



Zeolite-Loaded Titanium Dioxide Photocatalytic Cement-Based Materials for Efficient Degradation of Drinking Water Disinfection Byproduct Trichloroacetamide

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A two-step method was used to load TiO₂ on a cement matrix, and zeolite was chosen as intermediate support. TiO₂@Zeolite composite coated photocatalytic cement-based material (PCM) was prepared. Some advanced characterization technologies including X-ray diffraction (XRD), scanning electronic microscopy (SEM), energy dispersive X-ray spectroscopy (EDS), and BET specific surface area (SSA) test were applied to characterize the physicochemical properties of as-prepared PCM. Photocatalytic degradation of trichloroacetamide (TCACAm) was conducted to evaluate its photocatalytic efficiency. Results show that TiO₂@Zeolite composite can improve the adsorption ability of PCM and TiO₂ particles were dispersed on the surface of PCM homogeneously providing abundant active sites for photocatalytic reactions. Moreover, TiO₂@Zeolite composite can reduce the negative effect of cement on TiO₂. The synergetic effect of TiO₂@Zeolite composite can remarkably improve the photocatalytic degradation rate, reaching up to 97.8%. TiO₂@Zeolite composite coated PCM holds great promise to eliminate water pollution.

Keywords: TiO₂@Zeolite composite, photocatalytic cement-based material, water purification, photocatalytic degradation, disinfection byproducts

INTRODUCTION

Nowadays, water pollution is a big environmental health concern worldwide as multiple harmful substances such as antibiotics, microbes, and dyestuffs are detected in drinking water. It is urgent to eliminate these contaminants in aqueous environments to guarantee water safety (Srogi, 2007; Ahmed et al., 2010; Zangeneh et al., 2015; Liu et al., 2017). At present, chlorine disinfection is still the main method used to disinfect tap water, since it was first applied in England in 1897, due to high disinfection efficiency, low cost, and facile implementation (Hom, 1972; Winward et al., 2008). However, some carbon-disinfection by-products (C-DBPs) will be generated in the disinfection process, which can induce many diseases like cancer (Chu et al., 2012; Chang et al., 2013). Recently, some new disinfectors such as chloramine and ozone have been developed, but

the derived nitrogen-disinfection by-products (N-DBPs) are proved to be more toxic than C-DBPs (Chu et al., 2012). Moreover, tap water is usually transported over a long distance through water supply pipes, and then stored in concrete-made water storage structures before being delivered to households, and as a result N-DBPs will concentrate and bacteria will breed fast at the end of the network (Whelton et al., 2015). Consequently, a novel strategy should be proposed to deal with these emerging challenges.

Since Fujishima and Honda found the splitting of water on a TiO₂ anode under illumination, TiO₂ has been widely studied and used in environment remediation owing to its strong photo-induced oxidation ability (Fujishima and Honda, 1972; Vinu and Madras, 2012; Wen et al., 2015; Pawar et al., 2018). In detail, active oxygen species (AOS) generated on TiO₂ like hydroxyl radical ($\cdot\text{OH}$) can totally oxidize pollutants into water and carbon dioxide upon solar irradiation. Previous research has proved that heterogeneous photocatalysis exhibits specific superiority in eliminating aqueous pollutants in terms of low cost and harmless byproducts, when compared to conventional disinfection (Yoneyama and Torimoto, 2000; Karuppuchamy et al., 2007; Fuchs et al., 2009; Yamaguchi et al., 2010). Some pioneering works about using TiO₂ to purify water have been reported, which show high degradation efficiency toward pollutants. However, in most reported cases, TiO₂ has been employed in the form of nano-powder which is prone to agglomerate in aqueous environments due to its high surface energy, thus compromising its photocatalytic efficiency, and it is also difficult to recollect and reuse this powder TiO₂ (Zhang et al., 2003; Negishi et al., 2019a,b). In recent years, immobilization of TiO₂ on some support materials is promising to solve this problem, and among all support materials, cementitious material is a suitable one because of its strong binding property and chemical inertness (Chen and Poon, 2009; Jimenez-Relinque et al., 2015). So far, TiO₂-engineered photocatalytic cement-based material (PCM) has already been fabricated and applied in environment remediation such as depollution of NO_x (Seo and Yun, 2017), self-cleaning of building (Wang et al., 2014), and decomposition of volatile organic compounds (VOCs) (Aïssa et al., 2011), but few works about the application of TiO₂-incorporated PCM in water purification have been reported.

