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EDITED BY

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Nelson Mandela University, South Africa

*CORRESPONDENCE

Gustavo Koury Costa,
✉ gustavokoury@recife.ifpe.edu.br

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Energy management in pump-controlled actuators

Gustavo Koury Costa^{1*} and Nariman Sepehri²

¹Department of Mechanical Engineering, Federal Institute of Technology - IFPE, Recife, Pernambuco, Brazil, ²Department of Mechanical Engineering, University of Manitoba, Winnipeg, MB, Canada

Pump-controlled actuators, or more generically, hydrostatic actuators, have the significant advantage of not relying on valves to control the cylinders. This results in much better energy usage compared to traditional valve-controlled systems. However, it is possible to further increase energy efficiency by storing load energy in motoring quadrants and subsequently releasing the stored energy back into the circuit or making it available for other applications. Much work is needed to practically study energy storage in hydrostatic actuators. In this note, we review the two basic ways hydraulic energy can be saved in circuits using accumulators, emphasizing their advantages and drawbacks. The review is followed by a brief description of the current research being carried out at the University of Manitoba in Canada. We aim to show that research in this field is promising and demonstrates that hydraulic power transmission can not only be made efficient but also be used to regenerate load energy that would otherwise go to waste.

KEYWORDS

hydraulic circuits, hydraulic accumulators, hydraulic energy storage, hydrostatic actuators, pump-controlled actuators

1 Introduction

This paper focuses on pump-controlled actuators, where flow changes are produced exclusively at the pump (Costa and Sepehri, 2015). This is particularly important when the hydraulic circuit is closed, as in Figure 1A. In the figure, we observe that the cylinder can act both as an energy consumer (actuator) or as an energy supplier (pump). Hydraulic actuators, including hydraulic cylinders, can be controlled by adjusting the oil flow into and out of their chambers. Assuming fluid incompressibility, flow and piston velocity are directly proportional. The most common way to control speed is by gradually throttling the oil flow into or out of the cylinder chambers through directional and flow control valves. However, the added flow resistance significantly reduces the overall energy efficiency of the system. An alternative method is to change the oil flow directly at its source by adjusting the pump flow, either by altering its displacement or the pump shaft speed. This approach eliminates throttle losses and optimizes the system's energy performance. These two methods of controlling the hydraulic actuator are generally described as “valve-controlled” and “pump-controlled” systems. When the cylinder becomes the energy supplier, the pump (P) operates as a hydraulic motor. The weight, W , thus produces an input power, \mathcal{P}_i , when descending at a velocity, v , as expressed by the following equations:

