstrated the one-way transmission property of edge states existing at both zigzag and armchair edges. Now, we proceed to show the transport robustness of these one-way edge states in the presence of various types of defects, imperfections and sharp corners on the path. We must note that in our simulations, there exist two parallel perfect electric conductors clamping the air-hole GPC along the vertical direction (z direction) to avoid energy fluxes radiating into air. The line

source (white star) oscillating at $f_s = 5.90$ GHz is placed at the lower zigzag interface. Figure 3A shows the simulated result of one-way edge states in a perfect rectangular air-hole honeycomb GPC without any imperfections. The one-way edge states propagate along the zigzag and armchair interfaces to form a counterclockwise energy flux loop. Then, an imperfection interface can be created by moving a line of five air holes at the lower zigzag edge along the y direction with a distance of 0.55a, and the original positions of the moved air-holes are marked as five dotted circles, as plotted in Figure 3B. The electric field distribution shown in Figure 3B reveals that this imperfect interface still allows the EM wave propagating in one direction and forbidding backscattering. Figure 3C exhibits another common defected interface that can be constructed by replacing a honeycomb lattice of six air holes with six YIG cylinders of same size. As illustrated in Figure 3C, a new oneway interface between the air-hole GPC and the YIG material can be created, so that the edge states can turn around the defects without any back-reflection. We proceed to consider a regular right-angled trapezoid air-hole GPC including three types of sharp corners (60°-turn, 90°-turn and 120°-turn) and two types of edges (zigzag and armchair edges), as illustrated in Figure 3D. The schematic diagram of the partial structure (black dotted rectangle) is shown on the right panel of Figure 3D. It is a very common configuration in the previous works to be usually used to verify the transport robustness of

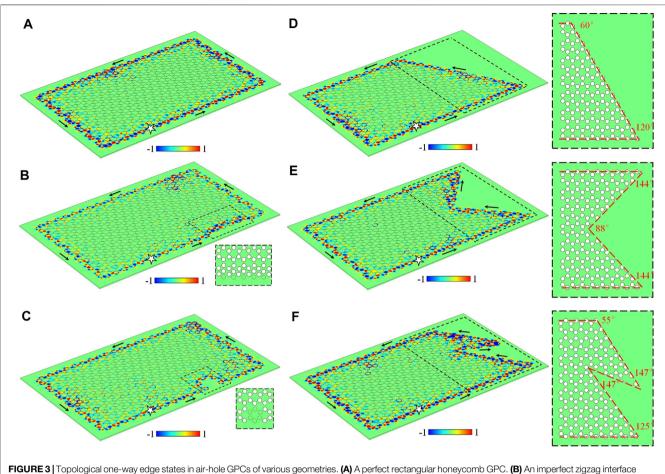
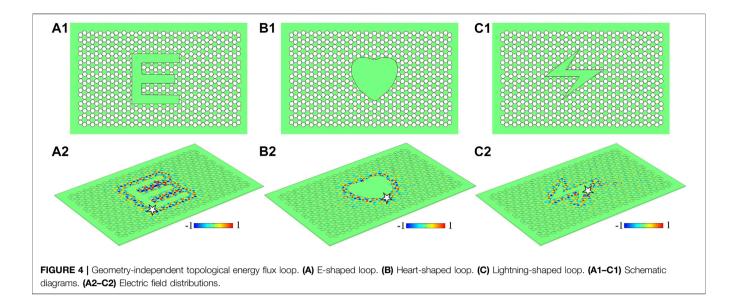


