



Holistic Design of Energy Pile Bridge Deicing System With Ontology-Based Multiobjective Decision Making

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Even though the energy piles have been applied for the bridge deicing system, the traditional design approach is commonly a single-domain and objective-oriented method and is consequently lacking means to comprehensively consider all the relevant factors, such as life-cycle cost, investment payback cycle, carbon emissions, etc. This paper presents a holistic designing tool, namely, OntoBDDS, was developed based on ontology method and SWRL rules. It can automatically provide financial, safety, and heat flux information for designers to evaluate and optimize the design scheme of a deicing system in the early design stage of a bridge. After semantic and syntactical validation of the OntoBDDS system, a case study was also conducted to demonstrate how to leverage knowledge query to provide a series of design alternatives autonomously through considering different design parameters. This case study also verified the practicability and feasibility of the OntoBDDS holistic decision-making system and indicated its potential to be applied for other engineering problems when dealing with multiobjective holistic design making.

Keywords: ontology, holistic design, energy pile, deicing, bridge

INTRODUCTION

Snow and icing are serious hazards that may severely influence the safety and the normal operation of a transportation system. A slippery road surface may cause accidents (Lee et al., 2014) and huge maintenance costs. Taking the United States as an example, the annual expense of ice and snow removal is more than 2.3 billion US dollars, accounting for 20% of the US Department of Transportation (DOT) winter road maintenance budget (Han and Yu, 2017). Therefore, how to remove the ice and snow of bridge safely and effectively has become an important issue to ensure the safe and efficient running of the transportation system.

Traditionally, the snow and ice on the pavement can be removed physically or chemically. The physical method, by which the snow and ice are removed by specially designed vehicles or shovels, is a labor-intensive yet low efficient method. The chemical methods also suffer from drawbacks such as corrosion to the bridge structure, pollution to the environment, and limited working scenario; most chemical ice removers are only effective below 3.9°C (Balbay and Esen, 2010). The energy pile system (Morino and Oka, 1994) provided another safe and efficient solution to the deicing problem. **Figure 1** demonstrates the schematic of the energy pile-based deicing system (EPBDIS) for a bridge deck. It utilizes energy piles to extract geothermal heat from underground and then pumps the heat into the exchange tubes beneath the bridge deck for deicing. Compared with the traditional methods, the EPBDIS is labor-free and ecofriendly (Miyamoto and Takeuchi, 2005; Brandl, 2006), which makes it promising in field applications.

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During the past decades, energy piles have been extensively studied theoretically and experimentally. In terms of thermal performance, a variety of numerical methods were proposed to study the heat transfer performance of the energy pile bridge deicing system and to verify its feasibility (Yari and Javani, 2010; Dupray et al., 2014; Han and Yu, 2017). Besides, many experimental studies and field tests were carried out to further validate the effectiveness of the energy piles. In Liu et al. (2007) and Balbay and Esen (2010), the authors conducted on-site experiments on the heat transfer performance of the energy pile bridge deck deicing system with a heat pump and verified its feasibility. Kong et al. (2019) and Bowers and Olgun (2015) studied and verified the thermal energy characteristics and feasibility of heat pump-free deicing systems based on field experiments. In addition, considering that the energy pile may cause temperature stress among the bridge structure, the influence of the energy pile on the bearing capacity was investigated by many researchers. In Laloui (2011) and Bourne-Webb et al. (2009), the effect of heat exchange on the bearing capacity of pile foundation was discussed. Subsequently, Amatya et al. (2012) and Ozudogru et al. (2015) discussed the response of energy pile's thermal performance with different end constraints and ground conditions. Loveridge and Powrie (2013) and Jeong et al. (2014) identified the key factors affecting the thermal-mechanical interaction of energy piles.

An optimal design of the energy piles shall comprehensively consider every related aspect, including the thermal exchange efficiency, load capacity, finial cost, and environmental impacts. However, previous studies mainly focus on a specific aspect of the energy pile, neglecting the influence of other factors. For example, Nagai et al. (2009) developed a numerical simulation program to predict the temperature field of the system and evaluate the system performance. Liu et al. (2018) considered the heat transfer performance of the system and its economy and verified the feasibility of the system in Canada. In addition, due to the technical complexity of the ground source heat pump system, the relevant information is distorted and misunderstood when it is transmitted between different professions and departments, causing unnecessary losses (Zhang and Liao, 2015), which means that the rational use of systems requires an accurate and recognized domain of knowledge to ensure the accuracy of information transfer.

As a new semantic web technology, ontology can construct accurate domain knowledge and has been widely applied for knowledge sharing and exchange in different fields (Ahmed et al., 2007). Ontology's interdisciplinary features enable interrelated domains to be considered together, and its semantic structure, logical reasoning capabilities, and other characteristics provide an effective method for cross-domain integrated design. More importantly, its language could be recognized by both humans and computers. The ontology has been widely applied in relevant fields of energy pile bridge deicing systems such as pile engineering, bridge engineering, and ground source heat pump system. Specifically, Yurchyshyna and Zarli (2009) proposed a framework for consistency checking in buildings based on ontology. Zhang and Liao (2015) presented an ontology framework for describing ground source heat pump systems, providing guidance for constructing different ground source heat pump systems. Ren et al. (2019) proposed an ontology framework for bridge maintenance. The above provides the methodology and guidance for constructing the ontology framework of the energy pile bridge deck deicing system.

Based on the aforementioned works, it is necessary to use ontology to develop a designing tool for the energy pile bridge deck deicing system, which can comprehensively consider the heat flux, bearing capacity, and a total investment of the system to achieve optimal design. This research developed a comprehensive design decision-making tool named OntoBDDS (ontology of bridge deck deicing system using energy pile) for the holistic design of energy pile bridge deck deicing system in the early design stage. The remaining of the paper is organized as follows: Development of OntoBDDS for Multiobjective Holistic Design describes the development and validation of OntoBDDS; Case Study presents a case study to demonstrate how the engineers can use this tool to design the deicing system.

DEVELOPMENT OF ONTOLOGY OF BRIDGE DECK DEICING SYSTEM FOR MULTIOBJECTIVE HOLISTIC DESIGN

Determination of the Primary Indicators for the Energy Pile-Based Bridge Deck Deicing System

The key design parameters of the energy pile bridge deck deicing system include equipment cost, the vertical bearing capacity, heat flux, etc.

The Equipment Cost

The total cost of equipment and facilities includes the cost of the heat transfer tubes of the foundation and the deck and cost of the heat pumps. The cost of heat transfer tubes of the foundation can be calculated by the following equation:

$$C^{\rm PT} = \sum_{i=1}^{n} C_i^{\rm PT} \times L_i^{\rm PT} \times N_i \tag{1}$$

in which *i* represents the *i*th type of pile; L_i^{PT} denotes the length of the *i*th type of pile; C_i^{PT} is the price of heat exchanger tube (RMB) per unit length of the *i*th pile type; N_i is the number of the *i*th pile type.

The cost of the heat transfer tubes imbedded in the bridge deck is expressed as

$$C^{\rm BT} = \sum_{j=1}^{n} C_j^{\rm BT} \times L_j^{\rm BT} \times N_j \tag{2}$$

where *j* represents the *j*th type of bridge deck; C_j^{BT} is the price of the heat transfer tube per unit length; L_j^{BT} is the length of the heat transfer tube of the *j*th type of bridge deck; N_j is the number of the *j*th type of bridge deck and C^{BT} is the total cost of the heat transfer tubes in the bridge deck.

The cost of the heat pumps can be easily attained by

$$C^{\rm p} = \sum_{k=1}^{m} C_k^{\rm p} \times N_k^{\rm p} \tag{3}$$

in which k represents the kth heat pump; C_k^P is the price of the kth type of heat pump; N_k^P is the number of the kth type of heat pump and C^P denotes the total cost of heat pump.

The total cost of equipment is expressed as

$$C^{\rm E} = C^{\rm PT} + C^{\rm BT} + C^{\rm P} \tag{4}$$

in which C^{PT} is the cost of the heat transfer tubes inside the foundation (in a unit of RMB); C^{BT} denotes the cost of the heat transfer tubs; C^{P} is the cost of the heat pumps and C^{E} is the total cost of all facilities.

