



In Vivo Pulse Wave Measurement Through a Multimode Fiber Diffuse **Speckle Analysis System**

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Continuous monitoring of in vivo pulsatile blood flow and pulse wave velocity (PWV) is important for clinical applications. These parameters are correlated with physiological parameters, such as blood pressure and elasticity of blood vessels. A multimode fiber diffuse speckle contrast analysis (MMF-DSCA) system was developed for fast measurement of in vivo pulsatile blood flow and pulse wave velocity. With MMF and CCD sensor, the diffuse speckle could be captured and processed with higher temporal resolution of 3 ms. We also induced for the first time an MMF-DSCA for evaluation of PWV, which allows estimation of the blood pressure continuously. To validate its performance, both phantom and in vivo experiments were conducted. The results demonstrate that MMF-DSCA could achieve fast pulsatile blood flow measurement with detailed information of the pulse wave profile and velocity. Taking the advantages of being simple and costeffective, the flexible system can be easily adapted for continuous monitoring of vital biosigns, such as heart rate, pulse wave, and blood pressure.

OPEN ACCESS

Edited by:

Chao Tian University of Science and Technology of China, China

Reviewed by:

Peng Li, Zhejiang University, China Cheng Wang, University of Shanghai for Science and Technology, China

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Specialty section:

This article was submitted to Medical Physics and Imaging, a section of the journal Frontiers in Physics

Received: 02 October 2020 Accepted: 09 December 2020 Published: 19 January 2021

Citation:

Teng Z, Gao F, Xia H, Chen W and Li C (2021) In Vivo Pulse Wave Measurement Through a Multimode Fiber Diffuse Speckle Analysis System. Front. Phys. 8:613342. doi: 10.3389/fphy.2020.613342

Keywords: pulse wave velocity, blood flow, multimode optical fibers, blood pressure, diffuse speckle

INTRODUCTION

Cardiopulmonary parameters, such as pulse wave velocity (PWV) and heart rate, are crucial for clinical diagnosing and daily healthcare monitoring [1]. PWV is the speed of the pulse wave generated by the heart and transfers along the arterials. It is considerably high (5-15 m/s) and carries information of cardiovascular function and vessel viability [2]. The monitoring and analysis of PWV provide a good vital biomarker to assess the status of cardiovascular system and microcirculation [3-6]. In clinic applications, PWV in the aorta has been estimated by measuring the delay in the foot of the wave between ascending aorta and femoral artery. But the intelligent instruments and skillful operators are needed to obtain reliable results. On the other hand, assessment of PWV is also important for daily healthcare monitoring, especially for infants and elderly [7].

Taking the advantages of noninvasive and real-time measurement, optical approach is an attractive way to measure in vivo blood perfusion, heart rate, and pulse wave. Most of the optical modalities require a coherent light source and follow the working principle of dynamic light scattering [8]. Laser speckle contrast imaging (LSCI) is a powerful tool for wide-field blood flow imaging of superficial tissue [9-11]. But the penetration depth limits its applications in deep tissue blood flow and PWV measurement. Considering the highly scattering properties of biological tissue, diffuse optical methods have been developed for blood flow index (BFI) measurement and obtaining the fast pulsatile blood flow in deep tissue. Among these methods, diffuse correlation spectroscopy (DCS) system [12-14] adopts high-sensitivity single-photon counting and correlator, which

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increases the hardware cost significantly with multiple channels. However, the fiber-based diffuse speckle contrast analysis (DSCA) system [15, 16] can be extended into multiple channels without significant additional cost and is still able to obtain deep tissue blood perfusion information at satisfied accuracy. Similar to LSCI, DSCA could perform with spatial processing algorithm, which will provide better temporal resolution.

