



Facile Synthesis of Sn/Reduced Graphene Oxide Composites With Tunable Dielectric Performance Toward Enhanced Microwave Absorption

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Electromagnetic (EM) wave absorbing materials are strongly desired for the reason that EM pollution has become a serious problem with the rapid development of modern technology, which brings harm to the environment and human health. Herein, nanocomposites of Sn/reduced graphene oxide (Sn/rGO) as a novel type of EM absorbing materials were synthesized via a facile and efficient strategy. Nanoscale SnO₂ microspheres were synthesized by sol-gel method, and the Sn/rGO composites were obtained after hydrothermal process with GO. Samples with different Sn content were fabricated (rGO:Sn = 30:1, 20:1, 10:1, mass ratio), and their EM wave absorption performance were analyzed. By changing the mass ratio of Sn and rGO, dielectric constant of the composites can be adjusted, and better impedance matching can be achieved. The unique capacitive structure and conductive network enable the material to have strong dielectric loss and excellent absorption performance. This research offers a new route for designing and fabricating high-frequency EM wave absorbing materials.

Keywords: new route, nanocomposites of Sn/rGO, tunable dielectric performance, high frequency absorption, excellent absorption performance

INTRODUCTION

With the rapid development of technology, electromagnetic (EM) interference has become a serious problem (Cao et al., 2018; Jia et al., 2018; Wei et al., 2018b; Wu G. et al., 2018; Lu S. et al., 2019), which not only causes damage to the operation of electronic devices, but also has a remarkable negative effect on human health (Liang et al., 2016, 2018; Oraizi et al., 2016; Smitha et al., 2016; Tian et al., 2017; Meng et al., 2018). The key to solve this problem relies on the development and application of EM wave absorbing materials (Batrakov et al., 2016; Liu T. et al., 2016). According to the loss mechanism, EM wave absorbing materials can be divided into dielectric materials and magnetic materials (Liu P. et al., 2018; Pang et al., 2018; Yang et al., 2018). However, magnetic materials will lose their magnetism at high temperature and thus cannot meet the application requirement in thermal environment. Therefore, a large number of researches and

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theories have been focused on designing dielectric materials with thin thickness, lightweight, wide absorption frequency range and strong absorption property (Liu et al., 2016; Liu P. et al., 2016; Song L. et al., 2017; Liu J. et al., 2018; Samadi et al., 2018; Wu F. et al., 2018; Xie et al., 2018; Liu et al., 2020).

Dielectric materials, such as carbon fibers (Shah et al., 2015), carbon coils (Hu et al., 2018), carbon nanotubes (Makarova et al., 2016), carbon black (Al-Ghamdi et al., 2016), are mainly carbon materials due to low density, high dielectric loss and adjustable surface properties (Guan et al., 2017; Xu et al., 2017; Wang S.S. et al., 2018; Wei et al., 2018a; Zhang L. et al., 2018; Wu et al., 2019), and a lot of researches have been conducted on them. Sun et al. synthesized a vertically arranged carbon nanotube array by means of chemical vapor deposition. Carbon nanotube has a multi-wall structure, with an average diameter of 11 nm and light weight. By changing the stacking angle, the absorption frequency can be precisely controlled to increase the microwave absorption intensity of CNTs. When the superposition angle between two adjacent carbon nanotubes is 90°, the best absorption performance is obtained, and the reflection loss reaches -47.66 dB (Sun et al., 2014). Chen et al. prepared a multiwall carbon nanotube (MWCNT)/graphene foam (GFs) composites (CGFs) with high efficiency microwave absorption using a simple solvent-thermal method. By changing MWCNT load and thermal reduction temperature, complex permittivity and conductivity of CGFs can be adjusted effectively. The introduction of MWCNT improves the EM wave absorption property of CGFs at low frequency and has the widest effective bandwidth of 16 GHz (Chen et al., 2017). Although carbon materials have good absorbing performance, light weight and wide effective frequency band at low frequency, they cannot meet the application requirement in harsh thermal environment.

