



# Stereo Perfect Metamaterial Absorber Based on Standing Gear-Shaped Resonant Structure With Wide-Incident-Angle Stability

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In this work, a single-band metamaterial absorber (MA) based on a three dimensional (3D) resonant structure is presented. The unit cell is composed of a standing gear-shaped resonator, which is embedded in the dielectric substrate. The proposed 3D MA is ultrathin with a total thickness of 2.3 mm, corresponding  $0.077\lambda_0$  at its center frequency. The simulation results demonstrate a high absorption peak at 10.1 GHz with absorptivity of 99.9%. The proposed 3D MA is insensitive to the polarization of the incident wave due to its rotationally symmetric structure. Moreover, the proposed 3D MA exhibits a wide-incident-angle stability, as absorptivity of more than 85% can be achieved for both TE and TM incidences with incident angle up to  $60^\circ$ . Most importantly, multiband electromagnetic wave absorption of the stereo MA can be enabled by adjusting the structural parameters of the standing gear. The proposed structure is compatible with 3D printing technology and has potential applications in electromagnetic shielding.

**Keywords:** metamaterial, absorber, three dimension, single-band, wide-incident-angle stability

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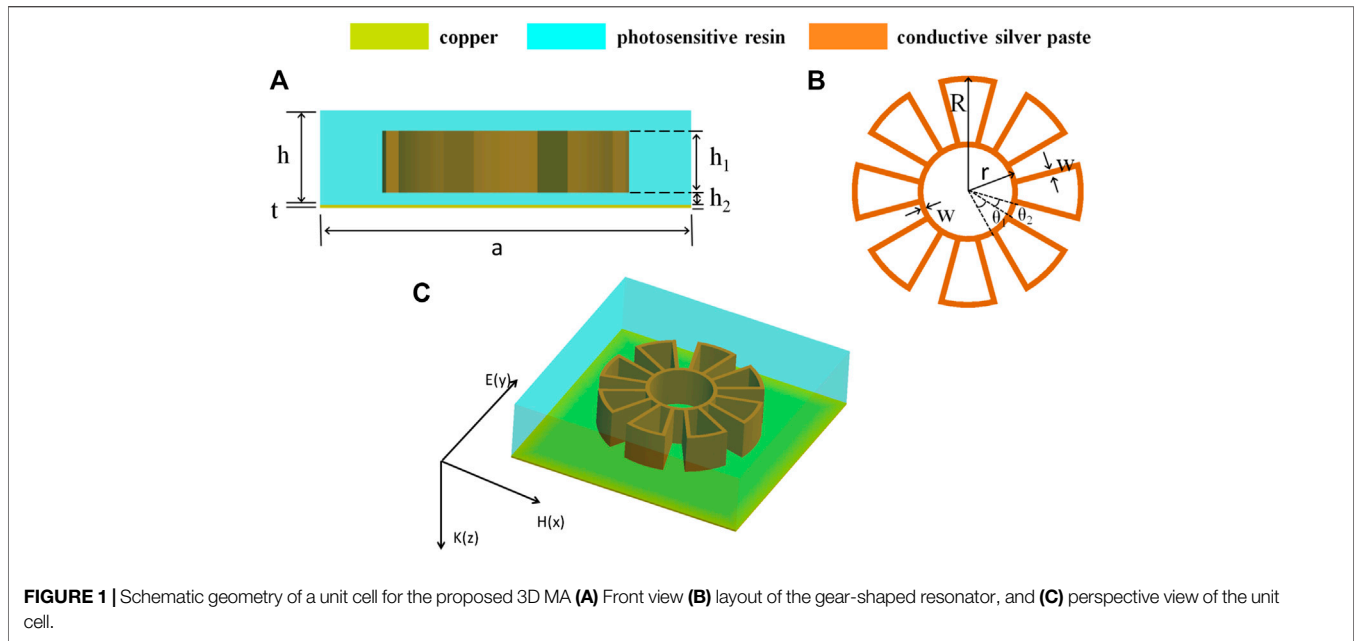
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## INTRODUCTION

Electromagnetic (EM) metamaterials that consist meta-molecules arranged in an array of subwavelength pe have attracted intense attention due to their unique properties, such as negative refractive index [1] and inverse Doppler effects [2]. Recently, the perfect absorber has been closely related to metamaterials, which has potential applications in biological sciences [3], sensing [4, 5], communications [6, 7] and solar energy harvesting [8].