Taking the advantages of flexibility and robustness, fiberbased diffuse optical methods are very popular in clinical applications of deep tissue blood flow measurement. Many systems use multimode (MM) source fiber [7, 17] to obtain the contrast information from the diffuse laser speckles and extract blood flow information. Therefore, it is also possible to use MM detection fiber combined with area array camera for diffuse pattern detection [18]. That makes the measurement rate of deep tissue blood flow the same as the frames per second (fps) of camera. Although sensing of pulsatile blood flow and heart rate has been previously demonstrated, other parameters such as PWV have not been further investigated. The previous works also indicated that PWV is highly related to the blood pressure (BP) and age [19]. Studying the properties and velocity of pulse wave of macro- and microcirculations may lead to an early diagnosis of many disorders [20].

In this paper, we presented a method for fast pulsatile blood flow and pulse wave velocity measurement in deep tissue. With the MM fiber delivering speckles pattern into the CCD sensor, the diffuse speckle contrast could be calculated spatially at each frame. The MMF-DSCA system achieves 300 Hz simultaneous measurement of pulsatile blood flow, which is further used to determine the pulse shapes and temporal delays propagation through the arterial tree. Both phantom validation and in vivo blood flow measurement are demonstrated. Thus, the linear regression model gives a good approximation between the BP and PWV. It is demonstrated that MMF-DSCA is one of the fastest noninvasive methods for deep tissue blood flow and pulse wave measurement. Taking the advantages of being simple and cost-effective, MMF-DSCA system can be easily adapted for clinical applications, such as continuous monitoring of heart rate, pulse wave, and blood pressure.

MATERIALS AND METHODS

Theoretical Background

From theoretical analysis, DCS and LSCI probe different aspects of the field autocorrelation curve, which shows how fast the optical signal loses its self-similarity [21]. The decay rate of this curve is a good indicator of flow speed. From DCS measurements, it is necessary to extract the speed by calculating the electric field temporal autocorrelation function $G_1(r, \tau)$ [22], as follows:

$$G_1(r,\tau) = \frac{3\mu'_s}{4\pi} \left(\frac{e^{-k(\tau)r_1}}{r_1} - \frac{e^{-k(\tau)r_2}}{r_2} \right)$$
(1)

$$k(\tau) = \sqrt{3\mu_a \mu'_s + \alpha \mu'_s k_0^2 \langle \Delta r^2(\tau) \rangle}$$
(2)

$$r_1 = \sqrt{\rho^2 + \left(\frac{1}{\mu'_s}\right)^2} \tag{3}$$

$$r_{2} = \sqrt{\rho^{2} + \left(\frac{1}{\mu'_{s}} + \frac{4}{3\mu'_{s}}\frac{1 + R_{eff}}{1 - R_{eff}}\right)^{2}}$$
(4)

where ρ is the distance between the source fiber and the detector fiber, μ_a is the absorption coefficient of the tissue, and μ'_s is the reduced scattering coefficient of the tissue. $R_{eff} = -1.440n^{-2} + 0.710n^{-1} + 0.668 + 0.00636n$ represents the effective reflection coefficient of the medium and the *n* is refractive index of tissue relative to air, $k_0 = 2\pi/\lambda$ is the wavenumber of light in the medium, λ is wavelength of the incident light, α is the fraction of dynamic photon scattering events in the medium, and $\langle \Delta r^2(\tau) \rangle$ is the mean square displacement of the moving scatterers in a delay time of τ . Brown model approximation is used in analysis and research; it defines $\langle \Delta r^2(\tau) \rangle = 6D_B\tau$, where D_B is the effective diffuse coefficient [23].

When a coherent light illuminates the blood perfused tissue, the speckle pattern is decorrelated. The level of blurring is quantified by the speckle contrast value, which could be calculated by the following equation [24]:

$$K^{2}(T) = \frac{2\beta}{T} \int_{0}^{T} (1 - \tau/T)g_{1}^{2}(\tau)d\tau$$
(5)

where *T* refers to the exposure time, β is the coherence factor determined by the ratio of detector pixel size to speckle size, and $g_1(\tau) = G_1(r, \tau)/G_1(r, 0)$ is the normalized electric field temporal autocorrelation function. In practice, $K = \sigma/I$, where σ and *I* are the standard deviation and the mean value of speckle pattern, respectively.