Heat Flux

The heat extracted by the energy piles can be obtained by

$$Q_{\text{source}} = \sum_{i=1}^{n} q_i^{\text{pile}} \times L_i^{\text{pile}} \times N_i$$
(5)

where *i* indicates the *i*th type of pile; q_i^{pile} denotes the heat attained by a unit length of the *i*th type of pile; L_i^{pile} is the length of the *i*th type of pile; N_i is the number of the *i*th type of pile and Q_{source} is the total heat extracted by energy piles.

According to Han and Yu (2017), the available heat for the deicing system can be calculated by

$$Q_{\text{heat}} = \frac{COP}{COP - 1} \times Q_{source} \tag{6}$$

in which *COP* is the coefficient of performance of the heat pumps (Self et al., 2013), Q_{source} is the total energy extracted by energy piles from underground; Q_{heat} is the heat available for deicing.

The heated area of the bridge deck is expressed as

$$A_{\text{heat}} = \sum_{j=1}^{n} a_j^{\text{heat}} \times N_j \tag{7}$$

where *j* represents the *j*th type of bridge deck; a_j^{heat} is the area of *j*th type bridge deck heated by energy pile deicing system; N_j [†] is the number of *j*th type bridge deck and A_{heat} denotes the total area heated by the deicing system.

Therefore, the heat flux of the bridge deck without an additional heat pump is

$$q = \frac{Q_{\text{source}}}{A_{\text{heat}}} \tag{8}$$

where Q_{source} is the total energy; A_{heat} is the heated area and q is the heat flux provided by the energy pile system without a heat pump.

Similarly, the heat flux of the bridge deck with a heat pump is as follows:

$$q_{\rm pump} = \frac{Q_{\rm heat}}{A_{\rm heat}} \tag{9}$$

where Q_{heat} is the total heat provided by the deicing system; A_{heat} is the heated area and q_{pump} represents the heat flux of the deicing system with heat pump.

Vertical Bearing Capacity

The bearing capacity provided by the energy piles can be obtained by

$$Q = \sum_{i=1}^{n} \frac{Q_i^{\text{vk}}}{K} \times N_i \tag{10}$$

in which *i* is the *i*th type file; Q_i^{vk} is the vertical bearing capacity of the *i*th type file; *K* is a safety factor; N_i is the number of the *i*th type file and Q denotes the total vertical bearing capacity.

Evaluation

The evaluation of a deicing system is conducted *via* a comparison between provided heat flux and required heat flux q_0 . Grades and criteria are listed in **Table 1**.

Design and Development of Ontology of Bridge Deck Deicing System The System Framework and User Guides of Ontology

of Bridge Deck Deicing System

The proposed designing tool, OntoBDDS, consists of four major components: the database, the management system of ontologies, the editing system of rules, and the querying interface, as illustrated in **Figure 2**. Of these four parts, the database provides a foundation of all functions. All data and ontologies of the energy piles and information of the deicing system are saved in the database in OWL (ontology web language) format. The management system of ontologies is the core part of OntoBDDS, and in this study, it is developed by Protégé 5.2. The editing system of rules can offer a reasoning function with SWRL (sematic web rule language), to realize the holistic design of energy pile deicing system. Moreover, engineers can use the querying interface to obtain feasible solutions to the designing problem. The essential components of the ontology system, OntoBDDS, are specified as follows:

Ontology editor

Protégé-OWL 5.2 provides a platform to create and update ontologies, which is compatible with most OWL files and has various plug-ins for a user to select. TABLE 1 | The evaluation of the energy pile deicing system for bridge deck.

Evaluation	Expression	Description					
Good	$q \ge q_0$	The energy pile deicing system can satisfy the heat flux requirement without a heat pump					
Feasible	$q_{\text{pump}} \ge q_0 \ge q$	The energy pile deicing system can satisfy the heat flux requirement with a heat pump					
Not feasible	$q_0 > q_{pump}$	The energy pile deicing system cannot satisfy the heat flux requirement					



Ontology reasoner

Pellet is an OWL reasoning engine that implements the services of basic reasoning and consistency checking for OWL ontologies.

Plug-ins

SWRLTab is a Protégé-OWL plug-in that edits the SWRL rules, while SQWRLTab is a plug-in that edits SQWRL rules for querying.

Based on OntoBDDS, engineers can conduct a holistic design of the energy pile deicing system following the process illustrated in **Figure 3**.

The Development of the Ontology of Bridge Deck Deicing System

The establishment of the OntoBDDS follows three major steps: Knowledge Identification, Knowledge Specification, and Knowledge Refinement. In the Knowledge Identification, the scope and the aim of the energy pile-based deicing system were determined on the basis of the function of the OntoBDDS and ontology models established previously. In the step of Knowledge Specification, a specification of the knowledge model is constructed by establishing a semiformed ontology model, which can be further refined by engineers according to their designing purpose. In the last step, the Knowledge Refinement step, the ontology model is validated and refined to reassure the accuracy and conciseness of the system.

In this study, the scope of the ontology model includes pile foundation engineering, bridge engineering, bridge deicing, and geothermal pump system. Heat flux, cost, and safety of the bridge structure are the major issues to be considered in holistic design. The key concepts and terms of the OntoBDDS follow the IFC standard and relative ontology models established previously (Ren et al., 2019). The key concepts and terms are shown in **Figure 4** using UML (Unified Modeling Language).

In this study, the Ontology Development 101 (Noy and Mcguinness, 2001) is utilized to develop the OntoBDDS. The Ontology Development 101 is a methodology widely accepted for establishing ontology systems because of its efficiency and simplicity. The detailed steps are illustrated in **Figure 5**. It can be further explained as follows:



Step 1: The relevant domain and scope of the ontology are determined based on basic questions (BQ) and competency questions (CQ).

Step 2: IFC framework of the building SMART is adopted as the main development standard for the exchanging and sharing of Building Information, which facilitates the concept development of information ontologies for the holistic design of energy pile system (Horrocks et al., 2004).

Step 3: A dictionary of key concepts and terms regarding the deicing systems is established, which includes maintenance, safety, financial cost, mechanical property, etc.

Step 4: According to the dictionary established in Step 3, general classes of the OntoBDDS are established as shown in Figure 6A.

Step 5: There are mainly two types of properties to describe the relevant classes, namely, object properties and data properties, which define the relationships between classes and represent the characteristics of class instances, respectively, as illustrated in **Figures 6B,C**.

Step 6: In this step, specific instances are created. Each instance represents a unique design solution of the energy pile-based deicing system. Step 7: SWRL rules for the holistic design of energy pile system are defined to improve the ontology's flexibility for calculating and reasoning. There are four types of atoms for SWRL rules, i.e., Class atoms, Individual Property atoms, Data Valued Property atoms, and Built-in atoms. In addition, the symbols of SWRL rules include the connection symbol ", the implication symbol ' \rightarrow ', and the question mark '?' (Guizzardi et al., 2008). The specific SWRL rules for the calculation of equipment cost of energy pile system is illustrated as follows:

Equation	$C^{E} = C^{PT} + C^{BT} + C^{P}$
SWRL:	De-icing_system(?DS)Pile_heat_exchanger_tube_cost(?DS,? pile_tube_cost)Bridge_deck_heat_ exchanger_tube_cost(?DS,? deck_tube_cost)Pump_cost(?DS,?pump_cost)swrlb:add(?total_cost,? pile_tube_cost, ?deck_tube_cost, ?pump_cost) -> Total_cost(?DS, ? total_cost)

Step 8: User can query design solutions by inputting SQWRL rules in SQWRLQueryTab of the Protégé query interface. An example of cost query for energy pile system is illustrated as follows: SQWRL De-icing_system(?DS)Total_cost(?DS,?total_cost)Q(?DS,? bearing_capacity)q0(?DS,?q_0)`q(?DS,?q_)q_pump(?DS,? q_heat_pump)Evaluation(?DS,?evaluation)has_pump(?DS, ? pump_type)->sqwrl:select(?DS,?total_cost,?bearing_capacity,? pump_type,?q_0,?q_,?q_heat_pump,?evaluation) compare the ontology model with existing models, while the other method is to establish a new ontology model by expanding the existing one (Green et al., 2002). In this study, the OntoBDDS is developed based on IFC and existing ontology models (Ren et al., 2019). Therefore, the semantic





Ontology Validation

Validation of the OntoBDDS system was performed to assure its accuracy and ability to provide the expected design function. The validation includes semantic correctness, syntactic correctness, and rules validation.

