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# Modeling of temperature dependence of $\Lambda$ -graded InGa<sub>x</sub>N solar cells for both strained and relaxed features

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The temperature dependence of  $\Lambda$ -graded InGa<sub>x</sub>N solar cells is studied through simulation using nextnano software.  $\Lambda$ -Graded structures have been designed by increasing and then decreasing the indium composition in epitaxial InGa<sub>x</sub>N layers. Due to polarization doping, layers of p-type and n-type doping arise without the need for impurity doping. Different individual structures are designed by varying the indium alloy profile from GaN to maximum indium concentrations,  $x_{max}$ , ranging from 20% to 90% pseudomorphically strained to a GaN substrate and from 20% to 100% for completely strain-relaxed materials and linearly decreases back to GaN. For In<sub>x</sub>Ga<sub>1-x</sub>N with  $x > \sim 0.9$ , if the material is strained to the GaN lattice constant, it is predicted to have a negative band gap. So this case is not considered here. The temperature dependence of the electrical and optical properties as they relate to the solar efficiency of the  $\Lambda$ -graded structures under relaxed and strained conditions are studied. Additionally, the dimensionless absorption coefficients are fitted and plotted as functions of the band gap under both strained and relaxed conditions at different temperatures. As a result, the generation rates as functions of the penetration depth within a cell can be calculated in order to obtain the solar cell parameters including efficiency for each  $\Lambda$ -graded structure at different temperatures. Under the strained condition, the  $x_{max}$ , where the solar cell efficiency reaches its maximum for each temperature, decreases as the temperature increases. At the same time, under the relaxed condition, at low temperatures ( $T = 100\text{--}400\text{ K}$ ),  $x_{max}$  is 100%, that is, grading to InN results in maximum efficiency, while at higher temperatures ( $T = 500\text{--}800\text{ K}$ ),  $x_{max}$  decreases with the increasing temperature.

## KEYWORDS

solar cell, InGa<sub>x</sub>N alloy, polarization doping, graded structure, strain, relax

## Introduction

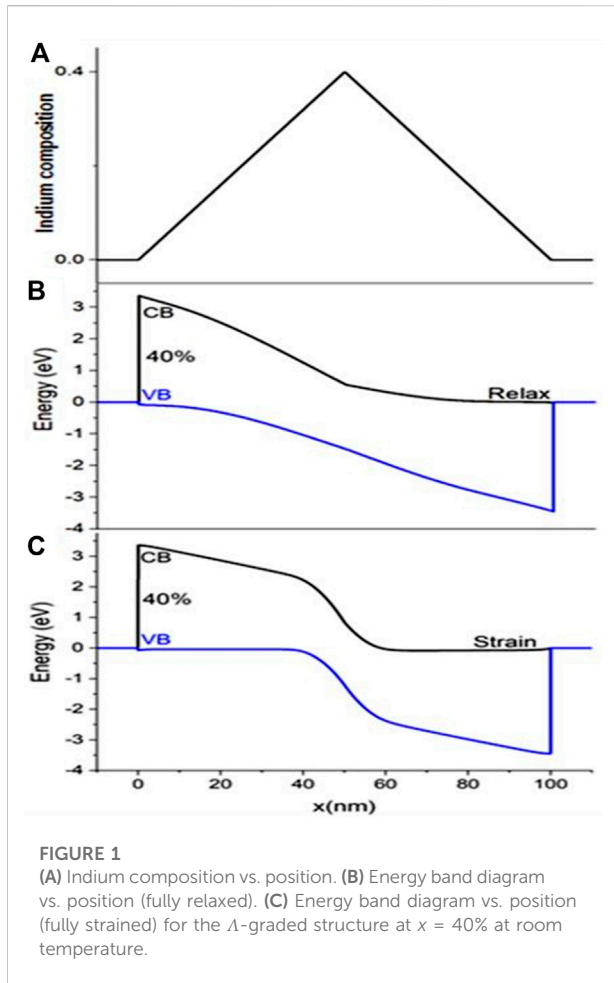
Ternary alloys of group III-N materials have great potential to be used in photovoltaic devices due to spectacular properties such as high thermal conductivity, high optical absorption ( $\sim 10^5 \text{ cm}^{-1}$ ), and high radiation resistance (Nakamura et al., 1995; Nakamura et al., 1996; Pozina et al., 2000; Bhuiyan et al., 2012; Kucukgok et al., 2016; Kazazis et al., 2018). Additionally, these materials have direct band gaps (Kazazis et al., 2018) which creates strong optical transitions for charge carriers between the conduction band (CB) and valence band (VB). Also, they have a tunable band gap, which covers almost the whole range of the visible solar spectrum from UV up to infrared (Bhuiyan et al., 2012; David and Grundmann, 2010; Routray and Lenka, 2018; Belghouthi and Aillerie, 2019; Cheriton et al., 2020). Several groups have reported that modeling efforts aimed at describing the solar cell parameters of devices made from InGaN alloys. For example, the solar efficiency for a single-junction  $\text{In}_{0.65}\text{Ga}_{0.35}\text{N}$  solar cell was reported to be 20.28% (Zhang et al., 2007). After assumption of the density of states (DOS) model, a higher solar efficiency for the same structure was reported at 24.95% (Shen et al., 2008). In this report, they considered recombination/generation in the solar cell rather than the lifetime model by neglecting defects. Another report was given that optical properties and physical models, such as Fermi–Dirac statistics, Auger recombination, and Shockley–Read–Hall recombination, and the doping and temperature-dependent mobility were taken into account in the simulation, which claimed the solar efficiency for a single-junction  $\text{In}_{0.622}\text{Ga}_{0.378}\text{N}$  solar cell to be 26.5% (Mesrane et al., 2015). In another report, in which InGaN p-n junction solar cells with various indium compositions and thicknesses of the upper p-InGaN and lower n-InGaN junctions are investigated theoretically (Feng et al., 2013), and the results indicated that an  $\text{In}_{0.622}\text{Ga}_{0.378}\text{N}$  solar cell, with optimal device parameters, can have 31.8 mA/cm<sup>2</sup>, 0.874 V,  $\sim 0.775$ , and  $\eta \sim 21.5\%$ .

In another report, a quantum well (QW) LED with graded InGaN QWs was studied, experimentally and theoretically. The advantages of using graded structures in comparison with fixed compositions of QWs were reported. A graded structure was determined, through simulations, to reduce carrier densities such that Auger recombination (which is the main cause of the lost efficiency through non-radiative recombination) was decreased. Graded structures also decrease polarization-induced interface charge density, which also contributes to efficiency loss, from approximately  $0.54 \times 10^{17} \text{ m}^{-2}$  to  $0.3 \times 10^{17} \text{ m}^{-2}$ . Moreover, the quantum-confined stark effect, which is significant in QWs, is much less significant in the graded structure. In QWs, this acts to increase the carrier lifetime, which dramatically increases the probability of capture by the contacts, but at the same time, it does decrease the absorptivity of the QW region. Additionally, graded structures increase the overlap of electron and hole wavefunctions, which also acts to increase the absorption. The external quantum efficiency (EQE) for the graded structure shows 39.23%, which is higher than that of the QW structure at 31.83%. At the end, they reported the

output for the graded structure to be  $\sim 150 \text{ A/cm}^2$  injection current, which is almost 30% higher than that of the QW device (Zhang et al., 2014).