Carbon materials can be compounded with other materials (metal, metal oxide, high transmittance material) in order to obtain good EM wave absorbing property at high temperature, for example, ZnO@MWCNTs, MnO2/RGO, RGO/ZnO CeO2-RGO, CoNi/rGO, Fe/graphene, Fe₃O₄-Fe/G, FeNi@NC/NCNT/NrGO, G/CoNi@NCNTA, NiFe/N-GCT, SiO2@Fe3O4/G and so on (Ren et al., 2013; Wen et al., 2013; Zhang et al., 2015, 2019a,b,c, 2020; Qu et al., 2016; Wang Z.Q. et al., 2018; Yan et al., 2018; Hu et al., 2019; Xu et al., 2020). Xia et al. focus on the synthesis of lithium aluminum silicate (LAS) glass-ceramic with high transmittance (>90 %; 1.7 mm; 2-18 GHz) to electromagnetic wave. And then, the LAS/rGO nanocomposites with low density, broad band, and strong absorption was designed. The dielectric properties of the composites were adjusted by LAS transmittance material with ultra-low complex dielectric constant. As a result, LAS/rGO nanocomposites possess ultra-high EM wave absorbing property. However, there are many deeper mechanisms to explore due to the elemental diversity of the LAS materials (Xia et al., 2018; Lu S. et al., 2019). Cao et al. synthesized ZnO nanocrystals modified multi-walled carbon nanotubes (ZnO@MWCNTS) by solution method. The addition of zinc oxide appropriately adjusts the complex dielectric constant, and this ultra-lightweight composite exhibits greater dielectric loss and high efficiency of EM wave absorption by generating additional interfacial interactions compared to physical mixing. A series of excellent properties of ZnO@MWCNTS indicate that it is a kind of absorbing material that can be used in high temperature environment (Wen et al., 2013). Wang et al. prepared CeO₂-rGO composites with good EM wave absorption property by onestep hydrothermal method. When the mass ratio of CeO2:GO is 10:1, the synthesized composite has a minimum reflection loss RL of -45.91 dB (2.0 mm, 13.28 GHz), which is 73.35 and 6.14 times better than CeO2 and RGO, respectively (Wang Z.Q. et al., 2018). Metal oxides can be introduced into carbon materials to adjust impedance matching and effectively improve the absorbing performance. However, a crucial issue for putting absorbing material into device application is to understand the physics of metal-carbon materials interface in the device. Hence, metal-carbon materials are studied in order to make more absorbents into devices. Zhao et al. synthesized graphene-coated Fe (Fe/G) nanocomposites for the first time and investigated their EM wave absorption properties. Due to the charge transfer at Fe-graphene interface in Fe/G, the nanocomposites show distinct dielectric properties, which result in excellent EM wave absorption performance in a wide frequency range. The minimum RL is about -45 dB at 7.1 GHz (3 mm). It provides a novel approach for exploring high-performance EM wave absorption material (Zhao et al., 2013). Therefore, it can be predicted that this mode has a good development prospect in the field of EM wave absorption, which chooses the non-magnetic metal with quite different conductivity from carbon materials for synthesis to regulate EM wave absorption property of composites.

Herein, we reported a facile and effective strategy to fabricate Sn/rGO composites. Sn microspheres were successfully coated by rGO via a one-step hydrothermal method. The microstructure and EM wave absorption property were investigated. Sn, with a low conductivity, was introduced to adjust the dielectric loss of the composites. The dielectric constant and impedance matching of composites were adjusted by controlling the ratio of samples mass. The result indicated that the improved properties of Sn/rGO composites can be attributed to their unique architecture and the conductivity differences between Sn microspheres and rGO. This work aimed to explore a facile method to compound dielectric materials with adjustable dielectric properties.

