



Structuring Free-Standing Foils for Laser-Driven Particle Acceleration Experiments

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The recent development of petawatt-class laser systems sets a focus on the development of ultra-thin free-standing targets to access enhanced particle acceleration schemes vital for future applications, such as, medical and laser-driven nuclear physics. Specific strategies are required to improve the laser-to-particle energy conversion efficiency and increase the maximum particle energy. One of the promising approaches is based on the target design optimization; either by tuning key parameters which will strongly affect the laser-matter interaction process (e.g., material, composition, density, thickness, lateral dimensions, and shape) or by using micro/nanostructures on the target surface. At ELI-NP, considerable efforts are dedicated to extend the target capabilities beyond simple planar target design and develop complex targets with tailored properties suitable for high-power laser-plasma interaction experiments, as well as for studies with gamma and positrons beams. The paper provides an overview of the manufacturing capabilities currently available within ELI-NP Targets Laboratory for providing users with certain types of solid targets, specifically micro/nanostructured gold and copper foils and microns thick, porous anodized alumina. Also, optimization studies of alternative patterns (micro/nanodots) on silicon substrate are presented for future implementation on metallic free-standing thin foils.

Keywords: structured targets, fabrication, optimization, free-standing, enhanced acceleration mechanism

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INTRODUCTION

As an integrated part of the ELI-NP facility, Target Laboratory provides the means for local fabrication, characterization, and microassembly of a broad range of solid targets. To ensure a successful experimental campaign, support throughout the process is ensured by the Target Laboratory team, from proposal evaluation of the target to technical feasibility and up to target delivery. Therefore, having an on-site Target Laboratory brings major benefits, e.g., avoiding the damage of fragile targets that usually occur during their transportation, meeting specific target requirements in terms of chemical stability and purity, and ongoing optimization of target key parameters. Also, custom-made possibilities and last-moment modifications and adjustments of the targets can be rapidly performed, using the feedback from the laser-matter interaction experiments. Thorough characterization of targets just before the shot can be locally provided, including for commercial targets, in the case additional data are required for the running experiments. Also, in the long run, additional reduced manufacturing costs due to internally developed technologies and

methodologies, leading to competitive costs when compared with targets purchased from similar laboratories, are among other advantages. Depending on the complexity of the target, the fabrication process may take from few days (for supported thin films, multilayered samples) up to few months (for nanostructured, ultra-thin free-standing targets). Due to the large sample areas accepted by the existing (on-site) equipment used in the manufacturing and characterization steps (up to 6 inch in diameter), a relatively large number of solid targets can be obtained in a single process.

For the ongoing commissioning experiments at ELI-NP with the 1 PW laser [1], planar targets are provided either as commercial ones (e.g., thin/thick plastic films and metallic foils) or prepared in our laboratory (e.g., thin/ultra-thin films deposited on a template or as self-supported). One example of such planar targets that have been prepared on-site is the multilayer targets made of a controlled ratio of Fe-C homogeneous film. These targets can be employed to produce laser-driven secondary radiation which can be used in radiobiological and space radiation studies [2, 3]. Moreover, thin free-standing plastic targets (CH targets) are handled in-house, with the main focus on films of tens of nanometres in thickness and a few millimetres in the lateral dimension. In addition, special attention is given to the surface quality of planar targets (e.g., Al, Au, and Cu foils), which can impact laser absorption and particle acceleration. They can be improved by means of several in-house techniques, such as cold-rolling, electropolishing, mechanical polishing, thermal treatments, and dry or wet etching processes. Current continuous R&D activities of the manufacturing processes are directed towards providing the users with free-standing micro/nanostructured targets, by patterning the front and the backside of the targets with gratings, microspheres, micro/nanoparticles, hemi-spherical, or porous materials [4–11]. For these free-standing patterned targets, multiple-step fabrication procedures are currently tested and implemented by combining different manufacturing techniques with additional precise microassembling and mounting processes. Moreover, special attention is given to their quality, reproducibility, and optimization of the manufacturing process parameters.

For proton and ion acceleration experiments, we aim to take advantage of the unique opportunities provided by the high-power laser system at ELI-NP (high repetition rate and multi-petawatt power) [12–15], in order to obtain ion beams with large particle flux and with energy distribution suitable for the envisaged studies. As the characteristics of the laser-driven ion beams substantially depend on the target composition and configuration, several strategies intrinsically include the development of complex, more advanced targets. For example, the front side of the foil can be grooved as a diffraction grating or patterned as coupled plasmonic nanostructures, to confine and enhance the local optical field around these nanopatterns, thus allowing the optimization of light-matter interaction at sub-wavelength scale. An additional strategy includes the use of free-standing ordered porous arrays, which can also be used as a template for growing aligned metallic nanowires on an ultra-thin high-Z substrate (tens to hundreds of nanometres thick),

foreseen to obtain high-Z and high-fluence accelerated ions for nuclear physics studies [16].

Although solid targets are intensively used in laser-plasma experiments, they exhibit some important limitations, as for instance, the need for a precise alignment before each shot, reducing the repetition rate of the shots; a poor resistance to the laser pre-pulse, that may lead to their destruction before the arrival of the main pulse, making the laser temporal contrast a critical factor. Moreover, thin and ultra-thin targets usually need to be grown on a substrate, then afterward requiring the removal of the support material [17, 18], that may be difficult and impact on the final quality. Another limitation, compared, for example, to gaseous targets, may be the difficulty in achieving mass production methods while keeping a good reproducibility; and that a significant amount of debris can be ejected during the laser-target interaction, which can severely damage the nearby optical elements. Using microelements on the front side of the target [19] provides strong coupling between the target and the laser by generating an intense electromagnetic field around their surface that can manipulate the electron dynamics, while structuring the backside gives mainly control on the ion beam geometrical characteristics [9, 11, 20, 21]. The energy absorption of the laser pulse is significantly enhanced depending on the shape and size of the microstructure; the laser-to-ion energy conversion efficiency is considerably increased [5, 22], leading to higher particle energy and flux. In this work, we give an overview of the manufacturing processes developed and currently available within ELI-NP Targets Laboratory for structuring free-standing metallic foils with nano- or microstructures as potential targets for the upcoming high-power laser experiments. For this, conventional structures have been chosen based on their correlation with future intended experimental campaigns, implementing and optimizing their manufacturing procedure on thin self-supporting metallic foils. Fabrication of porous alumina as prospective targets for laser-driven ion acceleration or as a template for metallic nanowires is also presented.

