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A general method to determine the optimal whitecapping dissipation coefficient in the SWAN model

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Whitecapping dissipation is a critical term in affecting the accuracy of wave height modeling. However, the whitecapping dissipation coefficient (C_{ds}), as a primary factor influencing whitecapping, is commonly determined through trial and error in various studies. In this study, we present a general method for calibrating the Simulating Waves Nearshore (SWAN) wave model using the whitecapping dissipation term, demonstrated through a detailed study in the South China Sea (SCS). Theoretical analysis reveals that the optimal C_{ds} value shows a one-to-one correspondence with the applied wind field. Expectedly, under high-quality wind field conditions, the optimal C_{ds} values tend to fall within a narrow range, regardless of the model domain or time span. Numerical experiments executed in the SCS further consolidated this inference, encompassing two common wind input schemes (ST6 and YAN) and three distinct whitecapping dissipation schemes (KOMEN, JANSSEN, and WST). Based on the experimental results, we have identified an optimal C_{ds} range for each whitecapping dissipation scheme. C_{ds} values within the optimal range consistently outperformed the default C_{ds} in the SWAN model. Subsequent experiments verified the method's applicability to the Gulf of Mexico and the Mediterranean Sea. The findings suggest that this research holds substantial promise for practical applications on a global scale.

KEYWORDS

SWAN, whitecapping dissipation coefficient, wind errors, ERA5, SARAL

1 Introduction

In recent decades, the third-generation wave models that can solve the spectral action balance equation without assuming *a priori* spectral shape (The WAMDI Group, 1988; Booij et al., 1999) have been widely developed and applied worldwide (Cavaleri et al., 2020; Shao et al., 2023). Among the terms in the wave action equation,

whitecapping, responsible for energy dissipation in deep water, remains one of the least understood physical aspects (Rogers et al., 2002; Cavaleri et al., 2019). Several whitecapping expressions had been proposed (Hasselmann, 1974; Komen et al., 1984; Janssen, 1992; Banner et al., 2000; Alves and Banner, 2003; Van der Westhuysen et al., 2007). Early whitecapping expressions were adjusted based on closing the energy balance of waves in fully developed conditions, as exemplified in the work of Komen et al. (1984) (hereinafter referred to as the KOMEN expression or KOMEN). Alves and Banner (2003) refined the KOMEN expression based on observations, proposing an expression predominantly reliant on the ratio of azimuthal-integrated spectral saturation to the saturation spectrum. Van der Westhuysen et al. (2007) proposed a novel whitecapping expression based on Alves and Banner (2003) but removed the dependence on mean spectra, increasing its suitability for nearshore applications. The Simulating Waves Nearshore (SWAN) model, one of the prominent representatives of third-generation wave models, provides 6 whitecapping expressions with 19 adjustable parameters (The SWAN team, 2021a).

Whitecapping plays a fundamental role in achieving the correct energy balance and significantly influences the accuracy of wave models (Roland and Arduin, 2014; Cavaleri et al., 2019). Therefore, the selection and tuning of the whitecapping scheme are crucial (Sun et al., 2022). The whitecapping dissipation coefficient (C_{ds}) is a key parameter that integrally controls the whitecapping dissipation, which is not dependent on the wave steepness or the wave number (Sun et al., 2022). Among all the parameters in the whitecapping schemes, C_{ds} is usually used as a tuning parameter in the calibration process (Cavaleri et al., 2018; Cavaleri et al., 2020). Extensive research indicates that suitable schemes and optimal parameters may vary by region or forcing wind field (Shao et al., 2023). For instance, in the Bohai Sea, the KOMEN expression effectively represents the wind-wave characteristics with the C_{ds} of $2.2E-5$ (Lv et al., 2014). Appendini et al. (2013) and Amarouche et al. (2019) improved the model performance using the expression proposed by Janssen (1992) (hereinafter referred to as the JANSSEN expression or JANSSEN) but with entirely different optimal C_{ds} in the Mediterranean Sea (MS). Appendini et al. (2013) achieved the optimal combination of C_{ds} at 1.5 and δ (the coefficient determining the dependence of whitecapping on the wave number) at 0.7, whereas Amarouche et al. (2019) found the optimal C_{ds} to be 1.0. Off the west coast of Norway, the expression proposed by Van der Westhuysen et al. (2007) provided the best performance with mixed swell-wind sea conditions (Van der Westhuysen et al., 2007; Christakos et al., 2021) found that default settings of the whitecapping dissipation scheme commonly led to overestimation of the peak frequency and underestimation of the energy level of the spectral peak during high wind speed conditions. Consequently, wave parameters such as significant wave height (SWH) and mean wave period may be underestimated (Elkut et al., 2021; Umesh and Behera, 2021). Although calibrating the model using C_{ds}

lacks a valid physical basis, as the simulated whitecapping dissipation may not accurately reflect realistic conditions, this approach is widely acknowledged for improving practical wave simulations (Wu et al., 2021; Bujak et al., 2023).