EXPERIMENTAL SECTION

Materials

Tin (II) chloride dihydrate (SnCl₂·2H₂O, A.R.) was purchased from Xilong Chemical Research Institute in China. Tetraethyl silicate (TEOS, A.R.), N-Hexane (A.R.) and Sodium hydroxide (NaOH, A.R.) were provided by Beijing Chemical Works Research Institute in China. 3-aminopropyltriethoxysilane $[NH_2(CH_2)_3Si(OC_2H_5)_3, KH-550]$ was obtained from Jinan Jinhui Chemical co. LTD. Graphene oxide (GO) dispersed solution (0.94 wt%) was purchased from Changzhou Sixth Element Material Technology co. LTD. All the chemical reagents were analytical grade and used without further purification. Ethanol and deionized water were used for all process of washing and dissolution.

Preparation of Nanoscale SnO₂ Microspheres

 $0.05 \text{ mol SnCl}_2 \cdot 2H_2O$ was dissolved in 6.2 mL anhydrous ethanol and 3.8 mL deionized water, and then stirred for 2–3 h to obtain uniform mixed solution at room temperature. After that, 5.7 mL tetraethyl silicate (TEOS) was added into the solution slowly and formed gel. The sample was aged for 24 h at room temperature, and then was aged for 2 days under 70°C. The obtained gel was soaked in *n*-hexane for 2 days under 50°C to replace solvent. The product was soaked in NaOH solution (2 mol/L), stirred for 30 min under 50°C. Finally, the solution was filtered, washed, dried and calcined at 550°C, and so the expected nanoscale SnO₂ microspheres were obtained.

Fabrication of Sn/rGO Composites

GO dispersed solution and 50 mL deionized water were mixed by ultrasonic for 2 h, previously prepared nanoscale SnO_2 microspheres and 1 mL KH-550 were added into the mixture, and stirred for 30 min. Then, the mixture was treated using hydrothermal method at 180°C for 12 h, After freeze drying, the powder was sintered at 800°C for 2 h (under Ar atmosphere). Finally, Sn/rGO composites were obtained. The schematic illustration of Sn/rGO composites is shown in **Figure 1**. Samples with different mass ratio of 10:1, 20:1 and 30:1 (GO: Sn) were named A1, A2, and A3, respectively. Pure rGO without Sn was used for comparison.

Characterization

The phase structure and crystalline component of the composites were analyzed using X-ray diffraction (XRD, DX-2700, with highintensity Cu- Ka radiation source). Raman spectra were acquired at room temperature by using a 532 nm laser (Renishaw, RM-1000). The morphology and microstructure of the composites were investigated by field emission scanning electron microscopy (SEM, MERLIN Compact) and transmission electron microscopy (TEM, JEOL-2100) with energy dispersive x-ray analysis (EDAX). The complex permittivity and complex permeability values in the frequency range of 2-18 GHz were obtained with a vector network analyzer (VNA, Agilent N5245A, United States). Sample rings for electromagnetic measurement were prepared by uniformly mixing the composites into paraffin (Sn/rGO: 5 wt%) and pressed into a ring mold with an outer diameter of 7 mm and inner diameter of 3 mm. The transmission line theory was applied to calculate the reflection loss (RL) so as to analyze the EM wave absorption property.

RESULTS AND DISCUSSION

Structural Analysis

Crystal phases of the samples were analyzed by XRD. XRD patterns of SnO₂, rGO, A1 (10:1), A2 (20:1) and A3 (30:1)