In the present work, the designed structure is a  $\Lambda$ -shaped graded structure in which the indium composition is linearly changed vs. position in the structure. Polarization doping plays a crucial role in the graded structure to reach high levels of doping, without using additional impurities in the lattice (LeGoues et al., 1992) as growing p-type InGaN alloys is one of the main technical challenges (Obloh et al., 1998; Van de Walle and Segev, 2007; Brochen et al., 2013; Ra and Lee, 2019; Narita et al., 2020). The graded structure provides polarization doping which creates p- and n-type layers. This is the result of changing the built-in polarization, creating a space charge,  $\rho$ , given by the following formula:  $-\nabla \cdot P = \rho$ . When the indium composition is increasing from GaN to InGaN, the background charge is generally negative ( $\rho < 0$ ), so positive charges (holes) are accumulated resulting in p-type doping. On the other hand, by decreasing the indium composition from InGaN to GaN, the background charge is generally positive ( $\rho > 0$ ) which attracts electrons resulting in n-type doping (Simon et al., 2010; Lee et al., 2015; Lv et al., 2021). For another ternary alloy, AlGaIn, the polarization doping is conceptually reversed in comparison with InGaN, that is, by increasing the aluminum composition from GaN to AlGaIn, the background charge is positive ( $\rho > 0$ ), and decreasing the aluminum composition results in a p-type region (Li et al., 2012). Optical properties of the  $\Lambda$ -shaped graded structure were already reported experimentally and with comparison of experiment simulation (Sarollahi et al., 2020), (Sarollahi et al., 2021).

Here, we present simulations of  $\Lambda$ -graded InGaIn solar cells. In addition, the effects of temperature and strain are studied using nextnano software. The graded structure consists of a symmetric double InGaIn-graded layer in which the indium composition linearly increases from GaN to a maximum value,  $x_{\text{max}}$ , and then linearly decreases from  $x_{\text{max}}$  back to GaN. The p- and n-type doping is provided solely by the polarization doping as explained previously. Both relaxed and strained conditions were considered because for higher  $x_{\text{max}}$  values, and it is not possible for a real structure to be either fully strained or fully relaxed. Therefore, we posit that any experimentally demonstrated result will fall somewhere between the two limits as described in the present work. For the strained cases,  $x_{\text{max}}$  is only considered between 20% and 90% because for  $x > 90\%$ , using the effective mass approximation, the band gap of InGaIn is found to be negative. On the other hand, under the relaxed condition,  $x_{\text{max}}$  is considered between 20% and 100%. As an example, the indium composition, strain-relaxed energy band diagram, and fully strained energy band diagram vs. position for  $x = 40\%$  are shown in Figures 1A–C, respectively. The structure thickness is 100 nm. According to Figures 1B,C, it is obvious that the first 50 nm (0–50 nm) is p-type due to the increasing indium composition, from GaN to  $x_{\text{max}}$ , and the second 50 nm (50–100 nm) is n-type due to the decreasing alloy composition back to GaN. Additionally, the



regions (–10–0 nm) and (100–110 nm) are defined to be ohmic contacts at the two edges of the device with no defined material composition.

## nextnano simulation and strategy

nextnano software, consisting of two different versions, nextnano3 and nextnano+, was used to simulate solar cell parameters. Within nextnano, we use a single-band, effective-mass approximation to calculate the band structure. Also, in order to obtain the light IV plot, the generation rates for each layer of the material must be calculated. In order to incorporate the generation rate of a varying alloy composition, the graded structure is approximated as a step-graded structure due to the fact that nextnano is limited to simulating the generation rate of a single composition at once. The generation rate for each individual layer is calculated using nextnano3, and then the layers are combined and imported into nextnano+ in order to calculate the light IV curve for the entire structure. The solar cell parameters such as the open circuit voltage,  $V_{OC}$ , short circuit

current,  $I_{SC}$ , solar efficiency,  $\eta$ , and fill factor,  $FF$  are then calculated from the light IV curve. All simulations were performed using 1-nm steps, as shown in Figures 2A,B, which show an example of the step-graded structure using  $x_{max} = 40\%$ .

In order to calculate the generation rate within each layer, the intensity of light incident on that layer and the absorption coefficient of that layer are required. The parameterization of the absorption coefficients is described as follows: the light intensity at each layer is determined by the exponential loss of intensity from the layer directly above, using the full solar intensity spectrum (AM 1.5G) as the source incident on the external surface of the device. For example, using 100 layers with the 100th layer facing the Sun, the light transmitted through the top layer and incident on the 99th layer would be given by  $I_{100} = I_0 \exp(-\alpha_{100}d)$ , where  $d$  is the thickness of each layer and  $\alpha_{100}$  is the absorption coefficient of layer 100. For subsequent layers, the intensity incident on layer  $n-1$  is calculated by  $I_n = I_{n+1} \exp(-\alpha_n d)$ . Then, these data are imported into nextnano3 layer-by-layer to obtain the generation rates for each layer, which are then compiled and imported into nextnano+ in order to obtain the light  $I$ - $V$  curve for each solar cell.

In this work, the effects of temperature on graded InGaN solar cells are studied, with the primary effect being to decrease the band gap as the temperature increases (O'Donnell and Chen, 1991; Wu et al., 2003; Cho et al., 2020). Solar cell parameters such as short-circuit current density, open-circuit voltage, efficiency, and fill factor are all therefore affected by changing the temperature (Belghouthi and Aillerie, 2019; Adeb et al., 2019; Boney et al., 2012). For each structure, the solar cell properties were studied between 100 K and 800 K. For simple homojunction solar cell structures, it is generally understood that there is a direct correlation between the band gap and the open-circuit voltage (Green, 1998; Blakesley and Neher, 2011; Nelson, 2003). However, the inverse is true for the short-circuit current density,  $J_{sc}$ , as it increases with the decreasing band gap due to an increase in the absorption coefficient and the associated increase in the generation rate (Feng et al., 2013).

## Strain: impact on device performance

Due to the 11% lattice mismatch between InN and GaN, InGaN structures grown on GaN substrates result in a significant strain. This strain generally manifests a decrease in the band gap, similar to the increase in temperature. Therefore, all the results of changing the temperature and thus changing the solar cell properties through the change in the band gap are similarly studied due to the induced strain in the films including the absorption coefficient and the resulting generation (Park and Chuang, 1999; Romanov et al., 2006; Masui et al., 2008; Azize and Palacios, 2010; Dreyer et al., 2013; Birner et al., 2006; Wierer et al., 2010; Golam Sarwar and Myers, 2012; Belghouthi et al., 2016). In this work, fully strained to GaN and bulk-relaxed lattices were considered. The true experimental realization of these structures is expected to fall between these two extremes.

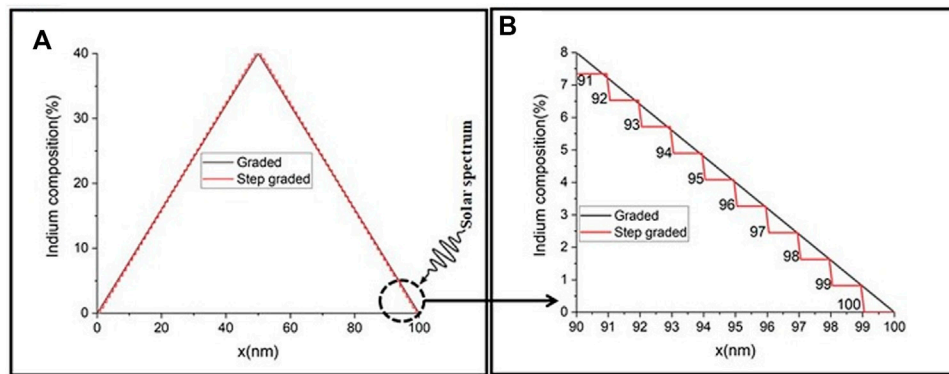


FIGURE 2

(A) Changing the graded structure to step-graded structure for calculating the generation rate in nextnano3. Direction of the solar spectrum and hitting position to the structure is shown as well. (B) Zoom in for 90–100 nm to show converting graded to step-graded structure in which the number of each layer is given in addition to the layer when light passes through the structure.