As most water storage constructions are manufactured of cement-basted materials, it is attractive to coat TiO₂ on these cement constructions to further improve drinking water quality. Although cement paste can immobilize TiO₂ particles firmly, its hydration products like C-S-H gel and Ca(OH)₂ can cover TiO₂, thus leading to a decline of photocatalytic activity (Chen et al., 2011). Due to the poor adsorption ability of cement matrix, only a small number of pollutant molecules will be captured by cement-based materials, which is not favorable for photocatalytic degradation reaction (Nazari and Riahi, 2011; Lee et al., 2013). So, it is of significance to reduce the negative effect of cement on photocatalysis for facilitating the application of TiO₂ coated PCM in water purification. In this paper, zeolite was selected as intermediate carrier, due to its high porosity and large specific surface area (SSA), and a two-step method was proposed to load TiO₂ on a cement matrix. Firstly, TiO₂ was dispersed

and anchored on the surface of zeolite, forming TiO₂@zeolite composite. And then TiO₂@zeolite composite was coated on cement paste. Degradation of trichloroacetamide (TCACAm) was conducted to evaluate the purification effect of the as-prepared TiO₂@zeolite composite coated PCM.

EXPERIMENTAL

Raw Materials

Conch brand P•O 42.5 cement was used in this study. Natural zeolite was produced in Henan province, China, and its chemical composition is shown in **Table 1**. All reagents including Tetrabutyl orthotitanate (TBOT), nitric acid (HNO₃), and absolute ethyl alcohol (CH₃CH₂OH) were provided by Sinopharm Chemical Reagent Co., Ltd., China.

Sample Preparation

TiO₂@Zeolite Composite Fabrication

Natural zeolite pre-treatment process: natural zeolite was washed by deionized water to eliminate impurities and heated in a 100°C drying oven for 1 h. Finally, treated zeolite was sieved by a standard sieve with a mesh number of 100. TiO₂ sol preparation process: 10 g TBOT was added into 80 g deionized water dropwise with continuous stirring, and 0.8 g HNO₃ was also incorporated to inhibit the fast hydrolysis of TBOT. After finishing adding TBOT, milky white suspension was obtained, and then thermotreated in a 40°C water bath for 24 h, thus gaining light blue TiO₂ sol. TiO₂ loading process: 1 g zeolite was added into a certain amount of TiO₂ sol, where TiO₂ accounts for 30% weight of zeolite. Then, the mixture was stirred for 1 h and followed with a 45-min ultrasonic treatment. Finally, the mixture was placed in a vacuum reactor with a pressure of 0.07 MPa for 5 h, and then heated in a muffle furnace for 4 h at different temperatures (200, 300, 400, and 500°C), obtaining TiO₂@zeolite composite. The specimens were labeled as n-TZ, where n stands for the final thermal treatment temperature and TZ represents TiO₂@zeolite composite, for instance, 200-TZ stands for the composite treated under 200°C. For comparison, pure TiO₂ sol was dried and heated at 200°C to obtain pure TiO₂ powder.

TiO₂@Zeolite Composite Coated PCM Fabrication

22 g cement and 8.8 g water were mixed for 5 min by a mixer, and the fresh cement paste was casted in a round mold with a diameter of 50 mm and a height of 8 mm. Before the hardening of the cement paste, a certain amount of TiO₂@zeolite composite was sprayed onto the surface of the cement paste, and demolded 1 day later. All specimens were cured in a standard curing chamber (20 ± 2°C, RH ≥ 95%) for 28 d. The samples were labeled as n-TZ-m-PCM, where n stands for the final thermal treatment temperature, m% stands for the mass ratio of

TABLE 1 | Chemical composition of natural zeolite/%.

SiO ₂	Al ₂ O ₃	Na ₂ O	CaO	MgO	Fe ₂ O ₃	FeO	TiO ₂	K ₂ O	P ₂ O ₅
60~70	17.8	4.2	2.6	0.8	1.6	1.2	0.6	3.2	0.26

TiO₂@zeolite composite to cement, TZ represents TiO₂@zeolite composite, and PCM represents PCM, for instance, 200-TZ-25-PCM represents that composite treated under 200°C was used and the composite to cement ratio was 25%. The schematic diagram of the TiO₂@zeolite composite coated PCM is shown in **Figure 1**.

Physicochemical Properties Characterization

X-ray diffraction (XRD) was used to analyze the crystal phase of as-prepared specimens, and the analysis was conducted on an X-ray diffractor equipped with a Cu K α ray source. The diffraction angle (2θ) ranged from 10° to 80° with the interval of 0.02° at the speed of 4°min⁻¹. Scanning electronic microscope (SEM) was applied to observe the micro-morphology of samples and energy dispersive X-ray spectroscopy (EDS) was adapted to investigate element distribution at a micro-area level. BET SSA test was used to characterize the pore structure of samples.

