



# Improvement in NO<sub>2</sub> Sensing Properties of Semiconductor-Type Gas Sensors by Loading of Au Into Porous In<sub>2</sub>O<sub>3</sub> Powders

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Porous (pr-) In<sub>2</sub>O<sub>3</sub> powders loaded with and without noble metals (Au, Pd, or Pt) were prepared by ultrasonic spray pyrolysis employing the PMMA microspheres as a template (typical particle size (ps): 28 or 70 nm with a diameter), and their NO<sub>2</sub> sensing properties were examined. The Au loading on the pr-In<sub>2</sub>O<sub>3</sub> was effective to increase the NO<sub>2</sub> response at lower operating temperature ( $\leq 200^{\circ}\text{C}$ ), while the metal loading of Pd or Pt were hardly effective. In addition, a decrease in the PMMA microspheres (from 70 to 28 nm in ps) largely increased the NO<sub>2</sub> response, and an optimized amount of Au loaded on the pr-In<sub>2</sub>O<sub>3</sub> sensor was 1.0 wt%. The decrease in the thickness of the sensing layer improved the NO<sub>2</sub> response and response speed. It was suggested that the Au loading enhanced the amount of the negatively adsorbed NO<sub>2</sub> on the bottom part of the sensing layer, leading to the increase in the NO<sub>2</sub> response. Furthermore, the introduction of additional macropores (ps: 150 nm) to the 1.0 wt% Au loaded pr-In<sub>2</sub>O<sub>3</sub> sensor increased the response to a low concentration of NO<sub>2</sub> (0.025 ppm) at 30°C. Therefore, it was found that easy gas diffusion from the surface to the bottom part of the sensing layer increased the effective concentration of NO<sub>2</sub>, and thus the NO<sub>2</sub> response was increased.

**Keywords:** NO<sub>2</sub> sensor, porous In<sub>2</sub>O<sub>3</sub> powder, loading of Au, ultrasonic spray pyrolysis, polymethylmethacrylate microsphere, ultrasonic-assisted emulsion polymerization

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## INTRODUCTION

Sensing performances of semiconductor-type gas sensors are largely improved by the morphological control of the sensing layer, probably due to the promotion of the gas reactivity on their oxide surfaces by an increase in the surface area per unit volume and the gas diffusivity in the sensing layer (Chen et al., 2014; Sun et al., 2014). Therefore, many researchers have reported the enhanced sensing performances by the structural modification of the sensing layer with rod-like (Wei et al., 2014; Takacs et al., 2015), plate-like (Chen et al., 2014; Guo, 2016), flower-like (Wang et al., 2014, 2015), or urchin-like structured oxide (Tang et al., 2013). Our group has also studied the introduction of ordered porous structures into metal-oxide layers of semiconductor-type gas sensors to enhance their gas diffusivity and surface area during the last 20 years (Hyodo et al., 2001, 2002, 2003, 2005, 2010, 2013, 2017; Hashimoto et al., 2008; Hieda et al., 2008; Firooz et al., 2010). For example, we synthesized mesoporous SnO<sub>2</sub> powders by utilizing the self-assembly of surfactants with a size of several nanometers, and their sensors showed the quite large H<sub>2</sub> response due to an increase in the specific surface area (Hyodo et al., 2001, 2002, 2003). We also reported macroporous SnO<sub>2</sub> layers fabricated by a sol-gel technique employing polymethylmethacrylate

(PMMA) microspheres (Soken Chem. & Eng. Co., Ltd., typical particle size (ps): 150, 400, 800, and 1,500 nm in diameter) as a template, and the one fabricated by using the smallest PMMA microspheres (ps: 150 nm) showed the largest H<sub>2</sub> response among them (Hyodo et al., 2005). In addition, we also attempted the fabrication of the macroporous In<sub>2</sub>O<sub>3</sub> powders by ultrasonic spray pyrolysis employing a precursor solution containing PMMA microspheres (ps: 150 nm), and their sensors showed much larger NO<sub>2</sub> response and quicker NO<sub>2</sub> response/recovery speeds than those of the conventional In<sub>2</sub>O<sub>3</sub> sensor prepared by the similar preparation technique employing a PMMA-free In(NO<sub>3</sub>)<sub>3</sub> aqueous solution (Hashimoto et al., 2008; Hyodo et al., 2010). Recently, we focused on the preparation of smaller-sized PMMA microspheres by an ultrasonic-assisted emulsion polymerization technique, and demonstrated an increase in the amount of sodium lauryl sulfate as a surfactant in the polymerization process of methyl methacrylate monomers decreased the size of the synthesized PMMA microspheres (Hyodo et al., 2013). In addition, the fabricated porous (pr-) In<sub>2</sub>O<sub>3</sub> sensor employing smaller-sized PMMA microspheres (ps: 26 nm) as a template in a precursor solution of ultrasonic spray pyrolysis was effective in improving the magnitude of NO<sub>2</sub> response to a low concentration of NO<sub>2</sub> (e.g., 1 ppm) at relatively low temperature (150°C) (Hyodo et al., 2017).

Another important technique to realize a large sensor response of semiconductor-type gas sensors is loading of a noble metal such as Au, Pd, Pt, etc., to metal oxides. The effects are known as the chemical and/or electronic sensitization phenomena (Yamazoe et al., 2003). Kim et al. reported the Au decoration on hematite nanotubes improved the magnitude of acetone response as well as acetone selectivity against ethanol (Kim et al., 2018b). Degler et al. clarified that the Au loading on the surface of SnO<sub>2</sub> accelerated negative adsorption of O<sub>2</sub> on the surface by the spillover effects, leading to the enhancement of the CO sensing performances (Degler et al., 2016a). They also demonstrated that the Pt loading on SnO<sub>2</sub> increased the CO response in humidified air, and nano-sized PtO<sub>2</sub> clusters on SnO<sub>2</sub> surface accelerated the CO oxidation reaction (Degler et al., 2016b). Ogel et al. synthesized Pd-loaded hollow-structured SnO<sub>2</sub> powders by a water-in-oil (w/o) microemulsion-based method, and found that the Pd loading on the outside of the SnO<sub>2</sub> shell was effective in achieving large CO response at lower operating temperatures ( $\leq 150^\circ\text{C}$ ) (Ogel et al., 2017). Kim et al. reported that the sensor of nitrogen-doped WO<sub>3</sub>-nanofiber functionalized with Pt nanoparticles by physical mixing showed the enhanced NO<sub>2</sub> response (Kim et al., 2018a). We also confirmed that the loading of Sb (Hieda et al., 2008) increased H<sub>2</sub> responses of pr-SnO<sub>2</sub> powders synthesized by ultrasonic spray pyrolysis employing the PMMA microspheres as a template.

In this study, we synthesized pr-In<sub>2</sub>O<sub>3</sub> powders loaded with and without a noble metal such as Au, Pd, or Pt by ultrasonic spray pyrolysis employing home-made PMMA microspheres (ps: 28, 70, 150 nm) as a template, and their NO<sub>2</sub> sensing properties were examined. On the basis of the results obtained, the effects of the introduction of well-developed porous structure into the spherical In<sub>2</sub>O<sub>3</sub> powders and the loading of the noble metal to the In<sub>2</sub>O<sub>3</sub> surface on their NO<sub>2</sub> sensing properties were discussed.