$$\begin{cases} W = mg \\ \mathcal{P}_i = Wv \end{cases} \quad (1)$$

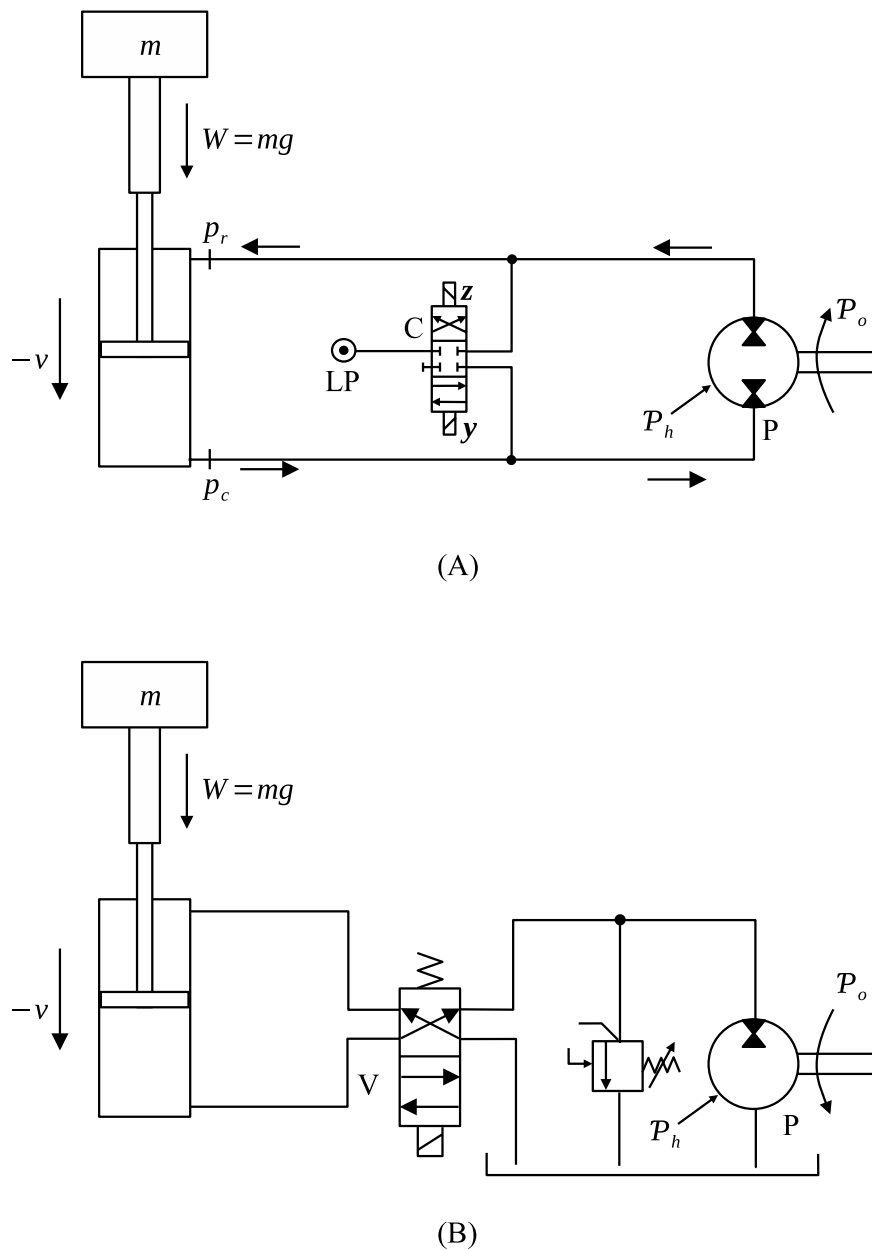


FIGURE 1 Load energy recovery: (A) closed-circuit and (B), open-circuit.

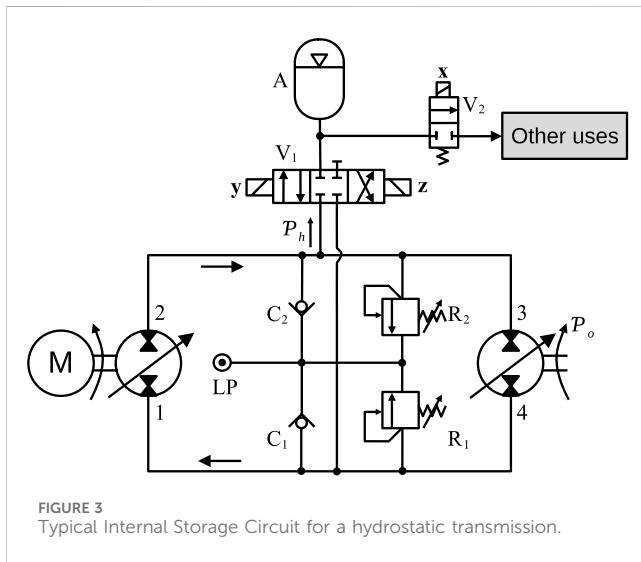
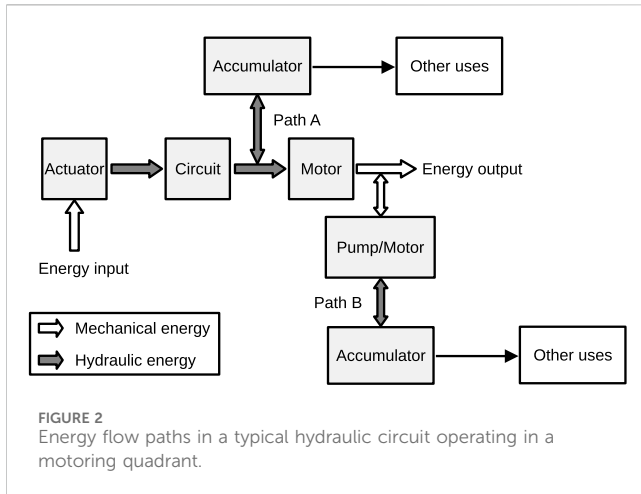
where m is the mass of the combined actuator rod and load, g is the gravitational acceleration and v is the cylinder rod velocity. Ideally, \mathcal{P}_i would reach the pump in its entirety. However, due to losses along the way, only a fraction, \mathcal{P}_o , of this input power is converted into mechanical energy at the pump shaft.

