



Entropy Optimization of Third-Grade Nanofluid Slip Flow Embedded in a Porous Sheet With Zero Mass Flux and a Non-Fourier Heat Flux Model

K. Loganathan^{1*}, G. Muhiuddin^{2*}, A. M. Alanazi², Fehaid S. Alshammari³, Bader M. Alqurashi⁴ and S. Rajan¹

¹ Department of Mathematics, Erode Arts & Science College, Erode, India, ² Department of Mathematics, University of Tabuk, Tabuk, Saudi Arabia, ³ Department of Mathematics and Statistics, Imam Mohammad Ibn Saud Islamic University, Riyadh, Saudi Arabia, ⁴ Department of Mathematics, Faculty of Arts and Science in Almandag, Albaha University, Albaha, Saudi Arabia

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*Correspondence:

G. Muhiuddin chishtygm@gmail.com K. Loganathan loganathankaruppusamy304@ gmail.com

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Loganathan K, Muhiuddin G, Alanazi AM, Alshammari FS, Alqurashi BM and Rajan S (2020) Entropy Optimization of Third-Grade Nanofluid Slip Flow Embedded in a Porous Sheet With Zero Mass Flux and a Non-Fourier Heat Flux Model. Front. Phys. 8:250. doi: 10.3389/fphy.2020.00250 The prime objective of this article is to explore the entropy analysis of third-order nanofluid fluid slip flow caused by a stretchable sheet implanted in a porous plate along with thermal radiation, convective surface boundary, non-Fourier heat flux applications, and nanoparticle concentration on zero mass flux conditions. The governing physical systems are modified into non-linear ordinary systems with the aid of similarity variables, and the outcomes are solved by a homotopy analysis scheme. The impression of certain governing flow parameters on the nanoparticle concentration, temperature, and velocity is illustrated through graphs, while the alteration of many valuable engineering parameters viz. the Nusselt number and Sherwood number are depicted in graphs. Entropy generation with various parameters is obtained and discussed in detail. The estimation of entropy generation using the Bejan number find robust application in power engineering and aeronautical propulsion to forecast the smartness of entire system.

Keywords: entropy generation, Christov-Cattaneo heat flux, third-grade nanofluid, porous medium, homotopy analytic technique

INTRODUCTION

Nanoliquids are the type of liquids that have small volumetric quantities of nanoscale $(10^{-9} - 10^{-7} \text{m})$ metallic (Cu, Ti, Hg, Fe, Ag, Au, etc.)or non-metallic particles (TiO₂, SiO₂, CuO, Al₂O₃, etc) taken as nano particles. Usually nanoliquids have a colloidal suspension of nanoparticles inside a base liquid for example water, oil, ethylene glycol, etc. Initially, Choi [1] proposed the "nanofluid" term. In general, the effective heat transfer enhancement has the reason of nanoliquids generally restrict up to volume fraction of nanoparticles. Therefore, in the latest technologies and engineering areas, nanoliquids receiving a phenomenal impact. Mushtaq et al. [2] attempted the numerical study of the nanoliquids induced by an exponentially stretchable sheet with rotating flow model. MHD nanoliquid flow toward a porous plate with internal heat generation effects was presented by Reddy and Chamka [3]. Shit et al. [4] studied the convective flow of hydromagnetic nanoliquid with entropy generation mechanism. Recently, Gireesha et al. [5] explained a Hall current effects of two-phase transient nanoliquid flow induced by a stretchable sheet. Reddy et al. [6] performed the combined convection flow of nanoliquid toward a semi-infinite vertical flat sheet with convectively heated boundary and Soret effect. Few more significant studies in this research area are seen in ref's [7-13].

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Due to various applications in different technical and industrial areas, the fluid flow problems toward a stretching surface have developed. It finds application in rubber and plastic sheets production, melt-spinning, production of glass-fiber, and metallic plate cooling systems. Sakiadis [14] studied the uniform velocity of a magnetohydrodynamic flow past a solid medium. Magyari et al. [15] examined the first order chemical reaction and heat generation combination on micropolar fluid flow induced by a permeable stretching surface. Gupta [16] analyzed the heat and mass transfer effects of a boundary layer flow induced by a stretchy sheet with suction or blowing impact. Magyari and Keller [17] exposed the fluid flow over exponentially extending sheet with heat and mass transfer impacts. Significances of thermal boundary layer flow for a linearly stretchy sheet with viscous dissipation were examined by Cortell [18]. The cutting-edge research reports on stretching sheet flow are highlighted in these works of literature [19-24].

Fluid flow saturated in the porous surface have numerous applications in various fields like geothermal energy, fuel cell technologies, material processing, etc. Chamkha et al. [25] described the free convective flow past an inclined plate fitted in a porous medium of variable porosity with solar radiation. Khan and Aziz [26] studied the natural convective flow with double diffusion caused by a vertical porous sheet. Oyelakin et al. [27] analyzed the slip flow of unsteady radiative Casson nanofluid toward a stretchy surface. Gorla and Chamkha [28] studied the nanofluid flow toward a non-isothermal vertical plat entrenched in a porous sheet. The same research group extended their work for different models for various applications [29–32].

Heat transport problems in the flow of liquids have been examined by several researchers for the last decade. In 1822, Fourier [33] constructed the heat conduction law. This states that "the heat transfer in a medium with inertial rate." A parabolictype equation was used to state the heat conduction equation. The problem rising at this time is that there exists no such object or material that satisfies Fourier's law, as argued by Cattaneo [34] when using thermal relaxation time to customize Fourier's law. Later, Christov [35] developed and joined the upper convected Maxwell fluid. This developed model is called a Christov-Cattaneo heat flux model. Loganathan et al. [36] studied the thermal relaxation time effects on Oldroyd-B liquid with second-order slip and cross-diffusion impacts. The Christov-Cattaneo heat flux model for a third-grade liquid with chemical reaction effects was examined by Imtiaz et al. [37].