MATERIALS AND METHODS

The micro- and nanostructured targets described in the present article have been obtained using the on-site fabrication and characterization capabilities available within the ELI-NP Target Laboratory, in an ISO 7 clean room environment [23]. Specifically, micro- and nanostructuring processes have been performed using an electron beam lithography system (DrawBeam EBL, Tescan) with proximity effect correction, implemented in the scanning electron microscope system. For the EBL process, 25–30 kV voltage has been used, while the specific process parameters are described in each target section. Reactive ion etching technique (RIE PlasmaPro Estrelas 100, Oxford Instruments Plasma Technology) for anisotropic dry etching processes by means of reactive plasma using a high-frequency (HF) generator, at 100–300 W, or inductively coupled plasma (ICP) unit, at 500–2500 W. The electrochemical setup used for aluminium anodization

included a water-cooled double-jacketed electrochemical cell with a two-electrode system, a DC power supply (PSU 400–3.8, Gw Instek), and 2 bench-top multimeters (Peaktech 4075 and Keithley DMM6500) for current and voltage monitoring connected to a PC interface.

Sample surface analyses, performed in different stages of the fabrication process, have been achieved using the atomic force microscopy technique (AFM NTEGRA, NT-MDT), with a whisker-type carbon tip (11.5 N/m force constant, 255 kHz resonant frequency, 10 nm tip curvature radius, and 1 μm tip length); an optical microscope (Nikon, bright or dark field modes); an optical profilometer (S Neox, Sensofar) using confocal imaging, profiling, and interferometric measurements; and scanning electron microscopy (SEM MAIA3, Tescan) with an electron backscatter diffraction system (EBSD e-Flash 1000, Bruker), for crystal orientation and grain-size distribution analysis, and energy-dispersive X-ray spectroscopy (EDS X-Flash, Bruker), for elemental analysis of the samples. Where applicable, surface cleaning of the self-supported foils was performed prior to their use by Ar⁺ ion-milling with a Kaufmann ion source (KDC160 model), integrated into an ultra-high vacuum sputter deposition system (UHV deposition cluster, Mantis Deposition). Lapping and polishing of the surface of the samples was carried out using diamond abrasive slurries on a compact M.M.8400 machine (LamPlan), equipped with an automatic dosing unit (M.M.709) and ceramic conditioning rings, while colloidal silica was used for super-polishing processes. Annealing treatments of the samples were conducted in a muffle furnace (L9/13/P330, Nabertherm GmbH) for thermal treatments under a controlled atmosphere up to 1,300°C.

The free-standing foils used as supports for micro- and nanopatterning were 3 μm or 10 μm thick commercial Au and Cu foils of 99.9% purity and 25 \times 25 mm² size (Goodfellow). All foils of 99.999% purity, 1 mm thick, and 150 \times 150 mm² size (Goodfellow) were used in the anodization experiments as raw material to attain free-standing anodic alumina films. Si wafers were used for preliminary tests on micro/nanodots and rods for

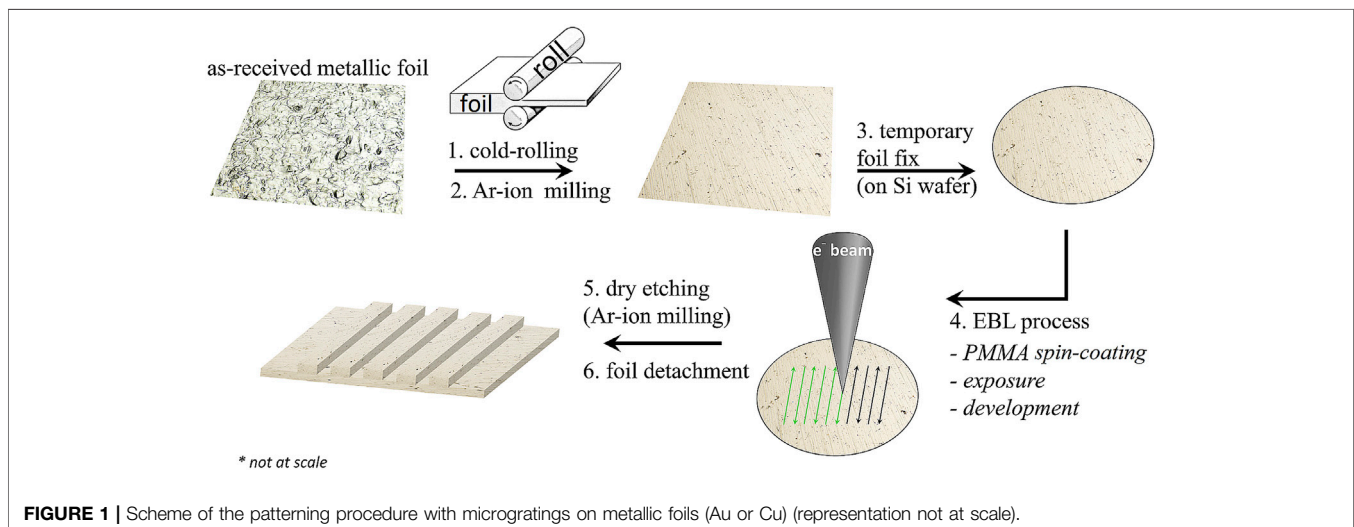
process optimization and tuning key parameters before process transfer to metallic foils.

MICRO/NANOSTRUCTURED TARGETS STRATEGIES

Metallic Gratings

To improve the laser-induced electron acceleration performances [24–26], the fabrication of patterned targets with ordered periodic gratings has also been considered. Such “grating” targets can be used for better control of the interaction of the ultra-intense laser pulse with matter via relativistic surface plasmons [25]. Compared to the previously reported studies, the approach presented in this paper is focused on the fabrication of gratings on thin free-standing metallic foils. Specifically, gold and copper foils have been patterned with periodic, one micron-size grating of rectangular or sinusoidal shape. A particular emphasis has been given to processes optimization, and several issues have been addressed, like handling difficulties, as the non-supported foils are easily bending, which was resolved by temporary fixing the self-supporting foil onto a one-inch Si wafer, providing better resistance to the foil and facilitating their handling. Additional issues involved the need for foils pre-processing before the patterning process, including cold-rolling and dry cleaning by controlled physical bombardment with Ar ions (i.e., Ar-ion milling). After the pre-processing of the foils, the gratings were fabricated using electron beam lithography and dry etching by Ar-ion milling. A schematic description of the fabrication procedure is depicted in **Figure 1** and will be presented in detail elsewhere [27].