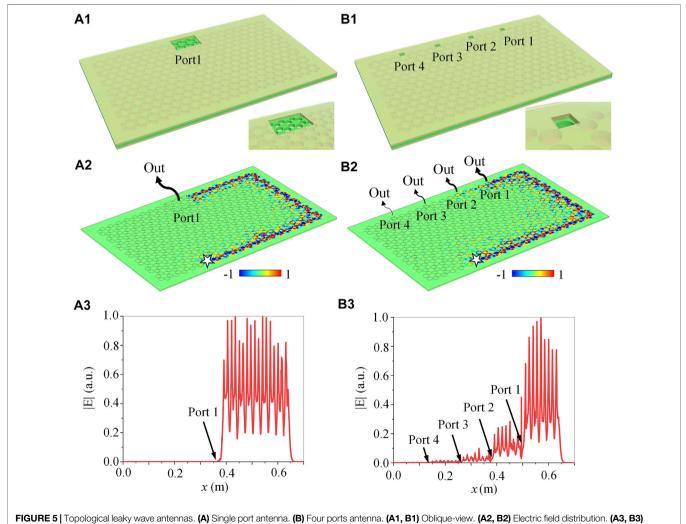
FIGURE 3 | Topological one-way edge states in air-hole GPCs of various geometries. (A) A perfect rectangular honeycomb GPC. (B) An imperfect zigzag interface is created by moving a line of five air holes at the lower zigzag edge along the *y* direction with a distance of 0.55*a*. (C) A defected zigzag interface is constructed by replacing a honeycomb lattice of six air holes with six YIG cylinders of same size. (D–F) Three irregular air-hole GPCs of various geometries. The angle of sharp corner is marked near the corner and the transport interfaces are marked as the red dotted lines.

topological edge states against the sharp corners. The simulated electric field distribution shows that the energy fluxes are strongly confined in the zigzag and armchair interfaces of trapezoid airhole GPC. They can transport along the lower zigzag edge, climb over the 120° sharp corner, continue to transport along the tilt zigzag edge, pass through the 60° -turn to the upper zigzag edge, bypass the left armchair edge, turn around the 90° -turn at the bottom left, and finally go back to the source to form a counterclockwise energy flux loop.

In addition to creating the common defects, imperfections and sharp corners to demonstrate the transport robustness of oneway edge states, we proceed to calculate the electric field distributions in two configurations of irregular interfaces and unusual sharp corners. Notably, a configurable, controllable and efficient way to construct these special structures is to fill the YIG material into the air holes as required. It can be seen that the EM waves can robustly transport along the atypical zigzag and armchair edges, and smoothly bypass a 88°-turn and two 144°-turns in a reflection-free way, as shown in **Figure 3E**. More intriguingly, the simulated electric field distributions shown in **Figure 3F** exhibit that the energy fluxes can almost perfectly transmit from the lower zigzag edge to the upper edge although there exist the irregular edges (not the zigzag and armchair edges) and unusual sharp corners (such as 55° -turn, 125° -turn, and 147° -turn).

We have verified that the topological one-way edge states are extremely robust against the backscattering from the defects, imperfections and unusual sharp corners at both regular and irregular edges outside the air-hole GPCs. Beyond the robust transport, these results also imply the possibility of implementing deformed topological energy flux loop of arbitrary geometries. So we further investigate the transport behaviors of EM waves in the energy flux loops of arbitrary geometries inside the air-hole GPCs, including E-shaped, Heart-shaped and Lightningshaped energy flux loops, as illustrated in Figures 4A1-C1. The excitation frequency of line source (white star) is $f_s = 5.90 \text{ GHz}$. The electric field distribution shown in Figure 4A2 shows that the energy fluxes are strongly confined at the interface of E-shaped loop and travel unidirectionally along the inside contour of air-hole GPC to form a counterclockwise energy flux loop. Again, both the contours of Heart-shaped and Lightning shaped energy flux loop also can be lighted by the line





Amplitude of electric field along the upper zigzag interface.

source due to the excitation of one-way edge states, as seen in **Figures 4B2,C2**. These simulated results exhibit that the geometry-independent topological energy flux loops can be created in the air-hole GPCs, which may provide the great opportunity to develop complex topological circuitry of arbitrary geometries for the robust transport of photons in classical wave regimes.