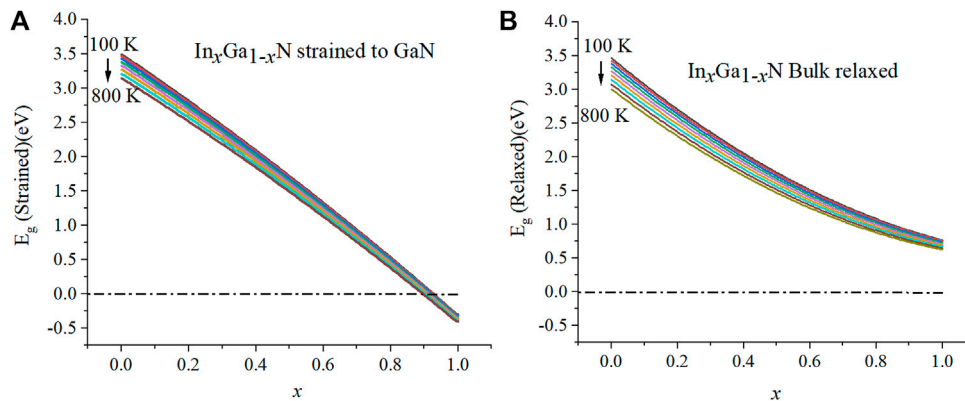


FIGURE 3

Temperature dependence of the energy band gap under the (A) strained condition and (B) relaxed condition (100–800 K).

nextnano software simulates the band structure in the envelope function approximation, using a single-band effective-mass approach (Nextnano, 2021). The electron motion is then determined by the one-electron Hamiltonian method, while multi-body effects are considered negligible (Birner et al., 2006).

The effect of temperature on the energy band gap was calculated between 100 K and 800 K, which is shown in Figures 3A,B, as functions of composition for the strained and relaxed conditions, respectively. Generally, as expected, the band gap is found to decrease with the increase in temperature. Somewhat surprisingly, though, we see that the band gap energy is predicted to be negative for  $\text{In}_x\text{Ga}_{1-x}\text{N}$ , strained to GaN with  $x > \sim 90\%$ . This high amount of strain would be difficult to pseudomorphically achieve and maintain in a single-composition thin film. However, within a graded composition structure, the localized strain can be much higher. In what follows,

regarding the strained graded structures, we generally limit our discussion to  $x < \sim 90\%$  in order to avoid the case where a solar cell has a negative band gap as this is not currently well defined. For the relaxed graded structures, we allow the composition to vary all the way to 100%, that is, pure InN.

For the base of the bulk relaxed band gap at low temperature,  $E_g$ , nextnano essentially uses Vegard's law to extrapolate between two components of an alloy with some associated bowing parameters. For  $\text{In}_x\text{Ga}_{1-x}\text{N}$ , this looks like:

$$E_g(\text{In}_x\text{Ga}_{1-x}\text{N}) = E_g(\text{InN})x + E_g(\text{GaN})(1-x) - b(x)(1-x), \quad (1)$$

where  $b$  is the bowing parameter. Different values have been reported for this bowing parameter. Shahab N. Alam et al. presented a review for bowing parameters in the group III-N

TABLE 1 Parameters for energy gap under strained and relaxed conditions in different temperatures.

Temperature (K)	$\alpha_{1S}$ ( $\times 10^{-1}$ )	$\beta_{1S}$	$\gamma_{1S}$	$\alpha_{1R}$	$\beta_{1R}$	$\gamma_{1R}$
100	-4.9286	-3.3137	3.5007	1.3990	-4.1052	3.4743
200	-4.9286	-3.2967	3.4751	1.3990	-4.0801	3.4372
300	-4.9286	-3.2715	3.4830	1.3990	-4.0486	3.3914
400	-4.9286	-3.2401	3.3922	1.3990	-4.0122	3.3387
500	-4.9286	-3.2037	3.3396	1.3990	-3.9718	3.2808
600	-4.9286	-3.1633	3.2816	1.3990	-3.9282	3.2185
700	-4.9286	-3.1196	3.2193	1.3990	-3.8818	3.1527
800	-4.9286	-3.0733	3.1536	1.3990	-3.8332	3.0840

ternary alloys. For InGaN, these values ranged between 1.4 and 3 eV (Kuo et al., 2001; Moret et al., 2009; Pelá et al., 2011; Alam et al., 2020). Additionally, there have been some reports which indicate that the bowing parameter has some compositional dependence (Caro et al., 2013; Moses et al., 2011), and some which claim no compositional dependence (Nawaz and Ahmad, 2012; Feng et al., 2013; Mesrane et al., 2015). We use the value for the bowing parameter given in the nextnano Material database,  $b = 1.4$  as a reasonable approximation (Vurgaftman et al., 2001; Wu et al., 2002; Vurgaftman and Meyer, 2003). At the same time, other bowing parameters may be possible, but we perform our calculations using this single value in order to learn the general response of the system. Any result which is dependent on the bowing is by its nature a second-order effect and should only minimally affect the present results.

In order to perform the two-step simulation that we have performed, that is, to calculate the generation rates in one software package and then import them to another, we required a full set of analytical relationships for the band gap values of all InGaN alloys at all temperatures. The band gap values were then used to determine the absorption coefficients, analytically, at each temperature. So, first, the band gaps as functions of composition, as shown in Figure 2, were fit to second-order polynomials for each temperature as follows (Sarollahi et al., 2022):

$$\begin{aligned} E_{g(Strain)} &= \alpha_{1S}x^2 + \beta_{1S}x + \gamma_{1S}, \\ E_{g(Relax)} &= \alpha_{1R}x^2 + \beta_{1R}x + \gamma_{1R}. \end{aligned} \quad (2)$$

The fitting was carried out in each individual temperature, for which the numbers are given in Table 1.

It is seen that  $\alpha_{1S}$  and  $\alpha_{1R}$  show constant values of -0.49286 and 1.3990, respectively. However, the other parameters vary with temperature and were subsequently fitted by polynomial functions of temperature of the following form:  $c_4T^4 + c_3T^3 + c_2T^2 + c_1T + c_0$ . The fitting parameters are given in Table 2.

The absorption coefficient for InGaN can be generally represented as follows (Brown et al., 2010; Belghouthi et al., 2015; Giannoccaro et al., 2016):

$$\alpha(\lambda) = \alpha_0 \sqrt{a(x)(E - E_g) + b(x)(E - E_g)^2}, \quad (3)$$

where  $E$  is the incoming photon energy given in eV and  $a$  and  $b$  are dimensionless fitting parameters. Belghouthi and Aillerie (2019); Belghouthi et al. (2016); and Belghouthi et al. (2015) determined experimentally  $a(x)$  and  $b(x)$  over the entire composition range to be

$$\begin{aligned} a(x) &= 12.87x^4 - 37.79x^3 + 40.43x^2 - 18.35x + 3.52, \\ b(x) &= -2.92x^2 + 4.05x - 0.66. \end{aligned} \quad (4)$$

Our goal is to reformulate the absorption coefficients to be the functions of band gap over the entire range of alloys. Once this calculation has been performed, Eq. 5 can be converted to functions of the band gap energies under strained and relaxed conditions by plotting and fitting the parameters in each individual temperature,  $a$  and  $b$ , as functions of the strained band gap energy under strain and relax conditions with respect to the GaN lattice constant,  $a(E_{g(Strain)})$ ,  $b(E_{g(Strain)})$  and  $a(E_{g(Relax)})$ ,  $b(E_{g(Relax)})$ , which are shown in each individual temperature in Figures 4A,B.