Photocatalytic Degradation Efficiency Characterization

TCAcAm solution preparation process: 0.5 g TCAcAm solid was added into 1 L deionized water and mixed evenly, and then the solution was diluted 100 times and the final concentration of TCAcAm solution was 5,000 μ g/L. Photocatalytic degradation process: the sample was suspended in a 3 L beaker, and then 1 L of TCAcAm solution with a concentration of 5,000 μ g/L was added to the beaker, and the position of the tested sample was adjusted to ensure its immersion in the TCAcAm solution. Before irradiating, the beaker containing the TCAcAm solution was placed in dark conditions for 8 h to construct the adsorption-desorption equilibrium, and then the LED lamp with a power of 12 W was switched on, and the liquid level of the solution in the beaker was 15 cm from the bottom of the light source, and 20 mL suspension was fetched at an interval of 1 h. For the control experiment, 1 L TCAcAm solution with a concentration of 5,000 μ g/L was added to a 3 L beaker, but no samples were added to the beaker. The beaker was placed in the same conditions, and 20 mL suspension was fetched at the same interval. Measurement of TCAcAm concentration: the fetched suspension was filtered and transferred into a 30 mL volumetric flask by using a large-capacity pipette. And then 20 mL TCAcAm solution and 4 mL of methyl tert-butyl ether (MTBE) extractant were added to a tube, and the mixture was vibrated for 2 min by a tube shaker and placed without stirring for 5 min. Gas chromatography-mass

spectrometry (GC/MS) was used to measure the TCAcAm in the upper extractant solution.

RESULTS AND DISCUSSION

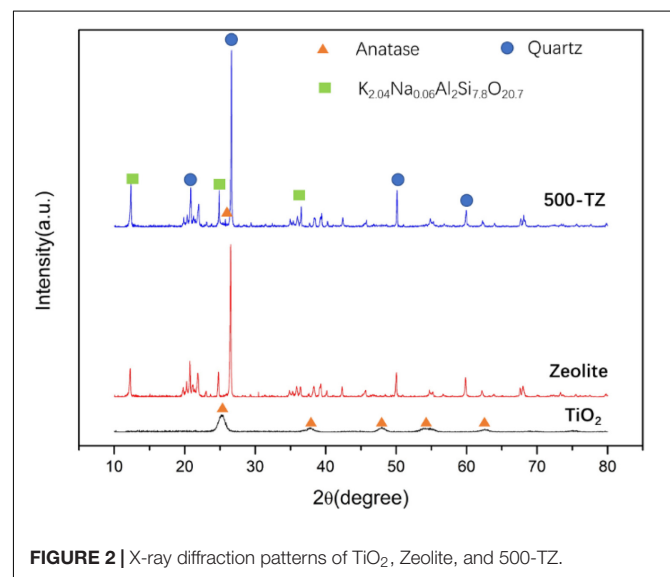
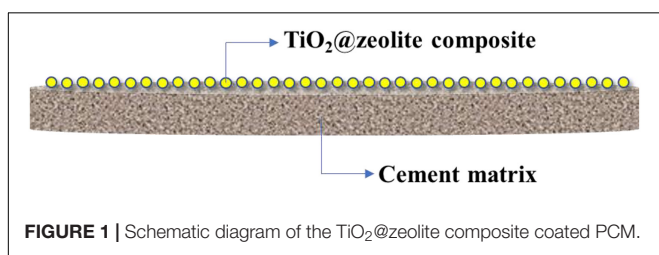
Microstructure of TiO₂@Zeolite Composite

XRD Analysis

As depicted in **Figure 2**, characteristic diffraction peaks of anatase were observed at 2θ (25.305°, 37.799°, 48.038°, 55.062°, and 62.690°) in the diffraction pattern of TiO₂ according to PDF#73-1764. This result illustrates that hydrolysis of TBOT and followed hydrothermal treatment can promote the formation of TiO₂, and TiO₂@zeolite composite based on this method will possess excellent photocatalytic activity. In the diffraction pattern of zeolite, characteristic peaks of quartz and K_{2.04}Na_{0.06}Al_{7.8}O_{20.7} were observed according to PDF#89-1629, indicating zeolite was symbiotic with quartz. For the 500-TZ sample, the main crystal phases were still quartz and K_{2.04}Na_{0.06}Al_{7.8}O_{20.7}, suggesting that thermal treatment did not destroy the structure of zeolite. After thermal treatment, the intensity of quartz and K_{2.04}Na_{0.06}Al_{7.8}O_{20.7} became stronger, indicating that its purity was improved. A weak diffraction peak was detected at 2θ (25.305°), which is the strongest diffraction peak of Anatase, confirming that TiO₂ was successfully loaded on zeolite. Due to the small amount of TiO₂ loading, only one peak of anatase was observed. And there is another possibility that because the crystalline grain size of TiO₂ was too small, the anatase diffraction intensity was weak (Jansson et al., 2015).