TOPOLOGICAL LEAKY WAVE ANTENNA

We have mentioned above that when the metallic plates of airhole GPC in vertical direction are removed, EM waves will leak into air. When the propagating wave is leaked out in air through a opened port, a leaky wave antenna will be formed [42, 43]. Utilizing this peculiar property, we can introduce small holes (or ports) in metallic plates (yellow) to allow EM waves to radiate outwards, thus, to achieve topological leaky wave antenna. It should be noted that one-way edge state in the rectangular airhole GPC system shown in **Figure 3A** is a closed energy flux loop surrounding entire system. To suppress one-way energy fluxes making a full round trip to affect the energy of line source, holes or ports we introduced should be guaranteed that all electric field amplitudes are released before making a full round trip.

We first consider a topological leaky wave antenna with a simple configuration. Only one antenna port (Port 1) of a size of 9.0×6.3 cm above the upper zigzag edge is opened, and its schematic diagrams are illustrated in Figure 5A1. The simulated results displayed in Figure 5A2 show that when the one-way energy fluxes reach Port 1, all of them directly leak into the air. As a result, no energy fluxes continue to propagate forwards to form a closed energy flux loop. The electric field amplitude distributions along the upper zigzag edge shown in Figure 5A3 also exhibit that when EM wave meets Port 1, the amplitude of its electric field sharply drops to zero, exactly in agreement with our expectations. It should be noted that attributed to the one-way nature of edge states, the output port does not backscatter any EM wave to affect the radiation property of line source. In contrast, in the conventional trivial leaky wave antennas, the energy fluxes backscattered from the output port will reflect back to the previous transport channel and even transmit back to the line source, thereby affecting the energy transmission and radiation efficiency in the whole antenna system. Therefore, the one-way property of edge states can overcome entirely the issue of backreflections and simplify the design of the leaky wave antenna.

On the other hand, we proceed to investigate the design of a topological leaky wave antenna array, made by cascading four antenna ports in the top metallic plate one after the other, as plotted in **Figure 5B1**. The size of these antenna ports is 1.6×1.6 cm, and the distance between the neighboring ports is 12.0 cm. As seen in **Figure 5B2**, when the energy fluxes reach Port 1, about 75% of them are released into air, and the rest continues to propagate forwards along the upper zigzag edge. All of energy fluxes will be completely leaked into air until they reach Port 4, as shown in **Figure 5B3**. Certainly, one can change the energy radiation ratio by modifying the size of each port and the distance between the neighboring ports. Similarly, because the backscattering of the topological one-way edge states is forbidden, the antenna ports do

not scatter back any EM waves, so that the second port with further downstream will not affect the output properties of the first port. However, for the conventional trivial leaky wave antennas, the energy fluxes will be scattered back from the second port and transmitted backward through the first port, so that the backscattering of output port has a significant influence on the energy transmission and radiation efficiency in the whole antenna system. Notably, this backscattering has also significant consequences in many other systems, specifically those systems seeded by a master oscillator whose performance may be strongly affected by reflected signals. It should be emphasized that by introducing the irregular edges of arbitrary geometries into the air-hole GPCs, the geometryindependent topological leaky wave antenna can also be realized.

CONCLUSION

In summary, we have demonstrated that the topological one-way edge states could exist in a rectangular air-hole honeycomb GPC biased by an external magnetic field. We have studied the projected band structures of zigzag and armchair edges and they both exhibited the transport behaviors of the topological one-way edge states. Besides, we have demonstrated that these unique states are not only strongly robust against various types of defects, imperfections and sharp corners, but also can unidirectionally transport along irregular edges of arbitrary geometries. Moreover, we have utilized the one-way property of edge states to overcome entirely the issue of back-reflections and provided the design of topological leaky wave antennas. Our findings open a new door towards the observation of nontrivial edge states in the air-hole topological photonic systems, and show the prototype of robustly topological photonic devices, such as geometry-independent topological energy flux loops and topological leaky wave antennas.

DATA AVAILABILITY STATEMENT

The raw data supporting the conclusions of this article will be made available by the authors, without undue reservation.

AUTHOR CONTRIBUTIONS

All authors contributed extensively to this work. CP, JC, and QQ performed the simulation. CP and JC drew the figures. JC, CP, and Z-YL wrote the manuscript. Z-YL supervised the project. All authors participated in discussions and reviewed the manuscript.

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