In the last decade, several scientists have researched entropy generation in the flow of fluids and heat transfer over a stretching surface. In various engineering and industrial divisions, the performance of heating and cooling are of massive importance in different electronic and energy issues. Aiboud and Saouli [38] examined the MHD viscoelastic fluid flow with the application of entropy analysis using Kummer's function. Makinde [39] presented the thermal radiation and Newtonian heating impacts of variable viscosity fluid caused by a semi-infinite plate using shooting quadrature and obtained the entropy generation number. Loganathan et al. [40, 41] verified the entropy analysis for the third grade and Williamson nanoliquid flow caused by a stretchable sheet with various effects. They employed HAM to solve the non-linear governing systems.

Based on our research in previously published works, entropy generation of third-grade nanofluid flow caused by a stretching sheet with a modified Fourier law has not been discussed with a high standard of scientific attention. As far as we noticed in literature, the studies taken for entropy generation are limited with some parameters viz the Brinkmann number, Reynolds number, Temperature difference parameter, and Hartmann number. We have extended our investigations to include thermal relaxation time, the Biot number, thermal radiation, slip parameter, porous parameter, etc. The effective collection and analysis of these results will open new gateways for diverse engineering application in various streams.

PROBLEM DEVELOPMENT

We were interested in analyzing the entropy and Bejan number of third-grade nanofluid saturated in a porous medium with Christov-Cattaneo heat flux. In **Figure 1**, the stretching parameter is taken along x direction where T_W and C_W are represented the wall temperature and concentration, respectively. T_{∞} and C_{∞} are used to index the ambient temperature and concentration, respectively. A convective heating temperature T_f is stimulated at the bottom of the sheet surface. The Buongiorno nanofluid [42] is used for the present case.



Based on his consideration, the slip mechanisms, namely, the Brownian diffusion, inertia, Magnus effect, diffusiophoresis, thermophoresis, gravity, and fluid drainage, were analyzed. He recommended that the thermophoresis and Brownian diffusion are essential slip mechanism in low dimensional materials.

The following is an incompressible fluid model containing body forces with the equation of continuity and motion:

$$div v = 0 \tag{1}$$

$$\rho \frac{dv}{dt} = divT + \rho b + J + B \tag{2}$$

Here, ρ is the fluid density, which is taken as a constant, ν is the velocity field, *b* indicates the body forces, *J* denotes the electric current, and *T* states the third-grade incompressible fluids Cauchy stress tensor [43]

$$T = -pI + \mu E_1 + A_1^* E_2 + A_2^* E_1^2 + \beta_1 E_3 + \beta_2 (E_1, E_2 + E_2 E_1) + \beta_3 (tr E_1^2) E_1$$
(3)

where μ , (E_1, E_2, E_3) and A_1^* , β_i indicate the viscosity coefficient, kinematics tensors, and material modulis as in

$$E_1 = L + (L)^T \tag{4}$$

$$E_n = \frac{d}{dt}E_{n-1} + E_{n-1}L + (L)^T E_{n-1}, \quad n = 2, 3, \text{and}$$
 (5)

$$L = \nabla v. \tag{6}$$

 $\frac{d}{dt}$ is expressed as the material time derivative

$$\frac{d()}{dt} = \frac{\partial()}{\partial t} + \nu. \nabla().$$
(7)

The relationship between Clausius-Duhem inequality and thermodynamically compatible fluid is stated by Fosdick and Rajagopal [44]:

$$\mu \ge 0, A_1^* \ge 0, \beta_1 = \beta_2 = 0, \beta_3 \ge 0$$
 (8)

$$\left|A_{1}^{*} + A_{2}^{*}\right| \le 2\sqrt{6\mu\beta_{3}} \tag{9}$$

$$T = -pI + \mu E_1 + A_1^* E_2 + A_2^* E_1^2 + \beta_3 \left(tr E_1^2 \right) E_1$$
(10)

Boussinesq and normal boundary layer approximations were considered by Pakdemirli [45]. We made the following assumptions:

- 1. The nanoparticles are small and of equal size to the pores.
- 2. The zero-mass flux of the nanoparticles is included.
- 3. Christov-Cattaneo heat flux is considering instead of normal heat flux.
- 4. The magnetic field in the fluid flow is ignored due to a lower magnetic Reynolds number.

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0 \tag{11}$$

$$u\frac{\partial u}{\partial x} + v\frac{\partial u}{\partial y}$$

= $v\frac{\partial^2 u}{\partial y^2} + \frac{A_1^*}{\rho} \left(u\frac{\partial^3 u}{\partial y^2 \partial x} + v\frac{\partial^3 u}{\partial y^3} + \frac{\partial u}{\partial x}\frac{\partial^2 u}{\partial y^2} + 3\frac{\partial u}{\partial y}\frac{\partial^2 u}{\partial x \partial y} \right)$
+ $2\frac{A_2^*}{\rho}\frac{\partial u}{\partial y}\frac{\partial^2 u}{\partial x \partial y} + 6\frac{\beta_1^*}{\rho} \left(\frac{\partial u}{\partial y}\right)^2\frac{\partial^2 u}{\partial y^2} - \frac{\sigma B_0^2}{\rho}u - \frac{v}{k_p}u$ (12)

