



# Green and Low-Cost Membrane Electrode Assembly for Proton Exchange Membrane Fuel Cells: Effect of Double-Layer Electrodes and Gas Diffusion Layer

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The success of fuel cells depends on the proper design of the electrodes and membrane allowing easy access of oxygen and protons. Using non-precious catalyst electrodes based on recyclable carbon nanostructures is most important to produce clean energy and increase the ability to commercialize the fuel cells. Herein, reduced graphene oxide (rGO) and graphene/magnetic iron oxide nanocomposite (rGO/MIO) are successfully synthesized as anode and cathode, respectively, from polyethylene terephthalate (PET) waste bottles using easy steps in order to simplify the method and reducing the production cost. While, the membrane is prepared from low cost and eco-friendly ternary polymers blend which are polyvinyl alcohol (PVA), polyethylene oxide (PEO) and polyvinyl pyrrolidone (PVP) then doped with sulfonated graphene oxide. The prepared electrodes have characteristic high porosity and their electrocatalytic performances are evaluated using three-electrode cell electrochemical studies as cyclic voltammetry and linear scan voltammetry combined with rotating disk electrode. A new assembly of the membrane between two non-precious catalyst electrodes as a single polymer electrolyte membrane fuel cell (PEMFC) was developed using a catalyst-coated membrane technique. The membrane electrode assembly (MEA) design parameters which affect its performance in hydrogen fuel cells as number of used catalyst layers (CL) or using gas diffusion layer (GDL) were evaluated in a single cell set-up with H<sub>2</sub>/O<sub>2</sub> operation and the results revealed that the performance MEA was enhanced with using GDL more than that of MEA without GDL by 66% at a current density of 0.8 A cm<sup>-2</sup> while the performance with double CL was better than that of the conventional single CL by 30% at a current density of 0.98 mA cm<sup>-2</sup>.

**Keywords:** graphene, graphene iron oxide composites, proton exchange membrane, membrane electrode assembly, hydrogen fuel cells

## INTRODUCTION

As a result of the rapid urbanization since the beginning of the last century, the global growth of fossil fuel energy consumption has increased, leading to an increase in environmental pollution rate. Consequently, environmental pollution has shifted research attention to get clean energy conversion and storage systems. Fuel cells are known as one of the cleanest energy conversion systems due to their high energy density, high energy-conversion efficiency, environmental safety, and other outstanding features (Frey and Linardi, 2004).

Among different types of fuel cells, the polymer electrolyte membrane fuel cell (PEMFC) is a promising green energy conversion technology for both portable and stationary devices, as well as transportation applications. This is may be due to its economic, high efficiency, low-temperature operation, zero or low emission and rapid start-up (Gouda et al., 2019). The conversion process of chemical to electrical energy in PEMFCs depends on two chemical reactions at anode and cathode where oxygen reduction occurs at the cathode and hydrogen oxidation occurs at the anode (Liu et al., 2019a) and both reactions need catalysts to reduce the electrochemical over-potential and to increase the voltage output. The oxygen reduction reaction (ORR) at the cathode is a multistep reaction involved with multielectron, thus the ORR reaction consumes most of the catalyst material. Consequently, the development of low cost, high-performance electrocatalysts for improving ORR kinetics is essential to reduce the cost of PEMFCs (Liu et al., 2019b). Pt-based composites are considered as the most efficient cathode catalysts, but they have disadvantages as high cost, crossover poisoning and low stability especially in acidic media (Choi et al., 2015). However, high-performance non-precious metal catalysts (NPMCs) simultaneously active for the ORR at the cathode and the hydrogen oxidation reaction (HOR) at the anode are desperately needed to replace these precious metals and to solve the drawbacks (Gupta et al., 2016). Under these circumstances, transition metal oxides (Gao et al., 2017; Lai et al., 2017), hybrid inorganic nanocarbon materials (Su et al., 2014; Ye et al., 2017) and carbon-doped metal-free heteroatom nanomaterials (Dumont et al., 2019) were used to substitute platinum for constructing highly efficient non-precious metal catalysts. Where, the promoted activity of doped carbon materials may be attributed to the electron-donating or electron-accepting behavior between adjacent carbon atoms and the heteroatoms, which modify the charge allocation in the carbon plane (Shen et al., 2014).

In addition to catalyst electrodes, the polymeric proton exchange membrane is one of the most important components of PEMFCs. Thus, development of the proton exchange membrane using non-perfluorinated based polymers as new alternative membranes attracted many researchers with the aim of replacing benchmark Nafion<sup>®</sup> membranes to reduce the production cost and to be closer to commercialization (Bakangura et al., 2016; Pourzare et al., 2016). However, the non-perfluorinated based polymers are usually modified chemically with several treatments, such as polymers blending, incorporation of doping agents in the polymer matrix as carbon-based nanomaterials and polymers sulfonation to improving the membrane properties

(Awang et al., 2015; Pourzare et al., 2016; Sedesheva et al., 2016; Pandey et al., 2017).

Recently, graphene (G) and graphene-based materials have received great interest as a promising material for fuel cell applications due to its remarkable advantages, such as; large specific surface area, mechanical flexibility, and good electrical conductivity. In particular, a significant improvement in the electrocatalytic activity of electrodes was observed with graphene or modified graphene as the catalyst support or as a metal-free catalyst (Iwan et al., 2015; Morales-Acosta et al., 2019). Moreover, the incorporation of graphene oxide (GO) or sulfonated graphene oxide (SGO) into a polymer matrix of the PEM (Li et al., 2017; Pandey et al., 2017; Qiu et al., 2017) enhance its ionic conductivity and improve its physicochemical properties (Beydaghi et al., 2014).