Focusing on the closed circuit shown in Figure 1A, we observe a directional valve (C) connecting each side of the cylinder to a low-pressure (LP) source. Valve C has been referred to as “compensation valve” (Costa and Sepehri, 2019), whose function is to match the flows coming from the cylinder to the flows going into and out of the pump. The control of valve C depends on the pressures on the piston and rod sides of the cylinder, p_c and p_r , respectively. Given the ratio between the piston as annulus area, α , it has been shown (Costa and

Sepehri, 2019) that, whenever $\alpha p_c > p_r$, solenoid y should be activated while solenoid z should be deactivated. Otherwise, solenoid z should be activated and solenoid y , deactivated.

Figure 1B shows another circuit, now using a 4×2 valve (V) to control the cylinder. There is more energy dissipation between the cylinder and the pump due to the losses within valve V. However, the circuit is simpler, as no special design is needed to match the flows coming out of the cylinder to the flows coming into and out of the pump.

As mentioned before, in both cases, Figures 1A, B, the input power at the cylinder, \mathcal{P}_i (Equation 1), is carried into the pump ports and then to the pump shaft. However, only a fraction of the input energy, \mathcal{P}_h , reaches the pump in the form of hydraulic energy, that is



$$P_h = \eta_c P_i \tag{2}$$

where $\eta_c < 1$ is the *circuit efficiency*. Here, we have an important difference between the circuits in Figures 1A, B. In the circuit in Figure 1B, the efficiency, η_c , is considerably smaller, due to throttling losses at valve V.

The power, P_h , is conveyed through the pump to its rotating shaft. As a result, a mechanical power, P_o , is finally output, according to the following equation:

$$P_o = \eta_p P_h \tag{3}$$

where η_p is the mechanical-hydraulic efficiency at the pump.

Power coming from the load is therefore transformed into hydraulic power and, subsequently, into mechanical power at the shaft. At both stages of power transformation, there may or may not be load energy recovery. In circuits where energy recovery is desired, two possible paths can be followed, as shown in Figure 2. In path A, an accumulator is connected in parallel to the hydraulic line coming from the cylinder, whereas in path B, mechanical energy flowing from the pump shaft is converted into hydraulic energy before

loading the accumulator. Note that although two accumulators are shown in the Figure, only one is needed, depending on the path that has been chosen. In the first case, we circumvent the losses at the pump, thus allowing more energy to be recovered. The drawback is that the “hydraulic stiffness” of the circuit is reduced, creating a cushion effect that is undesirable in some situations. Energy stored in the accumulator can either be returned to the circuit or used for other purposes, as indicated in the Figure.

From this point on, we shall refer to circuits following path A as “Internal Storage Circuits” (ISCs), while those following path B will be referred to as “External Storage Circuits” (ESCs).