$$u\frac{\partial T}{\partial x} + v\frac{\partial T}{\partial y} = \frac{k}{\rho c_p}\frac{\partial^2 T}{\partial y^2} - \frac{1}{\rho c_p}\frac{\partial q_r}{\partial y} + \frac{Q_0}{\rho c_p}(T - T_\infty) \quad (13)$$
$$+ \tau \left[D_B \frac{\partial C}{\partial y}\frac{\partial T}{\partial y} + \frac{D_T}{T_\infty} \left(\frac{\partial T}{\partial y}\right)^2 \right]$$

$$u\frac{\partial C}{\partial x} + v\frac{\partial C}{\partial y} = D_B \frac{\partial^2 C}{\partial y^2} + \frac{D_T}{T_\infty} \frac{\partial^2 T}{\partial y^2}$$
(14)

$$u = u_w (x) = ax + L \frac{\partial u}{\partial y}, \quad -k \frac{\partial T}{\partial y} = h_f \left(T_f - T_\infty\right),$$

$$D_B \frac{\partial C}{\partial y} + \frac{D_T}{T_\infty} \frac{\partial T}{\partial y} = 0 \text{ at } y = 0$$

$$u \to 0, \ T \to T_\infty, \ c \to c_\infty \text{ as } y \to \infty$$
(15)

The energy equation with a Cattaneo-Christov heat flux model is stated as

$$u\frac{\partial T}{\partial x} + v\frac{\partial T}{\partial y} + \lambda_T \left(u^2 \frac{\partial^2 T}{\partial x^2} + v^2 \frac{\partial^2 T}{\partial y^2} + \left(u\frac{\partial u}{\partial x}\frac{\partial T}{\partial x} + v\frac{\partial u}{\partial y}\frac{\partial T}{\partial x} \right) + 2uv \frac{\partial T^2}{\partial x \partial y} \right) + \left(u\frac{\partial v}{\partial x}\frac{\partial T}{\partial y} + v\frac{\partial v}{\partial y}\frac{\partial T}{\partial y} \right) = \frac{k}{\rho c_p}\frac{\partial^2 T}{\partial y^2} - \frac{1}{\rho c_p}\frac{\partial q_r}{\partial y} + \frac{Q_0}{\rho c_p} \left(T - T_\infty \right) + \tau \left[D_B \frac{\partial C}{\partial y}\frac{\partial T}{\partial y} + \frac{D_T}{T_\infty} \left(\frac{\partial T}{\partial y} \right)^2 \right].$$
(16)

Consider the transformation given below:

$$\psi = \sqrt{av}xf(\eta), \ u = \frac{\partial\psi}{\partial y}, \ v = -\frac{\partial\psi}{\partial x}, \ \eta = \sqrt{\frac{a}{v}}y,$$
$$v = -\sqrt{av}f(\eta), \ u = axf'(\eta), \ \theta(\eta) = \frac{T - T_{\infty}}{T_f - T_{\infty}},$$
$$\phi(\eta) = \frac{C - C_{\infty}}{C_{\infty}}.$$
(17)

The non-linear governing equations are:

$$f^{'''} + ff^{''} - f^{'^2} + \alpha_1 \left(2f'f^{'''} - ff^{i\nu} \right) + (3\alpha_1 + 2\alpha_2) f^{''^2} + 6\beta Ref^{'''}f^{''^2} - (Mf' + Kf') = 0$$
(18)

$$\left(1 + \frac{4}{3}Rd\right)\theta'' + Prf\theta' + PrS\theta - Pr\gamma f^{2}\theta'' - Pr\gamma ff'\theta' + PrNb \theta'\phi' + PrNt\theta'^{2} = 0$$
(19)

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$$\phi'' + Lef\phi' + \frac{Nt}{Nb}\theta'' = 0$$
⁽²⁰⁾

with the end points

$$f(0) = f_w, f'(0) = 1 + \Gamma f''(0), \theta'(0) = -Bi(1 - \theta(0)),$$

$$Nb \phi'(0) + Nt \theta'(0) = 1$$

$$f'(\infty) = 0, \theta(\infty) = 0, \phi(\infty) = 0$$
(21)

The non-dimensional variables are

$$\alpha_{1} = \frac{aA_{1}^{*}}{\nu}, \alpha_{2} = \frac{aA_{2}^{*}}{\nu}, \beta = \frac{a\beta_{1}^{*}}{\nu}, Re = \frac{u_{w}x}{\nu}, Pr = \rho C_{p}/k,$$

$$M = \sigma B_{0}^{2}/\rho a, Rd = \left(4\sigma^{*}T_{\infty}^{3}\right)/\left(kk^{*}\right), S = \frac{Q_{0}}{\rho c_{p}}, \gamma = \lambda_{T}a,$$

$$Bi = \frac{h_{f}}{k}\sqrt{\frac{\nu_{a}}{\nu}}, Nb = \frac{\tau D_{B}}{\nu}\left(C_{\infty}\right), Nt = \frac{\tau D_{T}}{\nu}\left(T_{f} - T_{\infty}\right).$$

The application of physical entitles is such that

$$Re^{\frac{1}{2}}C_{f} = f^{''}(0) + \alpha_{1}f^{\prime}(0)f^{'''}(0) + \beta Re[f^{''}(0)]^{3}$$
(22)

$$Re^{-\frac{1}{2}}Nu_{x} = -(1 + \frac{4}{3}Rd)\theta'(0).$$
(23)

The local mass transfer rate becomes identically zero due to the zero mass flux state [46]

$$Re^{-\frac{1}{2}}Sh = \frac{Nt}{Nb}\theta'(0).$$
(24)