The best fits for both cases are derived by

$$\begin{aligned} a(E_{g(Strain)}, T) &= \alpha_{2S}(T)E_{gS}^5 + \beta_{2S}(T)E_{gS}^4 + \gamma_{2S}(T)E_{gS}^3 + \eta_{2S}(T)E_{gS}^2 + \delta_{2S}(T)E_{gS} + \epsilon_{2S}(T), \\ b(E_{g(Strain)}, T) &= \alpha_{3S}(T)E_{gS}^4 + \beta_{3S}(T)E_{gS}^3 + \gamma_{3S}(T)E_{gS}^2 + \eta_{3S}(T)E_{gS} + \delta_{3S}(T). \end{aligned} \quad (5)$$

Under the strained condition, these parameters as functions of temperature are presented in Tables 3, 4, respectively.

Now, again all parameters are fit to a fourth-order polynomial in temperature given by  $d_4T^4 + d_3T^3 + d_2T^2 + d_1T + d_0$ . The resulting fitting parameters are shown in Table 5.

The same procedure is performed for the relaxed structure. The absorption coefficient parameters,  $a$  and  $b$ , are fit as functions of  $T$  and the relaxed band gap,  $E_{g(Relaxed)}$ , as follows:

$$\begin{aligned} a(E_{g(Relaxed)}, T) &= \alpha_{2R}E_g^5 + \beta_{2R}E_g^4 + \gamma_{2R}E_g^3 + \eta_{2R}E_g^2 + \delta_{2R}E_g + \epsilon_{2R}, \\ b(E_{g(Relaxed)}, T) &= \alpha_{3R}E_g^4 + \beta_{3R}E_g^3 + \gamma_{3R}E_g^2 + \eta_{3R}E_g + \delta_{3R}, \end{aligned} \quad (6)$$

with fitting coefficients given in Tables 6, 7.



TABLE 2 Parameters for  $\beta, \gamma$  under strained and relaxed conditions.

	$c_4$ ( $\times 10^{-13}$ )	$c_3$ ( $\times 10^{-10}$ )	$c_2$ ( $\times 10^{-7}$ )	$c_1$ ( $\times 10^{-5}$ )	$c_0$
$\beta_{IS}(T)$	1.2405	-3.9830	6.0808	1.4391	-3.3209
$\gamma_{IS}(T)$	-1.8655	5.9312	-8.7359	-3.3524	3.5122
$\beta_{IR}(T)$	0.97538	-3.4463	5.6944	2.6000	-4.1306
$\gamma_{IR}(T)$	-1.4015	4.6921	-8.0193	-5.5534	3.5137

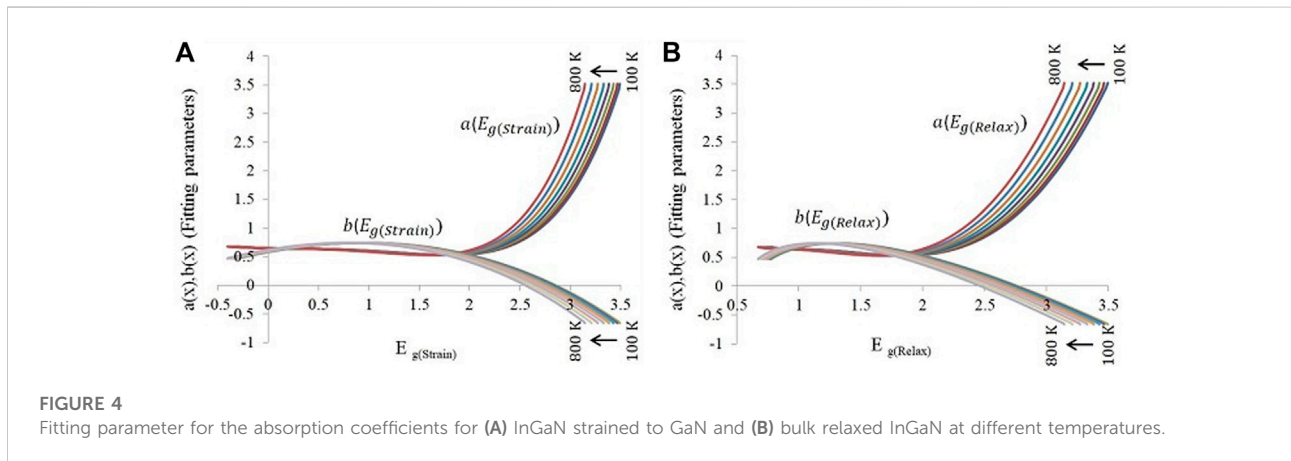


FIGURE 4 Fitting parameter for the absorption coefficients for (A) InGaN strained to GaN and (B) bulk relaxed InGaN at different temperatures.

TABLE 3 Fitting parameters for "a" the under strained condition at different temperatures.

T (K <sup>0</sup> )	$a(E_{g(\text{Strain})})$	$\alpha_{2S}$ ( $\times 10^{-2}$ )	$\beta_{2S}$ ( $\times 10^{-3}$ )	$\gamma_{2S}$ ( $\times 10^{-2}$ )	$\eta_{2S}$ ( $\times 10^{-2}$ )	$\delta_{2S}$ ( $\times 10^{-2}$ )	$\epsilon_{2S}$ ( $\times 10^{-1}$ )
100		1.1723	-8.4621	-5.7774	4.9491	-4.3511	6.5521
200		1.2051	-8.4067	-5.8204	4.7842	-4.2728	6.5481
300		1.2554	-8.3347	-5.8846	4.5488	-4.1689	6.5425
400		1.3220	-8.2552	-5.9630	4.2561	-4.0530	6.5359
500		1.4044	-8.1510	-6.0545	3.9169	-3.9357	6.5286
600		1.5027	-7.9913	-6.1600	3.5383	-3.8248	6.5209
700		1.6183	-7.7678	-6.2762	3.1225	-3.7269	6.5128
800		1.7527	-7.4551	-6.4015	2.6708	-3.6476	6.5044

Now, again all parameters for the relaxed condition as functions of temperatures are fit with a fourth-order polynomial,  $e_4T^4 + e_3T^3 + e_2T^2 + e_1T + e_0$ , with coefficients given in Table 8.

As mentioned previously, the  $\Lambda$ -graded structure is studied under fully strained to GaN and bulk relaxed conditions. In the absence of strain, pyro-electric polarization (spontaneous polarization) is the only polarization in the system:

$$P_{In_xGa_{1-x}N}^{ps} = -0.042x - 0.034(1-x) + 0.038x(1-x), \quad (7)$$

which is defined for  $In_xGa_{1-x}N$ , where  $x$  is the composition.

In contrast, in the presence of strain, piezo-electric polarization would be added to charges due to polarization (Belghouthi et al., 2016).

$$P_{In_xGa_{1-x}N}^{pz} = xP_{InN}^{pz}[\epsilon(x)] + (1-x)P_{GaN}^{pz}[\epsilon(x)]. \quad (8)$$

The piezo-electric polarization of the base InN and GaN are given by

$$\begin{aligned} P_{InN}^{pz}[\epsilon(x)] &= -1.373\epsilon(x) + 7.559\epsilon(x)^2, \\ P_{GaN}^{pz}[\epsilon(x)] &= -0.918\epsilon(x) + 9.541\epsilon(x)^2. \end{aligned} \quad (9)$$

Then, the total polarization is given by the simple sum of the piezo and the spontaneous components. The induced charges

TABLE 4 Fitting parameters for "b" under the strained condition at different temperatures.