Micro-Morphology

As shown in **Figure 3a**, zeolite is made up of plate-like units, forming a rough surface and some micron-sized slit-like pores. This structure contributes to the capture of TiO₂ particles when immersed in TiO₂ sol, thus leading to the homogenous



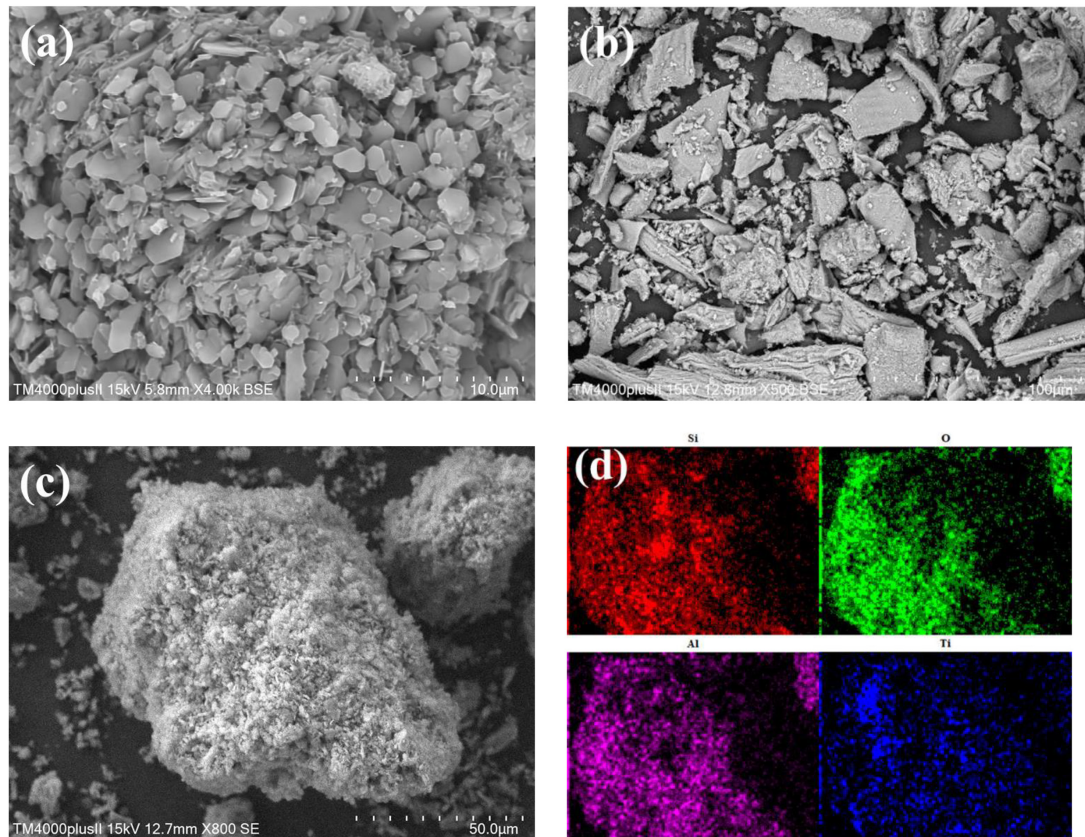


FIGURE 3 | Micro-morphology: (a) SEM of zeolite; (b) SEM of TiO₂; (c) SEM of 500-TZ; (d) elements distribution of 500-TZ.

distribution of TiO₂ particles on the surface of zeolite. **Figure 3b** depicts the morphology of pure TiO₂, after thermal treatment the nano-structure of TiO₂ is not observed and it presents a block-shape. This indicates that if nano-TiO₂ particles were not dispersed evenly and anchored firmly, they are prone to agglomerate, thus forming a densified structure and reducing its surface area. The rough surface of zeolite combined with the nano-structure of TiO₂ provides a possibility to synthesize the zeolite supported nano-TiO₂ composite (Ito et al., 2014; Maraschi et al., 2014). In **Figure 3c**, the surface of 500-TZ is coated with a flocculent layer and the edges and corners of zeolite gradually disappear after loading TiO₂, suggesting that porous TiO₂ had been mounted on the surface of zeolite. **Figure 3d** presents the primary elements distribution of TZ-500 (Si, O, Al, and Ti), Ti element is well dispersed on the surface of 500-TZ, further confirming the existence of TiO₂ and the homogeneous distribution of TiO₂. The unique structure of TZ-500 is attributed to TiO₂ modification. More specifically, in the TiO₂ sol, nano-TiO₂ particles existed stably due to the electrostatic repulsion. When heating TiO₂ sol, water was evaporated and surface charge was changed, and thus TiO₂ particles agglomerated. However, when zeolite was immersed in TiO₂ sol, the micro-nano structure of zeolite interacted with TiO₂ under the action of surface charge, nano-TiO₂ particles were fixed on the surface of zeolite, and

zeolite provided a large surface to disperse TiO₂ particles. Upon heating, water was evaporated, but TiO₂ particles will not get into agglomeration due to the anchoring of zeolite (Easwaramoorthi and Natarajan, 2009).