Most wave modeling studies typically involve conducting multiple experiments over a certain range of C_{ds} and determining the optimal C_{ds} based on simulation results (e.g., Akpınar and Ponce de León, 2016; Kutupoğlu et al., 2018; Bingölbali et al., 2019; Sun et al., 2022). Wu et al. (2021) proposed a novel C_{ds} calibration method that requires at least two experiments to determine the optimal C_{ds} . However, this method relies on a fitting formula based on experimental results, inevitably introducing fitting errors. Although both methods can obtain the optimal C_{ds} , they require significant time and computational resources. Therefore, finding a general method to determine the optimal C_{ds} value is necessary. Overall, the accuracy of wave model results, particularly in SWH, is strongly influenced by the forcing wind field and source term parameterization (Cavaleri and Bertotti, 1997; Zhai et al., 2021). The wind field provides positive energy flux to the wave model, while the dissipation term contributes to negative energy flux (Babanin et al., 2010). Thus, there exists a potential relationship between the wind field and C_{ds} . Based on this concept, it is theoretically feasible to calibrate the wave model.

This study aims to propose a general method for determining the optimal C_{ds} to improve the efficiency of wave simulation. The remaining parts of this paper are structured as follows. Section 2 describes the study area and bathymetry data. Section 3 details the primary data and methods, including the basic principle of SWAN, observations, and error metrics. Section 4 presents the theoretical basis of this work. In Section 5, numerical experiments are conducted to explore the characteristics of the optimal C_{ds} . Section 6 discusses the applicability of the conclusions we have obtained to different regions. Finally, Section 7 provides the conclusion.

2 Study area and bathymetry

The study area of this work encompasses the South China Sea (SCS; $104^{\circ}E-124^{\circ}E$, $0^{\circ}-25^{\circ}N$), as delineated by the solid black line box in Figure 1. The SCS is a typical semi-enclosed marine region, connected to the Pacific Ocean and the Indian Ocean through narrow straits or channels (Su et al., 2017; Ou et al., 2018). It features intricate topography, characterized by three distinct elements: the continental shelf that connects to the land, the continental slope at the outer edge of the continental shelf, and the central basin. As depicted in Figure 1, this region is marked by significant variations in water depth, with a maximum depth exceeding 5500 meters and an average depth of approximately 1200 meters. The general pattern is one of shallow waters in the north and south and deeper waters in the central area (Zhang et al., 2020). Given its strategic importance in shipping and trade routes, along with its abundant reserves of oil, natural gas, and fisheries, the SCS holds significant economic and geopolitical value (Wang, 2021).

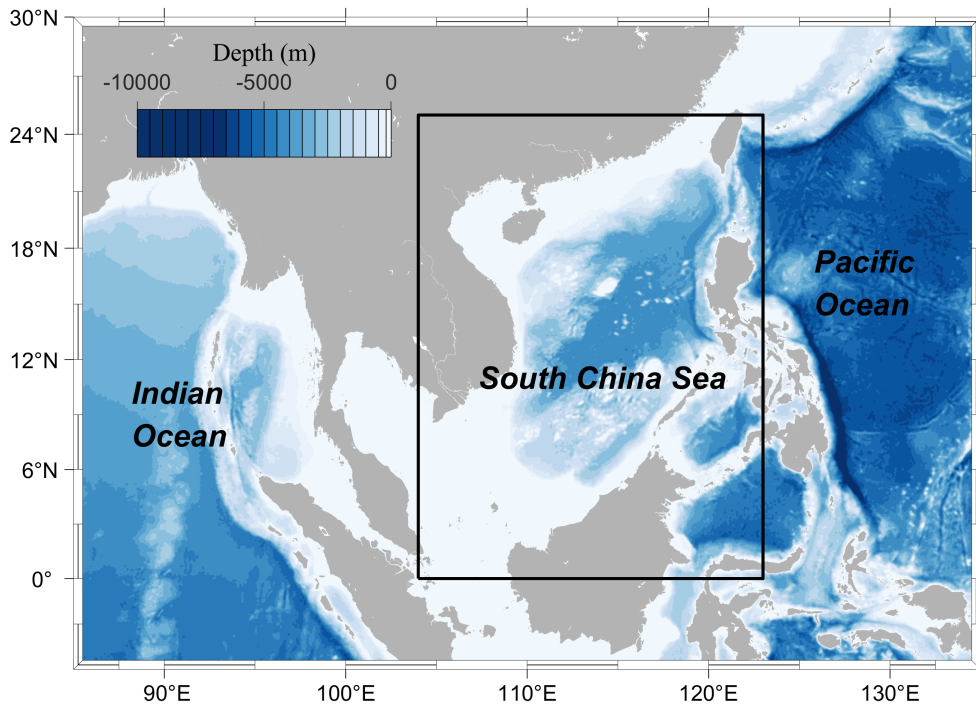


FIGURE 1 Bathymetry map of the study area. The black solid line frame denotes the SCS.