ENTROPY OPTIMIZATION

The entropy minimization optimization for fluid friction, heat, and the irreversibility of mass transfer are given below:

$$S_{gen}^{'''} = \frac{K_1}{T_{\infty}^2} \left[\left(\frac{\partial T}{\partial x} \right)^2 + \left(\frac{\partial T}{\partial y} \right)^2 + \frac{16\sigma^* T_{\infty}^3}{3kk^*} \left(\frac{\partial T}{\partial y} \right)^2 \right] \\ + \frac{\mu}{T_{\infty}} \left[2 \left(\frac{\partial u}{\partial x} \right)^2 + \left(\frac{\partial v}{\partial y} \right)^2 \right] + \left[\frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right]^2 \\ + \frac{RD}{C_{\infty}} \left[\left(\frac{\partial C}{\partial x} \right)^2 + \left(\frac{\partial C}{\partial y} \right)^2 \right] + \frac{RD}{T_{\infty}} \left[\left(\frac{\partial T}{\partial x} \right) \left(\frac{\partial C}{\partial x} \right) \\ + \left(\frac{\partial T}{\partial y} \right) \left(\frac{\partial C}{\partial y} \right) \right] + \frac{\sigma B_0^2}{T_{\infty}} u^2 + \frac{v}{k_p} u^2.$$
(25)

Using Equation (25) modified with the help of Equation (17),

$$S_{gen}^{'''} = \frac{K_1}{T_{\infty}^2} \left[\left(\frac{\partial T}{\partial y} \right)^2 + \frac{16\sigma^* T_{\infty}^3}{3kk^*} \left(\frac{\partial T}{\partial y} \right)^2 \right] + \frac{\mu}{T_{\infty}} \left(\frac{\partial u}{\partial y} \right)^2 + \frac{RD}{C_{\infty}} \left(\frac{\partial C}{\partial y} \right)^2 + \frac{RD}{T_{\infty}} \left(\frac{\partial T}{\partial y} \right) \left(\frac{\partial C}{\partial y} \right) + \frac{\sigma B_0^2}{T_{\infty}} u^2 + \frac{\nu}{k_p} u^2.$$
(26)

Dimensionless system of entropy generation is defined as:

$$E_G = Re\left(1 + \frac{4}{3}Rd\right){\theta'}^2 + Re\frac{Br}{\Omega}f''^2 + Re\left(\frac{\zeta}{\Omega}\right)^2 \lambda {\phi'}^2$$

$$+Re\frac{\zeta}{\Omega}\lambda\phi'\theta'+\frac{Br}{\Omega}(M+K)f^{'^{2}}.$$
(27)

The Bejan number states

 $Be = \frac{Entropy \text{ genration due to irrevesablity of heat and mass transfer}}{Total entropy generated}$

Be =

$$\frac{\left(\operatorname{Re}\left(1+\frac{4}{3}\operatorname{Rd}\right)\theta^{2}++\operatorname{Re}\left(\frac{\zeta}{\Omega}\right)^{2}\lambda\phi'^{2}+\operatorname{Re}\frac{\zeta}{\Omega}\lambda\phi'\theta'\right)}{\operatorname{Re}\left(1+\frac{4}{3}\operatorname{Rd}\right)\theta'^{2}+\operatorname{Re}\frac{Br}{\Omega}f''^{2}+\operatorname{Re}\left(\frac{\zeta}{\Omega}\right)^{2}\lambda\phi'^{2}+\operatorname{Re}\frac{\zeta}{\Omega}\lambda\phi'\theta'+\frac{Br}{\Omega}(M+K)f'^{2}}.$$
(28)

HOMOTOPY SOLUTIONS

There are several techniques available to solve non-linear problems. The homotopy analysis method (HAM) is initially constructed by Liao [47]. Moreover, he altered a non-zero auxiliary parameter [48]. This parameter shows the way to calculate the convergence rate. It also offers great independence with which to make the initial guesses of the solutions.

The initial guesses for satisfying the boundary conditions

$$f_0 = f_w + \left(\frac{1}{1+\Gamma}\right)1 - e^{-\eta}$$
$$\theta_0 = \frac{Bi * e^{-\eta}}{1+Bi}$$
$$\phi_0 = -\left(\frac{Nt}{Nb}\right) * \frac{Bi * e^{-\eta}}{1+Bi}.$$

 L_f , L_{θ} , and L_{ϕ} are the linear operators

$$L_f = f''' - f'$$
$$L_\theta = \theta'' - \theta$$
$$L_\phi = \phi'' - \phi$$

while obeying the resulting properties

$$L_f \left[E_1 + E_2 e^{\eta} + E_3 e^{-\eta} \right] = 0$$
$$L_\theta \left[E_4 e^{\eta} + E_5 e^{-\eta} \right] = 0$$
$$L_\phi \left[E_6 e^{\eta} + E_7 e^{-\eta} \right]$$

The zeroth order deformation is

$$(1-p) L_f \left[f(\eta; p) - f(\eta) \right] = p h_f \mathcal{N}_f \left[f(\eta; p) \right]$$
$$(1-p) L_\theta \left[\theta(\eta; p) - \theta_0(\eta) \right]$$
$$= p h_\theta \mathcal{N}_\theta \left[\theta(\eta; p), f(\eta; p), \phi(\eta; p) \right]$$

$$(1-p)L_{\phi} \left[\phi\left(\eta; p\right) - \phi_{0}\left(\eta\right) \right]$$

= $p h_{\phi} \mathcal{N}_{\phi} \left[\phi\left(\eta; p\right), \theta\left(\eta; p\right), f\left(\eta; p\right) \right]$