BET Analysis

Figure 4A displays isotherm adsorption-desorption curves of as-prepared samples. Hysteresis loops were observed in all samples, confirming the existence of mesoporous structure (Sing et al., 1985), but the shape of isotherms was different, indicating that the pore structure and surface property were altered through thermal treatment under different temperatures. At low relative pressure (<0.5), the N₂ adsorption volume of 200-TZ was approximate to that of 300-TZ and 400-TZ, but higher than that of 500-TZ. This demonstrates that the adsorption ability of 200-TZ, 300-TZ, and 400-TZ was higher than that of 500-TZ, which was also verified by the results of SSA in **Figure 4C**. In general, the higher the SSA is, the stronger the adsorption capacity is. It proves that thermal treatment can lead to an agglomeration of TiO₂, thus reducing its SSA, and the higher the temperature is, and more serious the agglomeration is. However, at high relative pressure (>0.5), the N₂ adsorption volume of 200-TZ was noticeably lower than that of 300-TZ, 400-TZ, and 500-TZ. This is probably caused by the pore size difference. As shown in **Figure 4B**, the most probable pore diameter shifted right with temperature, and 200-TZ had

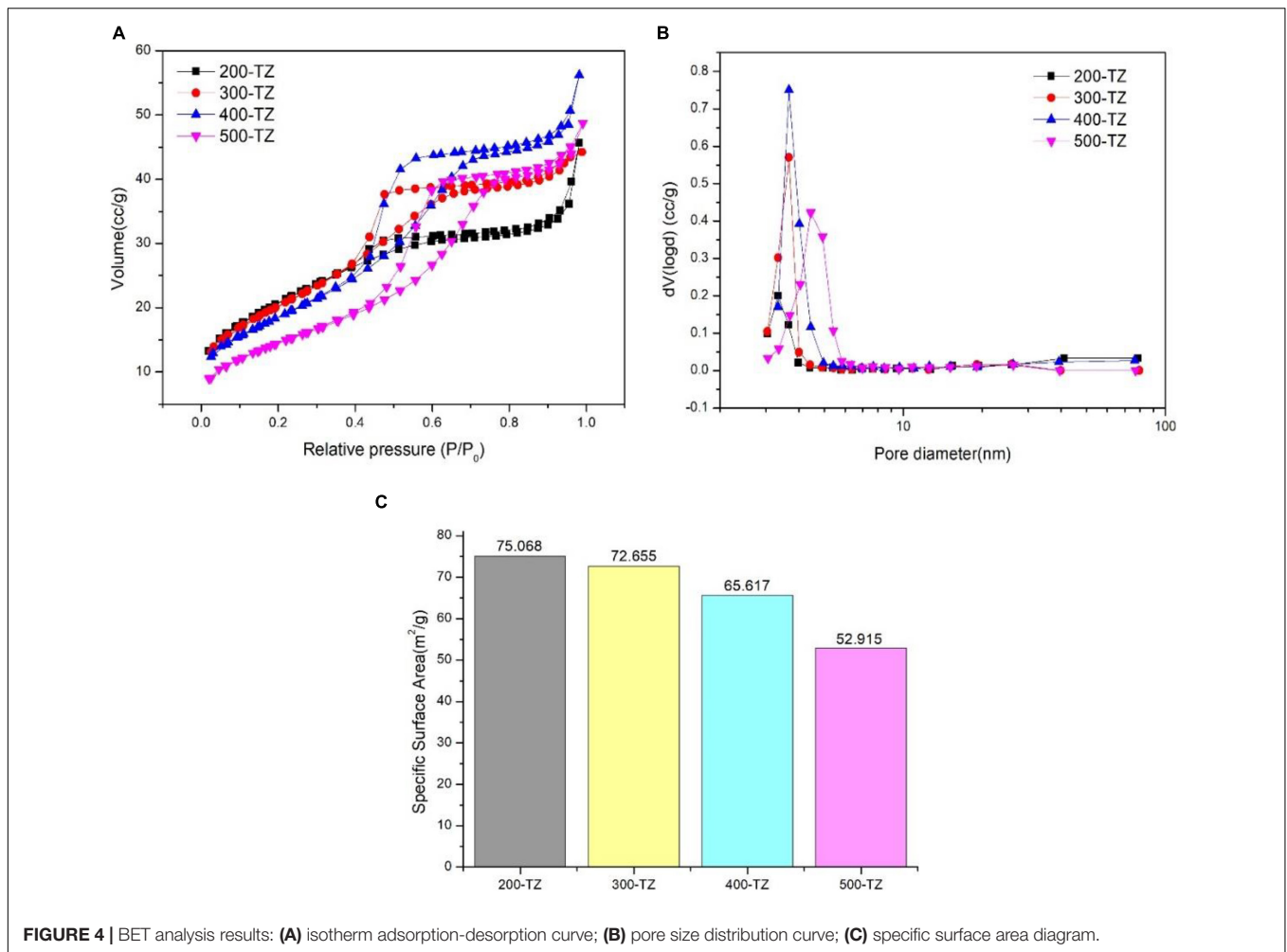


FIGURE 4 | BET analysis results: (A) isotherm adsorption-desorption curve; (B) pore size distribution curve; (C) specific surface area diagram.

the smallest pore diameter (about 3.5 nm). This phenomenon also verified the TiO₂ agglomeration resulted by thermal treatment.

Photocatalytic Degradation of TCaAm

It is well known that photocatalytic degradation contains three main processes: mass transfer, interphase adsorption, and photocatalytic oxidation. **Figure 5** compares different samples in terms of adsorption rate toward TCaAm without light. The adsorption rate increased with time and stayed constant after 5 h. And the stable adsorption rate of 200-TZ-25-PCM reached up to about 50%, which was higher than that of zeolite-PCM and TiO₂-PCM. This can be explained by the fact that, although zeolite is porous and has good adsorption capacity, after loading TiO₂ its pore structure was modified, so the adsorption capacity of 200-TZ-25-PCM was enhanced. On the other hand, compared with TiO₂-PCM, 200-TZ-25-PCM can disperse TiO₂ more evenly on the surface of cement paste and provide more adsorption sites, thus leading to a higher adsorption rate.

Figure 6 displays the effect of calcination temperature on the photocatalytic degradation rate toward TCaAm. The degradation rate was the highest at 200°C (97.6%), and it gradually decreased as the calcination temperature increased. It

