



Experimental Demonstration of X-Ray Fluorescence CT Using a Spatially Distributed Multi-Beam X-Ray Source

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X-ray fluorescence computed tomography (XFCT) is a high-sensitivity imaging modality for high-atomic elements such as gadolinium (Gd) or gold (Au). In order to improve the contrast of x-ray fluorescence (XRF) signals in the raw projection data, common XFCT systems use single-pixel x-ray spectrometers to record XRF photons stimulated by the pencil-beam x-ray source and achieve line-by-line scan of the whole object by translating the x-ray source or the object. However, this kind of design results in waiting time of the translation device. One improvement would be to replace the traditional x-ray tube with a spatially distributed multi-beam x-ray source and scan the whole object by switching the exposure of each focus. In this study, we present a design of the XFCT system using a spatially distributed multi-beam source, and a XFCT imaging experiment was performed to investigate its feasibility. Each cold cathode of the x-ray source used in this study was made of carbon nanotubes, and each focus was independently controlled by the electronic control system. The incident beam was collimated by a pinhole array to produce a pencil-beam source. The object scanned by the system was a polymethyl methacrylate (PMMA) cylinder (8 cm in diameter) with Gd (20 mg/ml) and I (100 mg/ml) insertions. Results show that the distribution of iodine (I) and Gd in a PMMA phantom was successfully reconstructed, but the imaging performance was limited by the collimation and exposure mode of the current distributed x-ray source. The practicality of the current distributed x-ray source used for XFCT scan and further optimization of the proposed system are discussed according to the experimental results.

Keywords: x-ray fluorescence, computed tomography, carbon nanotubes, spatially distributed multi-beam x-ray source, x-ray spectrometer

INTRODUCTION

X-ray fluorescence computed tomography (XFCT), which detects the characteristic x-rays emitted from the target element, is a high-sensitivity imaging modality for high-atomic elements such as gadolinium (Gd) or gold (Au). As the signal of XFCT is independent from background tissues, the concentration distribution of the target element obtained by XFCT has lower background noise and higher contrast than the traditional transmission CT [1, 2]. Therefore, XFCT has been considered as a promising approach for applications of imaging of certain elements with low concentration, such as *in vivo* imaging of nanoparticle probes [3–7].

Early studies of XFCT experiments often use synchrotron beams to stimulate x-ray fluorescence (XRF) photons [8]. The x-ray beam produced by the synchrotron beam is monochromatic and linear

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polarized so that the energy of incident photons can be adjusted to maximize the fluorescence field, and the Compton scattered background can be effectively reduced by optimizing the detection angle [9–11]. However, the research and application of XFCT based on synchrotron is limited by its requirement of space and cost. Although synchrotron beam is the ideal source for XFCT, researchers focus more on the XFCT system based on conventional x-ray tubes in recent years [12–15].

In order to improve the contrast of x-ray fluorescence (XRF) signals in the raw projection data, common XFCT systems use single-pixel x-ray spectrometers to record XRF photons stimulated by the pencil-beam x-ray source and achieve line-by-line scan of the whole object by translating the incident beam or the rotation stage [16–19]. Another kind of system design is to use a cone-beam source to irradiate the whole object and then use the panel detector with pinhole collimation to record the intensity and spatial information of XRF photons [20–24]. Compared with the linear design, the projection data obtained by the first kind of system have higher sensitivity and lower scattered background due to the high-energy resolution of the spectrometer. However, this kind of scan strategy results in waiting time of the translation device.

One improvement would be to replace the traditional x-ray tube with the spatially distributed multi-beam x-ray source [25–27] and scan the whole object by switching the exposure of each focus. Stationary CT technique using the distributed x-ray source, as well as its application on a transmission CT field such as baggage inspection, is now in rapid development due to its higher scanning speed than that of traditional spiral CT [28–30]. To our knowledge, relevant research report about XFCT using the spatially distributed multi-beam x-ray source has not been previously published. Therefore, a design of the XFCT system using the spatially distributed multi-beam source in this study and a XFCT imaging experiment was performed to investigate its feasibility.