The bathymetry data used in this study was interpolated from the General Bathymetric Chart of the Oceans (GEBCO¹) dataset. The GEBCO is a global terrain model that provides elevation data on a 15-arc-second interval grid with a resolution of almost 0.46 km (Weatherall et al., 2021). Due to its high resolution, GEBCO accurately depicts near-shore and deep-sea terrain, making it widely used in wave simulation (Akpınar et al., 2016; Kutupoğlu et al., 2018; Beyramzade et al., 2019; Sun et al., 2022).

3 Data and methods

3.1 SWAN model description

The third-generation wave model SWAN is developed at the Delft University of Technology (The SWAN team, 2021b). SWAN is well known for its implicit schemes and iteration techniques, which make the model performance more robust and economic, especially in shallow shelf seas. As a third-generation wind-wave model, SWAN computes the rate of change of wave action density (N) as follows

$$\frac{\partial N}{\partial t} + \frac{\partial c_x N}{\partial x} + \frac{\partial c_y N}{\partial y} + \frac{\partial c_\sigma N}{\partial \sigma} + \frac{\partial c_\theta N}{\partial \theta} = \frac{S_{tot}}{\sigma} \tag{1}$$

The first term on the left-hand-side represents the rate of change of N with time, and the second and third terms represent the propagation of waves in geographic space. c_x and c_y are the wave propagation velocities in the zonal and meridional directions respectively. The fourth term represents the shifting of the radian

frequency (σ) due to variations in depth and mean currents. The fifth term denotes the depth-induced and current-induced refraction in wave propagation direction (θ). The right side of this equation, S_{tot} is the superposition of all sink and source terms:

$$S_{tot} = S_{in} + S_{ds,w} + S_{ds,b} + S_{ds,br} + S_{nl3} + S_{nl4} \tag{2}$$

These six terms denote, respectively, wave growth by the wind, wave decay due to whitecapping, bottom friction and depth-induced wave breaking, nonlinear transfer of wave energy through three-wave and four-wave interactions. Detailed descriptions of these terms can be found in the SWAN scientific and technical documentation (The SWAN team, 2021b).

In SWAN, the whitecapping expressions are based on a pulse-based model (Hasselmann, 1974), and remodified by the WAMDI Group (1988):

$$S_{ds,w}(\sigma, \theta) = -\Gamma \tilde{\sigma}^{\frac{k}{k}} E(\sigma, \theta) \tag{3}$$

in which $\tilde{\sigma}$ and \tilde{k} represent the mean frequency and mean wave number respectively, and k is the wave number. Γ is a coefficient related to the wave steepness and has been adapted by Günther et al. (1992) from Janssen (1992):

$$\Gamma = C_{ds} \left((1 - \delta) + \delta \left(\frac{\tilde{s}}{\tilde{s}_{PM}} \right)^p \right) \tag{4}$$

where \tilde{s} is the overall wave steepness, and C_{ds} , δ and p are tunable coefficients. $\tilde{s}_{PM} = \sqrt{3.02 \times 10^{-3}}$ is the value of \tilde{s} for the Pierson-Moskowitz spectrum (Pierson and Moskowitz, 1964). C_{ds} has two different choices in SWAN, namely KOMEN and JANSSEN. The default value of C_{ds} is 2.36E-5 for KOMEN but 4.5 for JANSSEN.

1 <https://download.gebco.net/>.

Van der Westhuysen et al. (2007) divided the dissipation mode into breaking and non-breaking waves, which were active in different parts of the spectrum:

$$S_{ds,w}(\sigma, \theta) = f_{br}(\sigma)S_{ds,break} + [1 - f_{br}(\sigma)]S_{ds,non-break} \quad (5)$$

$$S_{ds,break}(\sigma, \theta) = -C_{ds} \left(\frac{B(k)}{B_r} \right)^{\frac{p}{2}} (\tanh(kh))^{\frac{2-p_0}{4}} \sqrt{gk} E(\sigma, \theta) \quad (6)$$

where $S_{ds,break}$ and $S_{ds,non-break}$ are the contribution by breaking and non-breaking waves, respectively. $B(k) = \int_0^{2\pi} c_g k^3 E(\sigma, \theta) d\theta$ is the azimuthal-integrated spectral saturation, B_r is a threshold saturation level. B_r and C_{ds} are both tunable parameters and the default settings in SWAN are $B_r = 1.75E-3$ and $C_{ds} = 5.0E-5$. However, the theory of non-breaking low-frequency waves is not yet mature, so $S_{ds,non-break}$ is usually replaced by KOMEN.