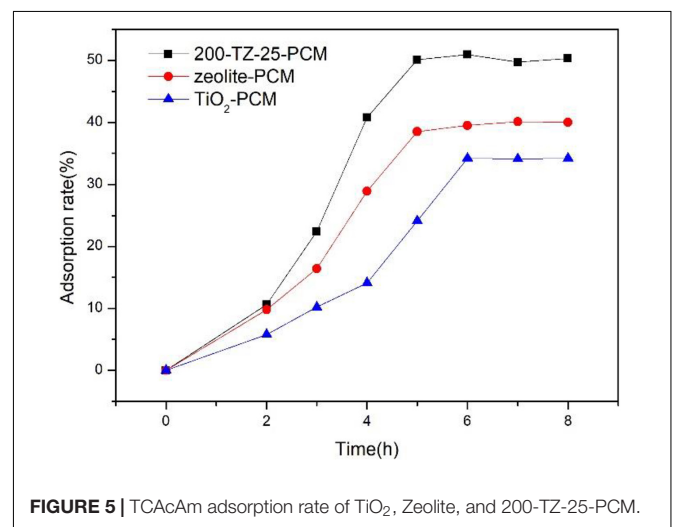
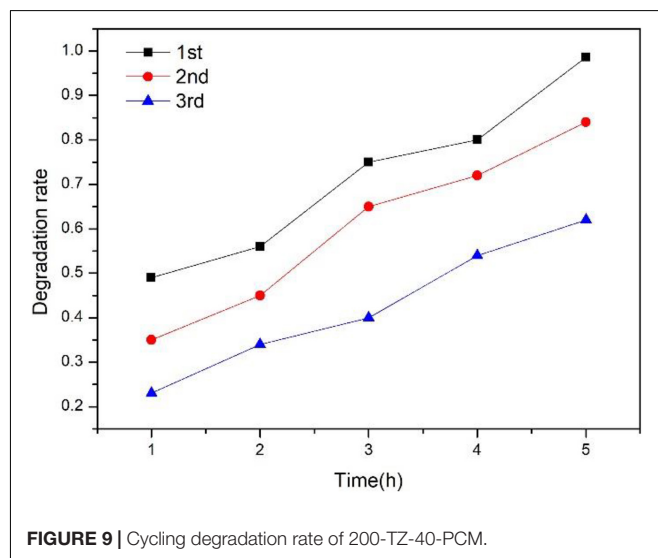
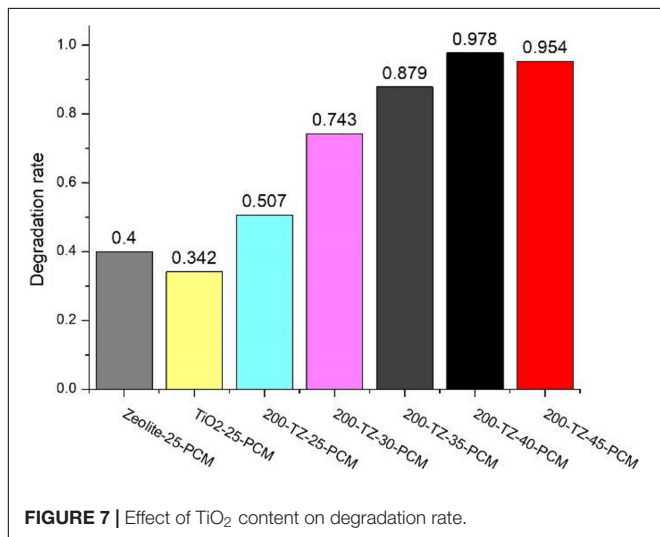
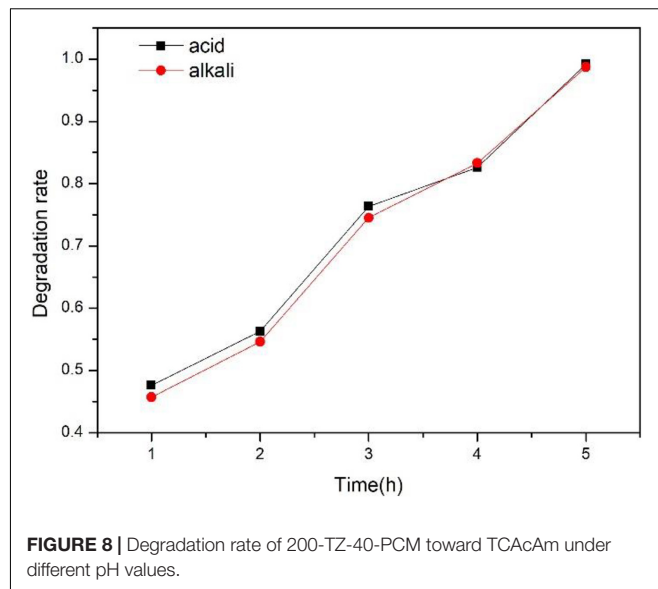
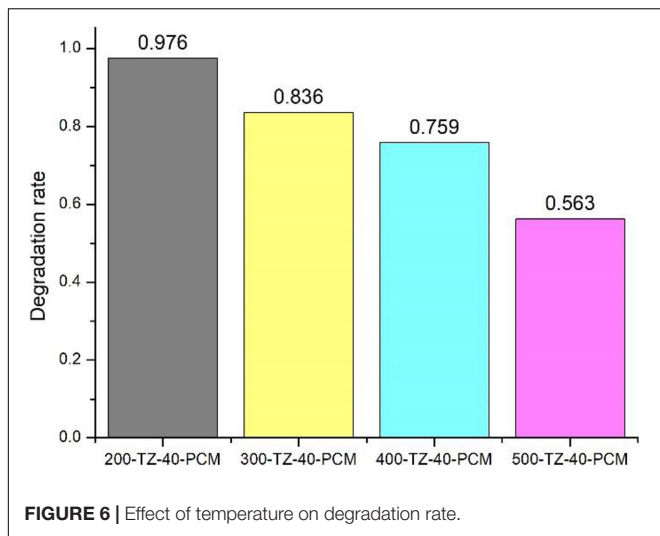


FIGURE 5 | TCaAm adsorption rate of TiO₂, Zeolite, and 200-TZ-25-PCM.

shows that the prepared photocatalytic PCM has the greatest photocatalytic activity under the calcination condition of 200°C. Because as the temperature increases, the size of the TiO₂@zeolite



composite particles became larger, resulting in the redshift of the optical energy gap, and the redox potential of electrons/holes became lower, and the activity of the catalyst decreased (Poon and Cheung, 2007).