The perfect metamaterial absorber (MA) was firstly presented by Landy et al. [9]. Since then the MAs have been designed to exhibit different characteristics such as single-band [10, 11], dual-band [12, 13], multiband absorption [14–17] and broadband absorption [18–21]. Till now, most of the reported MAs are based on planar resonators (2D structure) [11, 22–24]. However, the absorbing performance of the planar design will deteriorate significantly under oblique incidences with large incident angles.

Recently, the 3D printing technology [25] has experienced significant development and paved a way for the design and fabrication of 3D structures. One of the advantages of the 3D design scheme is that it can improve the design flexibility of the MA by providing additional freedom in structure design. Hence a 3D MA can enable higher absorption at oblique incidences. For instance, Wu et al. presented a symmetric all-metal three-dimensional (3D) MA by using two orthogonally oriented copper stand-up split ring resonators at THz frequency and obtained more than 90% THz wave



**FIGURE 1** | Schematic geometry of a unit cell for the proposed 3D MA (A) Front view (B) layout of the gear-shaped resonator, and (C) perspective view of the unit cell.

absorption for both TE and TM polarization with incident angle up to 60° [26]. Lv et al. [27] proposed a three-dimensional ultra-broadband metamaterial absorber with full graphite structure that exhibited excellent absorption properties at large incident angles.

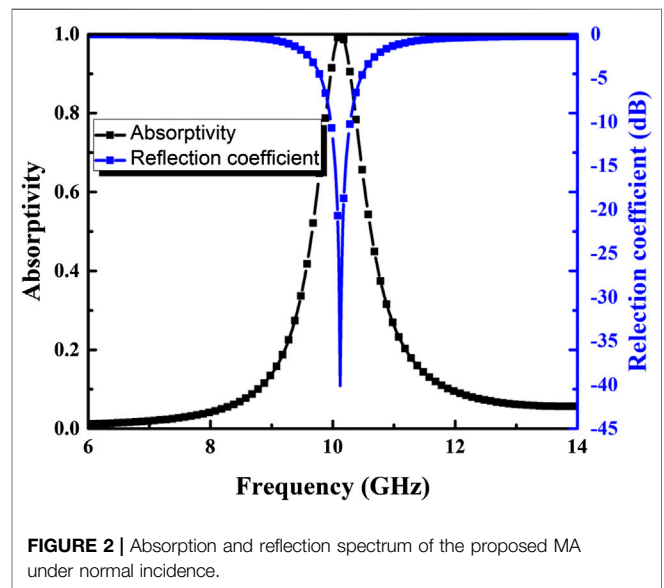
In this paper, a novel single-band and polarization-insensitive MA based on a 3D gear-shaped resonant structure is presented and near unity (99.9%) absorption at absorption peak frequency of 10.1 GHz under normal incidence is numerically demonstrated. Here, we introduce a new strategy on the design of 3D MAs by extruding planar resonator along its normal direction. Compared with the original planar resonant structure, the proposed structure can offer higher absorption for both TE and TM-polarized waves with large incident angles. The surface current and the field density distributions are investigated to explore the absorption mechanism of the 3D structure. Moreover, by adjusting the number of gear teeth, perfect single- or multi-band absorption can be achieved based on the stereo resonant structure. The proposed MA has the potential to be applied in the energy-harvesting and EM shielding applications.