are given in Figure 2. It is clear that rGO has a broad weak characteristic peak at around $2\theta = 22.3^{\circ}$, which can be assigned to the (002) crystal planes (Quan et al., 2017a; Xu et al., 2018). A1, A2, and A3 samples all maintain the same characteristic peak. With the increase of GO content, the characteristic peak becomes more obvious and higher. Meanwhile, the peaks at $2\theta = 26.6^{\circ}$, 33.8° and 51.8° correspond to (110), (101) and (211) plane of SnO₂ (JCPDS no.46-1088), where the interlayer spacing of (110) plane is approximately 0.33 nm. The interlayer spacing is calculated using Bragg equation (Feng, 2016; Li et al., 2018; Zhang N. et al., 2018), which is expressed as $d = \lambda/2\sin\theta = 26.6^{\circ}$ (Li et al., 2018). The characteristic peak of Sn can be found in A1, A2, and A3, located at $2\theta = 30.644$, 32.018, 43.871, 44.902, 55.330, 62.538, 64.576, 72.414, and 79.470 corresponding to the (200), (101), (220), (211), (301), (112), (321), (420), and (312) planes, respectively. And the width of the peak is narrower than that of SnO₂, indicating better crystallinity. In addition, the position of the peak has changed, which can be caused by the reduction of SnO₂ during calcination. This is further confirmed that the generation of new grains in Figures 4B–D. The majority of the XRD pattern of the Sn/rGO hybrids is found to be very similar. However, there is a slight shift in the position of the diffraction peaks, indicating that Sn is successfully anchored onto the rGO sheet and forms some interactions (Wang Z.Q. et al., 2018). As a result, chemical binding occurs between Sn and rGO because simple loads cannot cause peak offset. Among them, the KH-550 plays an important role in this process. It can enhance the interface bonding force between Sn and rGO, so that more Sn microspheres can grow on the rGO sheet (Lu S. et al., 2019). All the evidence points to the composites being synthesized.

The ordered degree of carbon material was distinguished by Raman spectroscopy. Figure 3 depicts the Raman spectra of rGO, A1, A2, and A3. Two prominent peaks of D and G are observed, which are around 1,330 and 1,580 cm^{-1} , respectively. It is obvious that there is a trend of the intensity ratio of D band to G band (I_D/I_G) for the samples (A3 > A2 > A1 > rGO) (Lin et al., 2015; Kumar et al., 2016; Zhang et al., 2016; Huang et al., 2017). As the content of Sn increases, the disordered and defect degree of the composites decreases, indicating the separation of rGO layers after fastening of Sn on rGO sheets and further restoration of the sp (Wu G. et al., 2018) network of rGO (It is consistent with the morphology of SEM and XRD results) (Liu J. et al., 2018; Wang Z.Q. et al., 2018). Notably, the slight blue shift of Raman peaks for the composites compared with rGO, which indicates Sn microspheres were successfully covered by rGO (Shu et al., 2018). And there is a charge interaction on multiple interfaces, which can improve the EM wave absorption property of the composites.

The morphologies of SnO_2 and A2 (20:1) with different magnification are shown in **Figure 4**. A1, A2, and A3 have the same shape and appearance, only differ in the concentration of Sn. In **Figure 4a**, SnO_2 shows a loose porous structure, which is composed of many microspheres (diameter is ~150 nm) with rough surface. As can be seen from **Figure 4b**, the reduced Sn microspheres are evenly distributed on the surface of rGO sheet. It's clear that the size of the microspheres has increased





(diameter is ~1.50 μ m), proving that SnO₂ is reduced to Sn during hydrothermal process, which is consistent with the XRD results. Figures 4c,d exhibit that Sn is not only attached to the surface of rGO sheet, but also tightly wrapped in the slice layer of rGO. There are multiple interfaces between Sn and rGO sheet (marked by a red dotted circle), which has a positive effect on EM wave absorption performance.

The microstructure of the annealed composites was further investigated by TEM. The obtained lattice spacing is 0.33 nm, which matches the (110) crystal planes of SnO₂ microspheres in **Figure 5a**. As shown in **Figures 5b,c**, Sn solid microspheres evenly distribute on the surface of rGO slice layer. **Figures 5e-g** are the energy spectra diagram of A2 corresponding to **Figure 5d**, which display the presence of the C, Sn, and O elements. These are consistent with SEM results.