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where $p \in [0, 1]$

 h_f , h_θ , and h_ϕ are the non-zero auxiliary constants, and \mathcal{N}_f , \mathcal{N}_θ , and \mathcal{N}_ϕ are the non-linear operators given by

$$\mathcal{N}_{f}\left[f\left(\eta;p\right), \theta\left(\eta;p\right)\right] = \frac{\partial^{3}f\left(\eta;p\right)}{\partial\eta^{3}} - \left(\frac{\partial f\left(\eta;p\right)}{\partial\eta}\right)^{2} \\ + f\left(\eta;p\right) \frac{\partial^{2}f\left(\eta;p\right)}{\partial\eta^{2}} \\ + \alpha_{1}\left(2\frac{\partial f\left(\eta;p\right)}{\partial\eta}\frac{\partial^{3}f\left(\eta;p\right)}{\partial\eta^{3}} - f\left(\eta;p\right)\frac{\partial^{4}f\left(\eta;p\right)}{\partial\eta^{4}}\right) \\ + (3\alpha_{1} + 2\alpha_{2})\left(\frac{\partial f\left(\eta;p\right)}{\partial\eta}\right)^{2} \\ + 6\beta Re\frac{\partial^{3}f\left(\eta;p\right)}{\partial\eta^{3}}\left(\frac{\partial f\left(\eta;p\right)}{\partial\eta}\right)^{2} \\ - (M+K)\frac{\partial f\left(\eta;p\right)}{\partial\eta}$$

$$\mathcal{N}_{\theta} \left[f\left(\eta; p\right), \theta\left(\eta; p\right), \phi\left(\eta; p\right) \right] = \left(1 + \frac{4}{3}Rd \right) \frac{\partial^{2}\theta\left(\eta; p\right)}{\partial\eta^{2}} \\ + Prf\left(\eta; p\right) \frac{\partial\theta\left(\eta; p\right)}{\partial\eta} - Pr\gamma \left[\left[f\left(\eta; p\right) \right]^{2} \frac{\partial^{2}\theta\left(\eta; p\right)}{\partial\eta^{2}} \\ - Pr\gamma f\left(\eta; p\right) \frac{\partial f\left(\eta; p\right)}{\partial\eta} \frac{\partial \theta\left(\eta; p\right)}{\partial\eta} + PrS\theta\left(\eta; p\right) \\ + PrNb \frac{\partial\theta\left(\eta; p\right)}{\partial\eta} \frac{\partial\phi\left(\eta; p\right)}{\partial\eta} + PrNt \left[\frac{\partial\theta\left(\eta; p\right)}{\partial\eta} \right]^{2}$$

$$\mathcal{N}_{\phi}\left[f\left(\eta;p\right),\theta\left(\eta;p\right),\phi\left(\eta;p\right)\right] = \frac{\partial^{2}\phi\left(\eta;p\right)}{\partial\eta^{2}} + Lef\left(\eta;p\right)\frac{\partial\phi\left(\eta;p\right)}{\partial\eta} + \frac{Nt}{Nb}\frac{\partial^{2}\theta\left(\eta;p\right)}{\partial\eta^{2}}$$

$$f(0; p) = f_{w}, f'(0; p) = 1 + \Gamma f^{''}(0; p), f'(\infty; p) = 0$$

$$\theta'(0; p) = -Bi(1 - \theta(0; p)), \theta(\infty; p) = 0$$

$$\phi'(0; p) = -\frac{Nt}{Nb}\theta'(0; p), \phi'(\infty; p) = 0$$

The m^{th} order deformation equations are

$$L_f \left[f_m \left(\eta \right) - \chi_m f_{m-1} \left(\eta \right) \right] = h_f R_{f,m} \left(\eta \right)$$
$$L_\theta \left[\theta_m \left(\eta \right) - \chi_m \theta_{m-1} \left(\eta \right) \right] = h_\theta R_{\theta,m} \left(\eta \right)$$
$$L_\phi \left[\phi_m \left(\eta \right) - \chi_m \phi_{m-1} \left(\eta \right) \right] = h_\phi R_{\phi,m} \left(\eta \right)$$

where

$$\chi_m = \begin{cases} 0, & m \le 1 \\ 1, & m > 1 \end{cases},$$

$$R_{f,m}(\eta) = f_{m-1}^{'''} + \sum_{k=0}^{m-1} \left[f_{m-1-k} f_k^{''} - f_{m-1-k}^{'} f_k^{'} \right] \\ + \alpha_1 \left(2f_{m-1-k}^{'} f_k^{'''} - f_{m-1-k} f_k^{i\nu} \right) \\ + (3\alpha_1 + 2\alpha_2) f_{m-1-k}^{''} f_k^{''} \\ + 6\beta Ref_{m-1-l}^{'''} \sum_{j=0}^{l} f_{l-j}^{''} f_j^{''} - (M+K) \alpha f_{m-1-k}^{'} \right]$$

$$\begin{aligned} R_{\theta,m}(\eta) &= \left(1 + \frac{4}{3}Rd\right)\theta_{m-1}'' + Pr\sum_{k=0}^{m-1} \left[\theta_{m-1-k}'f_k\right] \\ &- Pr\gamma\left[\left(f_{m-l-1}\sum_{j=0}^l f_{1-j}'\theta_j' + f_{m-l-1}\theta_l''\right)\right] \\ &+ PrNb\sum_{k=0}^{m-1} \theta_{m-1-k}'\phi_k + PrNt\sum_{k=0}^{m-1} \theta_{m-1-k}'\theta_k' \\ &+ PrS\theta_{m-1} \end{aligned}$$