## EXPERIMENTAL

### Synthesis of PMMA Microspheres

PMMA microspheres were synthesized by ultrasonic-assisted emulsion polymerization. Methyl methacrylate monomer (MMA; Wako Pure Chem. Ind., Ltd., 150 cm<sup>3</sup>) was washed with 0.05 M NaOH aqueous solution (1 dm<sup>3</sup>) for three times, to remove a polymerization inhibitor from the MMA monomer. The pure MMA monomer obtained (8 g), sodium lauryl sulfate (SLS; Nacalai Tesque, Inc., 0.1 or 0.5 g) as a surfactant and ammonium persulfate (Wako Pure Chem. Ind., 0.3 g) as an initiator were added to deionized water (100 cm<sup>3</sup>), and then the resultant oil/water (o/w) emulsion was ultrasonically treated by an ultrasonic homogenizer (Nissei Corp., US-150T, 19.5 ± 1 kHz). The polymerization of MMA to PMMA was initiated in the micelles, just upon the irradiation of strong ultra-sonic wave to the o/w emulsion at RT, and the temperature of the o/w emulsion increased from RT to ca. 65°C within 15 min. After the ultrasonic irradiation for 30 min, the aqueous dispersion containing PMMA microspheres was obtained (Hyodo et al., 2017). The particle-size distribution of the synthesized PMMA microspheres in the aqueous dispersion was measured at 25°C by dynamic light scattering (DLS; Malvern Instrument Ltd., HPPS), and the average particle size of PMMA microspheres in the aqueous dispersion was confirmed as ca. 70 or 28 nm for the additive amount of SLS of 1.0 g or 5.0 g, respectively.

### Preparation of pr-In<sub>2</sub>O<sub>3</sub> Powders by Ultrasonic Spray Pyrolysis

The aqueous dispersion containing PMMA microspheres (37.5 cm<sup>3</sup>) was mixed with 0.05 mol dm<sup>-3</sup> In(NO<sub>3</sub>)<sub>3</sub> aqueous solution (62.5 cm<sup>3</sup>) and the mixture was served as an aqueous precursor solution. In some cases, an appropriate amount of HAuCl<sub>4</sub>, Pd(NO<sub>3</sub>)<sub>2</sub>, or PtCl<sub>4</sub> aqueous solution (0.1 mol dm<sup>-3</sup>) was added to the precursor solution for the loading of Au, Pd, or Pt, respectively. Precursor mists were obtained by ultrasonication of the aqueous precursor solution in a plastic container equipped with a polyethylene thin film at one end, which was perpendicularly set over an ultrasonic vibrator (Honda Electric Co., Ltd., HM-303 N, 2.4 MHz) at a distance of 0.5–1.0 cm in water. A specially designed mist-supplier for the ultrasonic-spray pyrolysis was used to get uniform mists of the precursor solution (Hyodo et al., 2017). Only small droplets separated in a glass vessel were fed into an electric furnace heated at 1,000°C under flowing air (1,500 cm<sup>3</sup> min<sup>-1</sup>). As the mists were momentarily heated at the electric furnace, the evaporation of water and the thermal decomposition of In(NO<sub>3</sub>)<sub>3</sub> and PMMA microspheres simultaneously happened and spherical indium oxide powders are produced in the electric furnace under the air flow. The detail of the ultrasonic spray pyrolysis was already reported in our previous paper (Hyodo et al., 2017). The obtained porous powders loaded with and without noble metal were denoted as M(*m*)/pr-In<sub>2</sub>O<sub>3</sub>(*n*) and pr-In<sub>2</sub>O<sub>3</sub>(*n*) [M: the kind of noble metal, *m*: the loading amount of M (wt%), *n*: the diameter of PMMA microspheres (nm)], respectively. The microstructure of these powders was observed by scanning electron microscopy (SEM; JEOL Ltd., JSM-7500F) and transmission electron microscopy

(TEM; JEOL Ltd., JEM2010). The pore-size distribution and specific surface area (SSA) of these powders were measured by Barrett–Joyner–Halenda (BJH) and Brunauer–Emmett–Teller (BET) methods using N<sub>2</sub> adsorption-desorption isotherms (Micromeritics Instrument Corp., Tristar3000), respectively. Crystal phase of these powders was characterized by X-ray diffraction analysis (XRD; Rigaku Corp., RINT2200) using Cu K $\alpha$  radiation (40 kV, 40 mA), and their crystallite size (CS) was calculated from the (222) diffraction peak using Scherrer equation. Chemical state of the surface of these powders was characterized by X-ray photoelectron spectroscopy using Al K $\alpha$  radiation (XPS, Kratos Analytical Ltd., Axis Ultra DLD), and the binding energy was calibrated by using the C1s level (285.0 eV) from usual contamination.

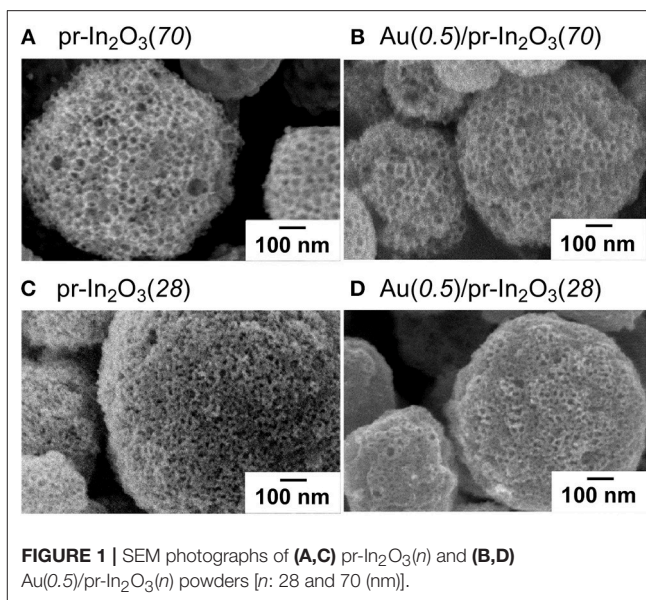
## Fabrication of Thick Film Sensors and Measurement of Their Gas Sensing Properties

The fabricated In<sub>2</sub>O<sub>3</sub>-based powder was mixed with an appropriate amount of  $\alpha$ -terpineol (generally, powder:  $\alpha$ -terpineol = 1: 2, in weight), and the obtained paste was screen-printed onto an alumina substrate equipped with a pair of interdigitated Pt electrodes (gap size: ca. 200  $\mu$ m), followed by drying at 100°C. In some cases, this paste was laminated three times to increase the thickness of the sensing layer, while the paste containing the larger amount of  $\alpha$ -terpineol (weight ratio: 1:5 or 1:10) was also prepared to decrease the thickness of the sensing layer. Then, they are calcined at 550°C for 5 h in ambient air. Gas responses of these sensors were measured to 0.025, 0.25, 1.0, and 5.0 ppm NO<sub>2</sub> balanced with dry air at a flow rate of 100 cm<sup>3</sup> min<sup>-1</sup> at 25–500°C. The magnitude of response to NO<sub>2</sub> was defined as the ratio ( $R_g/R_a$ ) of resistance in NO<sub>2</sub> balanced with air ( $R_g$ ) to that in air ( $R_a$ ). The obtained sensors were denoted as pr-In<sub>2</sub>O<sub>3</sub>( $n$ )- $t$  or M( $m$ )/pr-In<sub>2</sub>O<sub>3</sub>( $n$ )- $t$  [ $t$ : thickness of the sensing layer ( $\mu$ m)].