The flatness and roughness of the foils were found to be critical factors for fabricating high-quality gratings. These foils’ characteristics were significantly improved after a cold rolling process of the as-received foils, coupled with controlled Ar-ion milling. As shown in **Figure 2** for an Au foil, a notable reduction of the roughness was achieved, from 350 nm of the original foil down to 13 nm. This process along with surface plasma cleaning



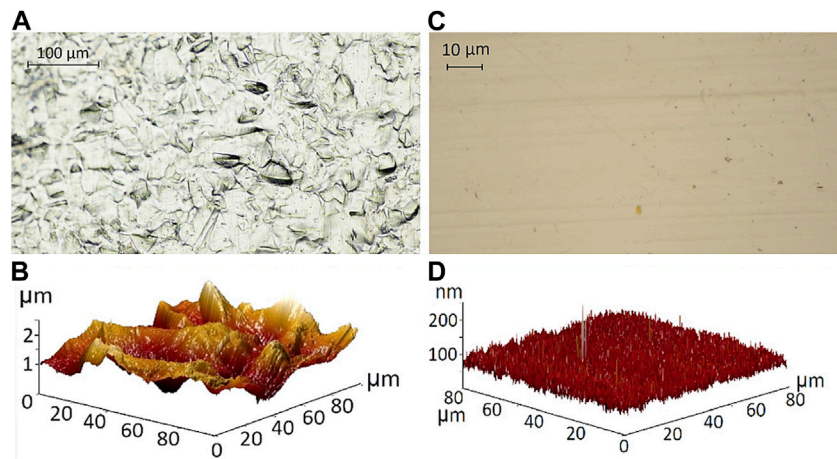


FIGURE 2 | (A,C) Optical images, and **(B,D)** AFM 3D images of the Au foils: **(A,B)** as-received, and **(C,D)** after cold rolling and Ar-ion milling.

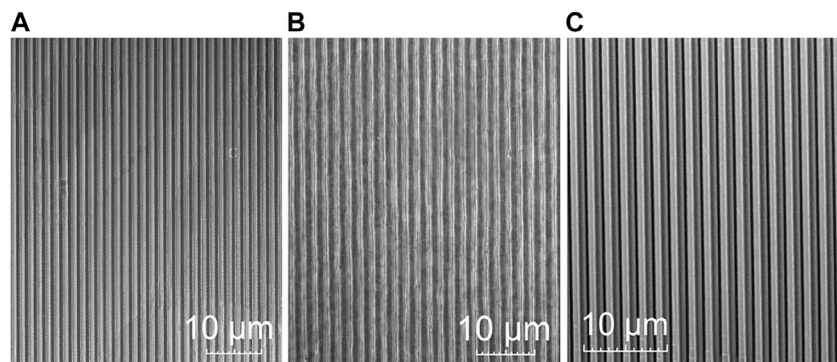


FIGURE 3 | SEM images of metallic gratings with 1 μm -wide and ~ 250 nm-deep groove etched on free-standing **(A)** Cu, **(B)** Au foils, and **(C)** on Au layer deposited on Si substrate.

operation on both sides was not detrimental and did not alter the average grain size, although a recrystallization process takes place at the surface of the foils. Experimental tests and theoretical simulations (using Monte Carlo simulations) allowed us to properly identify the following: (1) optimum exposure parameters for the EBL process (e.g., accelerating voltage, exposure dose, and step size) for $450 \times 450 \mu\text{m}^2$ write field; (2) adequate developing conditions, e.g., developing time, developer dilution, and temperature; (3) appropriate resist removal technique, among the different physical and chemical methods, and their effects on the quality of the gratings; (4) suitable etching key parameters (e.g., gas flow, rotation speed, time, source power, cooling time, temperature, and angle). The exposure of the 600 nm-thick positive PMMA photoresist spin coated on the Au or Cu foils was done using an electron beam acceleration voltage of 30 keV, exposure dosage of $300 \mu\text{C}/\text{cm}^2$, and beam step size of 30 nm for a beam radius of 18.5 nm. For the development, resist

removal, and etching processes, a mixture of 1:3 MIBK/IPA was used, for 120 s, followed by immersion in 1:9 MIBK/IPA solution for 30 s, at room temperature. Among different physical and chemical methods investigated to completely remove the hardened resist, while maintaining the quality of the structures, Ar-ion milling process (450 V and 100 mA, for 30 min) was found to be the most efficient. All Ar-ion milling steps were done at a pressure of 2×10^{-4} mbar Ar, with 7 rpm sample rotation, under room temperature. An angle of 45° between plasma direction and sample normal was used for yielding gratings with sinusoidal shape, and with normal incidence of the plasma to the sample surface, for rectangular shape gratings. A detailed description of the entire fabrication process is given in Ref. [27].

In **Figure 3**, the SEM images of metallic gratings patterned on 10 μm -thick Cu and Au free-standing foils (**Figures 3A,B**) and the gratings etched in 100 nm-thick Au layer deposited on Si substrate (**Figure 3C**) are illustrated. As can be observed, the

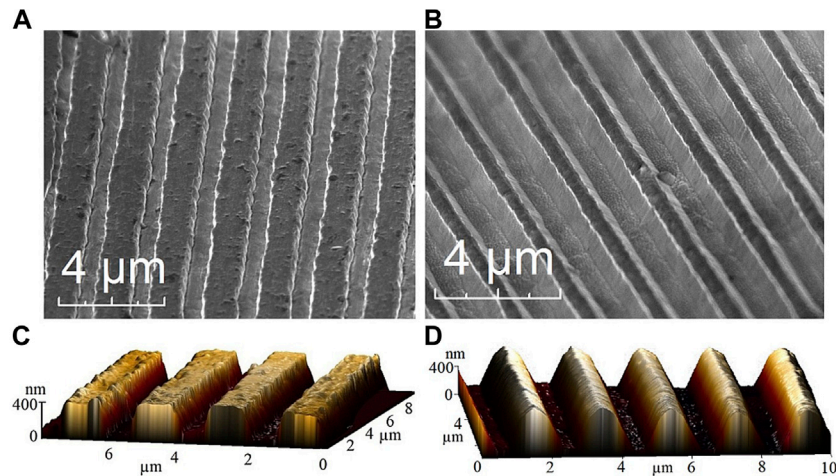


FIGURE 4 | (A,B) SEM micrographs and **(C,D)** AFM 3D-images of 1 μm -wide Au and Cu gratings, with **(A,C)** rectangular and **(B,D)** sinusoidal shapes.