### STRUCTURE DESIGN AND SIMULATION

**Figure 1** shows the geometry of a unit cell of the proposed single-band 3D MA. The standing gear-shaped 3D resonator made of silver ink with an electrical conductivity of  $\sigma = 5.88 \times 10^5$  S/m, is embedded in the dielectric substrate. Here, we select silver ink to construct metallic standing gear, as it is perfectly compatible with 3D printing technology. The substrate is realized on photosensitive resin with a relative permittivity of 2.9 and a loss tangent of 0.02. Moreover, in order to eliminate the EM wave transmission through the structure, a 0.017 mm thick copper

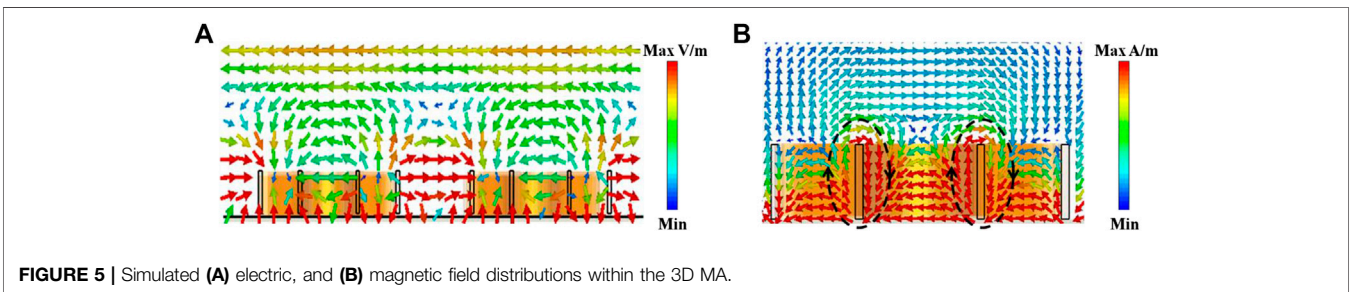
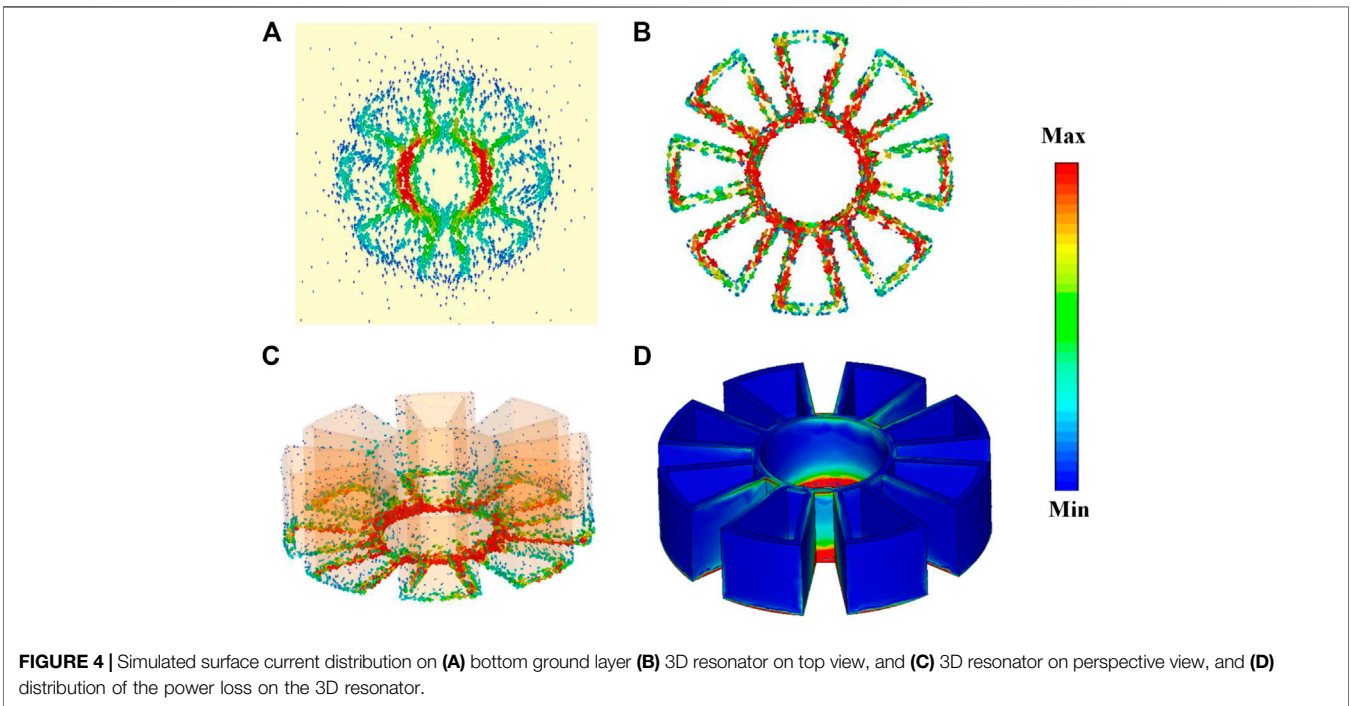
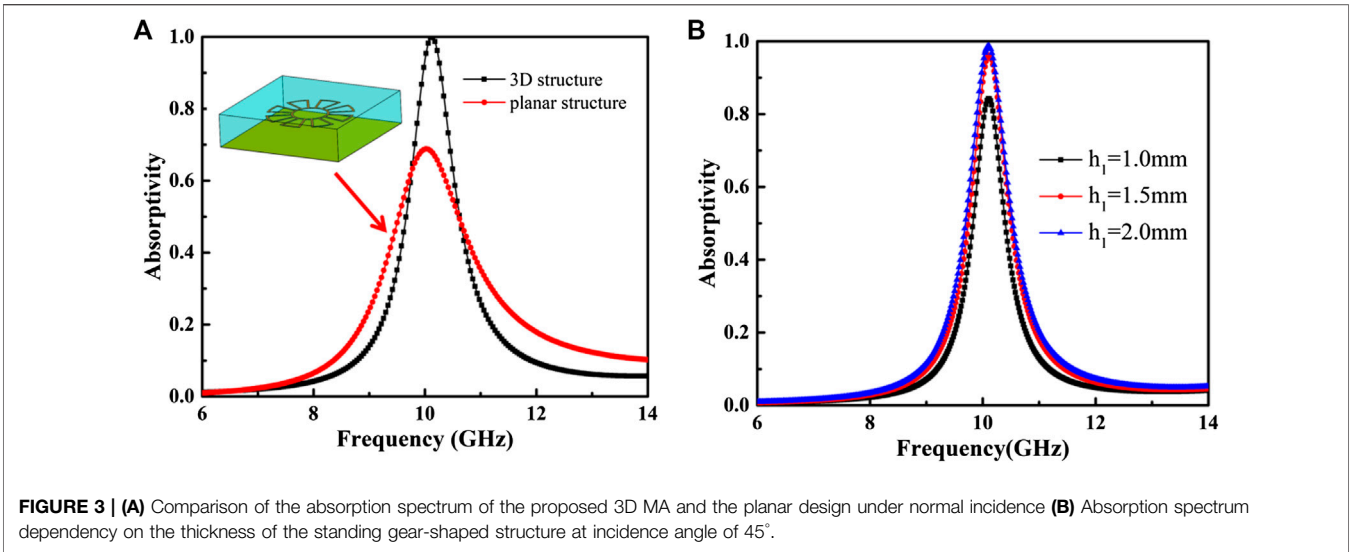
**TABLE 1** | Dimensions and parameters of the proposed 3D MA.