$$R_{\phi,m}(\eta) = \phi_{m-1}'' + Le \sum_{k=0}^{m-1} \phi_{m-1-k}' f_k + \frac{Nt}{Nb} \sum_{k=0}^{m-1} \theta_{m-1-k}' \theta_k'$$

$$f_m(0) = 0, f_m'(0) - \Gamma f_m''(0) = 0, \ \theta_m'(0) - Bi\theta_m(0) = 0,$$

$$\phi_m'(0) + \frac{Nt}{Nb} \theta_m'(0) = 0$$

$$f_m'(\eta) \to 0, \ \theta_m'(\eta) \to 0, \ \phi_m(\eta) \to 0 \text{as } \eta \to \infty.$$

with boundary conditions

$$f_m'(0) = f_m(0) = f_m'(\infty) = \theta_m(0) = \theta_m(\infty) = \phi_m(0)$$

= $\phi_m(\infty) = 0.$

The appropriate solutions $[f_m^*, \theta_m^*, \phi_m^*]$ are

$$f_m(\eta) = f_m^*(\eta) + E_1 + E_2 e^{\eta} + E_3 e^{-\eta},$$

$$\eta_m(\eta) = \eta_m^*(\eta) + E_4 e^{\eta} + E_5 e^{-\eta},$$

$$\eta_m(\eta) = \eta_m^*(\eta) + E_6 e^{\eta} + E_7 e^{-\eta}.$$

CONVERGENCE ANALYSIS

The auxiliary parameters h_f , h_θ , and h_ϕ act as a vital part of convergence series solutions. The h-charts of f''(0), $\theta'(0)$, and $\phi'(0)$ for Re, γ , and Nb are shown in **Figure 2**. From these curves, the straight line is referred as the h-curve. The convergent approximation is selected from this straight line of the curves. We note that h-curve of f''(0), $\theta'(0)$, and $\phi'(0)$ shrinks as we enhance the range of Re, γ , and Nb, which shows the larger order approximation will be needed if the larger value of Re, γ , and Nb is employed. Approximations values of HAM with CPU time is denoted in **Table 1**.



Order	- f ″(0)	- heta'(0)	$oldsymbol{\phi}'(0)$	CPU time (s)
1	0.5006	0.1603	0.0801	0.422
5	0.5018	0.1474	0.7550	3.688
10	0.5018	0.1454	0.7273	21.781
15	0.5018	0.1441	0.7205	83.750
20	0.5018	0.1435	0.0717	290.735
25	0.5018	0.1432	0.0716	985.219
30	0.5018	0.1432	0.0716	2166.670

COMPUTATIONAL RESULTS AND DISCUSSION

The numerical calculations of velocity, concentration, temperature, entropy generation, and the Bejan number are discussed in this section. The homotopy technique is used for solving the non-linear governing Equations (18)–(20) with boundary conditions (21). The graphical results of entropy, Bejan number, temperature, Nusselt number, nanoparticle concentration, Sherwood number, and velocity profiles are computed via different flow parameters included in this study

with the fixed values of $\alpha_1 = \alpha_2 = \beta = Bi = f_w = N_t = 0.2$, $Re = Pr = Le = \Gamma = 1.0$, $M = \gamma = 0.5$, Rd = 0.3, Hg = -0.1, $N_b = 0.4$, Br = 5.0, and $\lambda = \Omega = \zeta = 1.0$.

Impact on Velocity

It is observed from **Figure 3A** that the velocity is reduced to increase the values of the velocity slip parameter due to the ratio of stretching velocity and the viscosity of the fluid. The effect of the slip parameter in velocity has had more impact in the absence of a porous medium. **Figure 3B** indicates that the velocity diminishes when the magnetic field (M) raises. Improved Lorentz force is observed because of the increasing the values of M that opposes the fluid motion. Thus, we conclude that the velocity profile diminishes.

Impact on Temperature

The impact of the radiation parameter Rd on the temperature profile is examined in **Figure 4A**. The temperature in the radiation parameter is high. Comparing the radiation effects with Christov-Cattaneo and normal heat flux, we observed that the radiation effect is quite low for Christov-Cattaneo heat flux. **Figure 4B** displays the influence of the Biot number on the temperature profile. From this figure, we observed that temperature is a rising function of Bi close to the sheet. Since Bi affects more temperature near the surface. Heat transfer



resistance is higher within the body compared to the surface of the sheet for rising values Bi.

Impact on Nanoparticle Volume Concentration

In Figure 5A, the effect of concentration profile with growing values of the Brownian motion parameter Nb is depicted. In suction cases, higher values of Nb increase the concentration

profile close to that of the surface of the sheet, and, suddenly, the concentration begins to fall, stabilizing far away from the surface of the sheet. This is due to the appearance of passive surface conditions for the concentration profile. Moreover, the injection at the sheet shows the concentration is rising near the sheet, and it diminishes far away from the surface of the sheet. The influence of the thermophoresis parameter Nt in the concentration profile $\phi(\eta)$. is highlighted in **Figure 5B**. When





there is suction in the sheet, with a rise in Nt, the concentration of the liquid decreases near to thsheet at certain stage starts to fall and stabilize away from the endpoints of the surface of the sheet. When there is an injection at the sheet, higher values of Nt decreases the concentration profile near the sheet, and it increases far away from the surface of the sheet.