## RESULTS AND DISCUSSION

### Characterizations of pr-In<sub>2</sub>O<sub>3</sub>( $n$ ) and M( $m$ )/pr-In<sub>2</sub>O<sub>3</sub>( $n$ ) Powders and Their NO<sub>2</sub> Sensing Properties

**Figure 1** shows SEM photographs of representative pr-In<sub>2</sub>O<sub>3</sub>( $n$ ) and M( $m$ )/pr-In<sub>2</sub>O<sub>3</sub>( $n$ ) powders. All the In<sub>2</sub>O<sub>3</sub>-based particles were spherical with well-developed homogenous porous structures on the surface, due to the thermal decomposition of the PMMA microspheres. The pore size of the pr-In<sub>2</sub>O<sub>3</sub>(70) powder was larger than that of the pr-In<sub>2</sub>O<sub>3</sub>(28) powder, and the observed pore structure was unchanged by the loading of Au. **Supplementary Figures 1, 2** show their XRD patterns and pore-size distributions, respectively. **Table 1** summarizes crystallite sizes (CSs) calculated from their XRD spectra, most frequent values of diameter (mode diameters) of pores in pore-size distributions calculated from N<sub>2</sub> adsorption and desorption isotherms, and specific surface areas (SSAs) of pr-In<sub>2</sub>O<sub>3</sub>( $n$ ) and Au(0.5)/pr-In<sub>2</sub>O<sub>3</sub>( $n$ ) powders. All the powders were assigned to cubic In<sub>2</sub>O<sub>3</sub> and the CS of the pr-In<sub>2</sub>O<sub>3</sub>(70)



powder was larger than that of the pr-In<sub>2</sub>O<sub>3</sub>(28) powder. In addition, the pore diameter of the pr-In<sub>2</sub>O<sub>3</sub>(70) powder was also larger than that of the pr-In<sub>2</sub>O<sub>3</sub>(28) powder. For details, the pore diameter calculated from N<sub>2</sub> adsorption isotherm of the pr-In<sub>2</sub>O<sub>3</sub>(70) powder (ca. 80 nm) was much larger than that of the pr-In<sub>2</sub>O<sub>3</sub>(28) powder (ca. 30 nm), while the pore diameter calculated from N<sub>2</sub> desorption isotherm of the pr-In<sub>2</sub>O<sub>3</sub>(70) powder (ca. 30 nm) was slightly larger than the that of the pr-In<sub>2</sub>O<sub>3</sub>(28) powder (ca. 22 nm). Generally, the difference between pore diameters calculated from N<sub>2</sub> adsorption and desorption isotherms arises from the ink-bottle porous morphology of both the pr-In<sub>2</sub>O<sub>3</sub>( $n$ ) powders. Therefore, the pore diameter calculated from N<sub>2</sub> desorption isotherm reflects the width of the necks formed between the spherical pores, and the one calculated from N<sub>2</sub> adsorption isotherm reflects the diameter of spherical pores, which originates from the morphology of PMMA microspheres as a template. Actually, the size of pores on the surface of both the pr-In<sub>2</sub>O<sub>3</sub>( $n$ ) powders was quite similar to the pore diameter calculated from N<sub>2</sub> adsorption isotherm. Furthermore, the loading of Au hardly affected the values of their SSA and CS as well as their pore-size distributions, and the XRD peaks derived from Au were not confirmed in XRD spectra of the Au(0.5)/pr-In<sub>2</sub>O<sub>3</sub>( $n$ ) powders. The porous morphology on the surface of both the Au(0.5)/pr-In<sub>2</sub>O<sub>3</sub>( $n$ ) powders was also comparable to that of both the pr-In<sub>2</sub>O<sub>3</sub>( $n$ ) powders. These results indicate that Au could be highly dispersed in the Au(0.5)/pr-In<sub>2</sub>O<sub>3</sub>( $n$ ) powders.

**Figure 2** shows variations in response of the pr-In<sub>2</sub>O<sub>3</sub>(70)-20 and the M(0.5)/pr-In<sub>2</sub>O<sub>3</sub>(70)-20 sensors (M: Au, Pd, Pt) to 1 and 5 ppm NO<sub>2</sub> in dry air with operating temperature. **Supplementary Figure 3** shows their typical response transients. The magnitude of response of these sensors increased with a decrease in the operating temperatures, regardless of NO<sub>2</sub> concentration. The loading of Pd to pr-In<sub>2</sub>O<sub>3</sub>(70) was hardly effective in improving the NO<sub>2</sub> response and the loading of Pt



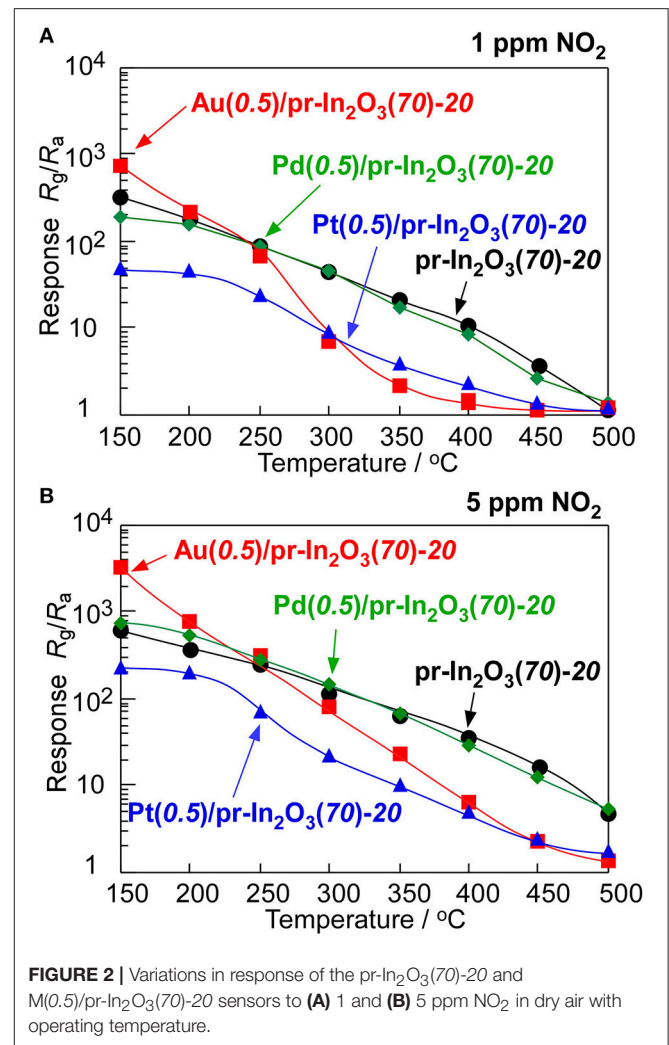
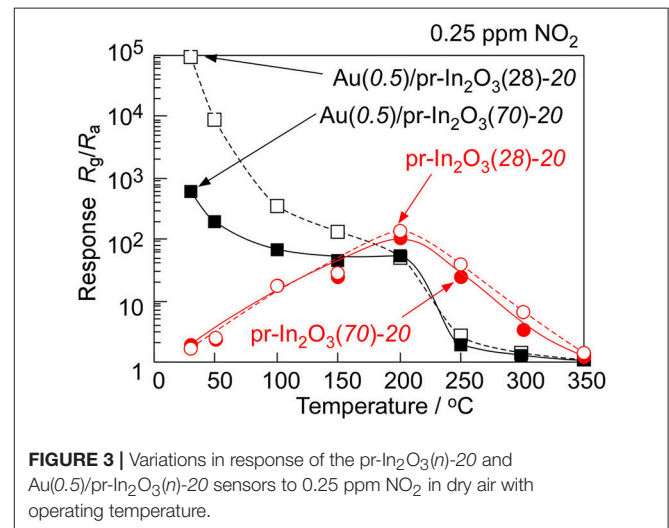
**TABLE 1** | Comparison of crystallite size (CS), pore diameter, and specific surface area (SSA) of the pr-In<sub>2</sub>O<sub>3</sub>(*n*), and Au(0.5)/pr-In<sub>2</sub>O<sub>3</sub>(*n*) powders.

| Sensor   | CS/nm | Pore diameter*/nm |            | SSA/m <sup>2</sup> g <sup>-1</sup> |
|--|-------|-------------------|------------|------------------------------------|
|  |       | Adsorption        | Desorption |                                    |
| pr-In <sub>2</sub> O <sub>3</sub> (70)         | 14.5  | 80                | 30         | 26.6                               |
| Au(0.5)/pr-In <sub>2</sub> O <sub>3</sub> (70) | 14.2  | 70                | 30         | 23.7                               |
| pr-In <sub>2</sub> O <sub>3</sub> (28)         | 12.9  | 30                | 22         | 37.8                               |
| Au(0.5)/pr-In <sub>2</sub> O <sub>3</sub> (28) | 12.9  | 30                | 22         | 34.3                               |