EM Wave Absorption Properties

To investigate the EM wave absorption properties of rGO, A1 (10:1), A2 (20:1) and A3 (30:1), the samples were mixed with wax (filler loading: 5 wt%) to analyze the relative complex permittivity and permeability. The electromagnetic parameters are important for EM wave absorbing material. As a kind of dielectric loss materal, the composites hardly exhibit any magnetic loss, so it







FIGURE 4 | SEM images of (a) SnO₂, (b-d) A2 with different magnification.

can be ignored. In **Figures 6C,D**, the real part and imaginary part of permeability for all samples are around 1 and 0, respectively. It can be noted from the magnetic loss tangent curve (**Figure 6F**) that the magnetic loss is almost 0. The zigzag fluctuations in the first half of the figures, which indicates that rGO and Sn/rGO composites are high dielectric material but weakly magnetic. The



FIGURE 5 | (a) HRTEM image of SnO₂, (b-d) TEM images of A2 and (e-g) energy spectra diagram of C, Sn, and O elements corresponding to (d).

 μ' and μ'' values of these samples have a small fluctuation in the 2–8 GHz frequency range, which is caused by the small size effect, surface effect, and spin wave excitations (Wang Z.Q. et al., 2018). Moreover, these permeability values are typical for materials that have no magnetic properties, which fluctuates in the range of 1 ± 0.2 and 0 ± 0.2, respectively (Li et al., 2018). The real part of permittivity represents energy storage capacity, and the imaginary part of permittivity can stand for energy dissipation, which can be expressed as follows according to Maxwell's equation and Debye theory (Zhang C. et al., 2017; Lu S.R. et al., 2019):

$$\varepsilon^{'} = \varepsilon_{\infty} + \frac{\varepsilon_{s} - \varepsilon_{\infty}}{1 + \omega^{2} \tau^{2}}$$
(1)

$$\varepsilon^{''} = \varepsilon^{''}_{p} + \varepsilon^{''}_{c} = \frac{\varepsilon_{s} - \varepsilon_{\infty}}{1 + \omega^{2} \tau^{2}} \omega \tau + \frac{\sigma}{\omega \varepsilon_{0}}$$
(2)

where ε_{∞} , ε_0 and ε_s are the permittivity at infinite frequency, dielectric constant of free space and the static frequency, respectively. $\varepsilon_{p}^{''}$ and $\varepsilon_{c}^{''}$ are the polarization loss and conductivity loss, respectively. ω is the angular frequency (2 π f), τ is the relaxation time of dipoles, σ is the conductivity which can be calculated based on measured ε' and ε'' . This work aims to adjust the dielectric constant based on conductivity, and focuses on the relationship between conductivity and the absorption property. In Figures 6A,B,E, We can see a clear curvilinear trend that A2 > A3 > A1 (besides rGO) of $\epsilon^{'}, \ \epsilon^{''}$ and tan $\delta_\epsilon~(\epsilon^{''}/\epsilon^{'})$ in 2–18 GHz. rGO shows the highest $\epsilon^{''}$ and tan $\delta_\epsilon,$ indicating that rGO has high dielectric loss capacity due to excellent conductivity. However, this can lead to high reflection at the absorber interface and poor impedance matching, resulting in low attenuation. In summary, the impedance matching of the composites can be adjusted by introducing Sn microspheres. A2 has the highest value of permittivity among the samples, demonstrating the best energy storage and dissipation capacity. The high complex permittivity of A2 can be ascribed to multiple

interfacial polarizations between Sn and rGO. In a heterogeneous system, electric charge can accumulate at the interface of two phases with different dielectric constants, leading to interfacial polarization (Maxwell-Wagner polarization). Sn microspheres have low conductivity, when recombined with rGO, oxygen vacancies enhance the conductivity of local electrons. According to free-electron theory, increased conductivity of A2 can lead to strong dielectric loss. Dielectric loss capacity is strengthened due to the charge transfer interaction between Sn microspheres and rGO. In **Figures 6E,F**, it can be seen that the values of tan δ_{ϵ} are higher than those of tan δ_{μ} (μ''/μ'), which proves that dielectric loss dominates in EM wave attenuation of the composites.