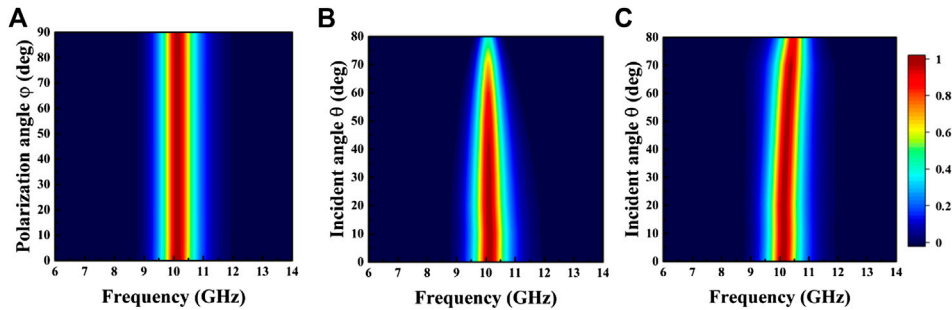
Parameter	Value (mm)	Parameter	Value (mm)	Parameter	Value (mm)
$a$	9	$h$	2.3	$w$	0.15
$R$	3	$h_1$	1.5	$\theta_1$	30°
$r$	1.3	$h_2$	0.1	$\theta_2$	15°



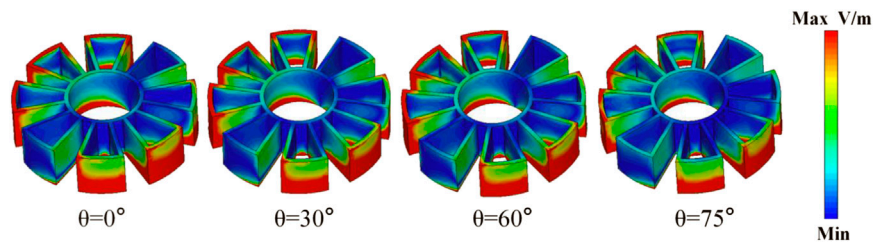
**FIGURE 2** | Absorption and reflection spectrum of the proposed MA under normal incidence.

plate with an electric conductivity of  $5.8 \times 10^7$  S/m is covered on the bottom of the structure as a ground plane. **Figure 1** shows the configuration of the unit cell structure, while the optimized parameters of the 3D MA are listed in **Table 1**. The simulation results were obtained using a finite-element method





**FIGURE 6** | Absorption spectra for (A) different polarization angles  $\varphi$  and different incidence angles  $\theta$  for (B) TE, and (C) TM polarization.



**FIGURE 7** | Simulated electric field distributions for TM polarization under different incident angles  $\theta$ .

(FEM). In the simulation, the unit cell boundary conditions were applied in  $x$  and  $y$  directions, and the open space boundary condition was utilized in the  $z$  direction. The absorptivity ( $A$ ) can be defined as  $A(\omega) = 1 - R(\omega) - T(\omega) = 1 - |S_{11}(\omega)|^2 - |S_{21}(\omega)|^2$ , where  $S_{11}(\omega)$  and  $S_{21}(\omega)$  are the reflection and the transmission coefficients, respectively. The transmission coefficient  $S_{21}(\omega)$  is zero due to the existence of copper ground. Therefore, the absorptivity can be simplified as  $A(\omega) = 1 - |S_{11}(\omega)|^2$ .

The simulated absorption spectrum of the proposed 3D MA under normal incidence is shown in **Figure 2**. It can be seen from **Figure 2** that there exists a sharp absorption peak located at 10.1 GHz with an absorptivity of 99.9%. Hence, the proposed MA exhibits perfect single band incident electromagnetic wave absorption.