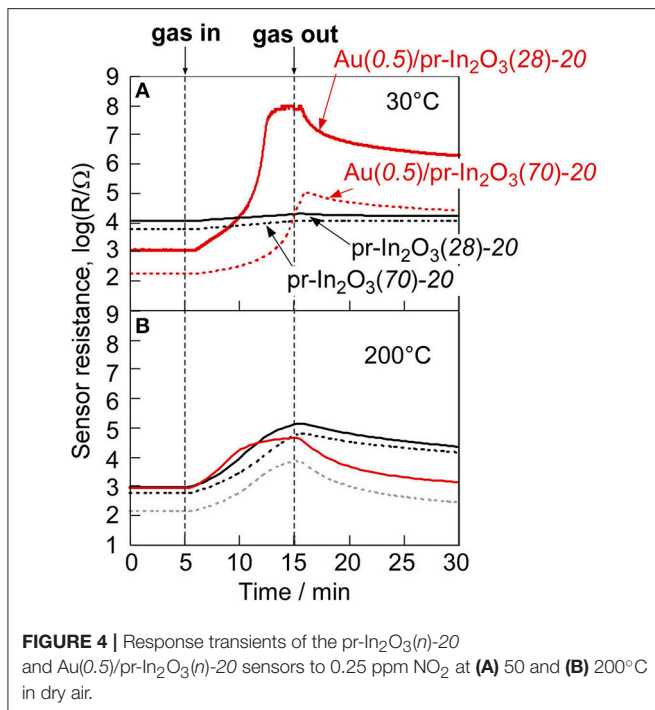
\*Mode diameter obtained from N<sub>2</sub> adsorption and desorption isotherms.

to pr-In<sub>2</sub>O<sub>3</sub>(70) had negative effect on the NO<sub>2</sub> response in the whole operating temperature range examined. On the other hand, the loading of Au increased the NO<sub>2</sub> response especially at lower temperatures ( $\leq 200^\circ\text{C}$ ), even though the NO<sub>2</sub> response of the Au(0.5)/pr-In<sub>2</sub>O<sub>3</sub>(70)-20 sensor was much smaller than that of the pr-In<sub>2</sub>O<sub>3</sub>(70)-20 sensor at higher temperatures of more than 300°C. In addition, the Au(0.5)/pr-In<sub>2</sub>O<sub>3</sub>(70)-20 sensor showed faster recovery speed at lower temperatures ( $\leq 300^\circ\text{C}$ ) than that of the pr-In<sub>2</sub>O<sub>3</sub>(70)-20 sensor. The loading of Au to pr-In<sub>2</sub>O<sub>3</sub>(70) is found to be effective to improve response properties at lower operating temperatures. Therefore, sensing properties of Au(0.5)/pr-In<sub>2</sub>O<sub>3</sub>(*n*)-20 sensors to further low concentration of NO<sub>2</sub> were evaluated at the lower operating temperatures. **Figure 3** shows variations in response of the pr-In<sub>2</sub>O<sub>3</sub>(*n*)-20 and the Au(0.5)/pr-In<sub>2</sub>O<sub>3</sub>(*n*)-20 sensors (*n*: 28, 70) to 0.25 ppm NO<sub>2</sub> with operating temperature in dry air. **Figure 4** shows response transients of the pr-In<sub>2</sub>O<sub>3</sub>(*n*)-20 and the Au(0.5)/pr-In<sub>2</sub>O<sub>3</sub>(*n*)-20 sensors (*n*: 28, 70) to 0.25 ppm NO<sub>2</sub> in dry air at 30 and 200°C. Both the pr-In<sub>2</sub>O<sub>3</sub>(*n*)-20 sensors showed quite a small response to 0.25 ppm NO<sub>2</sub> at 350°C, but their NO<sub>2</sub> response increased with a decrease in the operating temperature at 200–350°C. However, the NO<sub>2</sub> response of the pr-In<sub>2</sub>O<sub>3</sub>(*n*)-20 sensors decreased with a decrease in operating temperature at  $< 200^\circ\text{C}$ . In addition, the NO<sub>2</sub> response of the pr-In<sub>2</sub>O<sub>3</sub>(28)-20 sensor was comparable to that of the pr-In<sub>2</sub>O<sub>3</sub>(70)-20 sensor in the entire examined temperature range. On the other hand, the NO<sub>2</sub> responses of the Au(0.5)/pr-In<sub>2</sub>O<sub>3</sub>(*n*)-20 sensors increased with a decrease in operating temperatures, and especially they were much larger than those of the pr-In<sub>2</sub>O<sub>3</sub>(*n*)-20 sensors at  $< 150^\circ\text{C}$ . These results indicate that the loading of 0.5 wt% Au was effective in improving the NO<sub>2</sub> response, only at lower temperatures. In addition, the NO<sub>2</sub> response of the Au(0.5)/pr-In<sub>2</sub>O<sub>3</sub>(28)-20 sensor was much larger than that of the Au(0.5)/pr-In<sub>2</sub>O<sub>3</sub>(70)-20 sensor at the lower temperatures, and the Au(0.5)/pr-In<sub>2</sub>O<sub>3</sub>(28) sensor showed the largest NO<sub>2</sub> response (ca.  $1 \times 10^5$ ) at 30°C among the sensors. On the other hand, the response speed of these sensors at 30°C was much slower than that at 200°C, and their resistance did not recover to their original values.

**Figure 5** shows variations in response of the Au(*m*)/pr-In<sub>2</sub>O<sub>3</sub>(28)-20 sensors (*m*: 1.0, 1.5, 2.0, 5.0) to 0.25 ppm NO<sub>2</sub> in dry air with operating temperature in order to examine the effects of the loading amount of Au. **Figure 6** shows response transients of the Au(*m*)/pr-In<sub>2</sub>O<sub>3</sub>(28)-20 sensors (*m*: 1.0, 1.5, 2.0, 5.0) to

**FIGURE 2** | Variations in response of the pr-In<sub>2</sub>O<sub>3</sub>(70)-20 and M(0.5)/pr-In<sub>2</sub>O<sub>3</sub>(70)-20 sensors to (A) 1 and (B) 5 ppm NO<sub>2</sub> in dry air with operating temperature.**FIGURE 3** | Variations in response of the pr-In<sub>2</sub>O<sub>3</sub>(*n*)-20 and Au(0.5)/pr-In<sub>2</sub>O<sub>3</sub>(*n*)-20 sensors to 0.25 ppm NO<sub>2</sub> in dry air with operating temperature.