Semantic Validation

There are two methodologies to assure the semantic correctness of an ontology model. One method is to

correctness of the key concepts and terms is automatically validated.

Syntactical Validation

Syntactical validation can be conducted by reasoning engines. In this study, the OntoBDDS is developed using Protégé-OWL 5.2. The pellet reasoner embedded in Protégé-OWL 5.2 can be used to detect syntactical errors of OntoBDDS. **Figure 7** shows the log of running pellet plug-in for completed consistency checking of the OntoEPS.





Rules Validation

In this study, a plug-in called SWRLTAB is utilized to validate the rules preliminarily, as shown in Figure 8.

Then, in *Case Study*, a case study will be presented to further verify the effectiveness and feasibility of all the rules of OntoBDDS.

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CASE STUDY

Case Study Description

In this section, an energy pile-based deicing system for a bridge deck is designed to demonstrate the main functions of the OntoBDDS software. The prototype bridge is a three-span beam bridge constructed in Jiangyin of Jiangsu Province. Its configuration is illustrated in **Figure 9**.

As shown in **Figure 9**, the size of the bridge deck allows for no more than 20 energy piles to be constructed. Moreover, heat

TABLE 2 | The detail of the design solution.

Design	Р	ile		Pum	р		Bridg	je deck	Pile he	at exchanger	tube	Bridge dec	k heat exchan	ge tube
solutions	q _{pile} (w/m)	Q _{vk} (kN)	Туре	COP	Cost (RMB)	Number	A (m ²)	Number	Туре	Length (m)	Cost (RMB)	Туре	Length (m)	Cost (RMB)
DS-lane-single_U	27	6,500	Circulating pump		2,800	1	15	12	Single U	40	3	Lane type	90	3
DS-lane-single_U-heat pump	27	6,500	Heat pump	3	16,000	1	15	12	Single U	40	3	Lane type	90	3
DS-lane-P_2_U	31.5	6,430	Circulating pump		2,800	1	15	12	Parallel 2 U	80	3	Lane type	90	3
DS-integral-P_2_U- heat_pump	31.5	6,430	Heat pump	3	16,000	1	30	12	Parallel 2 U	80	3	Integral type	150	3
DS-integral-S_2_U	36	6,400	Circulating pump		2,800	1	30	12	Series 2 U	80	3	Integral type	150	3
DS-integral-S_2_U- heat pump	36	6,400	Heat pump	3	16,000	1	30	12	Series 2 U	80	3	Integral type	150	3
DS-integral-3_U	45	6,300	Circulating pump		2,800	1	30	12	3 U	120	3	Integral type	150	3
DS-integral-3_U- heat_pump	45	6,300	Heat pump	3	16,000	1	30	12	3 U	120	3	Integral type	150	3
DS-lane-5_U	54	6,250	Circulating pump		2,800	1	15	12	5 U	200	3	Integral type	150	3
DS-integral-5_U- heat pump	54	6,250	Heat pump	3	16,000	1	30	12	5 U	200	3	Lane type	90	3
DS-integral-spiral	63	6,200	Circulating		2,800	1	30	12	Single spiral	250	3	Integral type	150	3
DS-integral-spiral- heat_pump	63	6,200	Heat pump	3	16,000	1	30	12	Single spiral	250	3	Integral type	150	3



TABLE 3 | SWRL rules to calculate bearing capacity.

Rule 1

Calculating the bearing capacity: $Q = \sum_{i=1}^{n} \frac{Q_i^{k}}{K} \times N_i$

De-icing_system(?DS)has_pile(?DS, ?pile)*Pile(?pile)*Qvk(?pile, ?qvk)*Number(?pile, ?N)*K(?DS, ?k)*swrlb:divide(?x, ?qvk, ?k)*swrlb:multiply(?Q0, ?x, ?N) -> Q(?DS, ?Q0)

TABLE 4 | SWRL rules to calculate the total cost.

Rule 1	Calculating pile heat exchanger tube cost: $C^{PT} = \sum_{i=1}^{n} C_{i}^{PT} \times L_{i}^{PT} \times N_{i}$ De-icing_system(?DS)has_pile(?DS,?pile)Pile(?pile)Number(?pile,?N)has_pile_heat_ exchanger_tube(?pile_tube) Pile_heat_exchanger_tube(?pile_tube)Cost(?pile_tube,?cost) Length(?pile_tube,?L)swrlb:multiply(?pile_tube_cost,?cost,?L,?N)->Pile_heat_exchanger_ tube_cost(?DS,? pile_tube_cost)
Rule 2	Calculating bridge deck heat exchanger tube cost: $C^{BT} = \sum_{j=1}^{n} C_{j}^{BT} \times L_{j}^{BT} \times N_{j}$ De-icing_system(?DS)has_bridge_deck(?DS, ?deck) ^Bridge_deck(?deck) ^Number(?deck, ?N)` has_bridge_deck_heat_exchanger_tube(?deck,?deck_tube)Bridge_deck_heat_exchanger_tube(?deck_tube)`Cost(? deck_tube,?cost) ^ Length(?deck_tube, ?L) ^ swrlb:multiply(?deck_tube_cost, ?N, ?L, ?cost) -> Bridge_deck_heat_exchanger_tube_cost(?DS, ?deck_tube_cost)
Rule 3	Calculating pump cost: C ^P = ∑ _{k=1} ^m C ^P _k × N ^P _k ⊕ De-icing_system(?DS) ^ has_pump(?DS, ?pump) ^ Pump_type(?pump) ^ Cost(?pump, ?cost) ^ Number(?pump, ?N) ^ swrlb multiply(?pump_cost, ?cost, ?N) -> Pump_cost(?DS, ?pump_cost)
Rule 4	Calculating total cost: $C^{E} = C^{PT} + C^{BT} + C^{P}$ De-icing_system(?DS)Pile_heat_exchanger_tube_cost(?DS,?pile_tube_cost)Bridge_deck_heat_exchanger_tube_cost(?DS,?deck_tube_cost)Pump_cost(?DS,?pump_cost)swrlb:add(?total_cost, ?pile_tube_cost, ?deck_tube_cost, ?pump_cost) -> Total_cost(?DS, ?total_cost)

TABLE 5 SWRL rules to calculate h	heat flux.
Rule 1	Calculating the heat transferred by the energy pile: $Q_{\text{source}} = \sum_{i=1}^{n} q_i^{\text{pile}} \times L_i^{\text{pile}} \times N_i$
	De-icing_system(?DS)`has_pile(?DS, ?pile)^Pile(?pile)^Length(?pile, ?L)^Number(?pile, ?N)^q_pile(?pile, ?p_q)^swrlb:
	multiply(?Qs, ?p_q, ?L, ?N) -> Qsource(?DS, ?Qs)
Rule 2	Calculating the heat provided by heat pump: $Q_{heat} = \frac{OOP}{(OP-1)} \times Q_{source}$
	De-icing_system(?DS)has_pump(?DS, ?pump)^Pump_type(?pump)^COP(?pump, ?cop)^swrlb:subtract(?x, ?cop, 1)^
	swrlb:divide(?y, ?cop, ?x)^Qsource(?DS, ?Qs)^swrlb:multiply(?Qh, ?y, ?Qs) -> Qheat(?DS, ?Qh)
Rule 3	Calculating the area heated by the system: $A_{\text{heat}} = \sum_{i=1}^{n} a_i^{\text{heat}} \times N_i$
	De-icing_system(?DS)has_bridge_deck(?DS, ?deck)^Bridge_deck(?deck)^a_heated(?deck, ?a)^Number(?deck, ?N)^swrlb:
	multiply(?A, ?a, ?N) -> A_heated(?DS, ?A)
Rule 4	Calculating the heat flux without heat pump: $q = \frac{Q_{source}}{A}$
	De-icing_system(?DS)^Qsource(?DS, ?Qs)^A_heated(?DS, ?A)^swrlb:divide(?q_c, ?Qs, ?A) -> q(?DS, ?q_c)
Rule 5	Calculating the heat flux with heat pump: $q_{pump} = \frac{Q_{point}}{A_{pump}}$
	De-icing_system(?DS) ^ Qheat(?DS, ?Qh) ^ A_heated(?DS, ?A) ^ swrlb:divide(?q_p, ?Qh, ?A) -> q_pump(?DS, ?q_p)