The scheme of Van der Westhuysen et al. (2007) is always used in conjunction with the wind input scheme of Yan (1987) (hereinafter referred to as YAN), and the expression is given as

$$S_{im,YAN}(\sigma, \theta) = \left\{ \left[C_1 \left(\frac{U_*}{c_{ph}} \right)^2 + C_2 \left(\frac{U_*}{c_{ph}} \right) + C_3 \right] \cos(\theta - \theta_w) + C_4 \right\} \sigma E(\sigma, \theta) \quad (7)$$

where $C_1 = 4.0E-2$, $C_2 = 5.52E-3$, $C_3 = 5.2E-5$, $C_4 = -3.02E-4$ are constants (The SWAN team, 2021b), U_* and c_{ph} are the friction velocity and phase speed respectively. In SWAN, the whitewashing scheme of Van der Westhuysen et al. (2007) and YAN are usually treated as a stand-alone scheme, hereinafter referred to as WST.

Since the implementation of the ‘‘ST6’’ source term package (Rogers et al., 2012; The SWAN team, 2021b) (hereinafter referred to as ST6), its good performance at different spatial scales and weather conditions has made it widely used (Liu et al., 2019). According to Zieger et al. (2015) and Rogers et al. (2012), the wind input expression of ST6 is given as

$$S_{im,ST6}(\sigma, \theta) = \frac{\rho_a}{\rho_w} \sigma \{ 2.8 - [1 + \tanh(10\sqrt{B_n}W - 11)] \} \sqrt{B_n} WE(\sigma, \theta) \quad (8)$$

$$W = W_1(\sigma, \theta) - a_0 W_2(\sigma, \theta) \quad (9)$$

where B_n is the spectral saturation. W_1 and W_2 represent the positive and adverse wind inputs respectively and their magnitudes are dependent on the friction velocity U_* . a_0 is the wind scaling coefficient.

3.2 Model setup

In this study, we used the hindcast model SWAN Cycle III version 41.31AB². The SWAN model is operated in the third generation and non-stationary mode with a spatial resolution of $0.25^\circ \times 0.25^\circ$. A time step of 30 minutes is adopted, and each time step is iterated up to a maximum of 5 times. The JONSWAP (Joint North Sea Wave Project) spectrum is divided into 72 directions and

frequency bins between 0.04 Hz and 1.0 Hz. The JONSWAP spectrum is used for the bottom friction with C_b (the bottom friction coefficient) setting to 0.038 (Hasselmann et al., 1973). The study period spans from 2017 to 2021. To investigate the effect of different whitewashing schemes, we evaluate three schemes: KOMEN, JANSSEN, and WST. For KOMEN and JANSSEN, we employ the ST6 with the wind drag formula developed by Hwang (2011) and the wind scaling coefficient a_0 set to 28. For WST, we still use YAN as the wind input scheme. Due to computational resource limitations, we mainly conduct numerical experiments using these two wind input schemes, ST6 and YAN. The detailed settings of all experiments are provided in Table 1.

3.3 Atmospheric forcing data and observations

Forcing wind fields significantly affect the accuracy of wave models (Kutupoğlu et al., 2018; Yang et al., 2022). In this study, we utilized 10-m wind speeds (U_{10}) from three high-quality wind products to drive the wave model, namely the fifth-generation European Centre for Medium-Range Weather Forecasts (ECMWF) Reanalysis (ERA5³), the Cross-Calibrated Multi-Platform Version 2.0 (CCMP⁴), and the National Centers for Environmental Prediction (NCEP) Final Reanalysis Data (FNL⁵).

The latest atmospheric reanalysis data from ECMWF is ERA5, which supersedes ERA-Interim since September 2019 (Jiang et al., 2022). ERA5 offers a finer spatial grid, higher temporal resolution, and more vertical levels compared to ERA-Interim (Hersbach et al., 2020). The dataset used in this study has a horizontal resolution of $0.25^\circ \times 0.25^\circ$ and a temporal resolution of 1 hour. Previous studies have demonstrated the exceptional performance of ERA5 in our study area (Zhang et al., 2020; Feng et al., 2022; Yang et al., 2022; Zhai et al., 2023). Therefore, ERA5 was selected as the primary forcing wind field to drive the model.