T (K <sup>0</sup> ) b (E <sub>g</sub> (Strain))	$\alpha_{3S}$ (*10 <sup>-3</sup> )	$\beta_{3S}$ (*10 <sup>-3</sup> )	$\gamma_{3S}$ (*10 <sup>-1</sup> )	$\eta_{3S}$ (*10 <sup>-1</sup> )	$\delta_{3S}$ (*10 <sup>-1</sup> )
100	-1.4334	-5.2631	-1.5843	3.2516	5.8371
200	-1.4707	-5.3864	-1.5987	3.2337	5.8688
300	-1.5280	-5.5727	-1.6201	3.2084	5.9135
400	-1.6035	-5.8139	-1.6475	3.1772	5.9675
500	-1.6969	-6.1047	-1.6802	3.1411	6.0285
600	-1.807	-6.4518	-1.7176	3.1001	6.0945
700	-1.9374	-6.8500	-1.7595	3.0543	6.1646
800	-2.0877	-7.3056	-1.8058	3.0037	6.2376

TABLE 5 Fitting parameters for  $\alpha_{2,3}$ ,  $\beta_{2,3}$ ,  $\gamma_{2,3}$ , and  $\delta_{2,3}$  under the strained condition.

	$d_4$ (*10 <sup>-15</sup> )	$d_3$ (*10 <sup>-12</sup> )	$d_2$ (*10 <sup>-9</sup> )	$d_1$ (*10 <sup>-7</sup> )	$d_0$ (*10 <sup>-2</sup> )
$\alpha_{2S}(T)$	3.2292	-5.3453	11.166	2.5497	1.1591
$\beta_{2S}(T)$	1.6127	-0.028851	-0.094460	6.0338	-0.85226
$\gamma_{2S}(T)$	-1.9129	6.2866	-12.630	-10.242	-5.7549
$\eta_{2S}(T)$	-14.403	37.228	-54.148	-26.379	5.0260
$\delta_{2S}(T)$	8.3333	-29.283	27.948	13.9984	-4.3903
$\epsilon_{2S}(T)$	-5.5871	14.021	-14.777	-4.8307	65.539
$\alpha_{3S}(T)$	-0.37689	0.65164	-1.2848	-0.24658	-0.14186
$\beta_{3S}(T)$	-0.96212	1.8495	-3.9136	-1.8334	-0.52072
$\gamma_{3S}(T)$	-9.7538	26.168	-48.259	-16.068	-15.781
$\eta_{3S}(T)$	-16.761	37.266	-54.105	-41.261	32.608
$\delta_{3S}(T)$	24.621	-77.601	104.41	54.800	58.219

TABLE 6 Fitting parameters for "a" under the relaxed condition at different temperatures.

T (K <sup>0</sup> ) a (E <sub>g</sub> (Relaxed))	$\alpha_{2R}$ (*10 <sup>-2</sup> )	$\beta_{2R}$ (*10 <sup>-1</sup> )	$\gamma_{2R}$ (*10 <sup>-1</sup> )	$\eta_{2R}$ (*10 <sup>-1</sup> )	$\delta_{2R}$ (*10 <sup>-1</sup> )	$\epsilon_{2R}$ (*10 <sup>-1</sup> )
100	-3.0956	3.2293	-9.2215	9.3586	-3.3597	6.7996
200	-3.1867	3.2724	-9.1021	8.7958	-2.7976	6.6320
300	-3.3016	3.3236	-8.9330	8.0640	-2.897	6.4267
400	-3.4375	3.3799	-8.7106	7.1796	-1.2662	6.1966
500	-3.5899	3.4361	-8.4200	6.1362	-0.33829	5.9482
600	-3.7524	3.4867	-8.0444	4.9238	0.68589	5.6873
700	-3.9263	3.5264	-7.5666	0.35326	1.7975	5.4195
800	-4.1006	3.5488	-6.9667	1.9501	2.9891	5.1497

due to pyroelectric polarization are shown in Figure 6A. In addition, electron concentrations in the structure are given for  $T = 100$  K in Figure 5B. It is seen that a significant electron distribution penetrates into the p-type region for  $x_{max} > 60\%$ . At a maximum, when  $x_{max} = 100\%$ , the electron distribution is seen to penetrate  $\sim 15$  nm into the p-type region. When pyro-electric charges are negative, it means that the bound charges are

negative, so holes are attracted making it a p-type region. On the other hand, positive, bound, pyro-electric charges make an n-type region. It can be seen in Figure 5A that the pyro-electric background charge changes type roughly halfway through the layer, becoming a significant contribution to  $x_{max} > \sim 60\%$ . As a result, the simple p-n diode structure assumed for the device changes ultimately to a p-n-p-n-type structure.

TABLE 7 Fitting parameters for "b" under the relaxed condition at different temperatures.

T (K <sup>0</sup> ) b (E <sub>g</sub> (Relaxed))	$\alpha_{3R}$ (*10 <sup>-2</sup> )	$\beta_{3R}$ (*10 <sup>-1</sup> )	$\gamma_{3R}$	$\eta_{3R}$	$\delta_{3R}$
100	-5.4455	5.6637	-2.3312	3.7025	-1.2165
200	-5.4455	5.8865	-2.3883	3.7380	-1.2063
300	-6.1215	6.1816	-2.4633	3.7854	-1.1952
400	-6.6081	6.5468	-2.5548	3.8434	-1.1835
500	-7.2014	6.9839	-2.6622	3.9109	-1.1712
600	-7.9129	7.4971	-2.7855	3.9870	-1.1583
700	-8.7587	8.0926	-2.9250	4.0710	-1.1447
800	-9.7594	8.7791	-3.0814	4.1623	-1.1301

TABLE 8 Fitting parameters for  $\alpha_{2,3}$ ,  $\beta_{2,3}$ ,  $\gamma_{2,3}$ , and  $\delta_{2,3}$  under the relaxed condition.

	$e_4$ (*10 <sup>-14</sup> )	$e_3$ (*10 <sup>-11</sup> )	$e_2$ (*10 <sup>-7</sup> )	$e_1$ (*10 <sup>-5</sup> )	$e_0$ (*10 <sup>-1</sup> )
$\alpha_{2R}(T)$	0.15530	0.38662	-0.16432	-0.17156	-0.29989
$\beta_{2R}(T)$	-2.3295	-3.5568	0.88150	0.70854	3.1831
$\gamma_{2R}(T)$	12.547	-0.19956	1.8195	2.5264	-9.3455
$\eta_{2R}(T)$	-21.733	36.906	-10.232	-10.991	9.9623
$\delta_{2R}(T)$	16.867	-55.966	11.100	10.485	-3.9719
$\epsilon_{2R}(T)$	-5.9848	24.131	-3.6340	-2.8592	6.9840
$\alpha_{3R}(T)$	-1.9413	2.3602	-0.59423	-0.24222	-5.1751
$\beta_{3R}(T)$	10.559	-16.727	4.5115	2.2361	5.4502
$\gamma_{3R}(T)$	-20.73	48.074	-12.058	-4.6587	-22.771
$\eta_{3R}(T)$	7.6705	-32.052	8.4048	-0.92532	36.732
$\delta_{3R}(T)$	-194.13	480.52	-42.481	170.30	-14.517