TABLE 6 SWRL rules for ev	valuation.
Rule 1	Evaluation: good De-icing_system(?DS)q(?DS,?q_c)q0(?DS,?q_0)swrlb:greaterThanOrEqual(?q_c, ?q_0) -> Evaluation(?DS, "good")
Rule 2	Evaluation: feasible De-icing_system(?DS)q(?DS,?q_c)q0(?DS,?q_0)q_pump(?DS,?q_p)swrlb:lessThan (?q_c, ?q_0)^swrlb: greaterThanOrEqual(?q_p, ?q_0) -> Evaluation(?DS, "feasible")
Rule 3	Evaluation: not feasible De-icing_system(?DS) ^q_pump(?DS, ?q_p) ^q0(?DS, ?q_0) ^swrlb:greaterThan(?q_0, ?q_p) -> Evaluation(?DS, "not_feasible")

 TABLE 7 | SQWRL rules to query total cost, bearing capacity, q0, qpump, and evaluation.

SQWRL

De-icing_system(?DS) ^Total_cost(?DS, ?total_cost) ^Q(?DS, ?bearing_capacity) q0(?DS,?q_0)q(?DS,?q_)q_pump(?DS,? q_heat_pump)Evaluation(?DS,?evaluation) has_pump(?DS,?pump_type)->sqwrl:select(?DS,?total_cost,? bearing_capacity, ?pump_type,?q_0,?q_,?q_heat_pump,?evaluation)