## RESULTS AND DISCUSSION

**Figure 3A** compares the absorptivity of the proposed stereo structure and the planar design under normal incidence. It can be seen from the figure that the absorptivity of the stereo MA is much larger than that of the planar structure at peak resonant frequency. In order to analyze the dependence of the height of the stereo resonant structure ( $h_1$ ) on the EM wave absorption under oblique incidence, the influence of  $h_1$  on absorption spectrum at wave incident angle of  $45^\circ$  is simulated and the results are shown in **Figure 3B**. From **Figure 3B**, the absorptivity increases till a nearly perfect absorption with the increase of  $h_1$ , which demonstrates the outstanding absorbing performance of the proposed stereo structure at wide incidence angles.

The surface current distribution on the gear-shaped 3D resonator and the copper ground under the TM-polarized incidence at peak resonant frequency of 10.1 GHz are depicted in **Figure 4**. It can be seen from **Figure 4A** that the surface current on the stereo structure flows in the same direction along the E-field vector of the incident wave, where the electric resonance can be excited within the MA. Meanwhile, **Figure 4B** shows that the current is mainly concentrated in the inner ring of the standing gear-shaped structure, and the current flow direction in the copper ground is in reverse with that in the stereo resonant structure, as the anti-parallel current will lead to a magnetic resonance. Hence, both magnetic and electric resonances are responsible for EM wave absorption under normal incidence. **Figure 4C** illustrates the perspective view of the current distribution on the stereo gear-shaped resonator. Although the surface current is strongly concentrated in the bottom of the gear, the current flow on the side wall of the standing sectors also contributes the power consumption as shown in **Figure 4C**. The power loss distribution shown in **Figure 4D** confirms that the extra power consumption on the standing walls is responsible for the stronger absorption compared with planar structure. Moreover, from **Figure 4D**, one can anticipate more power dissipation on the walls by increasing the height of the standing gear, which is in accordance with our previous discussion of the absorption dependence on gear height  $h_1$ .

**Figure 5** shows the electric and magnetic field distributions to further explain the mechanism of the enhanced absorption of the stereo structure. It can be seen from the electric field distribution shown in **Figure 5A** that the strong coupling between adjacent

**TABLE 2** | The comparison of the absorption between the proposed MA and some reported MAs at different incident angles.

References	Structure	Normal	Absorption at 20°		Absorption at 40°		Absorption at 60°		Polarization insensitive
			TE	TM	TE	TM	TE	TM	
[25]	2D	95.8	>90	90	>90	80	>90	75	Yes
[26]	3D	99.6	>90	>90	>90	>90	>90	>90	Yes
[28]	2D	97.5	>90	>90	>90	>90	72	>90	Yes
[29]	2D	97	>95	>95	>95	>95	92	>95	Yes
This work	3D	99.9	99	99	98	99	86	99	Yes

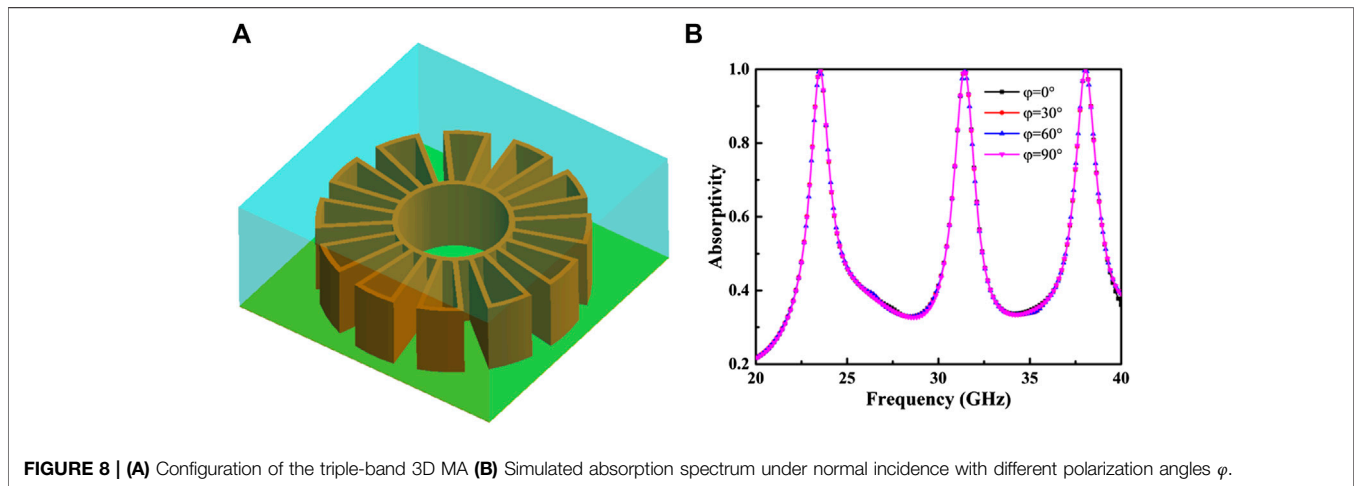
standing elements will enhance the intensity of electric resonance within the structure. Moreover, the magnetic field distribution illustrated in **Figure 5B** suggests that there exist two pairs of co-directional magnetic field rings due to the introduction of the standing walls. Since the magnetic rings can be regarded as an electric dipole, the oscillation of the dipole results in a strong electric response of the MA which further enhances the EM wave absorption.