Previous work established the fact that both speckle contrast and intensity autocorrelation carried information about the blood flow. Under certain conditions, the recovery of blood flow using both speckle contrast and field/intensity autocorrelation is equivalent. The contrast has the maximal sensitivity if the exposure time is of the order of the correlation time. And there is a linear correlation [25] between $1/K^2$ and BFI.

When the MMF is used, photons from the source fiber experience multiple scattering. The diffuser photons that reach the detector fiber will carry the information of blood flow in deep tissue. Because the speckle pattern output by an MMF is not ideal, it is necessary to correct the raw speckle pattern. In each measurement, we average 3,000 images and normalize them to the maximum intensity as the background intensity $I_M(x,y)$. The raw speckle pattern $I_o(x,y)$ will be divided by $I_M(x,y)$ to obtain the corrected result I (x,y), which is used for spatial speckle contrast calculation [18].

Pulse Wave Analysis

With MMF-DSCA system, BFI can be calculated spatially from each frame captured by the CCD camera. That makes the sampling rate much faster than DCS systems. The pulsatile changes of BFI are related to the pulse wave, which is an



indicator of cardiovascular status. The frequency spectrum of pulse wave provides additional information about the speed transverse to the beam axis, and this initial result merits a more detailed investigation. In this study, the frequency characteristic was analyzed and extracted by the Fourier transform, as

$$P(f) = \frac{1}{N} \left| \sum_{n=0}^{N-1} x_n e^{-2\pi j n f} \right|^2$$
(6)

where f represents the frequency of signal, N is the length of signal, and x_n is the signal amplitude.

The diastolic time is an important parameter that is highly related to the systolic blood pressure (SBP) and diastolic blood pressure (DBP). To determine the diastolic time, the first-order derivative algorithm was applied to the time-domain pulse waveform to obtain the characteristic points within one cycle. Then, linear regression analysis was performed between the diastolic time and BP.

As the pulse wave propagates through the arterial tree from the heart to the periphery, pulse wave velocity could be estimated by recording the pressure wave transition time (PTT) between two selected areas in the arterial tree. In this study, we choose the forearm and fingertip as the measuring locations. Considering time-varying BFI signal obtained at adjacent locations in forearm (*F1*) and fingertip (*F2*), when the pulse wave travels from *F1* to *F2*, the BFI feature keeps constant in the stream, resulting in the time series of $F1_B(t)$ and $F2_B(t)$ appearing in nearly identical shapes with a time lag of τ . Then, the cross-correlation function is used to determine the time delay between two time-varying dynamic speckle signals, as follows:

$$r_{xy}(k) = \frac{\sum_{t=1-k}^{N-k} \left(F1_B(t) - \overline{F1_B(t)} \right) \left(F2_B(t+k) - \overline{F2_B(t)} \right)}{\sqrt{\sum_{t=1-k}^{N-k} \left(F1_B(t) - \overline{F1_B(t)} \right)^2 \sum_{t=1-k}^{N-k} \left(F2_B(t) - \overline{F2_B(t)} \right)^2}}$$
(7)

$$PTT = \max_{k} \left[r_{xy}(k) \right] \tag{8}$$

where r_{xy} represents the correlation coefficient, k is the time difference of two signals, N is the maximum time difference, and

the $F1_B(t)$, $F2_B(t)$ are mean value of amplitudes of two signals, respectively. The average PWV can be evaluated with the following equation [26]:

$$PWV = L/PTT$$
(9)

where L is the arterial length between two selected areas.