Each cold cathode of the x-ray source used in the experimental device was made of carbon nanotubes, and each focus was independently controlled by the electronic control system. The incident beam was collimated by a pinhole array to produce a pencil-beam source. The object scanned by the system was a polymethyl methacrylate (PMMA) cylinder (8 cm in diameter) with Gd (20 mg/ml) and iodine (I) (100 mg/ml) insertions. The spectrum of

projection data was recorded by a single-pixel x-ray spectrometer. Results show that the distribution of I and Gd in a PMMA phantom was successfully reconstructed, but the imaging performance was limited by the collimation and exposure mode of the current distributed x-ray source. The practicality of the current distributed x-ray source used for XFCT scan and further optimization of the proposed system are discussed according to the experimental results.

MATERIALS AND METHODS

System Geometry

The structure of the x-ray source [31] used in this study is shown in **Figure 1A**. Multiple anodes are integrated in one vacuum chamber. Common x-ray tubes with single focus produce electron beams through the hot cathode, which results in high difficulty of integration and slow start. Therefore, the material of each cold cathode in this study is carbon nanotubes, which enables rapid switching of start–stop. The anode material is tungsten, and the spectrum is the same as the bremsstrahlung spectrum produced by conventional x-ray tubes with tungsten anodes. The x-ray exposure of each cathode–anode component is controlled by the corresponding electronic control system.

As shown in **Figure 1B**, the system design of the XFCT device in this study is composed of a spatially distributed multi-beam x-ray source arranged in a straight line, an array collimator made of tungsten, a rotation stage, and an x-ray spectrometer. The distance between the x-ray source and the collimator is 9.6 cm, and the distance between the center of the collimator and the rotation stage is 7 cm. The spectrometer is placed on the side of the beam path to collect the XRF signal stimulated along the path of the incident beam so that each pixel value of the projection data corresponds to the line integral of the intensity of the XRF signal along a certain path in the object. The distance between the spectrometer and the rotation stage is about 14 cm.

Pencil-Beam Collimator

As many anodes are integrated in one vacuum chamber, the internal structure of the x-ray source used in this study is compact and it is difficult to place the collimator inside the chamber, which





results in a long distance between the target and the pinhole collimator. Therefore, the incident photons will pass through not only the pinhole corresponding to the target but also the adjacent pinholes, forming multiple pencil beams (as shown in **Figure 2**).

The point spread distribution caused by array pinhole collimation will seriously affect the spatial resolution of the imaging system, so it is necessary to optimize the collimation parameters to reduce the loss of spatial resolution. In this study, the distance between the target and the collimator is 10 cm. Each

TABLE 1 Collimation results with different pinhole spacing.		
Pinhole spacing (mm)	Number of pencil beams	Proportion of the primary beam (%)
4	5	59.2
8	3	98.1
12	1	100

pinhole is 1 mm in diameter and 12 mm thick. The target spacing of each focus is 4 mm, so the pinhole spacing has to be the integral multiple of 4 mm. The collimation effect with different pinhole spacing was simulated, and the results are shown in **Figure 3**. The number of pencil beams produced by the collimator and the proportion of the primary beam are listed in **Table 1**. According to the simulation results, there are up to five pencil beams produced by the collimator is 4 mm with the proportion of the primary beam being only 59.2%. When the pinhole spacing is 12 mm, the collimation effect is ideal but the spatial resolution is extremely limited. Therefore, the design of the collimator with 8-mm pinhole spacing was applied in this study (3 pencil beams with the primary beam being only 59.1%).

Energy Calibration

Energy calibration of the x-ray spectrometer was performed before XFCT scan. $K\alpha$ XRF photons of different high-atomic



elements were used as the quasi-monochromatic source for energy calibration in this study. The fluorescent materials used for calibration were NaI (K α = 28.6 keV), GdO (K α = 42.9 keV), W (K α = 59.3 keV), and Pb (K α = 74.9 keV). Each material was irradiated by an x-ray tube (110 kVp, 0.5 mA), and the spectrometer was placed on one side of the beam line to record the XRF spectrum. The spectrum measurement results of different materials are shown in Figure 4.