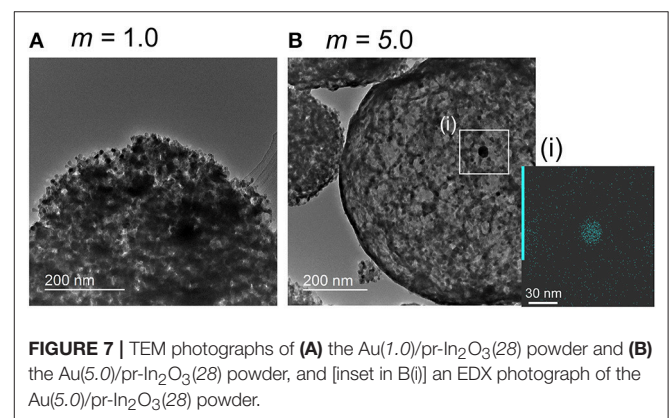
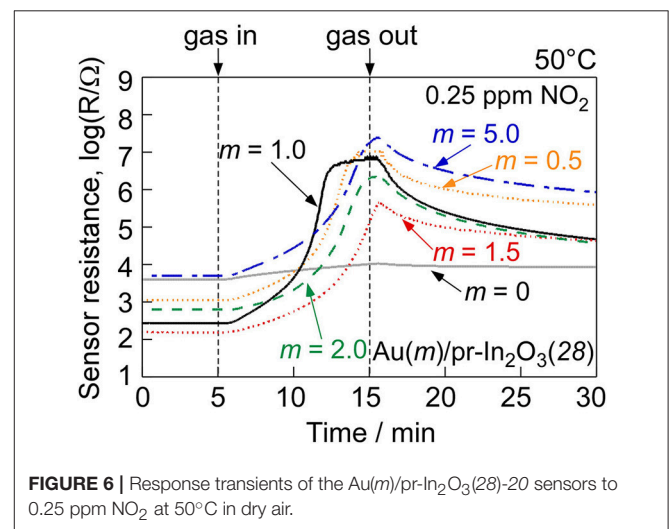
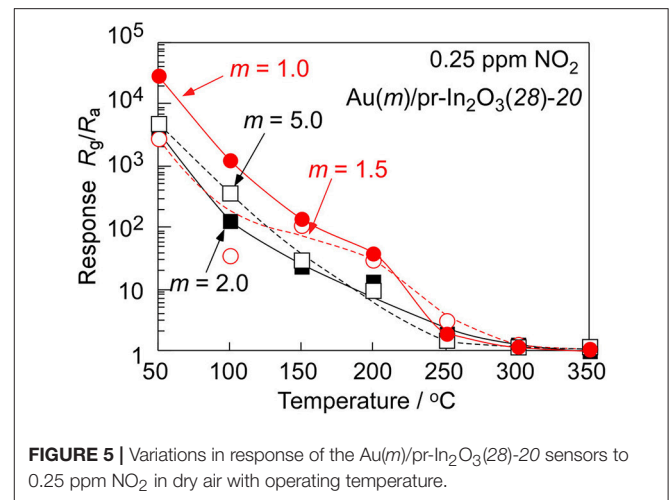
0.25 ppm NO<sub>2</sub> in dry air at 50°C. These Au(*m*)/pr-In<sub>2</sub>O<sub>3</sub>(28)-20 sensors also showed extremely large NO<sub>2</sub> responses at 30°C, as is the case with the Au(0.5)/pr-In<sub>2</sub>O<sub>3</sub>(28)-20 sensor, but the



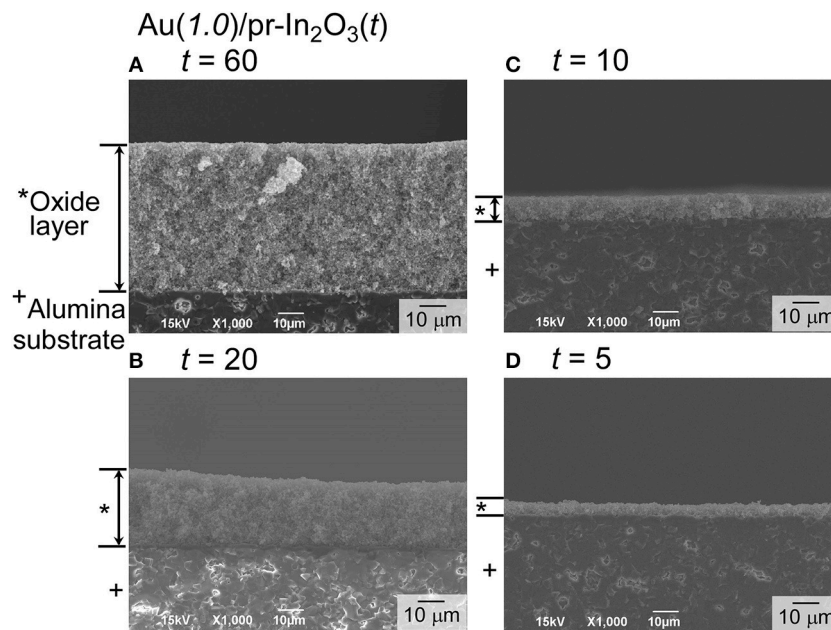
resistance values of these sensors in 0.25 ppm NO<sub>2</sub> were as large as 10<sup>9</sup> Ω, which is beyond the limitation of our measurement setup. Thus, we did not obtain correct response values at 30°C. The NO<sub>2</sub> response of all the Au(*m*)/pr-In<sub>2</sub>O<sub>3</sub>(28)-20 sensors increased with a decrease in the operating temperature, and the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28)-20 sensor showed the largest NO<sub>2</sub> response among them. All the Au(*m*)/pr-In<sub>2</sub>O<sub>3</sub>(28)-20 sensors showed quite slow response behavior. The resistance of the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28)-20 sensor most swiftly increased upon exposure to NO<sub>2</sub> and it reached a constant value, just like that of the Au(0.5)/pr-In<sub>2</sub>O<sub>3</sub>(28)-20 sensor. However, the resistance of other Au(*m*)/pr-In<sub>2</sub>O<sub>3</sub>(28)-20 sensors (*m*: 1.5, 2.0, 5.0) did not reach a constant value during the exposure period of NO<sub>2</sub> (10 min), which indicates that too large loading of Au (*m*: 1.5, 2.0, 5.0) slowed down the response speed to 0.25 ppm NO<sub>2</sub> in air.

### Effects of the Au Loading to pr-In<sub>2</sub>O<sub>3</sub>(*n*) Powders on the NO<sub>2</sub> Sensing Properties

The In<sub>2</sub>O<sub>3</sub>-based sensors generally respond to NO<sub>2</sub> since NO<sub>2</sub> molecules are negatively adsorbed on the oxide surface (Roso et al., 2017). The magnitude of NO<sub>2</sub> response of the pr-In<sub>2</sub>O<sub>3</sub>(*n*)-20 sensors was increased by the loading of a small amount of Au as shown in the previous section, which indicates that the highly dispersed Au nanoparticles loaded enhanced the amount of negatively charged NO<sub>2</sub> adsorbed on the oxide surface. Several researchers also reported an increase in the NO<sub>2</sub> response of the semiconductor-type gas sensors by Au loading onto the metal oxides, and they suggested an increase in the adsorption amount of NO<sub>2</sub> as a result of spillover effects (Choi et al., 2011; Mun et al., 2013; Shim et al., 2013). In addition, the Au(*m*)/pr-In<sub>2</sub>O<sub>3</sub>(28)-20 (*m*: 0.5, 1.0) sensors showed rather larger NO<sub>2</sub> response than the Au(*m*)/pr-In<sub>2</sub>O<sub>3</sub>(28)-20 (*m*: 1.5, 2.0, 5.0) sensors.



**Supplementary Figure 4** shows XRD patterns of the Au(*m*)/pr-In<sub>2</sub>O<sub>3</sub>(28) powders (*m*: 1.0, 5.0). The both powders were assigned to cubic In<sub>2</sub>O<sub>3</sub>, and a small amount of Au was detected in the Au(5.0)/pr-In<sub>2</sub>O<sub>3</sub>(28) powder. **Supplementary Figure 5** shows XPS spectra of In3d and Au4f of the pr-In<sub>2</sub>O<sub>3</sub>(28) and the Au(*m*)/pr-In<sub>2</sub>O<sub>3</sub>(28) powders (*m*: 1.0, 5.0). Two peaks