It is well-known that reflection loss (RL) value can be used to judge the EM wave absorption performance. Lower RL means more EM wave energy can be absorbed. According to the transmission line theory, the RL of the samples can be calculated by the following equations (Feng et al., 2016; Huang et al., 2017; Li et al., 2017; Song C.Q. et al., 2017; Zhang N. et al., 2017):

$$RL = 20lg \left| \frac{Z_{in} - 1}{Z_{in} + 1} \right|$$
(3)

$$Z_{\rm in} = \sqrt{\frac{\mu_r}{\epsilon_r}} \tan h \left(j \frac{2\pi f d}{c} \sqrt{\mu_r \epsilon_r} \right) \tag{4}$$

$$\varepsilon_r = \varepsilon' - j\varepsilon'' \quad \mu_r = \mu' - j\mu'' \tag{5}$$

where Z_{in} , μ_r , ε_r , f, d, and c are the normalized input impedance, the complex permeability, the complex relative permittivity, the EM wave frequency, the sample thickness and the EM wave velocity in vacuum.

Figure 7 shows the frequency dependence of reflection loss of rGO, A1, A2, and A3 with different thicknesses. The values of RL lower than -10 dB correspond to 90% energy absorption. The RL curves of rGO (**Figure 7A**) show that the value of RL_{min} is -21.49 dB with a thickness of 2.5 mm and a wide absorption



FIGURE 6 | (A) Permittivity real part, (B) permittivity imaginary part, (C) permeability real part, (D) permeability imaginary part, (E) dielectric loss tangent, (F) magnetic loss tangent of rGO, A1, A2, and A3.





Frequency range (GHz)	Thickness (mm)	Maximum RL (dB)	RL < -10 dB band width (GHz)	Filler loading (wt%)
11.76–18.00	2.5	-21.49	6.24	5
10.40-11.20	4	-11.50	0.80	5
12.48-18.00	3	-39.54	5.52	5
13.12-18.00	3	-19.27	4.88	5
	Frequency range (GHz) 11.76–18.00 10.40–11.20 12.48–18.00 13.12–18.00	Frequency range (GHz) Thickness (mm) 11.76–18.00 2.5 10.40–11.20 4 12.48–18.00 3 13.12–18.00 3	Frequency range (GHz)Thickness (mm)Maximum RL (dB)11.76–18.002.5-21.4910.40–11.204-11.5012.48–18.003-39.5413.12–18.003-19.27	Frequency range (GHz) Thickness (mm) Maximum RL (dB) RL < -10 dB band width (GHz) 11.76-18.00 2.5 -21.49 6.24 10.40-11.20 4 -11.50 0.80 12.48-18.00 3 -39.54 5.52 13.12-18.00 3 -19.27 4.88

TABLE 2 | Reported MA properties of typical rGO-based hybrids in the recent literatures.

Absorber	Loading (wt%)	RL _{min} (dB)	Bandwidth (GHz)	Thickness (mm)	References
Porous Cocoon-like rGO	7	-29.05	5.27	2.00	Shah et al., 2015
CeO ₂ -rGO	50	-45.90	4.50	2.00	Wang Z.Q. et al., 2018
rGO/MWCNTs/ZnFe ₂ O ₄	50	-23.80	2.60	1.50	Shu et al., 2018
MoS ₂ /rGO	60	-67.10	5.92	1.95	Quan et al., 2017a
rGO/Ni	10	-39.03	4.30	2.00	Xu et al., 2018
Sn/rGO	5	-39.54	5.52	5.00	This study



bandwidth (6.24 GHz). According to the requirements of thin thickness, lightness, broad effective absorption bandwidth and strong absorption ability for materials, rGO has weak EM wave absorption performance. Therefore, Sn microspheres were used to regulate impedance matching of the composites in this work. As we can see in Figures 7B-D, with the increase of Sn microspheres, the EM wave absorption performance shows a tendency to increase first and then decrease. Among them, A2 has the best performance with the minimum RL (-39.54 dB), thin thickness of 3 mm, and the broad effective absorption bandwidth (5.52 GHz). Other excellent parameters change less with the improvement of absorbing performance. Compared with A2, A1, and A3 have poor impedance matching and attenuation capability (Figure 8), which means they have weak energy storage and energy dissipation capacity (Figures 6A,B), resulting in poor EM wave absorption performance. The EM wave absorption performance of rGO, A1, A2, and A3 with the same filler loading (Sn/rGO: 5 wt%) is summarized in **Table 1**. In addition, **Table 2** summarizes typical rGO-based hybrids (in paraffin) and their corresponding MA properties reported in recent literatures.