In recent years, many researchers have been interested in turning the membrane electrode assembly (MEA) prototypes into commercially valuable products by improving its overall efficiency, increase current density and decrease the cost of the membrane and catalytic materials used. However, the results show that the true performance of the MEA for PEMFC is not only depended on the properties of the individual components but also depend on the MEA production method and the operating conditions in the cell (Aziz et al., 2018) such as the composition of electrode inks, electrode pressing, percentage of humidification and applied pressure on both electrodes, gas diffusion layer (GDL) materials used and cell temperature (Frey and Linardi, 2004; Thanasilp and Hunsom, 2010; Kim et al., 2015).

Motivated by these observations, this research concerns the production of low-cost MEA for PEMFC using non-precious metal graphene-based materials as catalytic electrodes prepared from the thermal dissociation of plastic waste using simple, one-pot, environmentally-friendly, and applicable synthesis method. While the polymeric proton exchange membrane was produced based on an ecological and simple approach via polymer crosslinking and casting techniques using a ternary crosslinked polymer containing poly (vinyl alcohol), poly (ethylene oxide) and poly (vinyl pyrrolidone) (Gouda et al., 2019) instead of benchmark Nafion<sup>®</sup> membranes. The polymer matrix doped with sulfonated graphene oxide (SGO) was used to enhance its mechanical properties and water retention of the membrane, whereas the sulfonic groups allowed keeping the membrane in a well-hydrated condition, thus improving the proton conductivity (Ayyaru and Ahn, 2017). However, to develop low-cost high-performance MEA, the fabrication procedures were tested using three types of MEAs and performance comparison was done to study the effect of gas diffusion layers (GDL) and the number of catalyst layers.

## MATERIALS AND METHODS

### Preparation of Electrode Materials

#### Preparation of Reduced Graphene Oxide (rGO)

Plastic bottles waste as sources of polyethylene terephthalate (PET) were used to prepare reduced graphene oxide (rGO). The PET bottle waste was ready to use as mentioned in a

previous study (El Essawy et al., 2017). Two grams of waste were introduced into an enclosed autoclave container and placed inside the center of an electric furnace at 800°C for 1 h. The resulting dark products were collected and crushed.

### Preparation of Reduced Graphene Oxide/Magnetic Iron Oxide Nanocomposite (rGO/MIO)

rGO/MIO nanocomposite was synthesized by using an inverse co-precipitation process based on the precursors of ferric chloride ( $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$ ), ferrous sulfate ( $\text{FeSO}_4 \cdot 7\text{H}_2\text{O}$ ), and the precipitator of ammonium hydroxide ( $\text{NH}_4\text{OH}$ ) (Ma et al., 2018). Twenty mL 0.2 M  $\text{NH}_4\text{OH}$  aqueous solution and 0.5 g of reduced graphene oxide (rGO) were added into a 250 mL four-neck bottle under  $\text{N}_2$  atmosphere for 30 min and 1.08 g  $\text{FeCl}_3 \cdot 6\text{H}_2\text{O}$  and 0.54 g  $\text{FeSO}_4 \cdot 7\text{H}_2\text{O}$  with a stoichiometric ratio  $[\text{Fe}^{2+}]:[\text{Fe}^{3+}]$  equal to 1:2, corresponding to  $\text{Fe}_3\text{O}_4$ , were dispersed using an ultrasonic dispersion method into 60 mL 1:1 (volume ratio) water-ethanol mixed solvents. The mixture was then poured rapidly into a four-neck bottle under vigorous mechanical stirring for 10 min with  $\text{N}_2$  bubbling throughout the reaction. The nanocomposites were separated magnetically, washed with deionized water until the throwdown solution became neutral then dried in a vacuum oven at 80°C for 24 h.

### Characterization of Electrode Materials

X-ray Diffraction (XRD) data (Shimadzu-7000, U.S.A.) was collected with a  $\text{CuK}\alpha$  radiation beam ( $\lambda = 0.154060$  nm). An X-ray Photoelectron Spectroscopy (XPS) Phi 5300 ESCA system (Perkin-Elmer, U.S.A) with Mg ( $\text{K}\alpha$ ) radiation (X-ray energy 1253.6 eV) was used. A Transmission Electron Microscope (TEM) (TECNAI G20, Netherland with EDX) was also used. The Brunauer-Emmett-Teller (BET) surface area and total pore volume were measured using Barret-Joyner-Halenda (BJH) adsorption methods.

### Electrochemical Measurements of Electrodes

The catalytic activity of rGO and rGO/MIO nanocomposites were tested for ORR in 0.1 M KOH electrolyte. The sample inks were prepared by ultrasonically a mixture containing 450  $\mu\text{L}$  of 2-propanol and 50  $\mu\text{L}$  of 10 wt % Nafion mixture solution with 2.5 mg of sample to form a homogeneous ink. Then a polished and clean glassy carbon (GC) disk electrode with 0.126  $\text{cm}^2$  geometric surface area was loaded with 10  $\mu\text{L}$  of suspension. Potentiostat/Galvanostatic (VoltaLab 40 PGZ301) with software Voltmaster4 was used for all electrochemical experiments.

The three-electrode electrochemical cell was used to conduct the electrochemical measurements at room temperature using 0.1 M KOH solution as the electrolyte. A graphite rod was used as the counter electrode, Hg/HgO (1 M NaOH) as a reference electrode and the tested prepared electrode material supported on GC as the working electrode. As electrode potentials presented in the manuscript refer to the Hg/HgO reference electrode. The electrolyte was saturated with  $\text{N}_2$  or  $\text{O}_2$  for 30 min before each electrochemical test.

Cyclic voltammetry (CV) was used to check the electrochemical activity of rGO or rGO/MIO in  $\text{N}_2$ -saturated electrolyte solution for three cycles with  $-0.8$  V to 0.2 V potential window at 100  $\text{mVs}^{-1}$  scan rate. Furthermore, the CV was also

recorded in  $\text{O}_2$ -saturated electrolyte for three cycles with  $-0.8$  V to 0.2 V potential window at 100  $\text{mVs}^{-1}$  scan rate to investigate the initial behavior of the electrode.