g system(2DS) ^ Total g_system(2DS) ^ has_g g_system(2DS) ^ dchas g_system(2DS) ^ dchas g_system(2DS) ^ d(2DS)	cost(705, rtotal v lid(705, rtotal v lid(705, rpile) ~ 6 Q1 selec value valu	t all the relevant informati t system(7DS) ^ Total_cost(q(7DS, ?c_) ^ q_pump(2DS norDS, ?c_pump tue) > s	ion ?DS, ?total_cost) / ; ?q_heat_pump)	Q(?DS, ?be	aring_capacity) ^ q0(?DS,	Evaluation(? nger_tube(? k, ?deck_tub , ?cost, ?N) ump_cost(?D ;multiply(?Q0 ?L, ?N) -> Ahe ?x) -> A_he ?x) ^ Osour	Pile_heat_ex Bridge_deck Pump_cost-t Total_cost-tl Q-the total Qsource- th A_heated-th Obeat_calcu	cahnger_tube c_heat_exchan he pump cos he total cost pearing capar e total heat e e total area h	_cost-the co ger_tube_co t :ity xtrated by p eated by th	ost ost
g_system(?DS) ^ has_g g_system(?DS) ^ Qtea g_system(?DS) ^ Qtea g_system(?DS) ^ Q(?D3 g_system(?DS) ^ q(?D3 g_system(?DS) ^ q(?D3 g_system(?DS) ^ q(?D3)	sile(7DS, 7pile) ^ c [Q1 select pridge_deck(7DS, pump(7DS, 7pump neat_exchanger_tu pile(7DS, 7pile) ^ c [Ok pridge_deck(7DS, pump(7DS, 7pump (7DS, 7puh) ^ A [rcce(7DS, 7Qs) ^ A [s. 2p_c) ^ a (2p_c) ? a [, 0, 0] rcce(7DS, 7Qs) ^ A [s. 2p_c) ^ a (2p_c) ? a [, 0, 0] rcce(7DS, 7Qs) ^ A [s. 2p_c) ^ a (2p_c) ? a [, 0, 0] rcce(7DS, 7Qs) ^ A [s. 2p_c) ^ a (2p_c) ? a [, 0, 0] rcce(7DS, 7Qs) ^ A [s. 2p_c) ^ a (2p_c) ? a [, 0, 0] rcce(7DS, 7Qs) ^ A [s. 2p_c) ^ a (2p_c) ? a [, 0, 0] rcce(7DS, 7Qs) ^ A [s. 2p_c) ^ a (2p_c) ? a [, 0, 0] rcce(7DS, 7Qs) ^ A [s. 2p_c) ^ a (2p_c) ? a [, 0, 0] rcce(7DS, 7Qs) ^ A [s. 2p_c) ^ a (2p_c) ? a [, 0, 0] rcce(7DS, 7Qs) ^ A [s. 2p_c) ^ a (2p_c) ? a [s. 2p_c) ? a [s. 2p_c) ? a (2p_c) ? a [s. 2p_c) ? a [s. 2p_c) ? a (2p_c) ? a [s. 2p_c) ? a [s. 2p_c) ? a (2p_c) ? a [s. 2p_c) ? a [s. 2	t all the relevant informati it system(?DS) ^ Total_cost(q(?DS, ?q_) ^ q_pump(?DS) nc?DS. ?oump type) -> sc	DS, ?total_cost) '	Q(?DS, ?be	aring_capacity) ^ q0(?DS,	inger_tube(? ;k, ?deck_tub , ?cost, ?N) ump_cost(?D ;multiply(?Q0 ?L, ?N) -> Ahe ?X) -> A_he ?X) ^ Osour	Pile_heat_ex Bridge_decl Pump_cost-1 Total_cost-tl Q-the total Qsource- th A_heated-th Oheat-calcu	cahnger_tube cheat_exchan the pump cos the total cost bearing capate e total heat e e total area h	_cost-the co ger_tube_co t :ity xtrated by p eated by th	ost ost oiles
g_system(?DS) ^ has_b g_system(?DS) ^ has_p g_system(?DS) ^ has_p g_system(?DS) ^ has_p g_system(?DS) ^ has_b g_system(?DS) ^ has_b g_system(?DS) ^ ohea g_system(?DS) ^ oheaa	oridge_deck(?DS, poump(?DS, ?pump leat_exchanger_tu status pile(?DS, ?pile) ^ f ok poindge_deck(?DS, poump(?DS, ?pump ?q_0) ^ f mrce(?DS, ?dS) ^ A s 2 a v A ourpois ? a 0, ?a	system(?DS) ^ Total_cost(q(?DS, ?q_) ^ q_pump(?DS pa(?DS, ?cump type) -> sc	?DS, ?total_cost) / , ?q_heat_pump)	Q(?DS, ?be	aring_capacity) ^ q0(?DS,	:k, ?deck_tub , ?cost, ?N) ump_cost(?D :multiply(?Q0 ?L, ?N) -> Q ?N) -> A_he ?x) ^ Qsour	Bridge_decl Pump_cost- Total_cost-tl Q-the total I Qsource- th A_heated-th Obeat-calcu	c_heat_exchan he pump cos he total cost bearing capa e total heat e e total area h	ger_tube_co t city xtrated by p eated by th	ost oiles
g_system(?DS) ^ has_p g_system(?DS) ^ Pile_f g_system(?DS) ^ has_p g_system(?DS) ^ has_p g_system(?DS) ^ has_p g_system(?DS) ^ has_p g_system(?DS) ^ Qhoa g_system(?DS) ^ Qcou g_system(?DS) ^ q(?DS g_system(?DS) ^ q(?DS)	sump(2DS, 2pump lieat exchanger tu sile(2DS, 2pile) ^ f Sile(2DS, 2pile) ^ f Ok Deicing_ ump(2DS, 2pump tt(2DS, 2Qh) ^ A h thrcre(2DS, 2Qs) ^ A S 2 a ch & 00205 C 4 0, 24	system(?DS) ^ Total_cost(q(?DS, ?q_) ^ q_pump(?DS pp(?DS, ?qump_type) -> sc	?DS, ?total_cost) / , ?q_heat_pump)	Q(?DS, ?be	aring_capacity) ^ q0(?DS,	, ?cost, ?N) ump_cost(?D :multiply(?Q0 ?L, ?N) -> Q ?N) -> A_he ?x) ^ Qsour	Pump_cost- Total_cost-ti Q-the total I Qsource- th A_heated-th Obeat-calcu	he pump cos ne total cost pearing capa e total heat e e total area h	t city xtrated by p eated by th	piles
g_system(?DS) ^ hig_f g_system(?DS) ^ has_r g_system(?DS) ^ has_r g_system(?DS) ^ has_r g_system(?DS) ^ has_r g_system(?DS) ^ Qsou g_system(?DS) ^ q(?D g_system(?DS) ^ q(?D g_system(?DS) ^ q(?D	teat_exchanger tu Status bile(?DS, ?pile) ^ F Ok oridge_deck(?DS, Deicing. pump(?DS, ?pump Deicing. tt(?DS, ?Qh) ^ A h ?q_0) ^ trcre(?DS, ?Qs) ^ A h As_pun ?q_0, ?q ?q_0, ?q	system(?DS) ^ Total_cost(q(?DS, ?q_) ^ q_pump(?DS pp(?DS, ?pump type) -> sc	?DS, ?total_cost) / ; ?q_heat_pump)	Q(?DS, ?be	aring_capacity) ^ q0(?DS,	ump_cost(?D :multiply(?Q0 ?L, ?N) -> Q ?N) -> A_he ?x) ^ Qsour	Q-the total I Qsource- th A heated-th	ne total cost bearing capa e total heat e e total area h	tity xtrated by p eated by th	piles
g_system(?DS) ^ has_g g_system(?DS) ^ has_g g_system(?DS) ^ has_g g_system(?DS) ^ has_g g_system(?DS) ^ Qoou g_system(?DS) ^ Q(?DS) g_system(?DS) ^ Q(?DS) ^ Q(SS) ^ Q(SS	sile(7DS, ?pile) ^ f sile(?DS, ?pile) ^ f sump(?DS, ?pile) ^ f sump(?DS, ?pump t(?DS, ?Qh) ^ A h hrcre(7DS, ?Qs) ^ A s 2 o c) ^ an(?DS ?q 0) ?q	system(?DS) ^ Total_cost(q(?DS, ?q_) ^ q_pump(?DS pp(?DS, ?pump type) -> sc	?DS, ?total_cost) ?), ?q_heat_pump)	Q(?DS, ?be	ering_capacity) ^ q0(?DS,	:multiply(?Q0 ?L, ?N) -> Q ?N) -> A_he ?x) ^ Osour	Q-the total Qsource- th A_heated-th Obeat-calcu	e total heat e e total area h	tity strated by p eated by th	piles
g_system(?DS) ^ has_p g_system(?DS) ^ has_b g_system(?DS) ^ has_p g_system(?DS) ^ Qhea g_system(?DS) ^ Qsou g_system(?DS) ^ q(?D3 g_system(?DS) ^ q(?D3	bile(?DS, ?pile) ^ F pridge_deck(?DS, pump(?DS, ?pump tt(?DS, ?Qh) ^ A h price(?DS, ?Qs) ^ A \$ 2a,c) ^ pt(?DS, ?Qs) ^ pt(?Qs) ^ pt(?DS, ?Qs) ^ pt(?Qs) ^ p	system(?DS) ^ Total_cost(q(?DS, ?q_) ^ q_pump(?DS 10(?DS, ?pump type) -> sc	?DS, ?total_cost) * `, ?q_heat_pump)	Q(?DS, ?be	aring_capacity) ^ q0(?DS,	?L, ?N) -> Q ?N) -> A_he ?x) ^ Osour	Qsource- th A_heated-th Obeat-calcu	e total heat e e total area h	xtrated by eated by th	piles
g_system(?DS) ^ has_b g_system(?DS) ^ has_p g_system(?DS) ^ Qhea g_system(?DS) ^ Qsou g_system(?DS) ^ q(?DS) g_system(?DS) ^ q(?DS)	bridge_deck(?DS, pump(?DS, ?pump rt(?DS, ?Qh) ^ A_h has_pun s 2a c) ∧ a(2DS) ?q_0) ^ has_pun ?q_0, ?g	system(?DS) ^ Total_cost(q(?DS, ?q_) ^ q_pump(?DS pp(?DS, ?pump type) -> sc	?DS, ?total_cost) ' ;, ?q_heat_pump)	Q(?DS, ?be	earing_capacity) ^ q0(?DS,	?N) -> A_he ?x) ^ Osour	A_heated-th	e total area h	eated by th	0.0
g_system(?DS) ^ has_p g_system(?DS) ^ Qhea g_system(?DS) ^ Qsou g_system(?DS) ^ q(?DS g_system(?DS) ^ q(?DS)	bump(?DS, ?pump tt(?DS, ?Qh) ^ A h trrce(?DS, ?Qs) ^ A s 2a c) ^ a0(2Ds) ?q 0, ?q	q(?DS, ?q_) ^ q_pump(?DS pp(?DS, ?pump type) -> sc	; ?q_heat_pump)	^ Evaluation	earing_capacity) qu(rD3,	(2x) ^ Osour	Oheat-calcu			A
g_system(?DS) ^ Qhea g_system(?DS) ^ Qsou g_system(?DS) ^ q(?D g_system(?DS) ^ q(?D	tt(?DS, ?Qh) ^ A H rq_0) ** irce(?DS, ?Qs) ^ A has_pun S 2a c) ^ a0(2DS ?q 0, ?q	$q(rDS, rq) \sim q_pump(rDS)$ p(rDS, rpump type) -> sc	s, (q_neat_pump)	··· evaluation			Queue cuica	lated by the G	OP and Qs	our
g_system(?DS) ^ Qsou g_system(?DS) ^ q(?DS g_system(?DS) ^ q(?DS	rce(?DS, ?Qs) ^ A nas_pun	npl/US. (pump type) -> sc	I I WARD ON	- I all	(rDS, revaluation)		q_pump			
g_system(?DS) ^ q(?DS g_system(?DS) ^ q(?DS	$(2q, q) \land q0(2pc) ?q 0, ?q$	prove and prove and prove and	wri:select(/DS, /t	stal_cost, ?b	earing_capacity, ?pump_type,		q			
g_system(?DS) ^ q(?DS	3, rq_c) qu(rD3, = .	_, ?q_heat_pump, ?evaluati	on)				good-q>q0			
	S, ?q_c) ^ q0(?DS,					-> Evaluatio	feasible-qpi	mp>q0>q		-
a system(?DS) ^ a pui	mp(?DS. ?a p) ^ <						not feasible			
	,							New Edit	Clone	Delet
lect all the relevant inf	ormation		Cancel	Ok						
total_cost	bearing_capacity	pump_type		q_0	q_	q_h	eat_pump		evaluation	
.0*^^xsd:float	"62000.0"^^xsd:float	:circulating_pump	"80.0"^^xse	d:float	"70.0"^^xsd:float	"105.0"^^xs	d:float	feasible		
.0*^^xsd:float	"64300.0"^^xsd:float	:circulating_pump	"80.0"^^xso	d:float	"70.0"^^xsd:float	"105.0"^^xs	d:float	feasible		
.0*^^xsd:float	"64300.0"^^xsd:float	:heat_pump	"80.0"^^xso	d:float	"35.0"^^xsd:float	"52.5"^^xsc	l:float	not_feasi	ble	
.0*^^xsd:float	"64000.0"^^xsd:float	:circulating_pump	"80.0"^^xso	d:float	"40.0" ^ ^ xsd:float	"60.0"^^xsc	float	not_feasi	ble	
.0*^^xsd:float	*62500.0*^^xsd:float	:circulating_pump	*80.0*^^xs	l:float	*120.0*^^xsd:float	*180.0*^^xs	d:float	good		
.0*^^xsd:float	"62500.0"^^xsd:float	:heat_pump	"80.0"^^xso	d:float	"60.0"^^xsd:float	"90.0"^^xsc	l:float	feasible		
.0*^^xsd:float	"62000.0"^^xsd:float	:heat_pump	"80.0"^^xso	d:float	"70.0"^^xsd:float	"105.0"^^xs	d:float	feasible		
.0*^^xsd:float	"63000.0"^^xsd:float	:heat_pump	"80.0"^^xso	l:float	"50.0"^^xsd:float	"75.0"^^xsc	l:float	not_feasi	ble	
)*^^xsd:float	"65000.0"^^xsd:float	:circulating_pump	"80.0"^^xso	d:float	"60.0"^^xsd:float	"90.0"^^xsd	l:float	feasible		
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.0*^^xsd:float	"64000.0"^^xsd:float	:heat_pump	"80.0"^^xso	d:float	"40.0"^^xsd:float	*60.0*^^xsc	l:float	not_feasi	ble	
.0*^^xsd:float	"65000.0"^^xsd:float	:heat_pump	"80.0"^^xsr	d:float	"60.0"^^xsd:float	"90.0"^^xsc	l:float	feasible		
	ect all the relevant inf total_cost 0^^^stadificat 0^^^stadificat 0^^stadificat 0^^stadificat 0^^stadificat 0^^stadificat 0^^stadificat 0^^stadificat 0^^stadificat 0^^stadificat	ect all the relevant information total_cost bearing_capacity 0^^Axsdificat *6200.01^^Axsdificat 0^^Axsdificat *64300.01^^Axsdificat 0^^Axsdificat *64300.01^^Axsdificat 0^^Axsdificat *64300.01^^Axsdificat 0^^Axsdificat *64300.01^^Axsdificat 0^^Axsdificat *65500.01^^Axsdificat 0^^Axsdificat *65000.01^^Axsdificat 0^^Axsdificat *65000.01^^Axsdificat 0^^Axsdificat *65000.01^^Axsdificat 0^^Axsdificat *65000.01^^Axsdificat 0^^Axsdificat *65000.01^^Axsdificat 0^^Axsdificat *65000.01^^Axsdificat 0^^Axsdificat *65000.01^^Axsdificat	ect all the relevant information total_cost bearing_capacity pump_type p*^^xxsdifloat "62000.0*^^xsdifloat scirculating_pump p*^xxsdifloat "64300.0*^^xsdifloat scirculating_pump p*^xxsdifloat "64300.0*^xsdifloat scirculating_pump p*^xxsdifloat "62500.0*^xsdifloat scirculating_pump p*^xxsdifloat "62500.0*^xsdifloat scirculating_pump p*^xxsdifloat "62500.0*^xsdifloat scirculating_pump p*^xxsdifloat "62500.0*^xsdifloat scirculating_pump p*^xxsdifloat "65000.0*^xsdifloat scirculating_pump p*^xxsdifloat "65000.0*^xsdifloat scirculating_pump p*^xxsdifloat "65000.0*^xsdifloat scirculating_pump p*^xxsdifloat "65000.0*^xsdifloat scirculating_pump p*^xxsdifloat "65000.0*^xsdifloat scirculating_pump p*^xxsdifloat "65000.0*^xsdifloat scirculating_pump	Cancel Cancel total_cost bearing_capacity pump_type 0^^^sxsdifloat *62000.0^^^sxsdifloat xirculating_pump *80.0^^^sxsdifloat 0^^sxsdifloat *64300.0^^sxsdifloat xirculating_pump *80.0^^sxsdifloat 0^^sxsdifloat *64300.0^*^sxsdifloat xirculating_pump *80.0^*^sxsdifloat 0^^sxsdifloat *64300.0^**sxdifloat xirculating_pump *80.0^*^sxsdifloat 0^**sxdifloat *64300.0^**sxdifloat xirculating_pump *80.0^*^sxsdifloat 0^**sxdifloat *62500.0^**sxdifloat xirculating_pump *80.0^*^sxsdifloat 0^**sxdifloat *62500.0^***sxdifloat theat_pump *80.0^*^sxsdifloat 0^**sxdifloat *63000.0^***sxdifloat ticrulating_pump *80.0^*^sxsdifloat 0^**sxdifloat *63000.0^***sxdifloat ticrulating_pump *80.0^*^sxsdifloat 0^**sxdifloat *63000.0^***sxdifloat ticrulating_pump *80.0^*^sxsdifloat 0^**sxdifloat *63000.0^***sxdifloat ticrulating_pump *80.0^*^*sxsdifloat 0^**sxdifloat *64000.0^***sxdifloat tierulating_pump *80.	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TABLE 8 | SQWRL rules to query total cost less than 20,000 RMB.