CCMP is a Level-3 ocean vector wind analysis product that provides high-quality global wind field data with a six-hour temporal resolution from 1988 to the present and a spatial resolution of $0.25^\circ \times 0.25^\circ$ (Wentz, 2015; Mears et al., 2019; Wu et al., 2022). Experimental validation conducted by Atlas et al. (2011) demonstrated a significant improvement in the accuracy of CCMP data compared to wind field measurements from individual satellite platforms, rendering it well-suited for oceanic and atmospheric research.

FNL is a global reanalysis product with a six-hour temporal resolution spanning from 1999 to the present and a spatial resolution of $1.00^\circ \times 1.00^\circ$ (Appendini et al., 2013; Chen et al., 2020). It employs an advanced data assimilation system and assimilates observation data from various sources. The product is founded upon the Global Data Assimilation System (GDAS) and is

² <https://swanmodel.sourceforge.io/>.

³ <https://cds.climate.copernicus.eu/>.

⁴ <https://data.remss.com/ccmp/v02.0/>.

⁵ <https://rda.ucar.edu/datasets/ds083.2/>.

TABLE 1 Parameter settings of SWAN model.

Model physics	Parameterization scheme	Parameters	Values
Wind input	ST6	HWANG	-
		a_0	28
	YAN	-	
Triad wave-wave interactions	LTA	Ur	0.01
Quadruplet wave interactions	DIA	λ	0.25
		$CnI4$	3E+7
Bottom friction	JONSWAP	C_b	0.038
Depth-induced wave breaking	CONSTANT	α	1.0
		γ	0.73
Whitecapping	KOMEN	c_{ds2}	-
	JANSSEN	c_{ds1}	-
	WST	c_{ds2}	-

prepared operationally every 6 hours using the identical model and assimilation scheme as the NCEP operational Global Forecast System (GFS).

The Satellite with ARGOS and ALtiKa (SARAL⁶) project is a joint mission operated by the Indian Space Agency (ISRO) and the French Space Agency (CNES), designed for ocean observations (Verron et al., 2015). AltiKa, SARAL’s primary payload, is the first spaceborne altimeter operating at the Ka-band frequency (35.75 GHz). The higher frequency leads to a smaller footprint (8 km diameter) and so a better spatial resolution (Verron et al., 2021). Since March 2013, SARAL has been providing along-track data for various physical oceanographic parameters on a global scale, including sea surface wind speed, SWH, and sea surface height (Verron et al., 2015). Recent studies have affirmed SARAL’s high accuracy, data quality, and availability (Sepulveda et al., 2015; Sharma et al., 2022). SARAL offers a range of processed data products at various levels. In this study, we utilized a delayed-mode version, specifically the Nadir altimeter Geophysical Data Record (GDR). We performed interpolation on the wind-forcing data and simulated SWH data through temporal (cubic spline) and spatial (nearest-neighbor) methods to align them with the altimeter data. To ensure the reliability of our validation results, we excluded the altimeter data that was more than 5 kilometers away from the nearest grid points. The variations in the quantity of valid altimeter data under different conditions are detailed in Table 2.

3.4 Error metrics

To accurately quantify the model performance, we employed two commonly used error metrics, including the index of agreement (d) proposed by Willmott (1982), and Slope. The specific formula for the d index is presented below

$$d = 1 - \frac{\sum_1^n (S_i - O_i)^2}{\sum_1^n (|S_i - \bar{O}| + |O_i - \bar{O}|)^2} \tag{10}$$

where O_i is the observed value, \bar{O} is the mean value of the observed data, S_i is the value of the wind products or model outputs, and n is the sample size. The d index displays the differences between simulated and observed means and variances, which reflect sensitivity to outliers in the observation data and insensitivity to additional and proportional variances between simulated and observed values (Zheng et al., 2023). Moreover, the d index is a standardized metric, with values ranging between 0 and 1, where values closer to 1 indicate higher consistency between two datasets (Willmott, 1982). The Slope provides an indication of the direction of errors and is calculated as the linear regression coefficient in the regression model $y = cx$. A Slope value greater (or less) than 1 signifies that S_i tends to be larger (or smaller) than O_i . This paper will primarily use the d index to measure the consistency between S_i and O_i , while the Slope will be used as a secondary measure to assess the direction of errors.

4 Theoretical basis

4.1 The wind errors and C_{ds}

With the wind input scheme determined, the forcing wind field, the only input variable, directly determines the magnitude of the input energy. However, errors in the wind field can affect the simulated SWH. Positive errors in the wind field lead to larger simulated SWH, while negative errors lead to smaller simulated SWH (Wu et al., 2020). Taking physical quantities in real environment as reference, positive errors in the forcing wind field require greater dissipation energy than in reality to maintain energy balance, whereas negative errors require less. It can be inferred that C_{ds} , which is the primary factor influencing dissipation energy, may exhibit a compensatory relationship with wind errors. In order to

⁶ <ftp://ftp-access.aviso.altimetry.fr>.