To study the electrochemical kinetics, linear scan voltammetry with rotating disk electrode technique (LSV-RDE) was used in  $\text{O}_2$ -saturated alkaline electrolyte solution in the 0.2 to  $-0.8$  V potential window at a scan rate of 5  $\text{mVs}^{-1}$  under several rotation speeds while keeping the  $\text{O}_2$  flow on the surface of the solution during the measurements. Koutecky-Levich equation (K-L equation) was used to determine the number of electrons involved in the electrochemical reactions as illustrated in Equations (1) and (2).

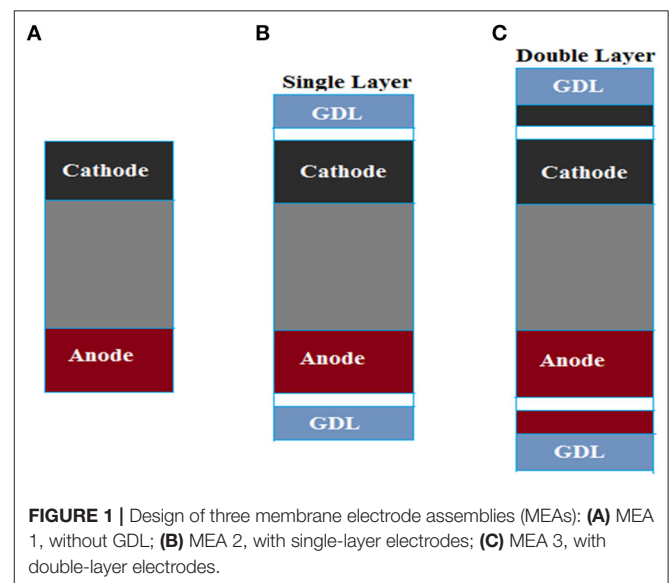
$$(1/j) = (1/j_k) + (1/j_d) = (1/j_k) + 1/(B\omega^{1/2}) \quad (1)$$

B was determined from the slope of the Koutecky-Levich plot according to Equation (2) given below,

$$B = 0.62 n F C_{\text{O}_2} D_{\text{O}_2}^{2/3} \nu^{-1/6} \quad (2)$$

where  $j$  is the measured current density,  $j_k$  and  $j_d$  are the kinetic and diffusion limiting currents densities; respectively,  $\omega$  is the speed of rotation in rpm, when the rotation speed is expressed in rpm the value of 0.62 is used,  $F$  is the Faraday constant (96,485  $\text{C mol}^{-1}$ ),  $D_{\text{O}_2}$  is the oxygen diffusion coefficient in the alkaline electrolyte solution ( $1.9 \times 10^{-5} \text{ cm}^2 \text{ s}^{-1}$ ),  $\nu$  is the kinematic viscosity ( $0.01 \text{ cm}^2 \text{ s}^{-1}$ ), and  $C_{\text{O}_2}$  is the oxygen concentration ( $0.0012 \text{ mol L}^{-1}$ ). Koutecky-Levich plot between  $(1/j)$  and  $(\omega^{-1/2})$  was plotted to obtain the number of electrons transferred ( $n$ ) from the slope and the kinetic-limiting current  $j_k$  from the intercept of the plot.

To determine the ionic conductivity of the prepared membrane and electrodes, resistance measurements were carried out by electrochemical impedance spectroscopy (EIS) technique at 5 mV in the frequency range of 0.1 Hz–500 kHz. The resistance is represented by the high-frequency intercept on the



real axis of the complex impedance plot. The ionic conductivity was determined from resistance according to Equation (3),

$$\sigma = d/RA \quad (3)$$

where  $\sigma$  is the membrane ionic conductivity ( $S\text{ cm}^{-1}$ ),  $A$  is the geometric area ( $\text{cm}^2$ ),  $d$  (cm) is the thickness and  $R$  ( $\Omega$ ) is the ohmic resistance.

### Preparation and Characterization of PEM

The PVA/PEO/PVP blended polymers matrix named as PVA/PEO/PVP-SGO-3 was prepared and characterized as previously described (Gouda et al., 2019).

### Preparation of Membrane Electrode Assembly

Spray method was used at the cathode and anode sides of the MEA. To identify an optimized fabrication concept, three types of MEAs were designed as depicted in **Figure 1** and the GDL used is carbon cloth (CeTech Carbon Cloth without MPL). The catalyst loading was adjusted to  $0.4\text{ mg cm}^{-2}$  on anode and cathode. Both electrodes had an active surface area of  $25\text{ cm}^2$ .