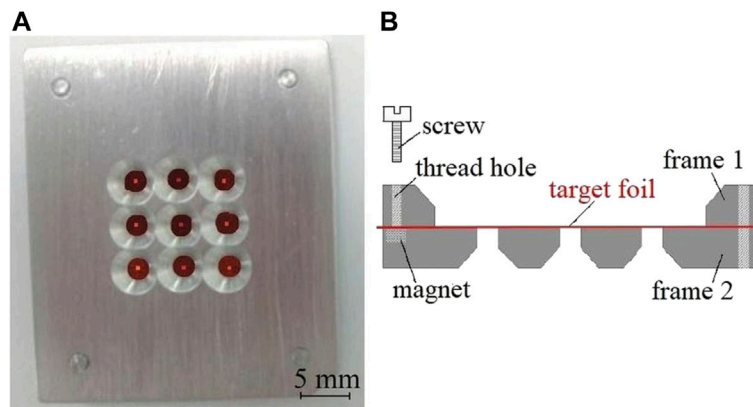


FIGURE 5 | Al holder with patterned Cu foil for assembly demonstration purposes: **(A)** front side and **(B)** cross-sectional view.

quality of the gratings and the edges of the grooves are significantly improved in the case of the Au layer on backing support, indicating a more controlled and stable process due to the beneficial effect of the better-defined surface of the substrate.

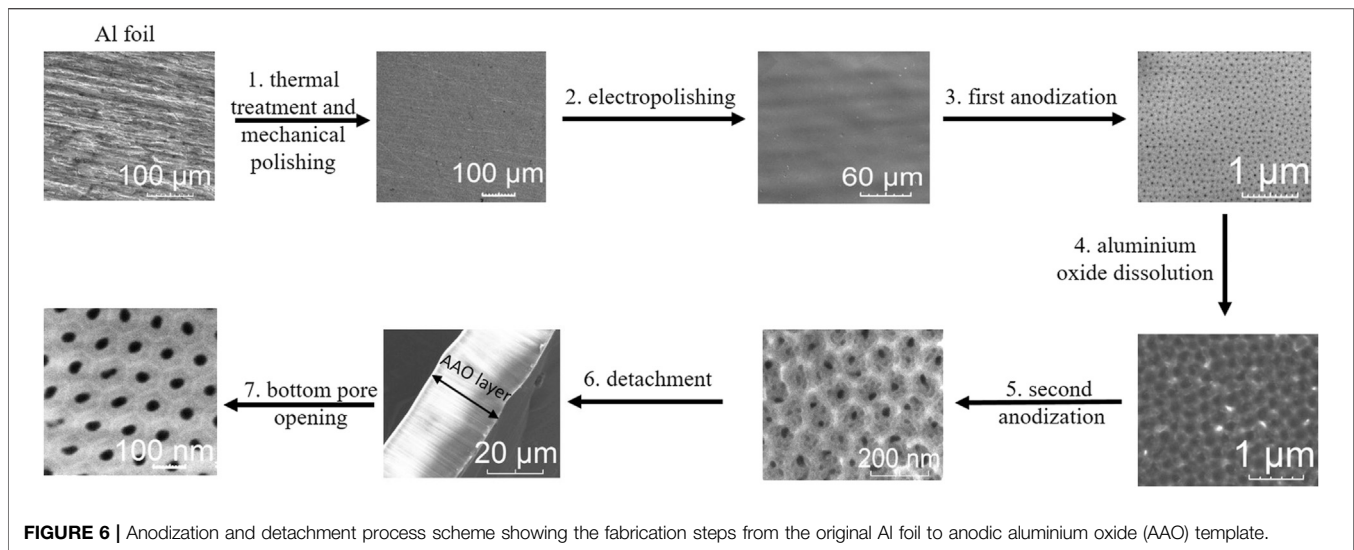
Figure 4 shows the different profile shapes of gratings made on self-supported metallic foils, showing the two investigated types: rectangular and sinusoidal. The different geometries of the patterns have been achieved by varying the etching angle between the sample surface and the plasma direction. The rectangular profile, characterized by vertical walls, has been obtained using a perpendicular direction of the Ar ions to the surface of the sample. For the sinusoidal (namely, trapezoidal) profile, a 45° angle of incidence with respect to the sample surface was used, leading to this type of gratings profile due to the shadowing effect of the photoresist.

The patterned foils have been mounted on custom-made aluminium (Al) holders, whose design allows for 9 individual areas, e.g., targets (see **Figure 5**), increasing considerably the

number of shots available in a single vacuum cycle of the interaction chamber. In experiments where full angular monitoring of the interaction is required (e.g., spatial distribution investigation of the high-energy particle beams and the characterization of the emission from the rear side of the target), the micrograting areas have been individually mounted on a thin capillary. Preliminary testing experiments of the structured foils, which will be presented elsewhere [27], showed that the electron beams emitted by the grating targets had up to 4 times higher flux than the flat foil. For the energy absorption, the grating targets were found to absorb 40% more of the laser energy than the flat foils, for a small laser incidence angle ($<30^\circ$); for higher incidence angles, similar absorption was measured.

Free-Standing Porous Alumina

Experimental studies on laser-driven particle acceleration, including particle-in-cell simulation, have been previously



reported on aligned nanowires, with sub-wavelength dimensions [28–33], which are similar in structure to the anodic aluminium oxide template (AAO). One of the approaches used to improve the laser absorption in the laser-driven ion acceleration experiments is the nanostructuring of the substrates in a brush-like geometry to obtain nanometre-sized rods standing in an upright position [31]. These structures have the advantage of increasing the hot electron density and temperature that in turn can lead to enhancement ratios of 2–3 for the maximum proton energy. By controlling the porosity and thickness of similar structures made of free-standing porous alumina targets, we propose to investigate the improvement of the energy of the accelerated ions at intensities beyond 10^{21} W/cm².