TABLE 2 Amount of valid altimeter data under different conditions.

Gribed data	ERA5	CCMP	FNL	Simulated SWH
Amount of valid data	68,827	67,929	16,803	68,181

explore this relationship, sensitivity experiments were conducted. Figure 2A illustrates simulations where the wind field was scaled by factors of 0.8, 0.9, 1, 1.1, and 1.2, with a constant C_{ds} value of $0.22E-5$. Likewise, in Figure 2B, simulations were performed using the same wind field but varying C_{ds} values. A comparison between Figures 2A, B reveals that, when C_{ds} is held constant, the simulated SWH gradually increases as the wind field increases. Conversely, when the wind field remains constant, the simulated SWH gradually decreases with increasing C_{ds} . Hence, when the wind errors are determined, the corresponding optimal value of C_{ds} can also be determined.

4.2 The errors in the wind fields

Currently, a wide range of wind field products are available, and with advancements in observation and assimilation techniques, these products consistently demonstrate high quality (Wu et al., 2020; Wu et al., 2022). However, the utilization of diverse assimilation data and methods in different wind field products results in variations in their errors. Figure 3 illustrates the interannual variations in the errors of three wind field products: ERA5, FNL, and CCMP. Analysis of the Slope values reveals a consistent underestimation of actual wind fields by ERA5 over 2017–2021, corroborating findings from previous studies (Shi et al., 2021; Son et al., 2023; Zhai et al., 2023). Furthermore, in 2019 and 2020, all three wind field products exhibited varying degrees of underestimation. When examining the trend of the d index, CCMP consistently displayed the highest quality with a d index of approximately 0.92, while FNL exhibited the poorest quality with a d index of around 0.89. In 2020, there was a fluctuation in the

quality of these three wind field products compared to the norm, with a d index of approximately 0.86. Overall, the d index of the three high-quality wind field products ranges from 0.86 to 0.93, and the Slope values are also near 1. This indicates that the errors in each wind field product are relatively stable.

Based on the findings in Section 4, it is hypothesized that when using high-quality wind field products, the optimal C_{ds} values will exhibit minimal variability. Therefore, conducting a series of numerical experiments to validate this hypothesis is essential.

5 Numerical experiments

In this section, we will conduct an extensive sensitivity analysis to validate whether the hypothesis proposed in the previous chapter still holds under different seasons, years, and wind field types. If confirmed, we will also determine the specific range of the optimal C_{ds} , which can greatly enhance the accuracy of wave simulation.

According to the conclusions in Section 4, there is a monotonic relationship between C_{ds} and simulated SWH. In other words, as C_{ds} increases, there will inevitably be an optimal simulation effect at a certain value. To determine this optimal simulation accuracy, we search for the maximum value of the d index. Guided by this principle, we initiate our experiments using one-tenth of the default C_{ds} as the starting point and apply a step size of $0.1E-5$ or 0.1 .

5.1 Sensitivity to different seasons

Firstly, we examine the seasonal characteristics of the optimal C_{ds} values under three distinct whitecapping dissipation schemes

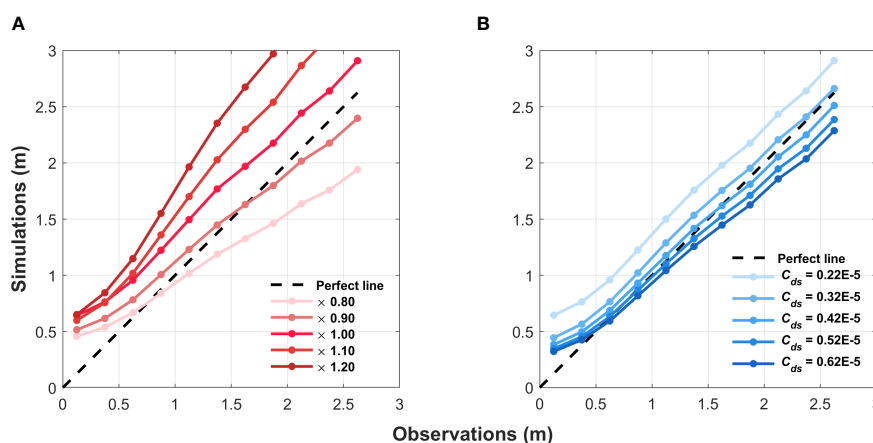


FIGURE 2 Bin-averaged scatterplots of simulated SWH versus the observations under (A) variable wind fields and (B) variable C_{ds} . In panel (A), ERA5 U_{10} is scaled at 0.8, 0.9, 1.1, and 1.2 times with a fixed C_{ds} value of $0.22E-5$. In panel (B), C_{ds} values are varied at $0.22E-5$, $0.32E-5$, $0.42E-5$, $0.52E-5$, and $0.62E-5$, while ERA5 U_{10} remains unchanged.