### Cell Polarization Measurements

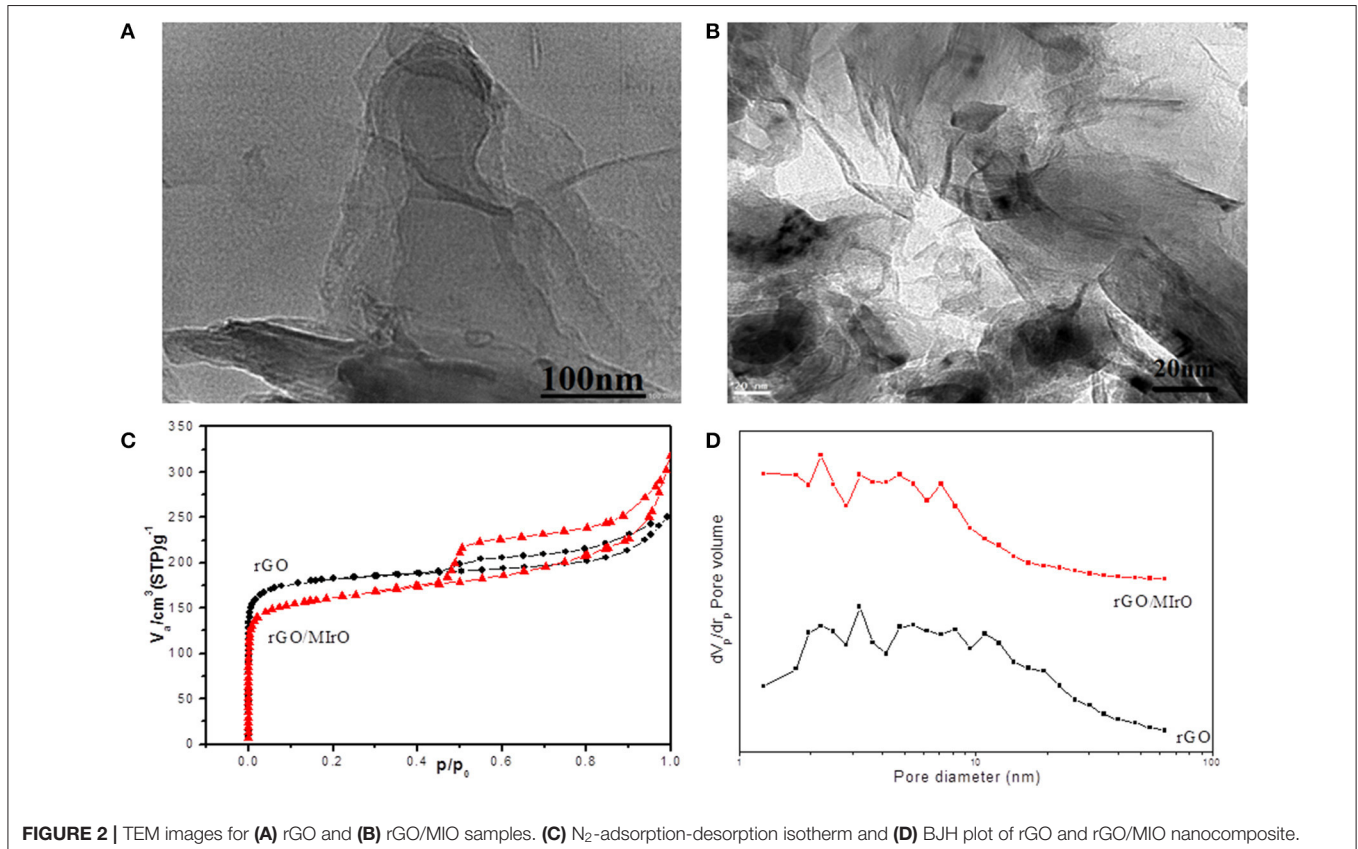
Polarization curves represent the trend of the losses affect PEM fuel cell performance. The single-cell was tested using Scribner Associates Model 850e test station. Fuel cell test station includes a computer-based control and data acquisition system based on advanced software for Electrochemical Research. The fuel

cell polarization curves are obtained from this software whereas the voltage vs. current density of the fuel cell with model assumptions: an ideal mixture of reactant gasses, steady-state conditions, isothermal process, and fully hydrated system. In this study, polarization curves were monitored with potentiostatic mode for determining maximum and minimum potential and current values. After that polarization curves were recorded with galvanostatic mode (differential currents were chosen as  $0.03\text{ A}$  at the low current region and  $0.05\text{ A}$  at the high current region). In this way, most current values were obtained at the low current density. Humidified hydrogen and oxygen gases were fed to the fuel cell with the same flow rate of  $250\text{ sccm}$ .

## RESULTS AND DISCUSSION

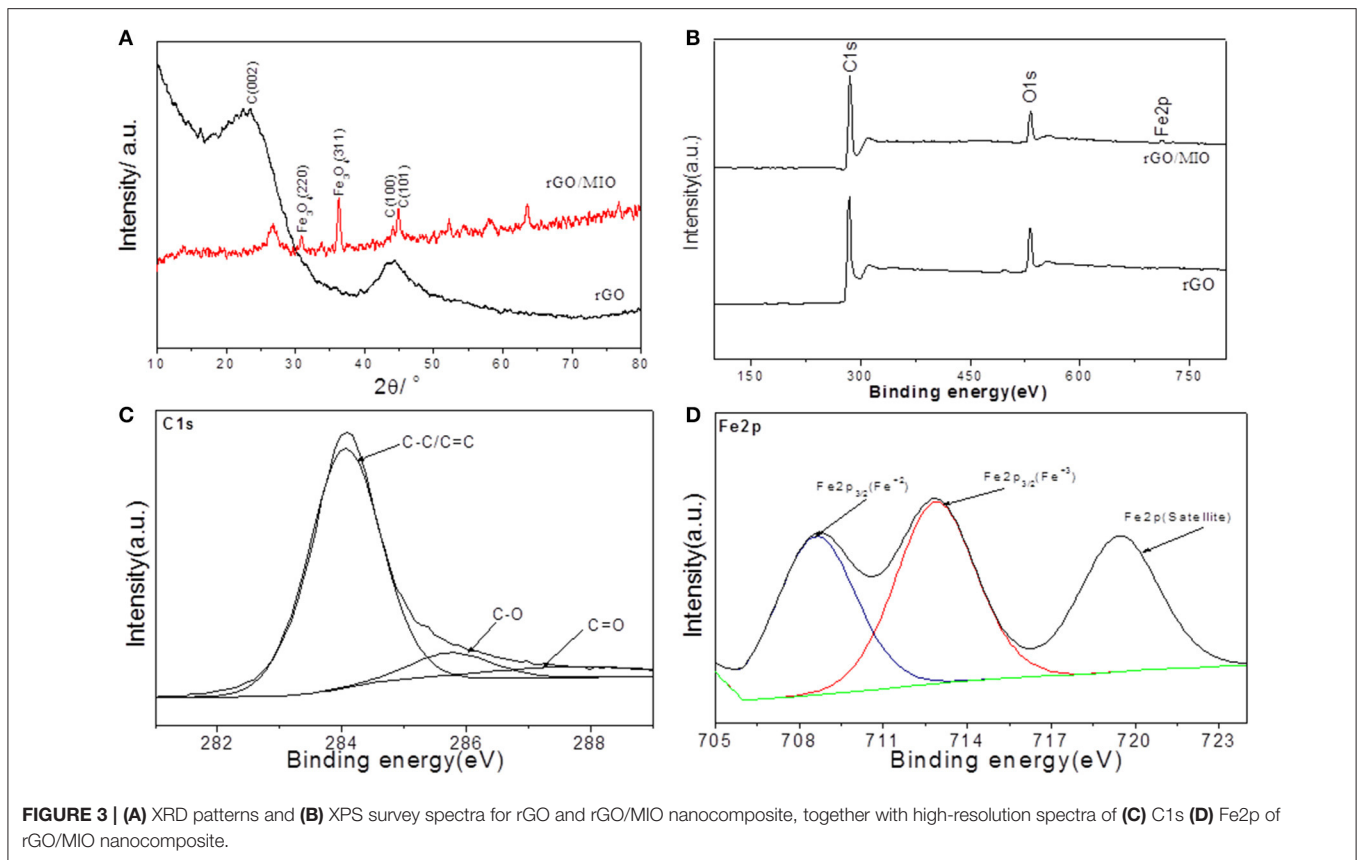
### Microscopic Visualization, Physical, and Chemical Characterizations of Electrodes Materials