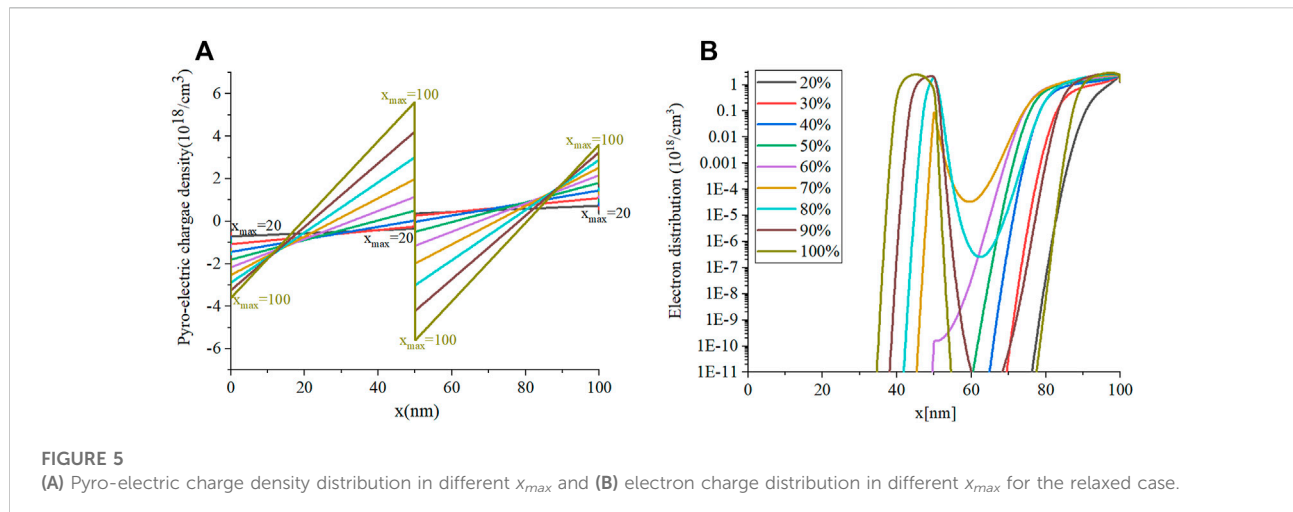


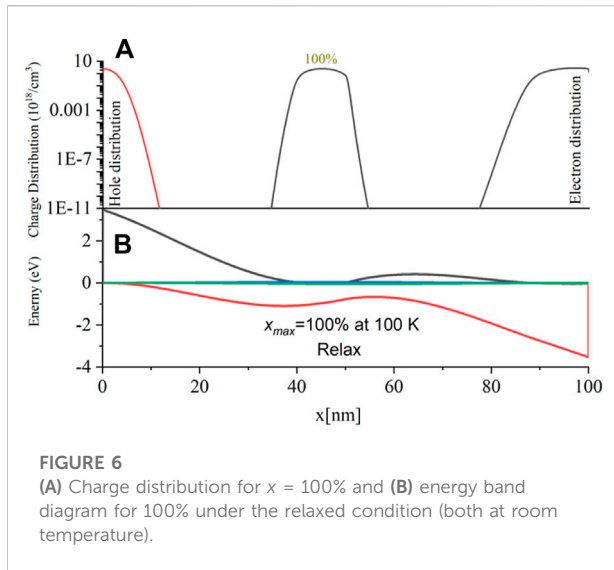
FIGURE 5

(A) Pyro-electric charge density distribution in different  $x_{max}$  and (B) electron charge distribution in different  $x_{max}$  for the relaxed case.

Figure 6A shows both the electron and hole concentration for the  $x_{max} = 100\%$  case. Here, the p-n-p-n-type structure can be seen; however, the hole concentration between  $\sim 60$  and  $\sim 80$  nm has effectively compensated the free electrons leaving the material with

vanishingly small free carriers of either type. However, now, we see for the band diagram of the  $x_{max} = 100\%$  device in Figure 6B that there are additional barriers for the current to flow through the device. This results in increased  $V_{oc}$  which we will see in the following paragraphs.





Now, with the absorption coefficients as functions of the band gap, which is a function of the temperature and composition, under strained and relaxed conditions, we can determine the generation rate as explained previously. This is shown for  $x_{max} = 70\%$  in Figures 7A,B for the bulk relaxed case and the strained to GaN case, respectively, over the temperature ranging from 100 K to 800 K. It can be seen that the strained material reaches much higher generation rates due to the lower band gap. At the same time, it is evident that the generation rates generally increase as a result of increasing temperature. This is also due to the decreasing band gap as the temperature increases.

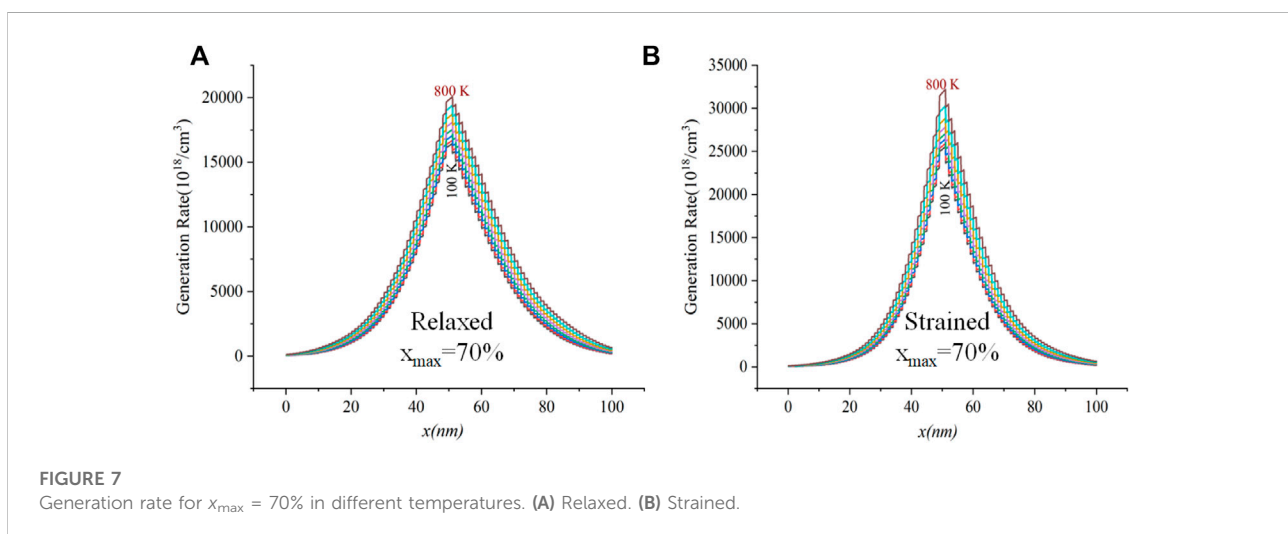
By importing the generation rates into nextnano, the  $J$ - $V$  curves used to calculate solar cell parameters can be calculated. Figures 8A,B show the  $J$ - $V$  curves, again for  $x_{max} = 70\%$ , for relaxed and strained materials, respectively, as the temperature is changed from

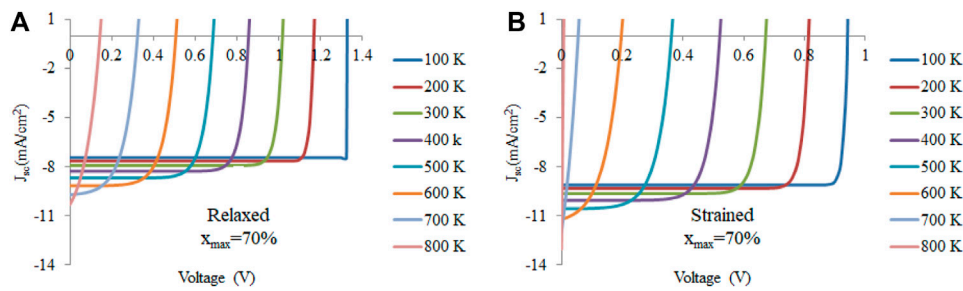
100 K to 800 K. Here, it can be seen that as the temperature decreases, the  $J$ - $V$  curves become more like an ideal diode curve.