Figure 7 shows the results of photodegradation of TCACAm on PCM with different TiO₂ content after 5 h of light. Zeolite-25-PCM stands that the TiO₂ content was 0, and TiO₂-25-PCM stands that the TiO₂ content was 100%. It can be seen that the degradation rates of Zeolite-25-PCM and TiO₂-25-PCM were relatively low, reaching 40 and 34.2%, respectively. The degradation rate of Zeolite-25-PCM was almost equal to its adsorption rate, indicating that Zeolite-25-PCM can only adsorb TCACAm under light, and TiO₂ particles will get into agglomeration in the cement hydration environment, so the degradation rate of TiO₂-25-PCM was the lowest (34.2%). At low TiO₂ addition, its photocatalytic degradation effect is poor and the adsorption governs the reaction, so the degradation rate of TiO₂-25-PCM was lower than that of Zeolite-25-PCM. Moreover, the degradation rate of 200-TZ-25-PCM was close to

its adsorption rate as shown in **Figure 5**. With TiO₂ content increased, the degradation rate rose rapidly, and it reached its highest point (97.8%) as TiO₂@zeolite composite content was 40%. This was owned to two effects. Firstly, the abundant channels and pores, and the large SSAs of zeolite benefited the mass transfer and adsorption. Secondly, the zeolite was an optimal support for TiO₂ due to the unique pore shape, internal pore volume, and channel size (Hashimoto, 2003; Matsuoka and Anpo, 2003; Corma and Garcia, 2004), and TiO₂ was proved to be homogeneously dispersed on the surface of the TiO₂@zeolite composite as the results of N₂ adsorption-desorption and SEM-EDS indicated, thus more active sites were provided. The synergistic effect led to a high photocatalytic efficiency. It should be noticed that the degradation rate of 200-TZ-45-PCM was lower than 200-TZ-40-PCM. This can be explained by the fact that when the content of TiO₂@zeolite composite was high,

it could not be dispersed homogeneously on the surface of cement and some active sites will be covered, so its photocatalytic degradation rate was lower even if it had higher TiO₂ content. The intermediate carrier method is effective to improve the photocatalytic performance of the PCM.

It can be seen from **Figure 8** that the degradation rate of 200-TZ-40-PCM toward TCACAm can reach 98.7 and 99.2% at 5 h under acidic (pH = 5) and alkaline conditions (pH = 11), respectively. It shows that in the process of photocatalytic degradation of TCACAm, the initial pH has little effect on the degradation rate. The reasons for the above phenomenon may be as follows: the pH value of the solution is an important factor that determines the physical and chemical species in the solution and the state of the molecules in the solution. In the case of acidic initial conditions (pH = 5) and alkaline initial conditions (pH = 11), since the pK_a value of TCACAm is 8.75, when the pH value of the solution was lower than 9, TCACAm existed in the form of C₂H₂Cl₃NO molecules, and as the pH value was lower than 8.75, it existed in the form of C₂HCl₃NO⁻. Therefore, regardless of acidic or alkaline conditions, TiO₂ had no additional adsorption effect on TCACAm due to the protonation of the charge on the TiO₂ surface, so acidity and alkalinity have no great effect on the photocatalytic degradation of TCACAm.

The results of the recycle degradation experiment of 200-TZ-40-PCM are shown in **Figure 9**. The first degradation rate reached up to 98.6% for TCACAm within 5 h. However, from the second cycle onward, the degradation rate decreased slightly. When the tests were recycled three times, the third degradation rate was 56.6%. The decrease in degradation rate is probably due to the occupation of TiO₂ active sites by TCACAm or the reaction products.

CONCLUSION

(1) Through the sol-gel method, TiO₂@zeolite composite catalyst was successfully prepared. SEM images and BET results showed

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that zeolite was porous and had large SSA. XRD and EDS results confirmed that nano-TiO₂ particles were homogeneously dispersed on the surface of zeolite.

(2) TiO₂@zeolite composite coated PCM had excellent adsorption ability. The synergistic effect of the surface adsorption of zeolite and the photocatalytic degradation of TiO₂ can significantly improve the photocatalytic degradation performance of the TiO₂@zeolite composite coated PCM. 200-TZ-40-PCM (TiO₂@zeolite composite content was 40% and thermal treatment temperature was 200°C) had the highest degradation rate (97.8%) within 5 h, which was about 2.86 times than pure TiO₂ coated PCM.

(3) The TCACAm degradation rate was regardless of pH value, and decreased with thermal treatment temperature. After several repeated experiments, the degradation rate had a declining trend.

DATA AVAILABILITY STATEMENT

The original contributions presented in the study are included in the article/supplementary material, further inquiries can be directed to the corresponding author/s.

AUTHOR CONTRIBUTIONS

GL: literature search, figures, and writing. WC: data collection. JZ: data analysis. WY: study design. AS: funding and data interpretation. All authors contributed to the article and approved the submitted version.

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Conflict of Interest: JZ was employed by the company Shanghai Construction Group Co., Ltd., Shanghai, China.

The remaining authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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