In order to understand the loss mechanism and relative factors, the following analysis was done. Two necessary conditions must be satisfied for absorbing material to have excellent absorption performance. On the one hand, good impedance matching means that the incident EM wave enters the material as complete as possible. It can reduce direct reflection on the surface of the material. On the other hand, attenuation characteristics means EM wave can be rapidly attenuated after entering the material. The following equations are used as a representation (Quan et al., 2017b; Zhao et al., 2017):

$$Z = \frac{Z_{\rm in}}{Z_0} = \sqrt{\mu_r / \varepsilon_r} \tag{6}$$



FIGURE 10 | (A) Simulations of the A2 thickness versus peak frequency under the 1/4λ model, (B) 3D presentation and (C) contour map of reflection loss for A2 with different thicknesses in the frequency range of 2–18 GHz.

$$\alpha = \frac{\sqrt{2}\pi f}{c} \times \sqrt{\left(\mu^{''} \varepsilon^{''} - \mu^{'} \varepsilon^{'}\right) + \sqrt{\left(\mu^{''} \varepsilon^{''} - \mu^{'} \varepsilon^{'}\right)^{2} + \left(\mu^{''} \varepsilon^{'} - \mu^{'} \varepsilon^{''}\right)^{2}} \quad (7)$$

Herein, Z, Z_0 , and α are the impedance matching ratio, impedance of free space and attenuation constant, respectively. The best impedance matching is obtained through the value of Z, which is Z = 1 (μ_r equals to ε_r). The higher the value of α , the stronger the ability to consume EM wave. In **Figure 8**, it can be found that the tendency of the impedance matching ratio is A2 > rGO > A3 > A1 (**Figure 8A**) and the trend of the attenuation constant is rGO > A2 > A3 > A1 (**Figure 8B**). Although rGO has the maximum attenuation coefficient, its impedance matching is poor, which means less EM wave can get into the material, resulting in higher RL value. According to the equations above, A2 shows the best EM wave absorbing property due to the best impedance matching and relatively large attenuation constant.

For non-magnetic materials, the value of $\epsilon^{''}$ represents its electromagnetic loss capacity. According to the Eq. 2, the $\epsilon^{''}$ is mainly enhanced by the σ of the Sn/rGO network, polarizations at the Sn- rGO and Sn – Sn interfaces, and

the defect-dipoles generated by the oxygen vacancies. The contributions of polarization $\varepsilon_p^{''}$ and conductivity $\varepsilon_c^{''}$ for samples have been compared, as shown in Figure 9. It is found that the conductivity loss plays a dominant role for all the samples. rGO has the highest value of conductivity loss, nevertheless, shows low EM wave absorption ability due to the poor impedance matching. A2 has high conductivity loss and proper impedance matching, consequently, demonstrates the excellent EM wave absorption performance (Figure 7). When Sn microspheres are anchored onto the rGO sheets, the mobile holes in the rGO sheets interact with the localized electrons on the Sn microspheres which are caused by oxygen vacancies via coulomb interactions, resulting in hole trapping at the vacancy sites and effective electron transfer. Owing to the presence of charge transfer between the Sn and rGO, the combined motion of the collective interfacial dipoles could further improve the EM wave absorption performance. And then the introduction of solid conductors increases the conductivity of A2 and provides an optimal conductive network, which maximizes the macroscopic current caused by carriers and facilitates the conversion of electromagnetic energy into heat energy. Whereas with the



increase of Sn, the conductive network is gradually repaired and the vacancy is reduced, which reduces the degree of electron transition and ultimately leads to the reduction of A3 conductivity loss. This provides strong support for the subsequent attenuation mechanism.