As shown in **Figures 2A,B**, the TEM images of rGO and rGO/MIO nanocomposite demonstrate an exfoliated, crumpled and transparent flake-like morphology with several layers, in addition to entrapped iron oxide nanoparticles inside the graphene matrix for sample rGO/MIO and the EDX results implies presence of iron oxide in small ratio about 4% (atomic%) and that confirmed from the XPS results.



**FIGURE 2 |** TEM images for (A) rGO and (B) rGO/MIO samples. (C) N<sub>2</sub>-adsorption-desorption isotherm and (D) BJH plot of rGO and rGO/MIO nanocomposite.





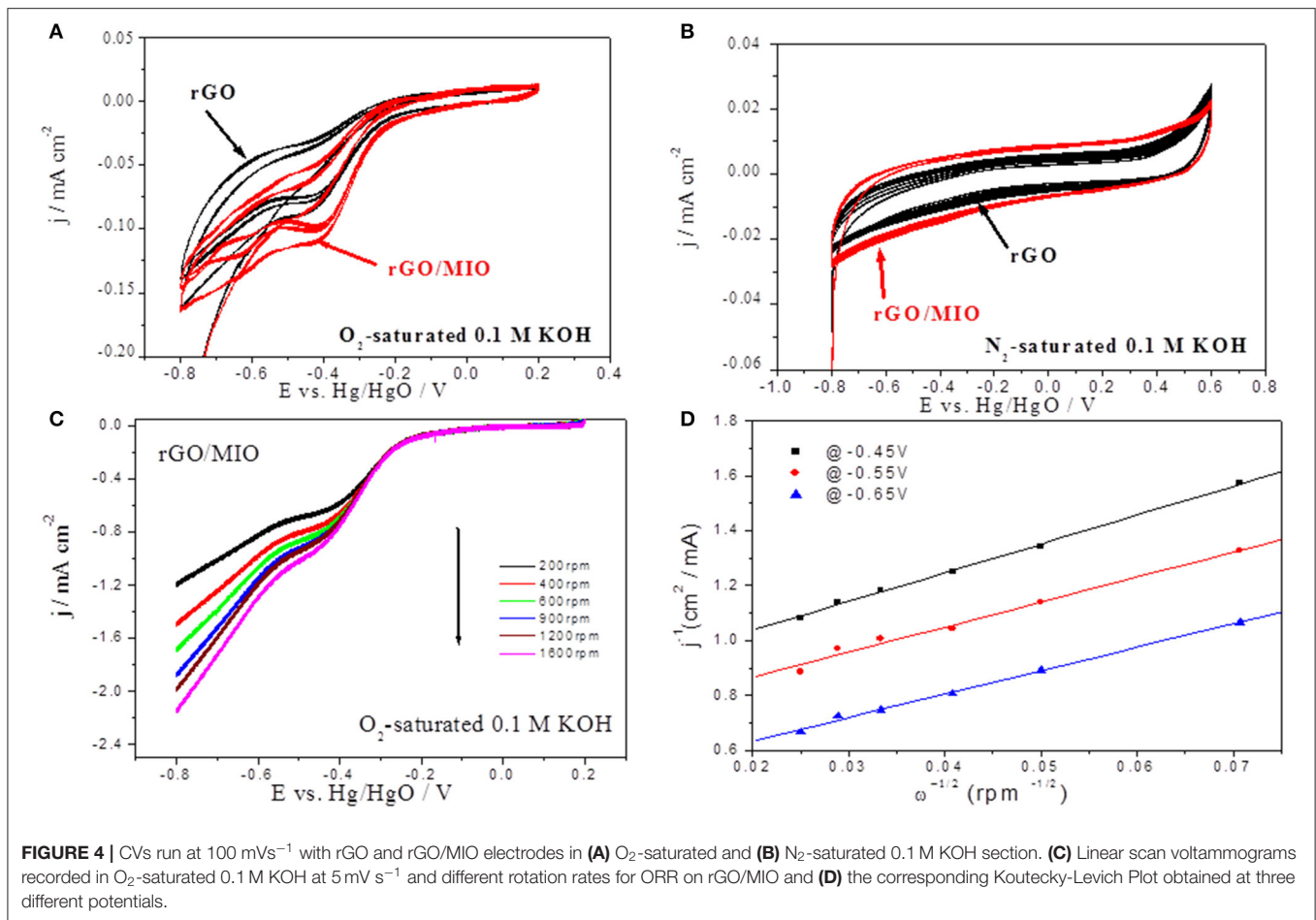
In order to investigate the surface porosity, an important factor affecting the mass transfer that affects the catalytic activity of the electrodes, the  $N_2$  adsorption and desorption isotherm test at 77 K was performed. As can be seen in **Figure 2C**, rGO, and rGO/MIO nanocomposite samples presented isotherms with hysteresis loop of the Type IV, according to IUPAC classification, in the relative pressure range of 0.4–1.0, and capillary condensation, indicating the coexistence of microporous and mesoporous structure, as confirmed from BJH plot (**Figure 2D**) with mean pore diameter of 2.2 and 5.1 nm for rGO and rGO/MIO nanocomposite, respectively. However, it was noticed that the surface area and the pore size of rGO/MIO nanocomposite is higher than that of rGO indicating that, the introducing of iron oxide nanoparticles avoids the aggregation and restacking problems which led to an obvious increase in BET surface area and pore size and that is a valuable characteristic for electrocatalytic applications.