## ABSORPTION SPECTRUM DEPENDENCE ON WAVE POLARIZATION AND INCIDENT ANGLE

In many practical applications, the characteristic of polarization-independent is an important criterion to evaluate the absorption performance of the MAs. **Figure 6A** illustrates the simulated absorption maps of the proposed MA under different polarization angles. It can be observed that the absorption of the MA is insensitive to different polarization angles, which is attributed to the rotationally symmetric layout of the cell structure.

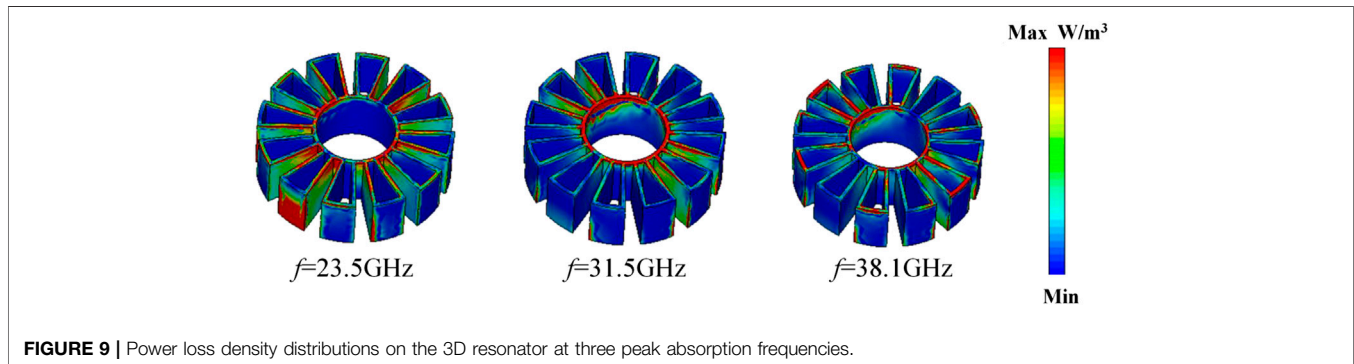
The absorbing performance of the stereo MA is further investigated for TE- and TM-polarized incidences at different incident angles, and the simulated results are shown in **Figures 6B,C**, respectively. For the TE-polarized incidence, the absorptivity remains above 85% with incident angle  $\theta$  up to 60°. However, the further increase of  $\theta$  leads to a dramatically degradation of EM wave absorption. For the TM-polarized incidence, the absorptivity remains greater than 90% when incident angle  $\theta$  reaches up to 80°. However, the absorption peak frequency slightly blue-shifted with the increase of  $\theta$ . Hence, the proposed structure exhibits wide-incident-angle stability for both TE and TM polarizations. In order to gain the electromagnetic response of the stereo structure under oblique incidences, the electric field distributions for TM-polarized incidence with incident angle  $\theta = 0^\circ, 30^\circ, 60^\circ$  and  $75^\circ$  are shown in **Figure 7**. It can be seen from the figure that both the distribution and the intensity of the electric field are insensitive to wave incident angle. Thus, the proposed stereo MA has a good capacity on effective EM wave absorption at wide incident angles. The equivalent circuit model for analysis of the absorption peaks under oblique incidence is not given in this paper. However, the mechanism can be briefly illustrated as follow: the impedance matching of free space and the input impedance of the stereo structure, which determines the absorptivity, is strongly dependent on the EM wave incident angle. Compared with the planar structure, the standing walls of the gear enables an extra compensation of impedance matching at wide incident angles, hence enhancing the wave absorption. In **Table 2**, we compared the performance of the proposed MA with some reported MAs at different incident angles. As it can be seen that our proposed structure exhibits stronger incident wave absorption under oblique incidences for both TE and TM polarization.