SQWRL

De-icing_system(?DS)^Total_cost(?DS, ?total_cost)^Q(?DS, ?bearing_capacity)^q0(?DS, ?q_0)q(?DS,?q_)q_pump(?DS,? q_heat_pump)Evaluation(?DS,?evaluation)has_pump(?DS, ?pump_type)swrlb:lessThan(?total_cost,20,000)->sqwrl: select(?DS, ?total_cost, ?bearing_capacity, ?pump_type, ?q_0, ?q_, ?q_heat_pump, ?evaluation)

Q2 select the total cost less Rule 1-1 -pile, heat exchange Rule 1-2 -bridge deck, heat Rule 1-3 pump cost Rule 3-1 the vertical bearing Rule 3-1 the vertical bearing Rule 3-1 the heat transfered Rule 3-2 the mea heated by Rule 3-3 the Qheat realise b. Rule 3-4 q. pump the heat re Rule 3-5 the heat realised b. Rule 4-2 feasible Rule 4-3 not feasible	Deiring_system(7DS) Ara Deiring_system(7DS) Ara Deiring_sys	All Cost(i) is pile(705) is	system(?DS) ^ Tot, _pump(?DS, ?q_hea sThan(?total_cost, _eeat_pump, ?evalua	al_cost(?DS, ?tot, t_pump) ^ Evalu 20000) -> sqwrl: tition)	al_cost) ^ Jation(?DS select(?DS	Q(?DS, ?beari , ?evaluation) 5, ?total_cost, ?	ng_capacit ^ has_pun ?bearing_c	y) ^ q0(?DS, ?q_0) ^ c np(?DS, ?pump_type) / apacity, ?pump_type, ?	q(?DS, ^ ?q_0,	valuation(?E valuation(?E ger_tube(?p ; ?deck_tube ?cost, ?N) -> mp_cost(?DE nultiply(?Q0, L, ?N) -> Qs 'N) -> A_hea x) ^ Qsourc	S S Pile_he b Pile_he b Pile_he Pi	at_excah _deck_h cost-the total bea ce- the to calculate p q>q0 e-qpump sible	nger_tubi eat_exchai pump coo total cost rring capa tal heat o tal area i d by the	e_cost-the nger_tube st icity extrated l neated b COP and	e cost e_cost-t by piles y the sy Qsour
				Ca	incel	Ok						New	Edit	Clone	Delete
SQWRL Queries OWL 2 RI	Q2 select the total cost le	ess than 20000 RMB						- E		1					
DS	total_cost	bearing_c	apacity	pump_type		q_0		q_		d_P	eat_pump		e	valuation	
DS-lane-parallel_2_U	"10840.0"^^xsd:float	*64300.0*^^xsd	float :circul	ating_pump	*8	0.0"^^xsd:floa	it	"70.0"^^xsd:float		"105.0"^^x	sd:float	fe	asible		
DS-integral-3_U	"15400.0"^^xsd:float	*63000.0*^^xsd	float :circul	ating_pump	*8	0.0"^^xsd:floa	t	*50.0*^^xsd:float	_	*75.0*^^xs	d:float	n	ot_teasibl	e	_
DS-lane-5_U	18040.0*^^xsd:float	"62500.0"^^xsd	float :circul	ating_pump	*8	0.0*^^xsdifloa	it	120.0*^^xsd:float		180.0*^^x	sdifloat	g	ood		
DS-lane-single_U	"8440.0"^^xsd:float	"65000.0"^^xsd	float :circul	ating_pump	*8	0.0"^^xsd:floa	it	"60.0"^^xsd:float		"90.0"^^xs	d:float	te	asible		
DS-integral-Series_2_U	"13000.0"^^xsd:float	*64000.0*^^xsd	float :circul	ating_pump	*8	0.0"^^xsd:floa	it	"40.0"^^xsd:float		*60.0*^^xs	d:float	n	ot_feasibl	e	
			Save as CSV		Rerun		с	lose	No Reason	erset. Selecta	reasoner from	the Reaso	ner menu	Show Ir	nferences
URE 12 Executio	on and results of q	uerying Table	8.					P	vo rteason	er set. Gelect a	easoner from	the Reaso	nermenu	• Show in	nerences