To obtain free-standing porous alumina (**Figure 6**), an Al foil of $20 \times 50 \times 1$ mm³ was annealed at 500°C for few hours to enhance the grain size in the metal [34], followed by mechanical polishing and then electropolished in a perchloric acid/ethanol mixture to improve the surface roughness (from 700 to 100 nm as the optical profilometer analysis has showed) and to lower the surface contaminants. The subsequent procedures included the two-step anodization in oxalic acid at 40V, 15°C, which transforms Al into aluminium oxide, resulting in a long-range honeycomb-like porous structure [35, 36]. After the first anodization, AAO was dissolved in a chromic/phosphoric acid mixture to eliminate the irregular template formed at the bottom [37]. The second anodization was performed under the same conditions, using an appropriate anodization time corresponding to the desired AAO thickness. For the free-standing AAO, a detachment method from the Al substrate was used by applying stair-like reverse biases in the same electrolyte used for anodization, usually from 18V to 24 V for 10 min each stair [38]. The bottom of AAO can be opened using a basic (NaOH 2M) or acidic (H₃PO₄ 0.5M) solution to obtain open pores at both sides of the template.

Several parameters of the process have been optimized to obtain arrays of vertically aligned porous alumina. To establish the composition of the electrolyte solution, phosphoric acid was

first used in the anodization process which resulted in not well-defined pore walls, while changing to the oxalic acid solution resulted in pores with straight walls. The anodization voltage allowed tuning the pores diameter, increasing the voltage resulting in an increase in their diameter. By increasing the anodization temperature, the chemical dissolution of oxide in the inner layer and the electrochemical formation of the anodic oxide layer are enhanced [39], resulting in a poor symmetry of the AAO template [40]. Also, a low temperature results in a slower growth rate of the AAO, thus fewer mechanical stresses [41], allowing the detachment of a defect-free, high-quality alumina free-standing layer; hence, 15°C was chosen as the optimum temperature. Moreover, the detachment method was adapted, by adjusting the time for each stair-like reverse bias and the electrolyte temperature, to suit the desired pores diameter and the thickness of the AAO template. A good reproducibility of the processes was observed, the samples showing good stability after long periods of time of storage at room temperature, in antistatic boxes.

The detached AAO is about 40 mm in length and 20 mm in width, with a thickness that can be varied between 5 and 100 μm. The AAO template density is around 2.7 g/cm³ and the porosity, defined as the ratio of the surface occupied by the pores to the whole surface area, is approximately 30%, for 40 nm pore diameter and 45 nm interpore distance. A focal spot of 5 μm focused on an AAO template characterized by these parameters would contain an average number of 3,000 pores. Using this technique, structures with pore sizes ranging from 10s to several hundreds of nm and aspect ratio up to 10⁴ can be created, with a porosity up to 70% and a corresponding porous template density of around 1 g/cm³.

The SEM and AFM images of the detached AAO template are shown in **Figure 7**. A homogeneous pore distribution was obtained, with the diameter of the distributed cylindrical pores ranging from 30 to 60 nm, as illustrated in **Figure 7A**. The thickness of the rear side barrier layer is about 50 nm, as shown in the SEM cross-section image from **Figure 7B**, with a honeycomb arrangement (**Figure 7C**);

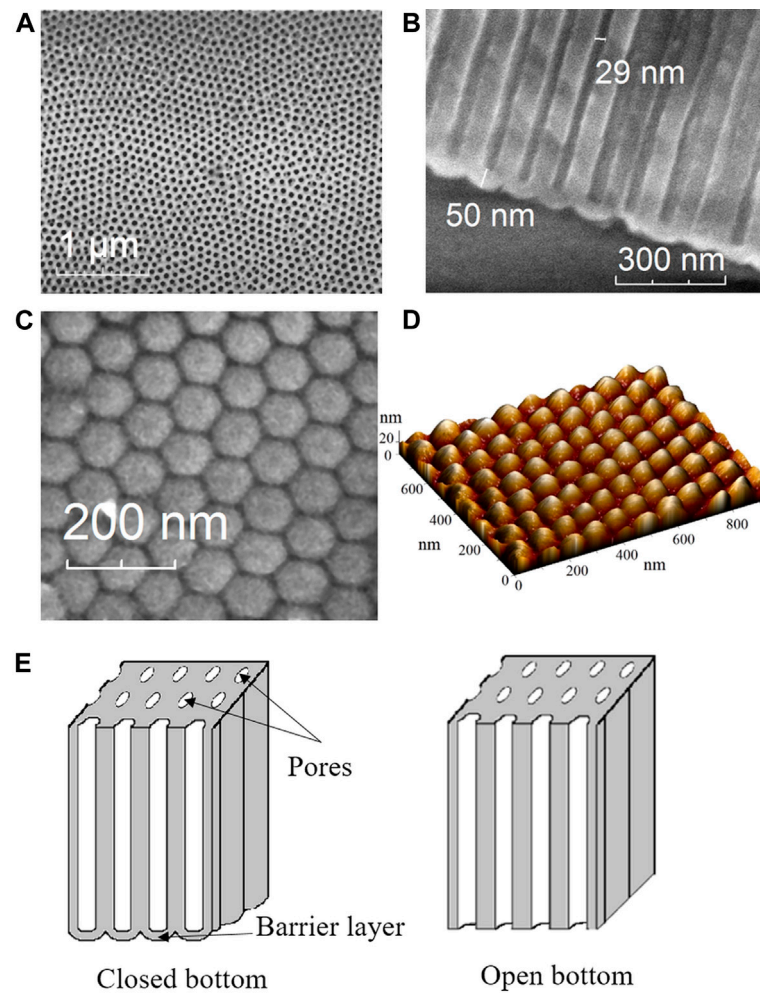


FIGURE 7 | SEM images of anodic aluminium oxide: **(A)** front view, **(B)** cross-sectional view, and **(C)** rear view. **(D)** AFM 3D-image of rear side of alumina and **(E)** schematic representation of the AAO template (left, with barrier layer; right, without barrier layer).

an AFM 3D view of the barrier curvature being shown in **Figure 7D**. In **Figure 7E**, schematic 3D images of the AAO templates with open and closed bottom pores is presented.