Other solar cell parameters such as open-circuit voltage ( $V_{oc}$ ), short-circuit current density ( $J_{sc}$ ), and solar efficiency for different  $x_{max}$  and  $T$  are obtained from the  $J$ - $V$  curves. As seen in Figure 10B, for the strained devices,  $V_{oc}$  decreases with an increase in  $x_{max}$  that is, a decrease in the band gap, which was expected (Green, 1998; Green, 1981). Under relaxed condition, the  $V_{oc}$  behavior is not linear with the band gap, as seen in Figure 10A. As shown previously in Figure 6, the electrons penetrate into the p-type region. At  $x_{max} > 80\%$ , when the penetrated charge density is almost equal to polarization doping charge,  $V_{oc}$  begins to increase. It means that for  $x_{max} > 80\%$  at low temperatures,  $V_{oc}$  is increased as energy band diagrams and shows the p-n-p-n structure instead of the p-n structure. However, the second p-layer is relatively weak. We believe that the changing carrier density for  $x_{max} > 80\%$  is the main reason for the increasing  $V_{oc}$  as shown in Figure 7. Finally, Figure 9C shows more details for  $V_{oc}$  at room temperature for high indium concentrations. Here, it can be seen that at  $x_{max} = \sim 88\%$ ,  $V_{oc}$  increases due to the charge penetration into the p-region and the resulting p-n-p-n structure. As shown in Figure 6B, Figure 7, doping concentrations due to structure change and carrier distribution are not linear.

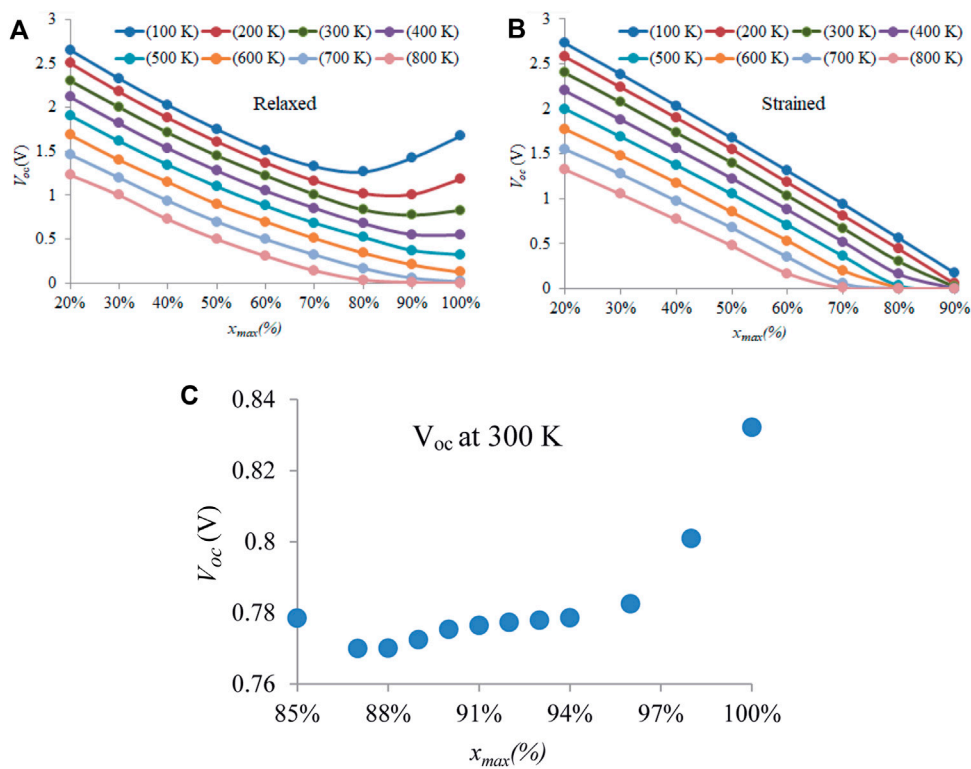
The open-circuit voltage,  $V_{oc}$  for the relaxed and strained conditions are shown in Figures 9A,B, respectively, while the short-circuit current density,  $J_{sc}$  for the relaxed and strained conditions is shown in Figures 10A,B, respectively. Generally,  $J_{sc}$  increases when the indium composition increases and lowers the band gap (Green, 1998; Green, 1981).

The fill factors were calculated and are displayed in Figures 11A,B for both the relaxed and strained devices, respectively. Under both conditions, the FF generally decreases as  $x_{max}$  increases. Similarly, as expected, the FF decreases with an increasing temperature. For the relaxed case, this is a relatively stable linear decay, which increases as  $x_{max}$  increases. However, for the strained case, the FF rapidly vanishes at the highest  $x_{max}$  values.





**FIGURE 8** J-V curve for  $x_{max} = 70\%$  for both the (A) relaxed condition and (B) strained condition are given at different temperatures (100–800 K).



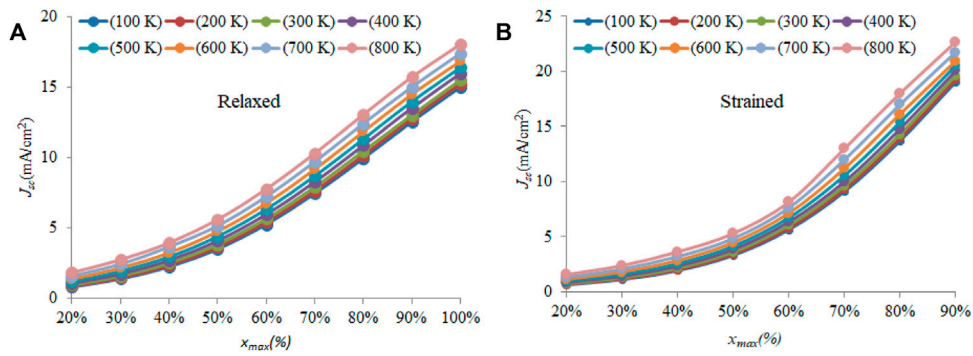
**FIGURE 9** (A) and (B)  $V_{oc}$  for both relaxed and strained conditions at different temperatures for different  $x_{max}$  (C) at room temperature for  $x_{max} = 85\%–100\%$ .

Finally, the total solar efficiency was calculated for all cases. This can be calculated using the following formula:

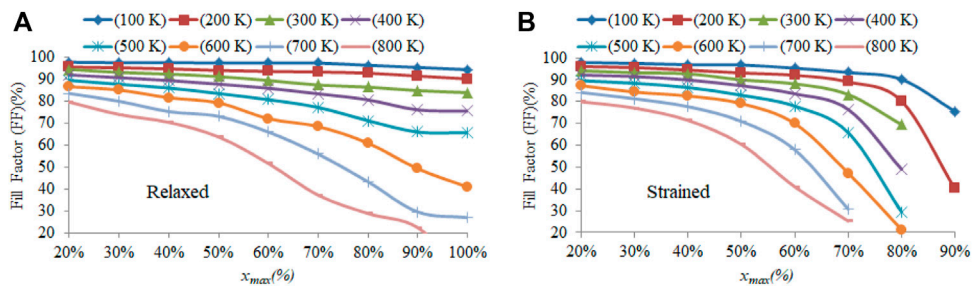
$$Efficiency (\%) = \frac{P_{max}}{P_{in}} = \frac{P_{max}}{100}, \quad (10)$$