transfer tubes will be embedded under the 12 pieces of bridge deck under car lanes. The bridge deck under the bicycle lanes or the sidewalk will not be heated by thermal tubes. Considering the heated area and the volume of circulating water, COP is set to 3, according to Self et al. (2013). Based on several different types of heat exchangers and heat pumps, 12 design solutions are offered by OntoBDDS. The details of each design solution are presented in **Table 2**.

Thereafter, OntoBDDS can generate new facts based on the ontology model and the 12 aforementioned designing solutions. The

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This section demonstrates how engineers can use OntoBDDS to perform inquiry designing solutions of bridge deck deicing system in accordance with specified requirements. The inquires can be conducted through inputting SQWRL commands in the SQWRLTab. For example, the total cost, bearing capacity, and heat flux can be obtained by the command shown in Table 7 and the querying results are illustrated in Figure 11. Engineers can compare each design and make preliminary decisions.

Specialized design requirements can also be easily satisfied by SQWRL querying. Table 8 shows the SQWRL querying command to filter design results with a total cost below 20,000 RMB. The querying results are illustrated in Figure 12. It can be seen that five designs satisfy this requirement and only three are graded as feasible.

Figure 13 illustrates the running results of Table 9, which aims to find design solutions with bearing capacity larger than 62,000 kN. It is shown that ten solutions are satisfying this requirement. Furthermore, the bearing capacities of all those filtered design solutions are of the same order of magnitude, which implies that the OntoBDDS can provide reasonable design solutions.

Hear flux and cost are also two major indicators of the deicing system. Table 10 demonstrates the SQWRL command to filter design solutions of a cost less than 20,000 RMB and acceptable heat flux. The querying results are illustrated in Figure 14. It can be seen that there are three acceptable design solutions. The solution with heat pump and 5-U type heat

SQWRL	De-icing_system(?DS)To

tal_cost(?DS,?total_cost)`Q(?DS,?bearing_capacity)`q0(?DS,?q_0)` q(?DS,?q_)`q_pump(?DS,? q_heat_pump)Evaluation(?DS,?evaluation)has_pump(?DS, ?pump_type)swrlb:greaterThan(?bearing_capacity,62000)->sqwrl:select(?DS, ?total_cost, ?bearing_capacity, ?pump_type, ?q_0, ?q_, ?q_heat_pump, ?evaluation)

FABLE 10 SQWRL rules to query feasible design solutions whose total cost is less than 20,000 RMB.							
SQWRL	De-icing_system(?DS) [*] Total_cost(?DS, ?total_cost) [*] Q(?DS, ?bearing_capacity) [*] q0(?DS, ?q_0) [*] q(?DS, ?q_) [*] q_pump(?DS, ?q_heat_pump) [*] Evaluation(?DS, ?evaluation) has_pump(?DS,?pump_type) [*] swrlb:lessThan(?total_cost,20,000) [*] swrlb: greaterThan (?q_heat_pump,?q_0)->sqwrl:select(?DS, ?total_cost, ?bearing_capacity, ?pump_type, ?q_0, ?q_, ? q_heat_pump,?evaluation)						

facts include the cost, heat flux, and bearing capacity among other features of each design solution. Figure 10 demonstrates the interface after running the ontology model and reasoning rules. The reasoning rules are also presented from Table 3-6. Thereafter, engineers can use a plug-in called SQWRLQueryTAB to inquire the generated facts and make a comparison of each design solution.

Application

Name		Q3 select the be	aring capacity greater t	han 62000kN			Comment
Name Of salest all the sales at inf	Delete enter (2DC) A T	Comment				hat a conc	Comment
Q1 select all the relevant int.	Delcing_system(2DC) A To	otal_cost(/				luation(?DS,	
Q2 select the total cost less	Delcing_system(7DS) A To	otal_cost(/)				luation(?DS,	
QS select the bearing capa	Delcing_system(2DS) A ha	s sile(2D2				s tube(2pile_Dile	heat avealancer tube cost the cost
Rule1 2 bridge deals best	Delcing_system(205) A ha	ok Ok				deals tube) Rei	heat excannger_tube_cost-tube cost
Rule1-2-bridge_deck_neat	Delcing_system(2DS) A ha	Deicing system(2DS) A Total cost(2DS 2	total cost) ^ O(2DS 2bea	ing capacity) A g0(2DS 2g 0) A g(2D	C bet 2ND b Due	age_deck_near_exchanger_tube_cost-
Rule1-3 pump cost	Delcing_system(2DS) A Pi	la heat and 2a) A a pump(2	DC 2a heat sump) A E	valuation (2DC 2 avaluation	A has sump(2DC 2sump type) A	s, pst, (N) - F Pur	al sest the total sest
Puls 2.1 the vertical bearing	Delcing_system(2DS) A ha	ne nila(2Dd nullhar nila)	(DS, rq_neat_pump) ~ E	valuation(PDS, revaluation	has_pump(rbs, rpump_type)	tink(200.2. 0.1	he total bearing conscitu
Rule2-1 the best transfored	Delcing_system(205) A ha	splie(2D) swrib:greater ina	an(?bearing_capacity, 62	.000) -> sqwn:select(/DS,	rtotal_cost, rbearing_capacity, rpump	type, upiy(rQ0, r Qr	ne total bearing capacity
Pulse 2 the area heated by	Delcing_system(205) A ha	s bridge	at_pump, ?evaluation)			A heata A h	parted the total area beated by the
Rule3-2 the Obest realise b	Deicing_system(2DS) ^ ha	s pump(2)				A Ocource(Oh	est-calculated by the COP and Ocour
Rule3-4 a nump the heat re	Deicing_system(2DS) ^ (12	heat(2DS 1				Qsource(Qri	sump
Rule3-5 the heat realised b	Deicing_system(2DS) ^ O	source(2D)				4.5	amp
Rule4-1 good	Deicing system(2DS) ^ g	205 20 0				4	od-a>a0
Rule4-2 feasible	Deicing_system(2DS) ^ q(2DS 20 c)				Evaluation/2 fea	sible-apump > a0 > a
Rule4-3 not feasible	Deicing_system(2DS) ^ g	numn(2D9				Evaluation(: rea	feasible
Naie 4 5 Not reasible	Deleting_system(:DS) q	pumptios		Cancel Ok		100	
							New Edit Clone Dele
SQ/WRL Queries O/WL 2 RL	Q3 select the bearing ca	pacity greater than 62000kN	1				
DS	total_cost	bearing_capacity	pump_typ	e q_	0 q_	q_heat_pur	np evaluation
DS-lane-parallel_2_U	*10840.0*^^xsd:float	*64300.0*^^xsd:float	:circulating_pump	*80.0*^^xsd:flo	at "70.0"^^xsd:float	"105.0"^^xsd:float	feasible
DS-integral-3_U	*15400.0*^^xsd:float	*63000.0*^^xsd:float	:circulating_pump	*80.0*^^xsd:flo	at "50.0"^^xsd:float	*75.0*^^xsd:float	not_feasible
DS-integral-parallel_2_U-h	*26200.0*^^xsd:float	*64300.0*^^xsd:float	:heat_pump	"80.0"^^xsd:flo	at "35.0"^^xsd:float	"52.5"^^xsd:float	not feasible
DS-integral-3_U-heat_pump	*28600.0*^^xsd:float	*63000.0*^^xsd:float	:heat_pump	"80.0"^^xsd:flo	at "50.0"^^xsd:float	"75.0"^^xsd:float	not feasible
DS-lane-5_U	"18040.0"^^xsd:float	"62500.0"^^xsd:float	:circulating_pump	"80.0"^^xsd:flo	at "120.0"^^xsd:float	"180.0"^^xsd:float	good
DS-lane-single_U-heat_pu	*21640.0*^^xsd:float	*65000.0*^^xsd:float	:heat_pump	"80.0"^^xsd:flo	at "60.0"^^xsd:float	"90.0"^^xsd:float	feasible
DS-integral-5_U-heat_pump	*33400.0*^^xsd:float	*62500.0*^^xsd:float	:heat_pump	"80.0"^^xsd:flo	at "60.0"^^xsd:float	*90.0*^^xsd:float	feasible
DS-lane-single_U	"8440.0"^^xsd:float	"65000.0"^^xsd:float	:circulating_pump	"80.0"^^xsd:flo	at "60.0"^^xsd:float	"90.0"^^xsd:float	feasible
DS-integral-Series_2_U-he	*26200.0*^^xsd:float	"64000.0"^^xsd:float	:heat_pump	"80.0"^^xsd:flo	at "40.0"^^xsd:float	"60.0"^^xsd:float	not_feasible
DS-integral-Series_2_U	"13000.0"^^xsd:float	"64000.0"^^xsd:float	:circulating_pump	"80.0"^^xsd:flo	at "40.0"^^xsd:float	"60.0"^^xsd:float	not_feasible
		Sa	ave as CSV	Rerun	Close		