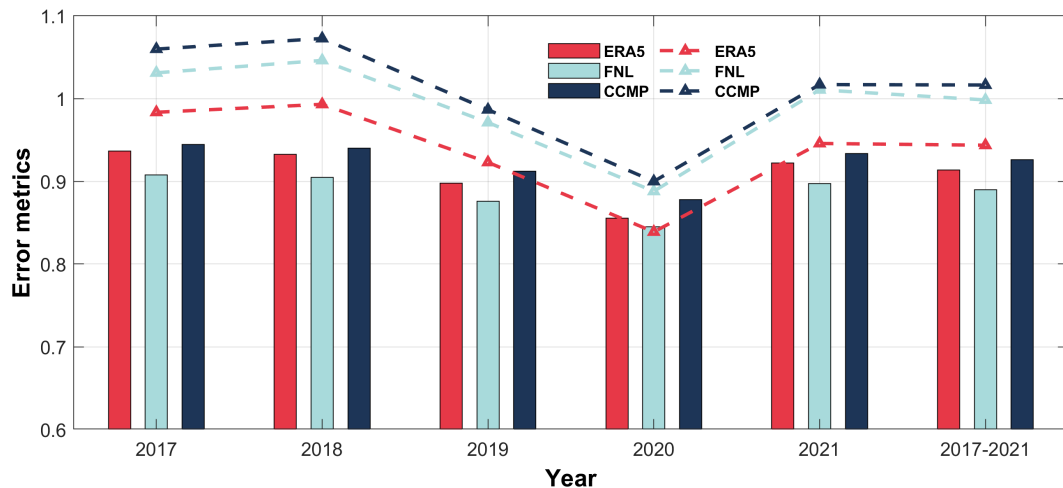


FIGURE 3 Time series analysis of wind field quality. Red, sky blue, and dark blue are ERA5, FNL and CCMP, respectively. The bars represent the d index, while the dashed line indicates the Slope value. The final point on the X-axis represents the overall error for a five-year period (2017–2021).

using ERA5 as the forcing wind field. Figure 4 illustrates the d index represented by purple bars, the Slope depicted by a black curve, and the maximum value of the d index indicated by a green dashed line, corresponding to the position of the optimal C_{ds} values. The comparison of the d index for each season reveals that the simulation performance in spring is notably inferior to that of other seasons, even when considering the optimal C_{ds} values, as the d index remains below 0.90. Analyzing the simulation results of the three schemes across different seasons shows that WST only achieves a d index above 0.90 in winter, suggesting that the overall simulation performance of KOMEN and JANSSEN surpasses that of WST.

Regarding the distribution of the optimal C_{ds} values, KOMEN remains fixed at $0.52E-5$, while JANSSEN ranges from $[0.66, 0.76]$, and WST fluctuates within the range of $[0.72E-5, 1.12E-5]$. It is important to note that reducing the step size of C_{ds} and increasing the number of experiments may yield more accurate values for the optimal C_{ds} , but this is expected to have only a minor impact on the experimental results. Based on the experimental outcomes, it is evident that the three whitcapping dissipation schemes exhibit seasonal fluctuations in the optimal C_{ds} values. However, the magnitude of these fluctuations is minimal.

Based on the observed variations in the Slope, it is evident that an increase in C_{ds} corresponds to a gradual decrease in the Slope, implying a systematic decline in the simulated SWH. This finding reinforces the conclusion established in Section 4. Additionally, it is worth mentioning that at the optimal C_{ds} values, all of the Slope consistently fall below 1, indicating an underestimation of the simulated SWH relative to the observed values. Notably, WST exhibits the most pronounced underestimation among the evaluated schemes.

5.2 Sensitivity to different years

To determine the optimal C_{ds} values for each year, we expanded the range of C_{ds} based on the experiments in Section 5.1. Figure 5 illustrates the interannual characteristics of the optimal C_{ds} values for the three whitcapping dissipation schemes. The optimal C_{ds} range is $[0.42E-5, 0.52E-5]$ for KOMEN, $[0.46, 0.86]$ for JANSSEN, and $[0.72E-5, 1.12E-5]$ for WST. Comparing the seasonal characteristics of the optimal C_{ds} values, JANSSEN exhibits a slightly larger fluctuation, while the other two schemes remain relatively consistent. Overall, we can conclude that the interannual variability of the optimal C_{ds} values is also very small.

Regarding the d index, the simulation performance in 2020 exhibits the poorest results, with the d index falling below 0.90 for all three schemes. When examining the d index of the optimal C_{ds} values, the simulation performance of KOMEN and JANSSEN is superior to that of WST, even in the year with the worst simulation performance in 2020.