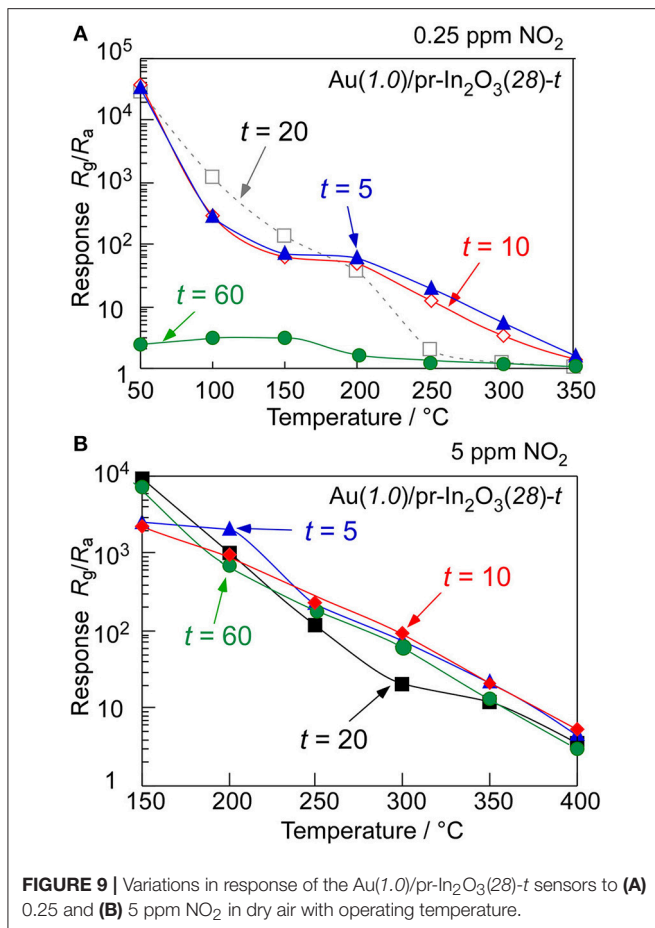


**FIGURE 8** | Cross-sectional views of the sensing layers of the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(70)-*t* sensors [*t*: (A) 60, (B) 20, (C) 10, and (D) 5 (μm)]. The weight ratio between the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28) powder and α-terpineol was 1:2 (*t*: 20 and 60), 1:5 (*t*: 10), 1:10 (*t*: 5). The paste for the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(70)-60 sensor was laminated three times to obtain the thickest sensing layer.

corresponding to In3d<sub>5/2</sub> (e.g., ca. 444.7, 444.7, and 444.8 eV for the pr-In<sub>2</sub>O<sub>3</sub>(28), the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28), and the Au(5.0)/pr-In<sub>2</sub>O<sub>3</sub>(28), respectively) and In3d<sub>3/2</sub> (e.g., ca. 452.2, 452.2, and 452.3 eV for the pr-In<sub>2</sub>O<sub>3</sub>(28), the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28), and the Au(5.0)/pr-In<sub>2</sub>O<sub>3</sub>(28), respectively) were observed, and all the In3d peaks indicate the chemical state of In<sup>3+</sup> (Atashbar et al., 1999; Wu et al., 2003). In addition, two peaks corresponding to Au4f<sub>7/2</sub> [e.g., ca. 83.9 eV for the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28) and the Au(5.0)/pr-In<sub>2</sub>O<sub>3</sub>(28)] and Au4f<sub>5/2</sub> [e.g., ca. 87.6 eV for the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28), and the Au(5.0)/pr-In<sub>2</sub>O<sub>3</sub>(28)] showed the chemical state of Au loaded on the pr-In<sub>2</sub>O<sub>3</sub> was metal (Seah et al., 1998; Liu et al., 2012). **Supplementary figure 6** shows SEM photographs and pore-size distributions of the Au(*m*)/pr-In<sub>2</sub>O<sub>3</sub>(28) powders (*m*: 1.0, 5.0). Well-developed spherical pores were observed on the surface of the both powders. The mode diameter in pore-size distribution calculated from the N<sub>2</sub> desorption isotherm of the Au(5.0)/pr-In<sub>2</sub>O<sub>3</sub>(28) powders was ca. 18 nm, which was smaller than those of the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28) powders (ca. 22 nm) and the Au(0.5)/pr-In<sub>2</sub>O<sub>3</sub>(28) powders (ca. 22 nm, **Table 1**). In addition, the SSA of the Au(5.0)/pr-In<sub>2</sub>O<sub>3</sub>(28) powders (33.1 m<sup>2</sup>/g) was smaller than that of the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28) powders (36.9 m<sup>2</sup>/g). Considering the SSA values of all the Au(*m*)/pr-In<sub>2</sub>O<sub>3</sub>(28) powders and the magnitude of NO<sub>2</sub> responses of all the Au(*m*)/pr-In<sub>2</sub>O<sub>3</sub>(28) sensors, the increase in the SSA was obviously effective in enhancing the NO<sub>2</sub> responses. **Figure 7** shows TEM images of the Au(*m*)/pr-In<sub>2</sub>O<sub>3</sub>(28) powders (*m*: 1.0, 5.0), together with an EDX image of Au in the Au(5.0)/pr-In<sub>2</sub>O<sub>3</sub>(28) powders. The TEM photographs showed that the Au loaded was highly dispersed in both the Au(*m*)/pr-In<sub>2</sub>O<sub>3</sub>(28) particles, while a quite large

Au agglomerate with a diameter of ca. 22 nm was also observed in a Au(5.0)/pr-In<sub>2</sub>O<sub>3</sub>(28) particle (particle (**Figure 7Bi**)). This result suggests the 5 wt% loading of Au exceeds the limit for the well-dispersion of Au on the pr-In<sub>2</sub>O<sub>3</sub> surface. In addition, the resistance of the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28)-20 sensor in air was much smaller than that of the pr-In<sub>2</sub>O<sub>3</sub>(28)-20 sensor, while the resistance of the Au(5.0)/pr-In<sub>2</sub>O<sub>3</sub>(28)-20 sensor in air was comparable with that of the pr-In<sub>2</sub>O<sub>3</sub>(28)-20 sensor (**Figure 6**). Subramanian et al., revealed the size of Au nanoparticles largely affects the flat band potential of Au/TiO<sub>2</sub>. They reported that the loading of 3-nm-diameter Au nanoparticles on TiO<sub>2</sub> induced a greater negative shift in flat band potential than that of 8-nm-diameter Au nanoparticles. Therefore, the size of the Au nanoparticles possibly affects the number of free electrons and thus decrease the resistance of the Au(*m*)/pr-In<sub>2</sub>O<sub>3</sub>(28)-20 sensors in air. The lower resistance of the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28) sensor in air is one of advantages to detect the oxidizing gases such as NO<sub>2</sub>, because the resistance increases by the negatively adsorption of NO<sub>2</sub>. Furthermore, the response of semiconductor-type gas sensors arises from the resistance change at the bottom part of the sensing layer between interdigitated Pt electrodes. Therefore, the NO<sub>2</sub> adsorption on the oxide surface at the upper part of the sensing layer decreases the effective concentration of NO<sub>2</sub> at the bottom part of the sensing layer at the initial process of the NO<sub>2</sub> response, and thus it brings a large delay to reach the maximum concentration (e.g., ca. 0.25 ppm in **Figure 6**) of NO<sub>2</sub>. Especially, the Au(5.0)/pr-In<sub>2</sub>O<sub>3</sub>(28)-20 sensor didn't reach to the steady-state value during the NO<sub>2</sub> exposure in this study, while the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28)-20 sensor reached to the almost constant value. This results showed the larger adsorption amount

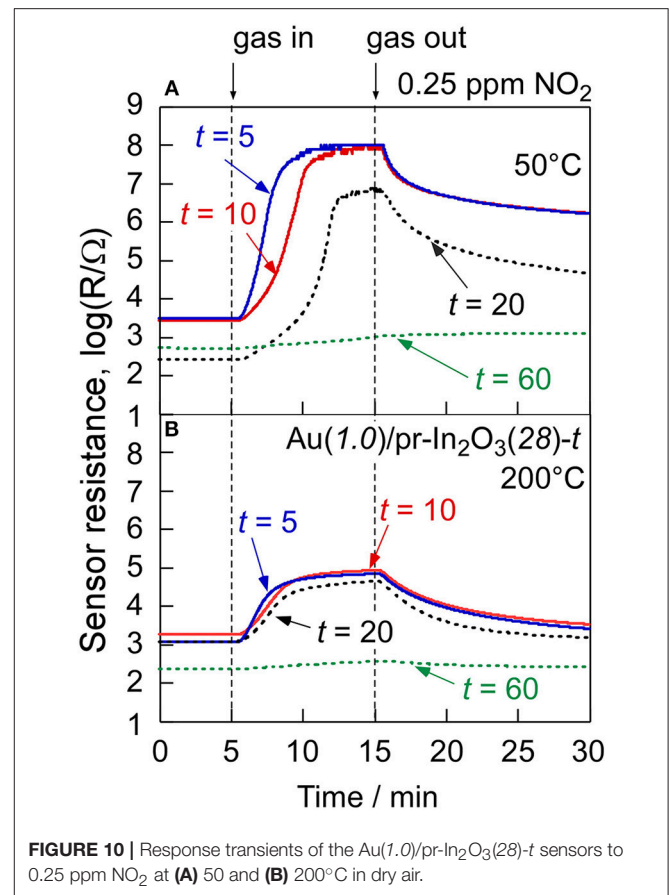




**FIGURE 9** | Variations in response of the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28)- $t$  sensors to (A) 0.25 and (B) 5 ppm NO<sub>2</sub> in dry air with operating temperature.