It can be seen from **Figure 10A** that the EM wave absorption performance is sensitive to thickness. As the thickness increases, the RL_{min} moves to lower frequency. This can be explained by the quarter wavelength (λ /4) matching mechanism (Shah et al., 2015; Shu et al., 2018). The relationship between thickness and corresponding frequency of absorption peak can be expressed by the equation as follows (Liang et al., 2017):

$$t_m = \frac{n\lambda}{4} = \frac{nc}{4f_m\sqrt{|\varepsilon_r\mu_r|}} \quad (n = 1, 3, 5, ...)$$
(8)

Herein t_m , f_m , and λ are the thickness of the absorber, the peak frequency and the quarter-wavelength at f_m , respectively. The physical meaning is when the t_m and f_m satisfy the equation above, the phase difference of the reflected EM wave will be 180° (the reflected wave comes from the upper and bottom interface). The induced offset effect causes the disappearance of both incident and reflected wave. As shown in Figure 10A, all the t^{exp} stars fit well with the simulated t^{sim} curve, conforming that the excellent EM wave absorption performance of A2 can be interpreted by the quarter wavelength matching model. Figure 10B depicts the 3D representation of reflection loss for A2. As we can see, the RL value of the maximum absorption at different frequency can be obtained by controlling the thickness of the EM wave absorber. Figure 10C shows the contour map of reflection loss for A2 with different thicknesses in the frequency range of 2-18 GHz. A2 exhibits the minimum RL (-39.54 dB) with a thickness of 3 mm at 9.60 GHz. It can be seen that the absorption band can span (<-10 dB) almost the whole frequency range (4–18 GHz) by optimizing the thickness. As a consequence, the quarter wavelength matching model is also well consistent with the contour map.

The attenuation mechanism of Sn/rGO composites is mostly conduction loss and polarization effect (see Figure 11). The excellent absorption performance is mainly attributed to the balanced impedance match and the unique capacitive structure. Sn has poor electrical conductivity. By forming heterogeneous structure with RGO in a moderate proportion, there is a balance between impedance matching and attenuation constant, which improves the EM wave absorption performance. When EM wave transmits into the material, it causes the directional migration of carriers, leading to oscillating current. Furthermore, the boundary charge leads to dielectric relaxation and polarization. Under the influence of EM field, the EM wave entering the material is repeatedly scattered, and a large number of positive and negative charge areas are formed on the pore wall, which promotes polarization loss and improves the overall absorption capacity. According to Coulomb interaction, the surface of the Sn microsphere has a higher concentration of aerobic vacancy, local electrons are generated on the smooth Sn microspheres and interact with the pores of rGO. As a result, electrons are captured by the holes in vacancy, which leads to effective electron transfer. The interface and defect dipole polarization provide the condition for capacitive structure, adjacent rGO sheets can form a kind of capacitive structure that helps polarize the EM field and reduces the power of the incident EM wave. Finally, the intricate conductive network formed in the composites generates dissipative current, partial conversion energy can be consumed during transmission, resulting in ohmic loss. All kinds of data and theories show that Sn/rGO composite is a new kind of absorbing material with high efficiency and good heat resistance prospect (Wen et al., 2013).

CONCLUSION

In summary, Sn/rGO composites with simple synthesis process and adjustable dielectric parameters was successfully prepared. The obtained dielectric materials possess excellent impedance matching and EM wave attenuation ability by adjusting the dielectric constant. And it also has excellent EM wave absorption performance with low filler loading (sample: 5 wt%), the minimum RL is -39.54 dB with 3 mm thickness at 9.60 GHz (effective absorption bandwidth: 5.52 GHz). The unique structure and conductive network are important for enhancing the EM wave absorption properties. The present study demonstrates that Sn/rGO composites have great potential in EM wave absorption field.

DATA AVAILABILITY STATEMENT

All datasets generated for this study are included in the article/supplementary material.

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AUTHOR CONTRIBUTIONS

TL did the experiment and processed the experimental data to writing the manuscript. LX, XH, TZ, BZ, and GW are responsible for reviewing the manuscript and putting forward suggestions for revision. JD and XT assisted with the experiment.

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Conflict of Interest: The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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