The channel number corresponding to the XRF peak was calculated using the second derivative peak search method, and the linear relationship between channel number and energy was then fitted by the least square method (as shown in **Figure 5**).





FIGURE 6 | X-ray fluorescence computed tomography experimental device based on the spatially distributed multi-beam source.



According to the calibration results, the position of XRF peaks of different materials can be determined and then the XRF signal intensity can be extracted from the spectrum of the projection data.

EXPERIMENTS

Experimental Device

The XFCT experimental device used in this study is shown in **Figure 6**. The phantom was irradiated by the x-ray source operating on pulse-out mode (110 kVp, 10 mA, 1% duty cycle) with a pinhole array collimator. A CdTe x-ray spectrometer (Amptek XR100) with lead shield was placed on one side of the rotation stage collecting the XRF photons. The pinhole spacing was 8 mm, and 11 targets were used to irradiate the whole phantom. Eighteen projection angles were scanned with the angle interval of 20° and the scanning time of 30 s per sample point, resulting in the total scanning time of about 100 min and the total exposure time of 59.4 s.

The collimation effect of a single cone-beam source was measured, and the results are shown in **Figure 7**. It can be seen that the primary beam was not an ideal circle, which is caused by the rectangle shape of the focal spot. In addition to the

primary beam directly facing the target, there were also a small amount of incident photons passing through the two adjacent pinholes, and the measured proportion of the primary beam was about 83.3%, which is relatively smaller than the simulation results in **Figure 3** due to the nonideal focal spot size. The point spread function (PSF) of each target was calculated according to **Figure 7** and was used for the calculation of the reconstruction system matrix.

Phantom

As shown in **Figure 8**, the phantom used in the XFCT experiment was a PMMA cylinder which was 8 cm in diameter with insertions of Gd (20 mg/ml) and I (40 and 100 mg/ml) solutions. Two kinds of fluorescent materials were scanned and imaged simultaneously using the experimental system shown in **Figure 6**.

Results

The spectrum of the projection data $(11 \times 18 \text{ sample pixels})$ was measured during the XFCT scanning. The Compton scattered background curve was fitted by the cubic polynomial method, and the XRF peaks of I and Gd in each sample pixel were then extracted. The fitting results are shown in **Figure 9**. The XRF signal of I and Gd after extraction from the raw projection data is shown in **Figure 10**. As the complete spectrum was already obtained, simultaneous scanning of multiple XRF signals from different elements was enabled.

The XFCT images (40 \times 40 pixels with the pixel size of 2.5 mm \times 2.5 mm) were reconstructed using the EM-TV algorithm:

$$f_{j}^{(k+1)} = \left(1 - \beta U_{j}^{TV(k)}\right) \frac{f_{j}^{(k)}}{\sum_{i=1}^{m} a_{ij}} \sum_{i=1}^{n} \frac{P_{i}}{\sum_{j'=1}^{n} a_{ij} f_{j'}^{(k)}} a_{ij}, \qquad (1)$$

where f_j denotes the *j*th pixel of the reconstructed image (*j* = 1, 2, ..., 1,600), P_i denotes the *i*th pixel of the projection (*i* = 1, 2, ...,







198), and a_{ij} denotes an element of the system matrix which can be expressed as

$$a_{ij} = C_{ij} S_{ij} P_{ij} , \qquad (2)$$

where C_{ij} is a constant related to the fluorescence yield of the target elements and scanning parameters, S_{ij} denotes the attenuation of incident photons and fluorescent photons in the object, and P_{ij} denotes the contribution of image pixel *j* to projection pixel *i*, which can be calculated according to the system geometry and the measured PSF of the incident beam.