of NO<sub>2</sub> on the surface of the sensing layer of the Au(5.0)/pr-In<sub>2</sub>O<sub>3</sub>(28)-20 sensor than that of the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28)-20 sensor, leading to a decrease in the NO<sub>2</sub> response. As a result, these facts suggest that the 1.0 wt% of Au loading on the pr-In<sub>2</sub>O<sub>3</sub> was the most effective in increasing the amount of NO<sub>2</sub> adsorbed on the bottom part of the sensing layer among the sensors. In addition, the response speed of the Au(0.5)/pr-In<sub>2</sub>O<sub>3</sub>(70)-20 sensor was much slower than that of the Au(0.5)/pr-In<sub>2</sub>O<sub>3</sub>(28)-20 sensor at 30°C, probably due to facile gas diffusion of the Au(0.5)/pr-In<sub>2</sub>O<sub>3</sub>(28)-20 sensor. Introducing the pores using the PMMA microspheres as a template improves gas diffusion from the surface part to the bottom part of the sensing layer. In addition, the sensing layer of the Au(0.5)/pr-In<sub>2</sub>O<sub>3</sub>(28)-20 sensor contains larger number of pores than that of the Au(0.5)/pr-In<sub>2</sub>O<sub>3</sub>(70)-20 sensor. This is because the PMMA microspheres were polymerized by using the same weight of MMA, and thus the concentration of PMMA microspheres (ps: 28 nm) in the precursor solution of ultrasonic spray pyrolysis was higher than that of the ones (ps: 70 nm). Therefore, the gases rapidly diffused to the whole sensing layer of the Au(0.5)/pr-In<sub>2</sub>O<sub>3</sub>(28)-20 sensor, leading to the faster response speed.

On the other hand, the NO<sub>2</sub> response of the pr-In<sub>2</sub>O<sub>3</sub>(70)-20 sensor was largely decreased by the small loading amount of Au at the higher temperatures ( $\geq 300^\circ\text{C}$ ) (Figure 2). Generally, the given amount of NO<sub>2</sub> partially converts to NO, especially at

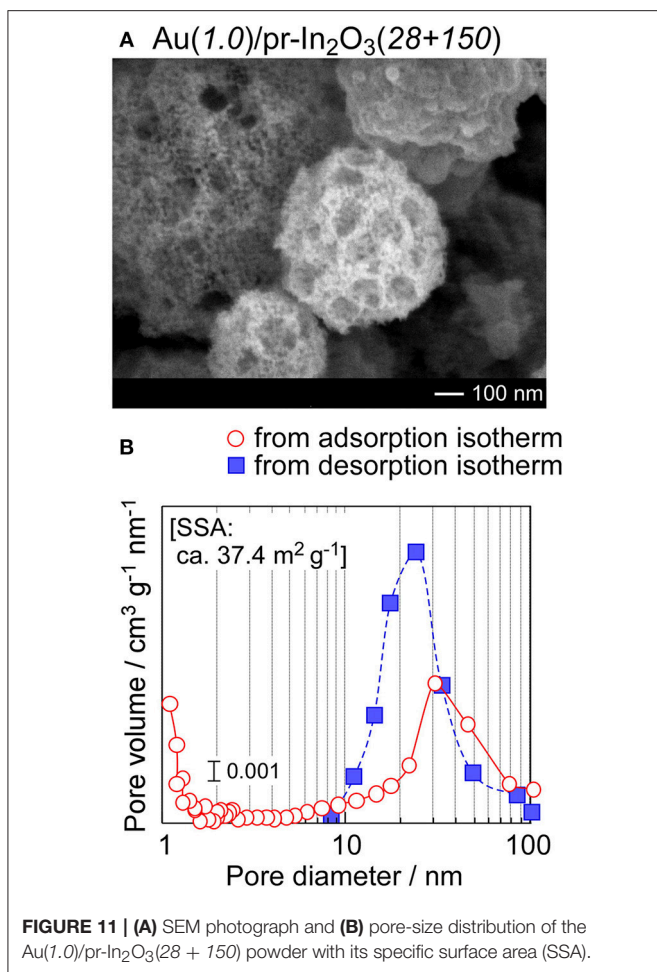


**FIGURE 10** | Response transients of the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28)- $t$  sensors to 0.25 ppm NO<sub>2</sub> at (A) 50 and (B) 200°C in dry air.

more than 200°C, and the ratio of conversion increased with an increase in the temperature (Miura et al., 2007; Kim et al., 2010). Therefore, the loading of Au onto the In<sub>2</sub>O<sub>3</sub> surface increased the decomposition efficiency from NO<sub>2</sub> to NO, leading to a reduction of the effective concentration of NO<sub>2</sub> at the bottom part of the sensing layer and a decrease in the NO<sub>2</sub> response of the sensor.

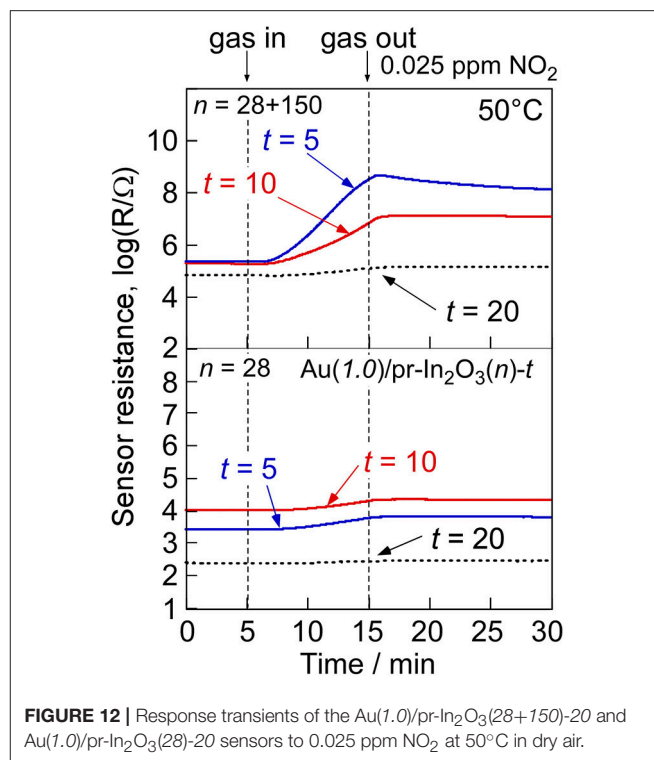
## NO<sub>2</sub> Sensing Properties of Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28)- $t$ Sensors

In order to understand effects of the Au loading, the NO<sub>2</sub>-sensing properties of the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28)- $t$  sensors ( $t$ : 5, 10, 60) were also examined. Figure 8 shows cross-sectional SEM photographs of the sensing layers of the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28)- $t$  ( $t$ : 5, 10, 20, 60) sensors, together with their thickness. Figure 9 shows variations in response of these sensors to 0.25 and 5 ppm NO<sub>2</sub> in dry air with operating temperature, together with that of the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28)-20 sensor. Figure 10 shows response transients of all these sensors to 0.25 ppm NO<sub>2</sub> in dry air at 50 and 200°C. The response of all the sensors to NO<sub>2</sub> increased with a decrease in the operating temperature, whereas only the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28)-60 sensor showed much smaller response only to 0.25 ppm NO<sub>2</sub> than others. The response speed of these sensors to NO<sub>2</sub> increased with a decrease in the thickness of the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28)- $t$  sensors, especially at 50°C. Among them, note that the response speed of the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28)-5 sensor was faster than that of the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28)-10



sensor, even though the magnitude of NO<sub>2</sub> response and the recovery speed of the both sensors were quite comparable to each other. This trend is understandable by a decrease in the NO<sub>2</sub> diffusion time from the surface part to the bottom part of the sensing layer between interdigitated Pt electrodes. In addition, the smaller NO<sub>2</sub> diffusion may bring the smaller NO<sub>2</sub> response, especially for the detection of lower concentration of NO<sub>2</sub>, because the effective concentration of NO<sub>2</sub> at the bottom part of the sensing layer won't change for a long time by the adsorption of NO<sub>2</sub> on the surface of the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28) during gas diffusion. The sensing properties to lower concentration of NO<sub>2</sub> at 50°C were examined in the next section.