Experimental Setup

The setup of MMF-DSCA system is shown in Figure 1. A long coherence length (>10 m) laser diode (785 nm, 15 mW, LP785-SAV50, Thorlabs, United States) was used to illuminate the sample. In order to achieve synchronization, a 50:50 1 \times 2 fiber coupler was used to split the light into two identical MMFs (d = 200 µm, NA = 0.22). For in vivo measurement, the first fiber was attached to the subject's forearm, near the brachial artery, while the second fiber was attached to the subject's fingertip. Two multimode fibers were used as detector fibers with the other ends touching onto the CCD directly. The distance of source-detector fiber can be adjusted in the range of 5-20 mm. To avoid the need to synchronize two cameras, the diffuse speckle pattern of both fibers was collected by a single CCD camera (Basler aca1920-155um, Germany). The magnification was adjusted to make sure the speckle patterns from the two fibers are projected without overlapping and meet the requirement of diffuse speckle sampling.

For speckle analysis, both the spatial resolution and exposure time are important for the sensitivity and dynamic range of flow measurement. In the MMF-DSCA system, the multimode fibers with core diameter of 200 um were used to collect the diffuse speckle of in vivo tissue, resulting in the spatial resolution of 0.2 mm. The size of a single speckle is about 11 μ m, which is twice the size of a single pixel size of 5.6 µm. That satisfies the Nyquist sampling criterion and maximizes the contrast of the imaged speckle pattern. However, each MMF speckle pattern contains more than 1,000 speckles, which provides a sufficient statistical sample to analyze the spatial speckle contrast. The exposure time is also important for the sensitivity and SNR of blood flow measurement. Dunn's results suggested that any exposure time greater than 2 ms will provide optimal sensitivity to blood flow changes [27]. However, the exposure time should also meet the requirement of monitoring the pulsatile blood flow. Considering



temporal resolution for pulse wave monitoring, we set the exposure time to be 3 ms.

In this paper, the diffuse speckle contrast was calculated spatially from each frame, resulting in that the temporal resolution for blood flow measurement is approximately 3.3 ms. The corresponding cross-correlation is calculated with **Eq.** 7, which has the same temporal resolution of 3.3 ms. According to the distance between two locations and the speed of PWV, the time delay of pulse waves is generally over 30 ms. It is demonstrated that the MMF-DSCA system has a sufficiently high temporal resolution for PWV measurement.

Most of the arteries are in the subcutaneous layer with depth varying from 2 to 10 mm below the surface. According to the theory of diffuse optics, the effective detection depth is around a half of source-detector separation. Since source-detector separation is 15 mm with *in vivo* measurement, the diffuse speckle signal is mainly from the depth range around 7.5 mm. The penetration depth is also demonstrated with Monte Carlo simulations and phantom experiments. The cloud map of the light intensity with Monte Carlo simulation is shown in **Figure 1**. The simulation results indicated that the penetration depth of diffuse light collected by the detection fibers is in the range of 5–12 mm. Based on the distribution of photon number and penetration depth, the average penetration depth is further

calculated to be 7 mm, which agrees with the theory of diffuse optics. The depth of MMF-DSCA measurement is also validated by the phantom experiments.

Phantom Experiments

To verify the performance of the system in deep tissue flow measurement, a phantom experiment was designed with a hollow plastic tube that was embedded inside a solid scattering phantom body ($\mu_a = 0.01 \text{ mm}^{-1}$, $\mu_s = 0.4 \text{ mm}^{-1}$). The tube was buried 5 mm underneath the phantom surface. Liquid with the similar scattering coefficient as blood was pumped through the tube by a peristaltic pump. Since the liquid was pumped by pinching the rubber tube through the rotating rollers of the peristaltic pump, a higher flow rate could be achieved by increasing the pinching frequency. During the experiment, the pumping rate was set from 0 to 0.56 ml/s with step size of 0.07 ml/s.

In Vivo Measurements

For *in vivo* measurements, the subjects were requested to sit on a chair and keep still during the experiments. The experiments were carried out on 10 healthy volunteers (including seven males and three females) aged 24–26. To evaluate the relationship between PWV and BP, the experiments were performed on five individuals during the recovery period after the stair climbing exercise, and the interval of each measurement was



10 min (5 times in total). The blood pressure was also measured by a commercial BP monitor.