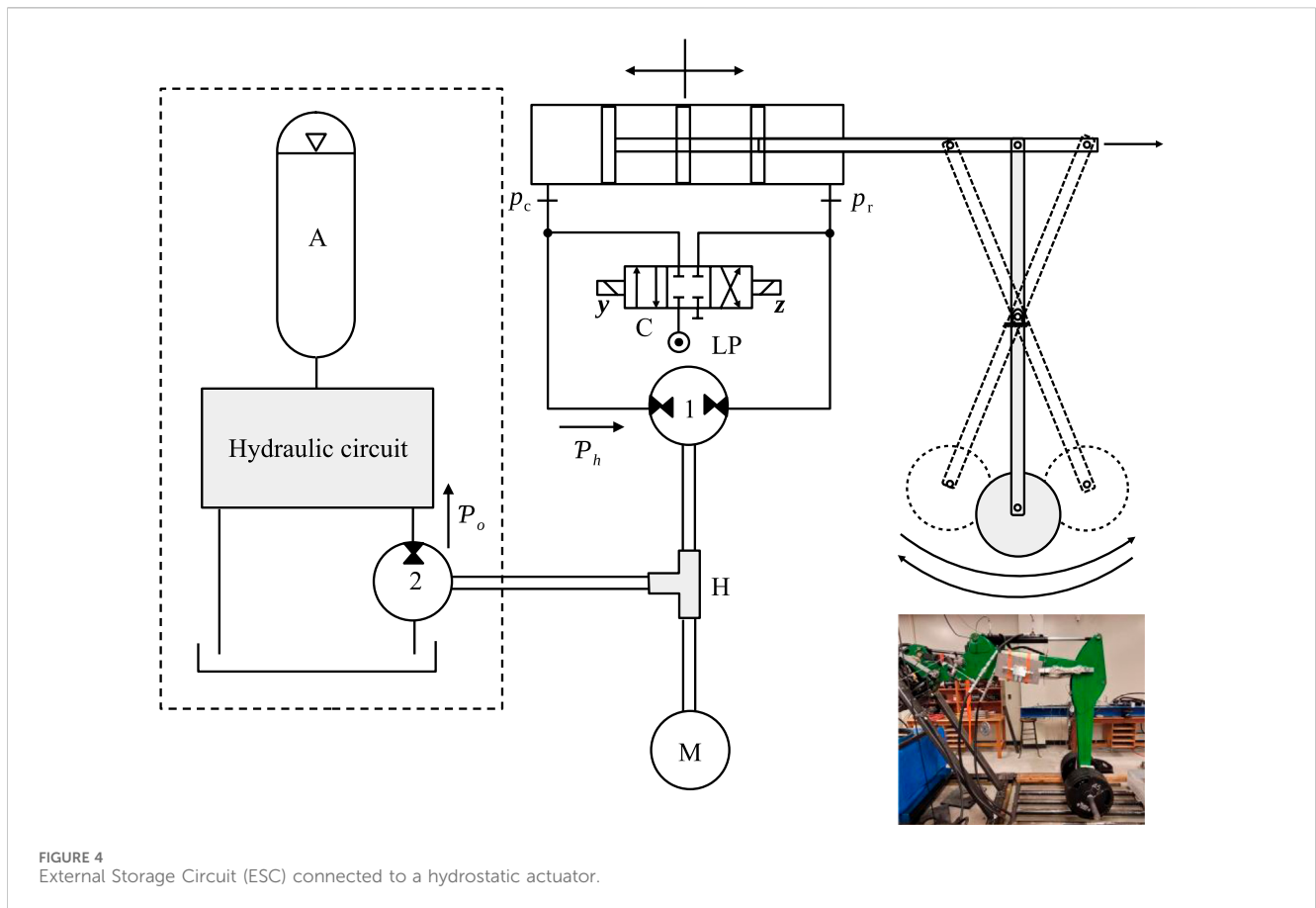
2 Internal storage circuits (ISC)

A typical ISC is represented in Figure 3, where the accumulator, A, communicates with lines 2–3 and 4–1 through a directional valve, V_1 , activated by two solenoids, y and z in an alternate manner. Valve V_2 , on the other hand, directs the hydraulic energy stored within A to “other uses,” through the activation of solenoid x. The figure shows a very generalized circuit, where variable displacement, fully reversible pumps are connected at both ends of the transmission. Some other elements are added to the circuit for sound operation. The relief valves, R_1 and R_2 are for pressure overshoot protection and the check valves, C_1 and C_2 , operate as anti-cavitation valves. Both relief and check valves are connected to a low-pressure source, LP, which can be an oil tank or a low-pressure accumulator.