In addition, the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28)-*t* (*t*: 5, 10) sensors showed larger response to 0.25 ppm NO<sub>2</sub> than that of the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28)-20 sensor at high temperatures more than 200°C. Furthermore, the response and recovery speeds as well as the magnitude of NO<sub>2</sub> response of the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28)-5 sensor were also comparable to those of the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28)-10 sensor at 200°C, because the gas-diffusion rate at 200°C was much higher than that at 50°C and thus the effects of thickness of the sensing layers on the NO<sub>2</sub>-sensing properties were decreased. On the other hand, the decrease in the response to a low concentration of NO<sub>2</sub> (0.25 ppm) with an increase



in the thickness of the sensing layers at more than 200°C is probably due to the decomposition of NO<sub>2</sub> in the sensing layer and thus the decrease in the effective concentration of NO<sub>2</sub> at the bottom part of the sensing layer. Since the increase in the thickness of the sensing layer increased the decomposition efficiency from NO<sub>2</sub> to NO to reduce the effective concentration of NO<sub>2</sub> at the bottom part of the sensing layer at more than 200°C, the NO<sub>2</sub> response of the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28)-*t* sensors decreased with an increase in the thickness of the sensing layer in the temperature range. However, the catalytic activity of the decomposition of NO<sub>2</sub> to NO over the oxide surface in air is not so high. Therefore, a decrease in the effective concentration of NO<sub>2</sub> at higher concentration (5 ppm) on the basis of the catalytic decomposition of NO<sub>2</sub> to NO is not significant to a decrease in the NO<sub>2</sub> response, compared to that at lower concentration (0.25 ppm) as shown in Figure 9.

## NO<sub>2</sub> Sensing Properties of Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28+150)-*t* Sensors

Easy gas diffusion of NO<sub>2</sub> from the oxide surface to the bottom part of the sensing layer enhances the NO<sub>2</sub> response and the response speed at low operating temperatures. Thus, the introduction of much larger pores has been attempted into the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28) powder. Commercial PMMA microspheres with a diameter of ca. 150 nm (Soken Chem. & Eng. Co. Ltd., MP-1451) were mixed into the precursor solution containing homemade PMMA microspheres with a diameter of ca. 28 nm, and then 1.0 wt% Au-loaded pr-In<sub>2</sub>O<sub>3</sub> powder with two kinds of spherical pores (Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28+150) powders) were prepared by ultrasonic spray



pyrolysis. **Figure 11** shows an SEM photograph and pore-size distribution of the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28+150) powder with its SSA. The SEM photograph shows that both macropores (80–100 nm in diameter) and mesopores (20–30 nm in diameter) are well developed in the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28+150) powder. The existence of the macropores was also confirmed in the pore-size distribution calculated from N<sub>2</sub> adsorption isotherm in a diameter range of 80–100 nm. These results strongly support that the macropores were based on the commercial large PMMA microspheres. On the other hand, the introduction of macropores has little effect on SSA. **Figure 12** shows response transients of the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28)-*t* and Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28+150)-*t* sensors (*t*: 5, 10, 20) to 0.025 ppm NO<sub>2</sub> in dry air at 50°C. The resistance of all the sensors gradually increased upon exposure to the very low concentration of NO<sub>2</sub>, and the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28+150)-*t* sensors showed larger NO<sub>2</sub> response than those of the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28)-*t* sensors. In addition, a decrease in the thickness of the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28+150)-*t* sensors increased the NO<sub>2</sub> response. Among them, the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28+150)-5 sensor showed the largest NO<sub>2</sub> response. This is because the introduction of the well-developed macropores improves the gas diffusion from the surface to the bottom part of the sensing layer and increases the effective concentration of NO<sub>2</sub> at the bottom part of the sensing layer. Therefore, it was confirmed that the smaller NO<sub>2</sub> diffusion brings the smaller NO<sub>2</sub> response due to the adsorption of NO<sub>2</sub> during gas diffusion, especially for the detection of the lower concentration of NO<sub>2</sub>.

## CONCLUSION

The NO<sub>2</sub> sensing properties of the pr-In<sub>2</sub>O<sub>3</sub> sensors loaded with and without noble metal (Au, Pd, or Pt) were examined, and factors for enhancing the NO<sub>2</sub> sensing properties were discussed. The Au(0.5)/pr-In<sub>2</sub>O<sub>3</sub>(70)-20 sensor showed larger NO<sub>2</sub> response at lower temperatures (≤200°C) than the pr-In<sub>2</sub>O<sub>3</sub>(70)-20 sensor, while the Pd or Pt loading were hardly effective for improving the NO<sub>2</sub> response. The NO<sub>2</sub> response

of the pr-In<sub>2</sub>O<sub>3</sub>(*n*)-20 sensors increased with a decrease in the operating temperature at 200–350°C, but their NO<sub>2</sub> response decreased with a decrease in operating temperature at <200°C. However, the NO<sub>2</sub> response of the Au(0.5)/pr-In<sub>2</sub>O<sub>3</sub>(*n*)-20 sensors increased with a decrease in operating temperature, and the Au(0.5)/pr-In<sub>2</sub>O<sub>3</sub>(28)-20 sensor showed the much larger NO<sub>2</sub> response than that of the Au(0.5)/pr-In<sub>2</sub>O<sub>3</sub>(70)-20 sensor at <150°C. Therefore, we concluded the highly dispersed Au nanoparticles enhance the amount of negatively charged NO<sub>2</sub> adsorbed on the oxide surface.

The Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28)-20 sensor showed the highest NO<sub>2</sub> response among the Au(*m*)/pr-In<sub>2</sub>O<sub>3</sub>(28)-20 sensors. The magnitude of response to 0.25 ppm NO<sub>2</sub> of the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28)-60 sensor was smallest and the response speed of the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28)-5 sensor was fastest among the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28)-*t* sensors at 50°C. In addition, the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28+150)-*t* sensors showed larger NO<sub>2</sub> response than those of the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28)-*t* sensors. A decrease in the thickness of the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28+150)-*t* sensors increased the NO<sub>2</sub> response. Among them, the Au(1.0)/pr-In<sub>2</sub>O<sub>3</sub>(28+150)-5 sensor showed the largest NO<sub>2</sub> response. It was suggested that the introduction of the well-developed macropores improves the gas diffusion from the surface to the bottom part of the sensing layer. And thus, the effective concentration of NO<sub>2</sub> at the bottom part of the sensing layer increased, leading to the large NO<sub>2</sub> response.

## AUTHOR CONTRIBUTIONS

TU, KK, TH, and YS: manuscript writing and results interpretation; KI: experiments.

## SUPPLEMENTARY MATERIAL

The Supplementary Material for this article can be found online at: <https://www.frontiersin.org/articles/10.3389/fmats.2019.00081/full#supplementary-material>

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**Conflict of Interest Statement:** The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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