RESULTS AND DISCUSSION

Phantom Result

As shown in **Figure 2**, the phantom results demonstrate the good correlation between the flow rate and $1/K^2$. Since the system provided a sampling rate at 300 Hz, the flow waveforms at each pumping period could be resolved clearly, as shown in **Figure 2A**. A good linear relationship between the pumping rate and the averaged BFI can be observed in **Figure 2B**. Because the MMF-DSCA system provides high temporal resolution, the periodical changes of the flow inside the phantom could be resolved clearly. Therefore, the roller pinching frequency can be calculated from the peak-to-peak time interval of the flow waveform. **Figure 2C** demonstrates a very good linear relationship between the flow rate and the measured pinching frequency.

In Vivo Result

Pulse Wave Measurement

The *in vivo* BFI measured with MMF-DSCA system are shown in **Figure 3A**. The temporal blood flow profile is in good agreement with previous research [28]. The pulse waveform in the forearm has more features within each cycle. Compared with the standard pulse waveform, the two obvious peaks are related to the main wave and the repulse wave. However, the pulse waveform from the wrist has sharper peaks and smoother repulse wave.

To quantify this difference, the time-domain pulse wave signals were Fourier transformed as shown in **Figure 3B**. The power spectra of the pulse waves demonstrate that the energy in higher frequency of pulse wave on forearm is greater than wrist, which is consistent with temporal profile. Meanwhile, the energy of both pulse waves is concentrated in the range of 0.5–10 Hz. The peaks in 1.4, 2.8, and 4.2 Hz are related to the heartbeat rate and its higher harmonic frequencies. It can be concluded that the frequency spectrum distribution of pulse waves in different parts of the human body is relatively consistent.

Compared with forearm, the radial artery at the wrist is shallower and far from heart. That makes its ascending branch steeper. As shown in **Figure 3**, the position and amplitude of the repulse wave descend, and the sharp corners of the waveform are smoother. The time-domain and frequency-domain characteristics of the pulse waves measured with our system also agree with the pulse theory [29].

Correlation Between Blood Pressure and Pulse Wave

In order to analyze the features of the pulse wave in more detail, the individual waveforms of one heart beat were averaged during a period of five adjacent pulse cycles. After baseline correction and noise reduction, the division of temporal pulse wave characteristics is shown as Figure 4A. With systolic peak, dicrotic notch, and diastolic runoff, the well-known characteristics for arterial pulsation behavior could be observed clearly. The waveform of the directed movement shows three peaks located at 0.93 ms, 1.08 ms, and 1.15 ms and relative heights of 87.25, 83.30, and 84.31, respectively. Among them, the first peak (P1) represents maximum vascular pressure and there is a shoulder compared to a second peak (P2) and is followed by a shallower third peak (P3). The diastolic time could be calculated with first-order differential algorithm and selected to validate the correlation between the temporal characteristic and BP.

The linear relationship between the diastolic time and BP (SBP and DBP) is shown in **Figure 4B**. Because the diastolic period occupies most of the time in a cardiac cycle, the amount of blood transported by the large artery to the periphery may decrease with the reduction of diastolic time. As a result, the vascular part is filled with blood and induces a much higher pressure. These results were measured during the resting period on seven volunteers. Diastolic times (t) and BP measured with different volunteers all passed the *t* test with significant *p* < 0.05. The result demonstrates that the diastolic time could be preliminarily used for BP prediction.

To test the reliability and consistency of this approach, the *in vivo* experiments were conducted with seven healthy subjects. Every subject was tested more than 10 times. The statistical parameters, such as the average value and standard deviation,



FIGURE 4 | (A) Recognition of characteristic points of pulse wave and division of time periods. (B) Correlation of the diastolic time and blood pressure.



were calculated with each subject's results. As shown in **Figure 4**, the diastolic time varied in the range of 5% with stable PWV measurement.