Impact on Entropy Generation

The Effects of distinct fluid parameters on the entropy generation profile are highlighted in Figures 6A-G. Figure 6A depicts the influence of porous parameter in entropy profile. Initially, the entropy rate increases for the porous parameter at a certain stage ($\eta = 0.6$) before it becomes to fall. The responses of the slip parameter on entropy generation were succinctly depicted in Figure 6B. From this figure, it was obviously noted that entropy generation was inversely proportional to slip parameter. This causes a decrease in large values of slip parameter and temperature gradients in the boundary layer when retaining the fluid friction as we proceed. This occurrence induces a suppression in entropy generation since heat transfer was committed. Figures 6C-E displayed the impact of the suction injection parameter (f_w .), material parameter (β) and Biot number (Bi) on the entropy profile (E_G). Our examination obtained that higher range of f_w , reduces the entropy generation profile, and the entropy generation rate is enhanced for higher β and Bi.

The effect of thermal relaxation time (γ) on the entropy genation profile is sketched in **Figure 6F**. It is obvious that thermal relaxation time is small for temperature and heat transfer rates. In addition, domination of the irreversibility in heat transfer affected the heat flux. Thus, we have seen a small increase in the entropy of the system. Performance of *Nt* and *Nb* on entropy generation profile (E_G) is shown in **Figures 6G,H**, which shows that entropy is increased with an increase of *Nt*, whereas E_G is inversely proportional to *Nb*. The Brownian motion induces the nanoparticles temperature, but it reduces the temperature gradient on wall. As a result, entropy generation parameter reduces where *Nt* is directly proportional to temperature gradient and creates ambient atmosphere for higher values of E_G .

Impact on the Bejan Number

The Bejan number (*Be*) is a dimensionless quantity that specifies the ratio of entropy generation between heat transfer and the total entropy generation where Bejan numbers take values from 0 to 1. If *Be* is nearly equal to 1, the entropy generation will become more due to heat transfer. It is clear from **Figure 7A** that, with an escalation in the applied magnetic field, there is an augmentation in the Bejan number. The consequence of heat transfer entropy develops as we move up from the surface. The entropy effect has full domination because of the heat transfer while it is also outlying from the region. This is the reason behind how the augmenting value of *M* brings a stronger frictional effect, which leads to an increase in the liquid temperature. There is also a consequent development in the Be, as shown in **Figure 7A**. From **Figure 7B**, it is observed that the *Be* is increased for the increase in the slip parameter (Γ). Physically, larger values of (Γ) enhance the temperature gradient inside the regime, which induces the Bejan number and irreversibility of heat transfer.

Figure 7C states that, with the rise of the radiation constant Rd, the Bejan number is boosted. This is due to the total entropy generation dominated by thermal irreversibility. Figure 7D shows the effect of the thermal relaxation time (γ) on the Be. At first, the *Be* is augmented for higher values of γ at a sudden point ($\eta = 2.2$). Consequently, the Bejan number profile reduces for the values of γ . Figure 7E shows that the Bi displays a trend of raising the Be. The demonstration of such an increasing trend of the Bejan number explains how the entropy production near the surface is large due to the liquid friction-at least relative to that of the heat transfer irreversibility. The variation of the Brinkmann number Br is sketched in Figure 7F. This figure shows that the Bejan number is reduced, as we have to enhance the Br. Figures 7G,H shows the influence of thermophoresis (*Nt*) and Brownian motion (Nb) parameters on the Bejan number. From these plots, we note that Nt and Nb have inverse effects on the Bejan number profile.

Impact on Physical Entities

Figures 8–11 illustrate the effects of different physical parameters on the local Nusselt number and local Sherwood number. The influence of f_w and γ on Nu_x is shown in **Figure 8**: heat transfer decays for higher values of f_w and γ . The same phenomena can be observed for larger values Hg and γ on the Nusselt number profile, as presented in **Figure 9**. The combined effects of Nb and M as well as Nt and M are shown in **Figures 10, 11**, respectively. From these figures, we conclude that thermophoresis (Nt) and Brownian motion (Nb) parameters have produce the converse trend in the mass transfer rate.







NUMERICAL CODE VALIDATION

In this segment, we examine the code validation of early published works of literature. **Table 2** validates the results of



TABLE 2 | Validation of -f''(0) and $-\theta'(0)$ for the limiting case $M = 0, K = 0, Nb = 0, Nt = 0, Rd = 0, S = 0, and Bi \rightarrow \infty$.

Order	-f" (0)		<i>-θ'</i> (0)	
	Imtiaz et al. [37]	Present	Imtiaz et al. [37]	Present
1	0.81450	0.8145	0.72778	0.727778
5	0.81211	0.812208	0.58070	0.580701
8	0.81235	0.812345	0.57779	0.577789
14	0.81235	0.812353	0.57871	0.578711
17	0.81235	0.812353	0.57878	0.578778
25	0.81235	0.812353	0.57878	0.57877
30	0.81235	0.812353	0.57878	0.57877
35	0.81235	0.812353	0.57878	0.57877

-f''(0) and $-\theta'(0)$ for the limiting case M = 0, K = 0, Nb = 0, Nt = 0, Rd = 0, S = 0, and $Bi \rightarrow \infty$ with Imtiaz et al. [37]. Moreover, the skin friction rate is also validated by the same literature [37] when M = K = 0 (see **Table 3**). **Table 4** exhibits the matching results of reduced Nusselt number with the references [20, 49–51]. From the above validation, results show that the current simulation is considered an efficient one.