TABLE 9 | SQWRL rules to query bearing capacity greater than 62,000 kN.

FIGURE 13 | Execution and results of querying Table 9.

Intitled-ontolo	gy-19 (http://www.semantic	cweb.org/lichaoji/on	tologies/2019/4/untitled-ontology	(-19)			 Search 	
Active Ontology × Entities	× Classes × Object Pro	operties × Data Pr	operties × Individuals by class	× DL Query × SWRLTab	× OntoGraf × SQWRLTab ×			
Name		🔬 Edit	🛃 Edit				Comment	
21 select all the relevant inf.	Deicing_system(?DS) ^ To	eicing_system(?DS) ^ Total_cost(?D						
12 select the total cost less.	. Deicing_system(?DS) ^ To	ystem(?DS) ^ Total_cost(?D_Name						
13 select the bearing capa	Deicing_system(?DS) ^ Total_cost(?D_Q5 select feasible design solutions whose cost less than 20000 RMB					^ Evaluation(?DS,		
4 select the feasible desig.	Deicing_system(7DS) ^ Total_cost(7D) Comment					Evaluation(?DS,		
25 select feasible design s	Deicing_system(?DS) ^ To	otal_cost(?L			 A Evaluation(?DS,) 			
ule I - I - pile_heat_exchange.	Deicing_system(?DS) ^ has_pile(?DS)					<pre>changer_tube(?pile Pile_heat_excahnger_tube_cost-the cost .</pre>		
ule1-2-bridge_deck_heat	Deicing_system(?DS) ^ has_bridge_d Status							
lule1-3 pump cost	Dercing_system(7DS) ^ has_pump(7D							
ule1-4 total cost	Deicing_system(?DS) ^ Pi	le heat exc					Pump_cost(?DS, Total_cost-the total cost	
ule2-1 the vertical bearing.	. Deicing_system(?DS) ^ ha	as_pile(?DS, Deicing	system(?DS) ^ Total_cost(?DS, ?t	otal_cost) ^ Q(?DS, ?bearin	rib:multiply(?QU, ? Q-the total bearing capacity			
ule3-1 the heat transfered.	. Deicing_system(?DS) ^ ha	as_pile(?DS, q(?DS,	'q_) ^ q_pump(?DS, ?q_heat_pum	p) ^ Evaluation(?DS, ?evalu	ation) ^ has_pump(?DS,	q, ?L, ?N) -> Qso Qsource-	the total heat extrated by pile	
cule3-2 the area heated by	Deicing_system(?DS) ^ ha	as_bridge_d ?pump	type) ^ swrlb:lessThan(?total_cos	t, 20000) ^ swrlb:greaterTh	an(?q_heat_pump, ?q_0) ->	(a, (N) -> A heate A heated	-the total area heated by the s	
ule3-3 the Qheat realise b.	. Deicing_system(?DS) ^ ha	as_pump(/L sqwrl:se	lect(?DS, ?total_cost, ?bearing_ca	pacity, ?pump_type, ?q_0, ?	q_, ?q_heat_pump, ?evaluation)	p, ?x) ^ Qsource(Qheat-cal	Iculated by the COP and Qsou	
ule3-4 q_pump the heat re.	Deicing_system(?DS) ^ Q	heat(/DS, /				q_pump		
e3-5 the heat realised b Dercing_system(7DS) ^ Qsource(7DS					9			
kule4-1 good	Dering_system(7DS) $\land q(7DS, 7q_c)$							
Rule4-2 feasible	Deicing_system(7DS) ^ q(7DS, 7q_C)							
Rule4-3 not feasible	Deicing_system(?DS) ^ q	_pump(7DS,	6			not feasit	ble	
			Ca	ncei Ok			New Edit Clone Delet	
SQWRL Queries OWL 2 RL	Q5 select feasible design	n solutions whose co	st less than 20000 RMB					
DS	total_cost	bearing_ca	pacity pump_type	q_0	q_	q_heat_pump	evaluation	
DS-lane-parallel 2 U	*10840.0*^^xsd:float	*64300.0*^^xsd:	float :circulating_pump	*80.0*^^xsd:float	"70.0"^^xsd:float	*105.0*^^xsd:float	feasible	
DS-lane-5_U	"18040.0"^^xsd:float	"62500.0"^^xsd:	float :circulating_pump	"80.0"^^xsd:float	"120.0"^^xsd:float	"180.0"^^xsd:float	good	
DS-lane-single U	"8440.0"^^xsd:float	"65000.0"^^xsd:	float :circulating pump	"80.0"^^xsd:float	"60.0"^^xsd:float	"90.0"^^xsd:float	feasible	
			Save as CSV	Rerun	Close			

transfer tube offers the least cost and highest heat flux and therefore is the optimal solution.

CONCLUSION AND FUTURE WORK

Based on the ontology modeling method and the SWRL language, this paper establishes an integrated design system for energy pile bridge deck deicing systems. The OntoBDDS system is developed and provides designers with a simple and easy-to-use optimization design tool. The system provides designers with indicators on the economy, heat flux, and safety aspects of the design plan, so that the designer can choose and optimize the plan.

At the same time, this article uses a design example to demonstrate how engineers should use this system to optimize the design of the energy pile bridge deck deicing system when considering different design requirements. The example also shows the feasibility of the system. This ontology model is also developed based on the IFC standard and an existing, verified ontology model. The correctness of its semantics, grammar, and rules have also been verified. At the same time, the example shows how the system can be used when focusing on different design priorities, such as cost, safety, and heat flux to achieve the optimal system configuration and satisfy engineering requirements.

The concept of using OntoBDDS tools and an ontology framework as illustrated in this article can also be applied to other energy pile projects, such as energy tunnels, integrated design of building energy pile systems, etc. In future work, this ontology-based integrated design concept can be extended to all aspects of engineering, and further efforts will be placed on developing knowledge acquisition methods involving more semantic explication (such as during cross-disciplinary interaction in a large-scale numerical analysis). Further development in this area can help basic or cross-domain reasoning in practical scenarios.

DATA AVAILABILITY STATEMENT

The data used to support the findings of this study are available from the corresponding author upon request.

AUTHOR CONTRIBUTIONS

PZ, CC, CL, and CZ conceived and designed the research work. PZ, CL, and HL analyzed the data. PZ, CL, and HL prepared original draft. CC and CZ reviewed and edited the paper. All authors contributed to the article and approved the submitted version.

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