As can be seen in **Figure 3A** the XRD pattern of the rGO sample showed  $2\theta$  main peak at  $26^\circ$  and  $44.3^\circ$  which corresponds to the (002) and (100) reflections. For rGO/MIO sample, a slight shift for (002) plane was due to introducing of  $Fe_3O_4$  nanoparticles between the rGO nanosheets thus increasing the interlayer spacing and that is beneficial to promote charge transfer in electrodes materials. However, the peaks at  $2\theta$  values of  $30.28$  (220) and  $35.78$  (311) are in good agreement with the inverse cubic spinel phase of  $Fe_3O_4$  (ICDD card no.01-07-5088).

To explore the graphitic content and carbon speciation in rGO and rGO/MIO samples, X-ray photoelectron spectroscopy (XPS) was used. As shown in **Figure 3B**, the obtained material was formed with a high amount of carbon and a low amount of oxygen, in addition to traces of iron for rGO/MIO sample. The chemical bonding composition of rGO/MIO nanocomposite was investigated as shown in the high-resolution C1s and Fe2p spectra (**Figures 3C,D**). The peak in C1s at 284.19 eV corresponding to  $sp^2$ -hybridization (C-C bond and C=C), demonstrates that most of the C atoms are arranged in a honeycomb lattice, and the fitted peaks centered at 285.87 and 287.88 eV are assigned to C-O and C=O respectively. The Fe2p spectra reveal the presence of two components assigned to  $Fe^{2+}$  and  $Fe^{3+}$  oxides, where  $Fe^{3+}$  is the dominant component. Only  $Fe2p_{3/2}$  is represented due to overlapping occurring between  $2p_{3/2}$  and  $2p_{1/2}$  edges (Otero et al., 2008; Molchan et al., 2015).

### Half Cell Electrochemical Measurements

rGO and rGO/MIO samples were prepared from one-step thermal dissociation process of PET waste and have two-dimensional mesoporous structures with large surface area, pore volume, and pore size, being appropriate for electrocatalytic applications. To evaluate the ability of using prepared rGO and rGO/MIO as electrocatalysts in fuel cell application, the electrocatalytic activity of the prepared electrodes toward ORR was evaluated using cyclic voltammetry (CV), linear



scan voltammetry (LSV) combined with rotating disk electrode (RDE) technique and electrochemical impedance spectroscopy (EIS).