Because of the differential cylinder area in single-rod hydrostatic actuators, energy storage in hydrostatic actuators is not as popular as in hydrostatic transmissions. In fact, a lot of research has been directed to single-rod pump-controlled actuators through the years (Costa and Sepehri, 2019; Frankenfield, 1984; Hewett, 1994; Rahmfeld and Ivantysynova, 1998; Wang et al., 2012; Altare and Vacca, 2015; Caliskan et al., 2015; Heybroek et al., 2012; Karvonen, 2016; Williamson, 2010; Williamson and Ivantysynova, 2008; Imam et al., 2017; Stelson, 2011; Ivantysynova, 2008) and, although considerable progress has been made, these circuits are still subject to much research (see, for example, Ketelsen et al., 2019).

Examples of ISCs for hydrostatic transmissions can be found in (Pourmovahed et al., 1992a; 1992b; Hippalgaonkar and Ivantysynova, 2016a; 2016b; Bertolin and Vacca, 2021; Sprengel and Ivantysynova, 2013; Feng et al., 2023). Energy storage through accumulators have also been used in circuits with valve-controlled cylinders (Xia et al., 2018; Ranjan et al., 2020; Li et al., 2022; Casoli et al., 2016; Li et al., 2015; Lin et al., 2016; Li and Zhao, 2021). However, to the best of our knowledge, nothing has been published about hydrostatic actuators (pump-controlled actuators). In fact, only a single reference about an ESC (Wendel, 2002), besides an explanation of its operational principles (Costa and Sepehri, 2015) are all that can be found for pump-controlled actuators. The reasons for this have been explained at the beginning of this section: it is important to, first, solve the differential cylinder problem, before exploring load energy management.

One drawback of ISCs is that, whenever the accumulator is loading there is a considerable reduction of the effective bulk modulus of the circuit, reducing its hydraulic stiffness (Costa and Sepehri, 2015). Problems arising from this effect have been reported in hydraulic hybrid vehicles (Sprengel and Ivantysynova, 2013).



Another drawback is the fact that the circuit pressure frequently needs to be risen to a higher level at the accumulator, so that it may be effectively used to help driving the load (Xia et al., 2018). Circuits with a variable-displacement motor at the load-end are advantageous, in this case, due to their capacity for changing the circuit pressure by adjusting the motor displacement (an example can be found in Hippalgaonkar and Ivantysynova, 2016a; 2016b).

We have seen that ISCs have the advantage of being able to store a greater fraction of the energy coming from the load. However, due to the difficulties concerning the construction of closed circuits with a single rod actuator, most of the applications so far have been applied to hydrostatic transmissions and valve-controlled actuators. In recent years however, some new developments have been made towards solving the differential area problem of the cylinder in hydrostatic actuators. In particular, we cite reference (Costa and Sepehri, 2019), where excellent and promising results were shown. In the following section, we briefly present the current research that has been carried out in the tele-robotics laboratory of the Mechanical Engineering Department, in the University of Manitoba, Canada, where a new proposal of an ESC is under investigation.

3 External storage circuits

The greatest difference between ISCs and ESCs is the smaller capacity for storing energy of the latter. This is simply because a fraction \mathcal{P}_o (Equation 3), and not \mathcal{P}_h (Equation 2) ends up being

available for storage. On the other hand, the versatility of ESCs, which can be mechanically coupled to any kind of circuit, is a considerable advantage. Basically, once a separate energy storage circuit is developed, it can be used to store and reuse energy regardless of the hydraulic application. To compensate for the smaller storage capacity, ESCs are better coupled with pump-controlled actuators, where throttling losses due to valve control are not present.

Figure 4 shows how an ESC, similar to one, currently mounted in the Tele-Robotics Laboratory of the Mechanical Engineering Department of the University of Manitoba. The test rig, in the laboratory, drives a cylinder attached to a dangling weight, as shown in the small picture at the low-right corner. The hydraulic circuit, therefore, can operate in a four-quadrant mode, with the load alternatively pushing and pulling the cylinder rod. In the circuit, an electric motor drives a pump, connected to the cylinder, and another pump which is responsible for loading the accumulator. A power hub, H, is responsible for splitting the power coming from the electric motor between the main pump and the accumulator pump. It also can divert power coming from the main pump, connected to the cylinder, to the pump connected to the accumulator. Means of mechanically engaging and disengaging the three shafts (clutches, for example) may be available, but are not shown in the figure for convenience.