For laser-driven experiments, the AAO template is cut into strips about 1 cm long and 1–2 mm wide, with a thickness ranging from 5 to 20 μm . Then, they are attached on a custom-made C-shape frame mounted on a stalk a few centimetres long (**Figure 8A**), and eventually assembled on a 16 positions target wheel which is used in the experimental setup. The final free-standing AAO targets can be delivered either with closed or opened bottom pores (i.e., both sides with pores exposed). During the experiment, before each shot, the target is precisely aligned in the required position with the help of an imaging system (**Figure 8B**). A laser probe beam, derived from the main beam, is used to probe the expanding plasma in the forward and backward directions by shadowgraphy and interferometry. Setting the proper delay between the probe beam and the main beam allows us to take snapshots of the

plasma evolution during the interaction. **Figure 8C** shows a typical shadowgraph image of a 20 μm -thick free-standing AAO taken before shooting.

Triangle-Like Metallic Patterns

Self-assembly of polystyrene (PE) microspheres into a structured monolayer has proved to be a low-cost time-efficient process, compared to standard electron beam lithography and photolithography techniques. This technique allows subsequent monolayer coating with one or multi-layered materials which, followed by chemical dissolution of PE beads, leads to customized ordered size-controlled arrays, of triangle-like shape or hemispherical cup-shaped microparticles. Used as such, PE microspheres proved to be effective on large surfaces as structured targets for laser-accelerated particles despite the highly diffractive nature of these structures [42]. In this matter, foils can be nanostructured by using an inexpensive, but versatile technique, of commercial polystyrene

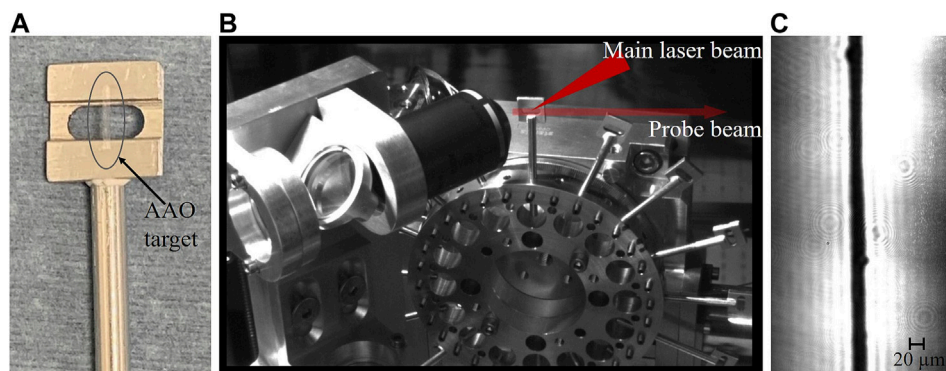


FIGURE 8 | (A) Front side of the free-standing AAO mounted on a C-shaped Al-frame, prepared for assembly on the experimental setup. **(B)** Experimental setup showing the targets mounted on a rotating target wheel and the online imaging system used for laser focal spot optimization and target alignment. **(C)** Shadowgraph image of a 20 μm -thick free-standing AAO target aligned in shooting position.

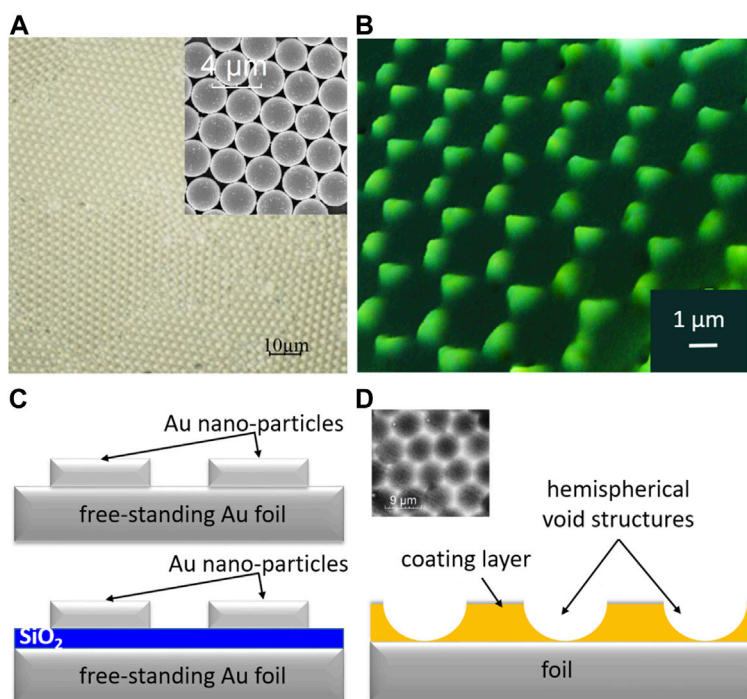
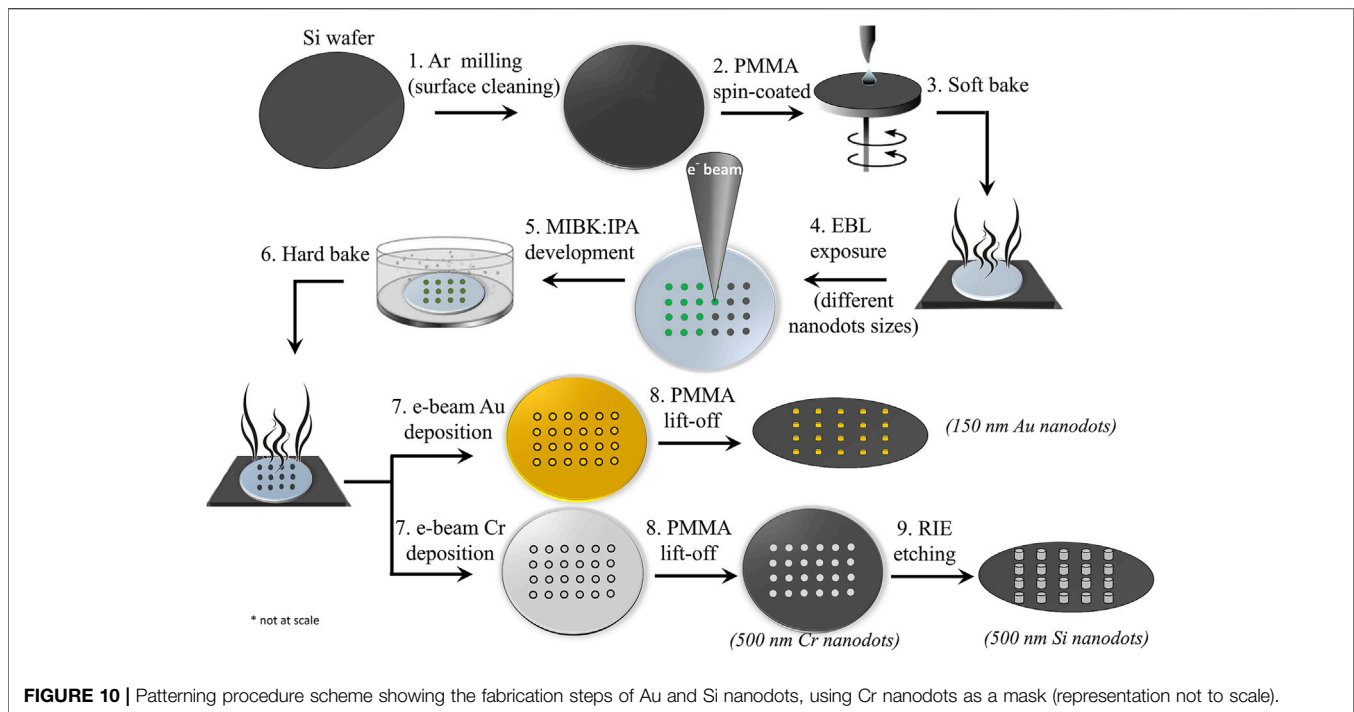