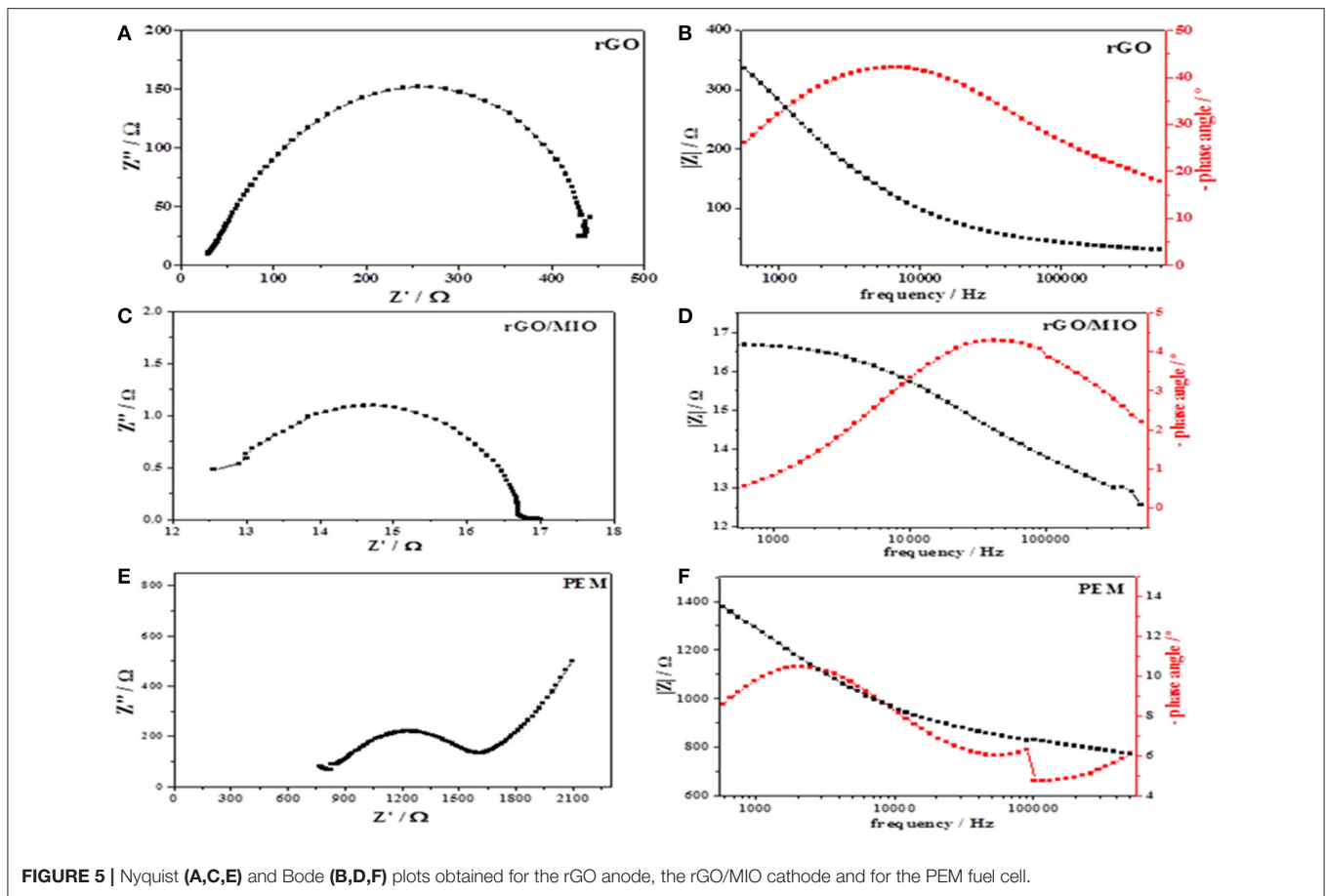
The CV curves of both samples in  $\text{O}_2$ -saturated 0.1 M KOH electrolytes are shown in **Figure 4A**, where both samples showed cathodic current peaks. It is noticeable that the rGO/MIO sample has earlier onset potential than the rGO sample, in addition to higher reduction current density, suggesting higher ORR activity of rGO/MIO. **Figure 4B** shows the CVs of both samples in  $\text{N}_2$  saturated 0.1M KOH electrolyte with the two samples showing similar behavior. From the previous CV survey, the prepared RGO material was selected to be used as the fuel cell anode and rGO/MIO was selected as the cathode material.

The ORR kinetics of the prepared rGO/MIO catalyst electrode were further studied by the LSV-RDE technique in  $\text{O}_2$ -saturated 0.1 M KOH electrolyte at different rotation rates (200, 400, 600, 900, 1,200, 1,600 rpm). As shown in **Figure 4C**, LSV curves confirmed its electrocatalytic performance in almost one-step process with an onset potential of ca.  $-0.25 \text{ V}$  and the diffusion current increased with the increasing of the rotation rate which confirm that the reaction is diffusion-controlled under the tested condition. Moreover, three regions of interest can be distinguished, namely, the diffusion-controlled region at potential  $E < -0.3 \text{ V}$ , the mixed diffusion kinetic region at potential  $-0.1 \geq E \geq -0.3 \text{ V}$ , and the kinetics controlled

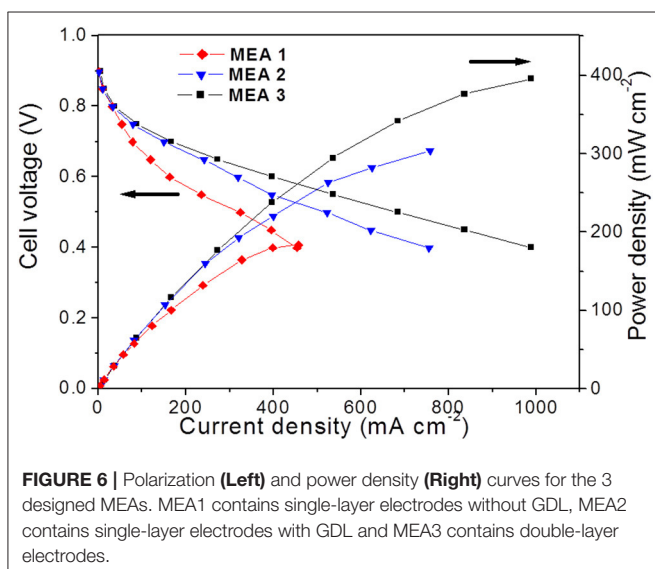
region at  $E \geq -0.1 \text{ V}$ . To calculate the number of electrons transferred during ORR, the Koutecky–Levich plots (K-L plot) at different potentials ( $-0.45 \text{ V}$ ,  $-0.55 \text{ V}$ , and  $-0.65 \text{ V}$ ) were plotted (**Figure 4D**) and the average electron number was calculated. A value of about four electrons was found, suggesting a direct four-electron pathway for ORR ( $\text{O}_2 + 4\text{H}^+ + 4\text{e}^- \rightarrow 2\text{H}_2\text{O}$ ), being this path the preferred (and more favorable) for fuel cell processes (Zhang et al., 2015).

It is known that electrochemical impedance spectroscopy (EIS) allows estimating ionic and electric conductivity of different systems. It is accepted that the high-frequency region of an impedance spectrum is associated with the internal ohmic resistance and the contact capacitance in the granular electrode structure, whereas the medium and low-frequency regions represent the charge-transfer resistance and the mass transport resistance, respectively (Yuan et al., 2010).