The circuit in Figure 4 uses a novel ESC (Chithravelpillai, 2022; Chithravelpillai et al., 2024). Besides the excellent energetic efficiency in pumping quadrants, which is inherent to the main circuit configuration described by Costa and Sepehri (2019),

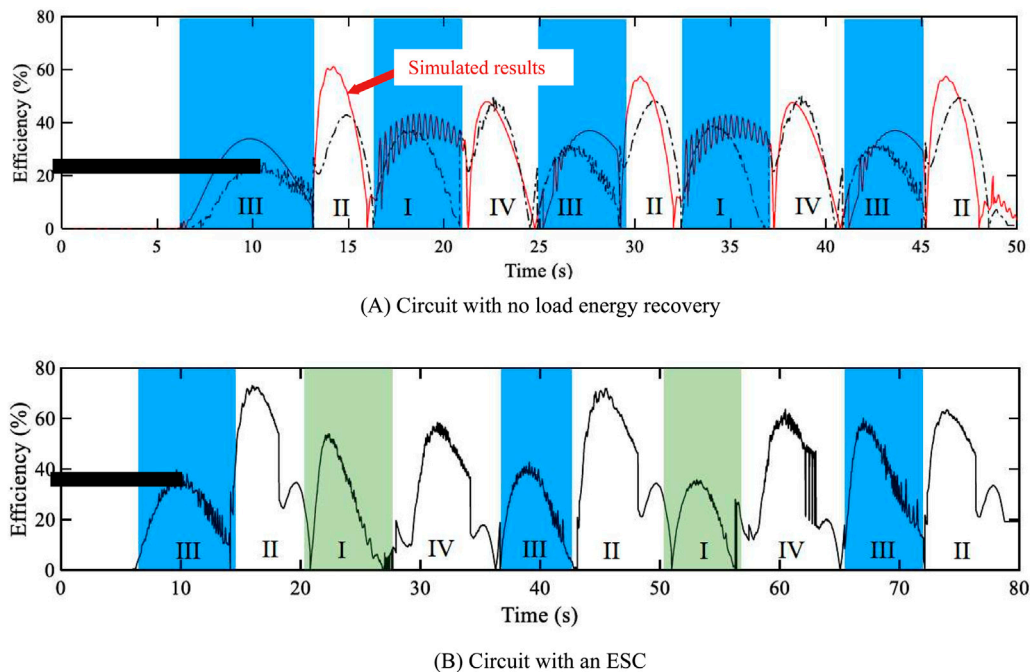


FIGURE 5
Efficiency comparison using experimental results: (A) circuit without load energy recovery; (B) circuit incorporating ESC as in Figure 4 (Chithravelpillai, 2022).

preliminary experiments have shown that stored energy from the load during motoring quadrants has almost doubled the circuit efficiency in pumping quadrants, where the stored energy is reused to assist the electric motor, M (Chithravelpillai, 2022), as shown in Figure 5. Figure 5A shows the results (from both simulations and experiments) where no energy storage device was used and, therefore, no load energy could be recovered. Figure 5B shows efficiency for the same circuit incorporating an ESC. We see that the maximum efficiency has nearly doubled in quadrant III, where the stored load energy is reused to drive the load.

The ESC Pump 2 in Figure 4 may be substituted with a variable displacement pump, allowing for adjustment of the accumulator pressure. As it stands, the circuit enables the reuse of the accumulated energy to assist the cylinder in pumping quadrants. Variations of the circuit could include using the accumulated energy to drive an external device (“other uses” in Figure 2).

4 Conclusion

Reutilization of load energy in hydraulic circuits has already become a reality and it is increasingly necessary in a greener minded society. Pump-controlled, single-rod, actuators have come into play. This note has shown that there is great prospect and expectation that hydraulics will play a decisive role in energy recovery systems. Recent experiments carried out at the University of Manitoba have been very encouraging in this respect. Expectations are that in a near future, a fully functional circuit can be developed and industrialized. Until then, more experiments are expected, and more advances can be anticipated.

Data availability statement

The original contributions presented in the study are included in the article/Supplementary material, further inquiries can be directed to the corresponding author.

Author contributions

GC: Writing—original draft, Writing—review and editing. NS: Writing—review and editing.

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Conflict of interest

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