FIGURE 9 | (A) Optical image of a monolayer of polystyrene microparticles deposited on metallic foil, **(B)** optical profilometry 3D image of Au microstructures created by microsphere assisted lithography, and **(C)** scheme of structures based on Au nanoparticles and Au MIM patterns. **(D)** Scheme of the hemispherical void structures that can be used on both target sides; (inset) the SEM image of 4.5 microns hemispherical voids.

microspheres-assisted lithography [43]. Taking advantage of this technique, in this article, a solution containing $10 \pm 0.5\%$ polystyrene microspheres, with an average diameter of $3 \mu\text{m}$ ($0.12 \mu\text{m}$ standard deviation), was deposited on $10 \mu\text{m}$ thick Au foils (placed on a Si substrate, as support) using drop-casting or dip-coating methods. The microspheres solution (Magsphere Inc.), containing an anionic surfactant, had 1.05 g/ml of polymer density.

The drop-casting method resulted in a monolayer of self-assembled polystyrene microspheres; in the second method, dip-coating, as described by J. Limpouch et al. [5], a rearrangement of the microspheres takes place on the surface of the water solution, followed by the recovery of the floating microsphere monolayer onto the metallic foil. The monolayer is then dried in air for solvent evaporation, resulting in the microspheres patterned foils, as shown in **Figure 9A**. Triangle-shaped metallic



patterns can be obtained by depositing a gold layer via DC sputtering and then by mechanical or chemical removal of the beads. This final step exposes the remaining metallic microstructures formed between the microspheres, which served as a mask. The diameter of the microspheres is then the sole parameter in controlling both the spacing and the lateral dimensions of the micro/nanostructures. A 3D optical profilometry image, acquired in white-light interferometry mode, is presented in **Figure 9B** for the resulting Au microstructures arranged in an ordered hexagonally shaped array. Additional ongoing tests are currently being undertaken for improving the process for increased reproducibility for large area coverage, along with the implementation of the fabrication process on thinner Au and Cu foils. The aim is to obtain a better-controlled process for yielding increased reproducibility over a large area of high-quality ordered metallic microstructures on free-standing metallic foils. Moreover, for controlled low-field absorption tests, an updated scheme of the envisaged Au micro/nanoparticles structures including a dielectric layer is shown in **Figure 9C**. The metal-insulator-metal (MIM) multilayer leads to a significantly improved absorption (>98%) if specific dimensions/critical coupling conditions are fulfilled [44], the nanostructure acting as a Fabry-Pérot resonator cavity leading to a nearly perfect absorption. In addition, a variant of this technique can be employed to create hemispherical void structures (**Figure 9D**) that can be transferred on the front and/or backside of the free-standing foils [21, 45].

Micro/Nanodots

Sub-wavelength structures (<800 nm) on the target surface can control laser reflection and improve energy absorption [46], but due to their reduced dimensions, they are more fragile to high laser

pre-pulse; thus, additional consideration has to be provided to the laser parameters to protect these structures. In this regard, ordered metallic micro- and nanoscale dots (called micro/nanodots) have been obtained by a combination of EBL, metal deposition, and ion etching. Preliminary studies, described here, were performed on Si substrate for process optimization, with later on transfer of the process on thin free-standing metallic foils.

The manufacturing procedure is briefly described in **Figure 10**. Respectively, 150 nm-wide Au nanodots and 300 nm–1 μm -wide Cr dots have been obtained by exposing to the electron beam (25 kV voltage, 0.096 nA exposure current) the drawn pattern of the microdots in the positive PMMA resist, previously spin-coated onto a silicon wafer (1,000 rpm, ramp 20, 60 μL , 1 min, and ≈ 120 nm thickness). After the development of the exposed areas (MIBK:IPA solution 1:3), the surface was covered either by Au or Cr layer, deposited by e-beam evaporation (9 kV voltage, 2.5×10^{-7} mbar pressure; growth rates of 1.3 $\text{\AA}/\text{s}$ for Cr and 1.6 $\text{\AA}/\text{s}$ for Au, respectively), followed by lift-off procedure (in puddle acetone and ultrasound bath), resulting in a structured surface with metallic microdots. The thickness of the deposited metallic layer was chosen as one-third of the PMMA resist thickness to facilitate the lift-off process. For Au features, a 3 nm Ti layer was added as an adhesion promoter by e-beam deposition (0.8 $\text{\AA}/\text{s}$ growth rate, 60 mA current, and 9 kV voltage). Examples of the obtained metallic dots of different sizes are given in SEM images from **Figure 11**, for Au nanodots (**Figure 11A,B**) and Cr microdots (**Figure 11C,D**).