KEY RESULTS

The present research work examines the entropy generation influence on third-grade nanoliquid flow caused by a stretching sheet in the appearance of Magnetic field, radiation, and convective heating effects. Christov-Cattaneo heat flux replaces

α1	α2	β	Re	Imtiaz et al. [37]	Present
0.0	0.1	0.1	0.1	0.04605	0.04605
0.1				1.06680	1.06680
0.2				1.17470	1.17470
0.1	0.0	0.1	0.1	1.12010	1.12010
	0.1			1.06680	1.06680
	0.2			1.01830	1.01830
	0.1	0.0		1.06290	1.06290
0.1		0.1		1.06680	1.06680
		0.2		1.07030	1.07030
		0.1	0.0	1.06290	1.06290
			0.1	1.06680	1.06680
			0.2	1.07060	1.07060

TABLE 4 | Matching results of reduced Nusselt number with the restricting case $Rd = Ec = M = Nt = Nb = \gamma = S = K = \Gamma = f_w = 0$, and $Bi \to \infty$.

Wang [49]	Gorla and Sidawi [50]	Khan and Pop [20]	Makinde and Aziz [51]	Present
0.1691	0.1691	0.1691	0.1691	0.1691
0.4539	0.5349	0.4539	0.4539	0.4539
0.9114 1.8954	0.9114 1.8905	0.9113 1.8954	0.9114 1.8954	0.9114 1.8954
	Wang [49] 0.1691 0.4539 0.9114 1.8954	Wang [49]Gorla and Sidawi [50]0.16910.16910.45390.53490.91140.91141.89541.8905	Wang [49]Gorla and Sidawi [50]Khan and Pop [20]0.16910.16910.16910.45390.53490.45390.91140.91140.91131.89541.89051.8954	Wang [49]Gorla and Sidawi [50]Khan and Pop [20]Makinde and Aziz [51]0.16910.16910.16910.16910.45390.53490.45390.45390.91140.91140.91130.91141.89541.89051.89541.8954

ordinary heat flux. HAM is employed to validate the nonlinear governing equations. Results of velocity, temperature, nanoparticle volume concentration, the system of entropy, the Bejan number, mass, and heat transfer rates are presented graphically. We obtained the following main upshots:

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- 1. A falling tendency of the velocity profile is detectable while we keep increasing the values of the velocity slip and magnetic field parameter.
- 2. An augmentation in the range of radiation parameter and Biot number causes an increasing trend.
- 3. The concentration of the nanoparticle volume fraction is found to be a diminishing function of the thermophoretic parameter. On the other hand, a contrary impact is identified for the Brownian motion parameter.
- 4. The irreversibility of the system rises as we keep enhancing the values of the Biot number, thermal relaxation time, material parameter, and the Brinkmann number, but an inverse occurrence takes place as we increase the slip parameter and suction/injection parameter.
- 5. The Bejan number increases with greater values of the slip parameter, Biot number, thermophoresis parameter, magnetic parameter, and radiation parameter, whereas it reduces for larger values of the Brinkmann number and Brownian motion parameter.

DATA AVAILABILITY STATEMENT

The raw data supporting the conclusions of this article will be made available by the authors, without undue reservation.

AUTHOR CONTRIBUTIONS

All authors listed have made a substantial, direct and intellectual contribution to the work, and approved it for publication.

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Conflict of Interest: The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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LIST OF SYMBOLS

a	Stretching rate (s^{-1})
Bi	Biot number
Be	Bejan number
Br	Brinkman number
B ₀	Constant magnetic field ($kgs^{=2}A^{-1}$)
С	Concentration (kgm^{-3})
Cp	Specific heat $(J k g^{-1} K^{-1})$
C_{∞}	Ambient concentration (kgm^{-3})
C _w	Fluid wall concentration (kgm^{-3})
Cf_{x}	Skin friction coefficient
D _B	Brownian diffusion coefficient $(m^2 s^{-1})$
DT	Thermophoretic diffusion coefficient $(m^2 s^{-1})$
E _G	Entropy generation parameter
$f(\eta)$	Velocity similarity function
f _w	Suction/injection parameter
h _f	Convective heat transfer coefficient ($W m^{-1} K^{-1}$)
α ₁ , α ₂ , β	Fluid parameters
k	Thermal conductivity ($W m^{-1} K^{-1}$) K Porous parameter
L	Auxiliary linear operator
Le	Lewis number
Μ	Magnetic parameter
\mathcal{N}	Non-linear operator
Nb	Brownian motion parameter
Nt	Thermophoresis parameter
Nu _x	Nusselt number
Pr	Prandtl number
Q ₀	Dimensional heat generation/absorption coefficient
q	Heat flux ($W m^{-2}$)
Rd	Radiation parameter
Re	Reynolds number
Sh _x	Sherwood number
S	Heat generation parameter
S ^{'''} _{gen}	Local volumetric entropy generation rate $(Wm^{-3}K^{-1})$
S ₀ '''	Characteristic entropy generation rate $(Wm^{-3}K^{-1})$
Т	Temperature (K)
T_{∞}	Ambient temperature (K)
T _f	Convective surface temperature (K)
U _W	Velocity of the sheet $(m s^{-1})$
u,v	Velocity components in (x, y) directions $(m s^{-1})$
$v_w > 0$	Suction velocity
$v_w < 0$	Injection velocity
x,y	Cartesian coordinates (m)
GREEKS	
Xm	Auxiliary parameter
$\phi(\eta)$	Concentration similarity function
1'	Slip parameter
γ	Dimensionless thermal relaxation time
η	Similarity parameter
λ_T	I nermal relaxation time
λ	Dimensionless constant

(Continued)

Kinematic viscosity $(m^2 s^{-1})$
Dimensionless temperature difference
Temperature similarity function
Ratio of the effective heat capacity
Density (kgm ⁻¹)
Electrical conductivity $(S m)$
Stream function $(m s^{-1})$
Dimensionless concentration difference