Another advantage of the proposed standing gear-shaped resonant structure is the adjustable perfect single- or multi-band absorption. In general, by increasing the amount of the



**TABLE 3 |** Dimensions and parameters of the triple-band 3D MA.

Parameter	Value (mm)	Parameter	Value (mm)	Parameter	Value (mm)
$A$	8	$h$	3.4	$W$	0.15
$R$	3.6	$h_1$	2.1	$\theta_1$	$20^\circ$
$R$	1.6	$h_2$	0	$\theta_2$	$10^\circ$



gear teeth, the resonant modes within the structure will also increase due to the enhanced coupling between these adjacent teeth. Hence, one can anticipate more absorption peaks with larger counts of gear teeth. For instance, a perfect triple-band absorption can be achieved by optimizing the structural parameters of the stereo structure. The layout and the absorption spectrum of the triple-band MA are illustrated in **Figure 8**, while the detailed parameter dimensions of the unit cell structure are listed in **Table 3**. The simulation results demonstrate three distinct absorption peaks at 23.5, 31.5, and 38.1 GHz with absorption of 99.9, 99.5, and 99.9%, respectively. **Figure 9** shows the power loss density distributions of the stereo triple-band MA for TE-polarized incidence at three resonant frequencies. It can be seen from **Figure 9** that the incident power is significantly consumed at the side wall and the top plane of the standing gear-shaped resonator for these three resonant peaks, which is different from the absorption mechanism discussed earlier in the article. Hence, the stereo

structure provides more degree of freedom in constructing multi-functional MAs compared with the planar design.

## CONCLUSION

A standing gear-shaped perfect metamaterial absorber with wide-incident-angle stability is presented in this paper. The stereo resonator that is constructed with conductive silver ink, can be embedded into the substrate using 3D printing technology. The rotationally symmetric structure enables the polarization-independent absorption of the proposed MA under normal incidence, while the stereo resonator also endows the MA with good absorbing capacity at wide incident angles. The simulation results demonstrate and validate that the proposed MA exhibits near unity single-band absorption under normal incidence. Moreover, for oblique incidences, the proposed MA maintains

absorptivity above 85 and 95% up to incident angles of 60° and 80° for TE and TM polarizations, respectively. In addition, a perfect multi-band absorption can be achieved by adjusting the structural parameters of the stereo structure. The stereo absorber has potential applications in the energy harvesting and stealth fields.

## DATA AVAILABILITY STATEMENT

The raw data supporting the conclusions of this article will be made available by the authors, without undue reservation.

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## AUTHOR CONTRIBUTIONS

GD conceived the research, wrote the manuscript; KL and HS conducted simulations and analysis, ZY and JY conducted analysis; KL wrote the manuscript.

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**Conflict of Interest:** The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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