After the metallic micro/nanodots manufacturing process, using the obtained features as a mask in a supplemental etching step employing reactive ion etching (RIE), micron-sized elongated patterns have been successfully obtained (**Figure 12**). Specifically,

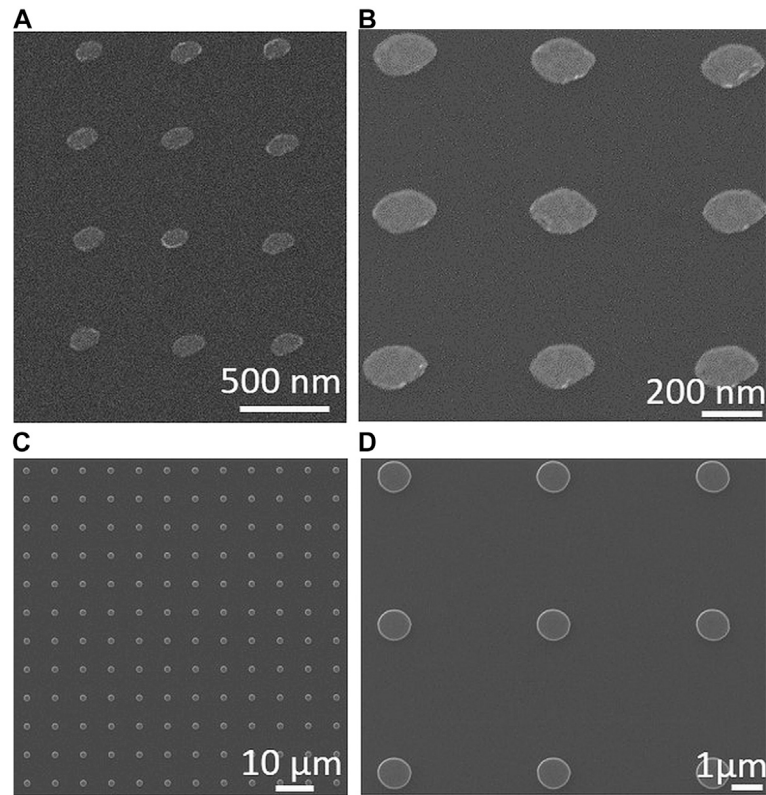


FIGURE 11 | SEM images of **(A,B)** 150 nm-wide Au nanodots and **(C,D)** 1 μm-wide Cr microdots.

arrays of 500 nm- or 300 nm-wide silicon microdots have been fabricated using different-sized Cr microdots as a mask. Experimental tests for the optimization parameters of the RIE process have revealed an optimum composition of 90:10 $\text{CHF}_3:\text{O}_2$, at 20°C, RF power 120 W, and a pressure of 0.1 mbar, leading to an etching rate of Si of 0.6 nm/s. In **Figure 12**, a selection of the SEM micrographs of the obtained Si microdots of 500 nm wide and 110 nm height is presented (**Figures 12A,B**), and 300 nm wide and 200 nm height (**Figures 12C,D**), respectively.

These nanostructures benefit from the highest possible geometrical control, allowed by e-beam or ion lithography, on relatively large surfaces [47]. This reflects into a high quality and reproducible type of structures. Once the process parameters have been optimized, to obtain the best quality of the structures (shape, sharp edges, precise spacing and dimensions, and homogeneous (regular) arrangement of the micro/nanodots), the reproducibility of these structures is ensured for a large number of samples. We can accurately control the diffraction channel of the structure through separation distance control, with nm precision. The interaction between such structures and the laser pulse, in particular the prepulse, can be tuned by changing the wavelength of their localized resonance via dimensions and material choice [48, 49].

As for the stability of these structured targets, Si and Au micro/nanodots are well known to be stable over long periods, while Cr microdots targets are recommended to be stored in controlled temperature and humidity conditions, as surface oxidation may occur.

CONCLUSION

We presented here research directions within ELI-NP for producing structured targets that can be used for more efficient coupling between high-intensity laser pulses and solid targets, and to improve the acceleration and the characteristics of the ion beams. As laser-plasma interaction at the target's surface is sensitive to surface modulations, we developed several technologies for producing complex targets with structured surfaces. Micrometre- and nanometre-scale structures, such as periodic grating, metallic micro/nanodots, were fabricated on free-standing Cu and Au foils or on Si substrates by conventional techniques, such as electron-beam lithography and dry etching, or by microsphere assisted lithography. For surface ion acceleration, porous materials (alumina) were developed, using electrochemical methods. Ongoing research is directed towards optimizing the target's design to allow their use in the foreseen high-power laser experiments.

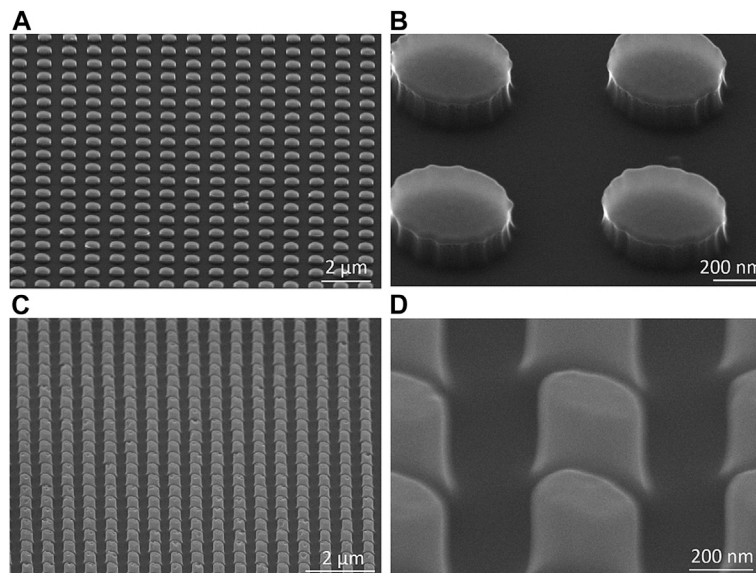


FIGURE 12 | SEM micrographs of **(A,B)** 500 nm-wide and **(C,D)** 300 nm-wide Si microdots fabricated using Cr dots as a mask.

DATA AVAILABILITY STATEMENT

The original contributions presented in the study are included in the article; further inquiries can be directed to the corresponding author.

AUTHOR CONTRIBUTIONS

CG: conceptualization, performed experimental work, formal analysis, writing the manuscript—original draft preparation, review, and editing; SI: performed the experimental work and editing the manuscript part on alumina; PG: conceptualization, review, and editing the manuscript; MC: review and editing the manuscript, performed experimental work; DD: conceptualization, review and editing the manuscript; DP: performed experimental work of mounting, assembly and frames and holders fabrication; VL: conceptualization, performed experimental work, formal analysis, review, and editing the manuscript.

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