The parameter β (β = 0.25 in this study) controls the weight of TV norm U_i^{TV} , which can be expressed as

$$U_{j}^{TV(k)} = \frac{\partial \left(\sum_{m,n} \sqrt{\left(f_{m,n}^{(k)} - f_{m,n+1}^{(k)}\right)^{2} + \left(f_{m,n}^{(k)} - f_{m+1,n}^{(k)}\right)^{2}}\right) / \partial f_{m,n}^{(k)}}{\sqrt{\left(f_{m,n}^{(k)} - f_{m,n+1}^{(k)}\right)^{2} + \left(f_{m,n}^{(k)} - f_{m+1,n}^{(k)}\right)^{2} + \varepsilon}}, \quad (3)$$

where *m*,*n* is the coordinate of image pixel *j* and ε is a small value preventing the denominator to be zero.

The reconstructed images of the two elements are shown in **Figure 11** and the image fusion result is shown in **Figure 12**. According to the experimental results, the distribution of I and Gd in a PMMA phantom was successfully reconstructed, which indicates the feasibility of XFCT imaging using a spatially distributed multi-beam x-ray source. However, it can also be seen that the spatial resolution and scanning efficiency of this experimental device are not optimal. There are two main factors which limit the image performance: one is the distance between the pinhole collimator and the target, which results in an imperfect pencil beam and reduction of spatial resolution; the other factor is the pulse-out mode of the x-ray source used in this study with low duty cycle (1%), which seriously reduces the scanning efficiency and image sensitivity.



DISCUSSION

One main factor limiting the practicability of the XFCT system with pencil beam is the long scanning time. The movement of the pencil-beam source is required to scan the whole object, which results in waiting time of mechanical movement. An XFCT experimental device based on a spatially distributed multibeam source using carbon nanotubes is presented in this study. Compared with the traditional design of the XFCT



system, the translation of the pencil-beam source was replaced by successive exposure from different focal spots. The exposure of each focal spot can be switched instantly so that the time consumption caused by translating the x-ray source is avoided.

The distribution of I and Gd was successfully reconstructed, which indicates the feasibility of XFCT imaging using the proposed system. As the x-ray source used in this experimental device was originally designed for transmission CT, there is still room for further improvement of its spatial resolution and scan efficiency. However, these defects are not in imaging principle and can be solved by optimization of the collimation and exposure mode of this x-ray source specifically for XFCT imaging.

The spatial resolution of the projection was 8 mm in this study, and only half the number of the focal spots was used (the spacing of the focal spots is 4 mm). As we are unable to place the external collimator inside the chamber limited by the compact chamber design, the distance between the focal spot and the collimator results in weakness of the collimating effect and reduction of the spatial resolution. A new design of the vacuum chamber taking into consideration the pinhole collimation may enable the collimator to be close to the focal spot so that all the focal spots could be used and the sampling density of each projection angle could be improved effectively.

Although there was no time consumption caused by translating the x-ray source, the total scan time (about 100 min) of the experiment was still much longer than the real exposure time (59 s) because the x-ray source in this study was operating on pulse-out mode with the duty cycle of only 1%. The total scan time could be further reduced by

making full use of the duty cycle, such as switching the focal spots instead of waiting for the next pulse of the current focal spot, and then collecting data of the corresponding projection.

CONCLUSION

A design of the XFCT system using a spatially distributed multibeam x-ray source is presented in this study. Simultaneous XFCT imaging of I and Gd was performed on an experimental device to investigate the feasibility of the proposed system, and the distribution of I (40 mg/ml) and Gd (20 mg/ml) in a PMMA phantom was successfully obtained. The limitations of the current experimental device and corresponding improvement methods are discussed according to the experimental results. Our future work will focus on further optimization of the spatial resolution and scanning efficiency of the current system.

DATA AVAILABILITY STATEMENT

The raw data supporting the conclusions of this article will be made available by the authors, without undue reservation.

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AUTHOR CONTRIBUTIONS

The research about the XFCT using a spatially distributed multibeam x-ray source was proposed by ZC. The research funds were provided by ZC. The experiments were designed by LL and were carried out by SZ. The manuscript was written by SZ and revised by ZC and LL.

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Conflict of Interest: The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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