As shown in **Figures 5A,C,E** the incomplete semicircle that is potential independent has been assigned to different features, namely to internal ohmic resistance ( $R_{\text{ohm}}$ ), represented by high-frequency intersection of the semicircle with the x-axis, charge-transfer resistance ( $R_{\text{ct}}$ ), represented by the diameter of the semicircle, and contact capacitance in the granular electrode structure, represented by straight line at the high-frequency end of the semicircle (Fischer et al., 1998). As for the incomplete semicircle, it refers to a distributed resistance effect (Paganin



**FIGURE 5** | Nyquist (A,C,E) and Bode (B,D,F) plots obtained for the rGO anode, the rGO/MIO cathode and for the PEM fuel cell.



**FIGURE 6** | Polarization (Left) and power density (Right) curves for the 3 designed MEAs. MEA1 contains single-layer electrodes without GDL, MEA2 contains single-layer electrodes with GDL and MEA3 contains double-layer electrodes.

et al., 1998). From Nyquist plots, the calculated ionic conductivity of anode (rGO), cathode (rGO/MIO) and PEM are 0.3, 7, and 0.07  $\text{mS cm}^{-1}$  respectively. Furthermore, the Nyquist semicircle of the rGO/MIO sample is smaller than that of the rGO sample, indicating that it has lower resistance and better charge

transfer. However, the main reasons for the higher conductivity (lower resistance) of rGO/MIO nanocomposite (than the original rGO sample) could be attributed to the following points: (i) the introduction of iron oxide nanoparticles slightly increased the degree of graphitization, which is beneficial for promoting the charge transfer (Liu et al., 2019a) (2) and (ii) iron oxide nanoparticles accelerate the electron transfer, which in turn enhances the conductivity of the rGO/MIO nanocomposite (Yang et al., 2017). In addition, the relaxation time peak from Bode plot (Figures 5B,D) is not well clear. However, this is favorable for the cathode material in fuel cells (Qayyum et al., 2016). On the other side, for rGO sample the Nyquist semicircle at low frequency characterized by higher polarization resistance more than rGO/MIO and that is a characteristic property for anode material (Siracusano et al., 2018). An incomplete semicircle ended with a straight line in the high-frequency range was detected for PEM as shown in Figure 5E and that attributed to the membrane characteristic property, however the Bode plot shown in Figure 5F exhibits two time constants at high frequencies and that is related to the membrane structure (Zhao-Luo et al., 2018).

## Cell Performance

In general, MEA fabrication can come from two techniques. The first one is based on spraying the catalyst ink directly

onto the membrane, followed by a hot pressing step, while in the second technique the catalyst ink is directly sprayed onto the GDL and then hot-pressed onto the membrane (Frey and Linardi, 2004; Kim et al., 2015). The advantage of these techniques is that the catalyst loading can be adjusted by simply weighing the MEA or the GDL before and after coating with the catalyst ink but there is a risk of irregular catalyst transfer from the transfer film to the membrane. For that reason, an investigation on a cell performance of the developed MEA fabrication technique combining effect of using GDL and number of CLs was conducted using single-cell measurements with H<sub>2</sub>/O<sub>2</sub> operation, however only easy steps were chosen in this preparation technique without using assembly hot pressing in order to simplify the method and reduce the production cost with regard to maximal performance in addition to, preventing a distortion in the pore structures of catalyst layers and gas diffusion layers.

**Figure 6** shows the performance and power densities of the fabricated MEA 1, MEA 2 and MEA 3, whereas the lowest performance was for MEA 1, which was fabricated by using catalyst-coated membrane technique without GDL, compared to MEA 2, which was fabricated by using the same technique but using carbon cloth without a microporous layer as GDL. The addition of GDL to MEA facilitates the transport of interrupted gas and formed water through the electrochemically active areas of the MEA (Omran and Shabani, 2017). It also prevents leakage of the electrode material throughout the MEA, thus leading to a performance enhancement of MEA 2 of 66% when compared to MEA 1.

The effect of the number of CLs also affects the performance of fabricated MEA 2 and MEA 3 examined and compared here. The electrode ink was sprayed onto the membrane only as in MEA 2 and onto the GDL and the membrane as in MEA 3. The results show that the highest power densities up to 395 mWcm<sup>-2</sup> at 988 mA cm<sup>-2</sup> can be produced from MEA 3 with GDL and double-layered electrodes. Consequently, this result confirms the MEA performance depends on the electrode CLs number and morphology, and that could be referred to increasing the mass transport through the double layer electrodes, in addition to providing an effective path channel for water removal through the larger pores of the high porosity CL coated onto GDL.

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## CONCLUSIONS

This work contributes toward sustainable materials processing with upcycling technology to produce highly added-value products from reduced graphene oxide and reduced graphene oxide/magnetic iron oxide nanocomposite, produced from the thermal dissociation of plastic waste using simple, one-pot and applicable method. The prepared materials can be used as active catalyst electrodes with high durability for ORR in fuel cells, and hence get the benefits of simultaneous waste management and increasing the possibility for commercialization of low-temperature fuel cells by decreasing its production cost. Moreover, to develop high-performance MEAs and to identify the optimum fabrication conditions, three types of MEAs were designed. The optimum one is the MEA designed with a double-layer electrode involving an inner catalyst layer prepared by the catalyst-coated membrane (CCM) method and an outer catalyst layer directly coated on the gas diffusion layer to increase the catalyst utilization. Further investigations need to be carried out to elucidate the effect of using GDLs with a microporous layer on the performance of MEAs obtained in combination with the followed preparation technique.

## DATA AVAILABILITY STATEMENT

All datasets generated for this study are included in the article.

## AUTHOR CONTRIBUTIONS

MG fabricated the PEM and MEA. ME also participated in MEA fabrication, carried out CV and impedance measurements, and analyzed the experimental data. AA and MY performed and analyzed the data of fuel cell test station for fabricated MEAs. DS supervised and revised the manuscript. NE proposed the project, carried out electrodes preparation and characterization, and wrote the manuscript with input from the other coauthors.

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**Conflict of Interest:** The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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