$$P_{max} = FF * J_{sc} * V_{oc}.$$

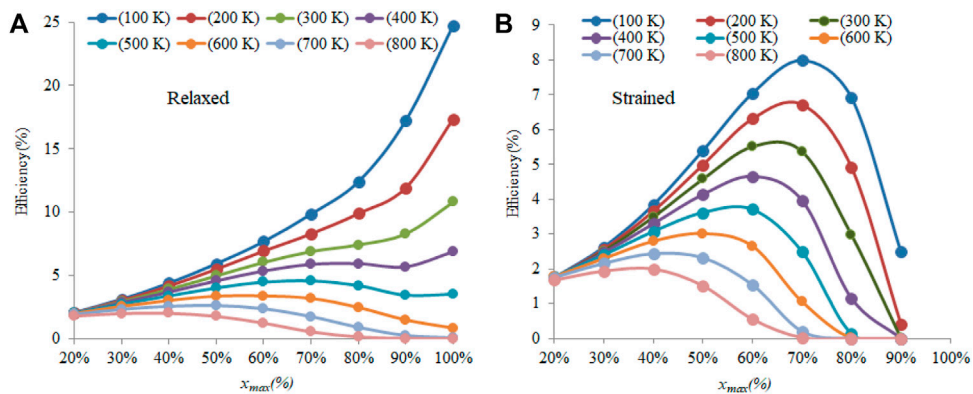
Figures 12A,B show the solar efficiencies as functions of  $x_{max}$  for temperatures ranging from 100 K to 800 K, for the relaxed and strained devices, respectively. Under the relaxed condition, the devices reach the maximum efficiency when  $x_{max} = 100\%$ , that is, InN, for the lower temperatures from 100 to 400 K. For the higher temperatures, the maximum efficiency shifts toward lower  $x_{max}$ .



**FIGURE 10**  
 $J_{sc}$  for both (A) relaxed and (B) strained conditions at different temperatures for different  $x_{max}$ .



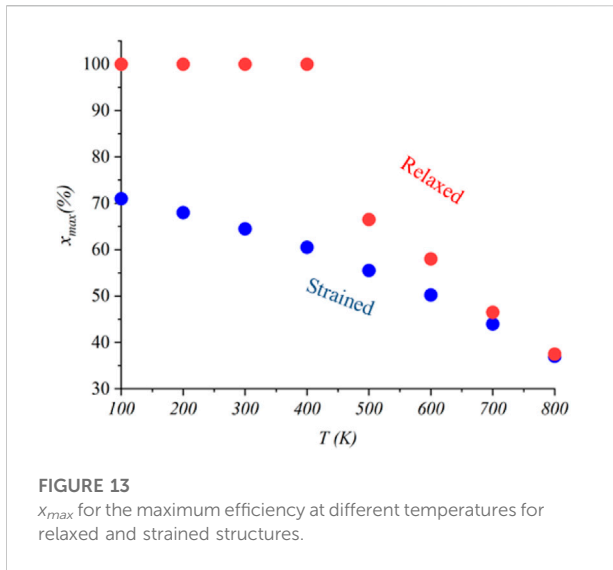
**FIGURE 11**  
 Fill factor for the (A) relaxed condition and (B) strained condition for different temperatures. The lines are just guides to the eye.



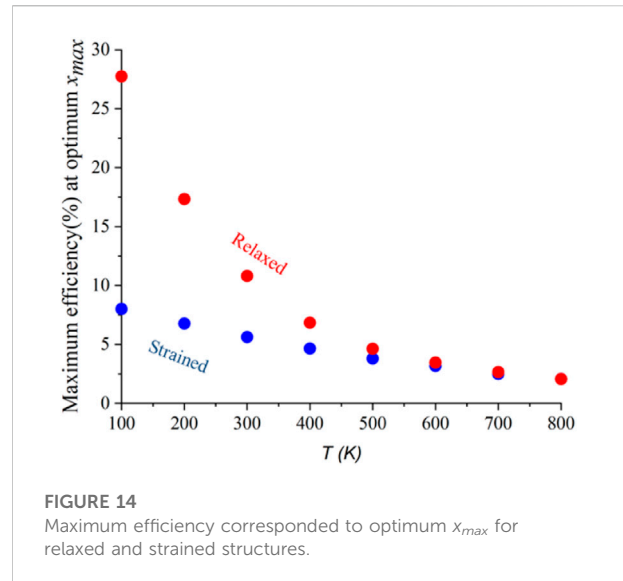
**FIGURE 12**  
 Efficiency for both (A) relaxed and (B) strained conditions at different temperatures for different  $x_{max}$ .

For the strained structures, the maximum efficiency from high to low temperatures is linearly shifted toward low  $x_{max}$  due to sharp dropping of  $V_{oc}$  for high  $x_{max}$  at high temperatures which reduces  $P_{max}$ .

Figure 13 summarizes  $x_{max}$  found to maximize the efficiency for each temperature for both the strained and relaxed cases. Here, we see that for the strained structure, the maximum  $x_{max}$  decreases monotonically from 71% to



**FIGURE 13**  
 $x_{max}$  for the maximum efficiency at different temperatures for relaxed and strained structures.



**FIGURE 14**  
Maximum efficiency corresponded to optimum  $x_{max}$  for relaxed and strained structures.

37% as the temperature increases. At the same time, though, for the relaxed structures, for low temperatures (100–400 K), the maximum  $x_{max}$  is 100%, while for higher temperatures (500–800 K), it also demonstrates a monotonic decrease from ~65% to 35%.

The maximum efficiencies found for each maximum  $x_{max}$  at each temperature is given in Figure 14. It shows that the efficiency for the relaxed structures at low temperatures is much higher than that for the strained structures, which are due to the sudden drop in  $V_{oc}$  at low temperatures. The maximum efficiency at high temperatures monotonically decreases and is almost the same as the strained structure at high temperatures (600–800 K).

## Conclusion

$\Lambda$ -graded InGaN solar cells were designed to make p-n junction solar cells by polarization doping. Solar cell parameters under both bulk relaxed conditions and fully strained to GaN conditions were studied using nextnano software. A Vegard's law-like equation was defined to calculate the energy band gap under strained conditions as functions of temperature. Several fitting methods were performed to have analytical representations of the absorption coefficient as a function of band gap and temperature (for both relaxed and strained structures). In order to perform the simulations, the graded structures were converted to step-graded structures with a 1-nm step. The generation rate was obtained for each layer, then imported into nextnano software in order to simulate the light  $J$ - $V$  curves. The solar cell parameters were then extracted from

these structures under strained and relaxed conditions.  $V_{oc}$  for the relaxed structures sharply increase for low temperatures (100–400 K). The free carrier densities and band structures for these structures show that the as-designed p-n diode structures are converted into p-n-p-n structures due to the conversion of the polarization charge density from negative to positive within the compositional grading as a result of the effective bowing parameter of the InGaN polarization. Finally, the maximum  $x_{max}$  was determined for each temperature for both strained and relaxed conditions. This work demonstrates that this  $\Lambda$ -graded InGaN solar cell design could be extremely useful in constructing a solar cell for the purpose of operating in high-temperature environments. At the same time, these designs have shown great potential overall with efficiencies up to ~25% for thin-film designs of only 100 nm. Thicker films would most certainly increase on this number.

## Data availability statement

The original contributions presented in the study are included in the article; further inquiries can be directed to the corresponding authors.

## Author contributions

MS: idea, Matlab—nextnano simulation, literature review, and writing. MZ-A: MATLAB simulation. MA: nextnano simulation. RA: literature review and MATLAB simulation. MM: literature review—writing—solar cell. MR: literature

review—material. RA: literature review—material. YM: supervision. MW: PI, main idea, supervision, and writing.

## Conflict of interest

The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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