Correlation Between Blood Pressure and Pulse Wave Velocity

To obtain the PWV, the pulse waves of forearm and fingertip were measured simultaneously. As shown in **Figure 5**, in addition to the different pulse shape, the pulse wave of fingertip is slightly delayed to forearm. The time delay between two locations is caused by the pressure wave propagation along the artery tree. At the cardiac frequency, the mean delay time is about 33.34 ms. Accordingly, the length of the arterial tree pass between the measured spots was about 34.50 cm. Based on **Eq. 9**, the PWV is about 10.36 m/s. Given the PWV determined in the human vascular system, as well as the theory of pulse propagation, our results seem realistic.

To determine the relationship between BP and PWV, the experiments were performed on five subjects. During exercise, the cardiac output and blood velocities are both increasing. That may cause additional flow resistance and consequent raise of blood pressure. The experimental results were approximated and validated by linear regression and presented in Figure 6. The coefficient of determination values between the SBP and PWV is in the range of 0.88-0.95. Thus, the linear regression model gives a good approximation between BP and PWV. However, SBP is highly related to the blood vessel elasticity, because it is caused by the heart's active and instantaneous pumping of blood. A rise in SBP causes temporary stiffening of the vessels, which results in a higher PWV. Meanwhile, DBP, which is related to the diastolic time and vascular recovery period, is not sensitive to changes in blood vessel elasticity. As a result, linear approximation of the relation between DBP and PWV shows lower level of correlation.



These results demonstrated that MMF-DSCA system achieved fast pulsatile blood flow measurement and extraction of the PWV and BP. However, this system and method also have some disadvantages. The fiber probe needs to be fixed on the location, and the measurement may be influenced by the motion artifacts. In clinical applications, the artifacts can be eliminated with improvements of fiber probe design and signal process. The fiber probe should be carefully designed and combined with special cuffs to fix the probe more stably on the arm and fingertip. Because the motion artifacts are generally embodied as DC or low-frequency signals, high-pass filtering can be used to eliminate the artifacts. Therefore, modern signal process methods, such as wavelet and empirical transverse decomposition filtering method, should also be used for further processing. Furthermore, with multiwavelength light sources, this system could be extended to measure oxygen saturation.

CONCLUSION

We present an MMF-DSCA system for measuring instantaneous blood flow and pulse wave velocity in deep tissue. With a CCD sensor, the diffuse speckle could be captured and processed at each frame. This approach enabled the observation of PWV in deep tissue with a temporal resolution of 3 ms. Optical synchronization of the speckle patterns measured in different body parts was achieved by using 2 MM fibers and a single CCD camera. The simultaneous measurement of pulsatile blood flow in different parts could be further analyzed to obtain the pulse wave characteristics. In this work, we also induced for the first time MMF-DSCA system for evaluation of PWV, which allows estimation of the systolic blood pressure. Taking advantages of being simple and cost-effective, the flexible system will be further developed for continuous monitoring of vital biosigns, such as heart rate and blood pressure, as part of individual healthcare.

DATA AVAILABILITY STATEMENT

The original contributions presented in the study are included in the article/Supplementary Material, further inquiries can be directed to the corresponding author.

ETHICS STATEMENT

Ethical review and approval was not required for the study on human participants in accordance with the local legislation and institutional requirements. The patients/participants provided their written informed consent to participate in this study.

AUTHOR CONTRIBUTIONS

CL was responsible for conceptualization, project administration, and funding acquisition. ZT was responsible for methodology, software, validation, formal analysis, investigation, data curation, and writing—original draft preparation. WC was responsible for resources and visualization. HX was responsible for writing—review and editing. FG was responsible for supervision. All authors have read and agreed to the published version of the manuscript.

ACKNOWLEDGMENTS

The authors thank every volunteer who offered help with the experiments. The authors acknowledge the financial support provided by the National Natural Science Foundation of China (81871396, 81971657, 81871393, and 81671727) and Tianjin Natural Science Foundation (19JCYBJC29100 and 19JCTPJC42200).

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Conflict of Interest: The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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