As highlighted in Section 4.2, the quality of the wind field in 2020 displayed fluctuations, with its Slope significantly lower than that of other years. This discrepancy indicates a severe underestimation of the actual wind field by the wind field product in 2020. Referring to Figure 5, it is evident that the optimal C_{ds} value for 2020 is the smallest among the five years. This finding further strengthens the confirmation of the compensatory relationship between the wind errors and C_{ds} , as elucidated in Section 4.

To address the potential impact of short-term disruptions on the overall quality of the wind field, we considered the period from 2017 to 2021 as a unit, as depicted in Figures 5P–R. Comparing the optimal C_{ds} values for the five years to that of 2021 reveals a complete equivalence between them. In Figure 3, the Slope and d

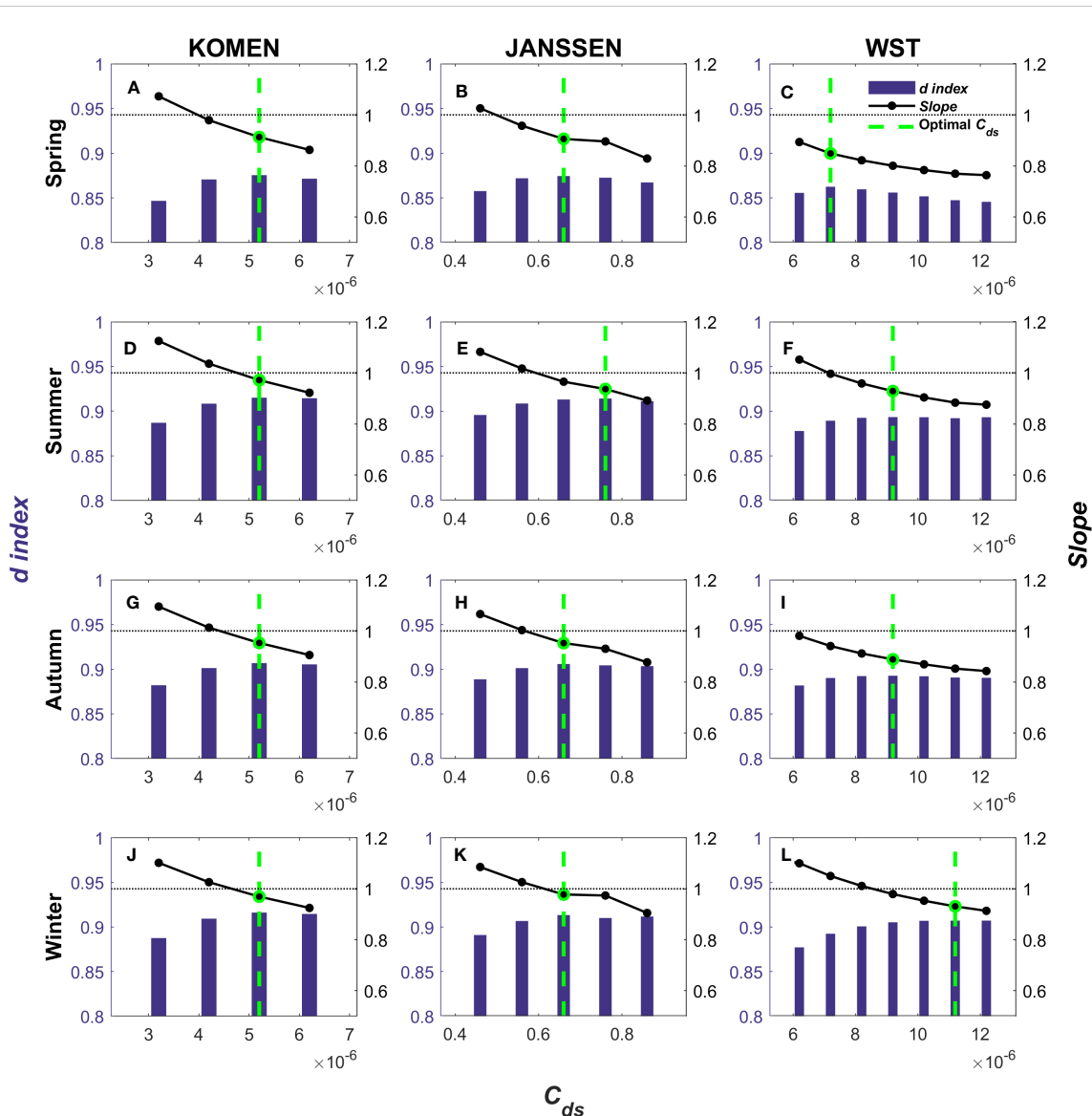


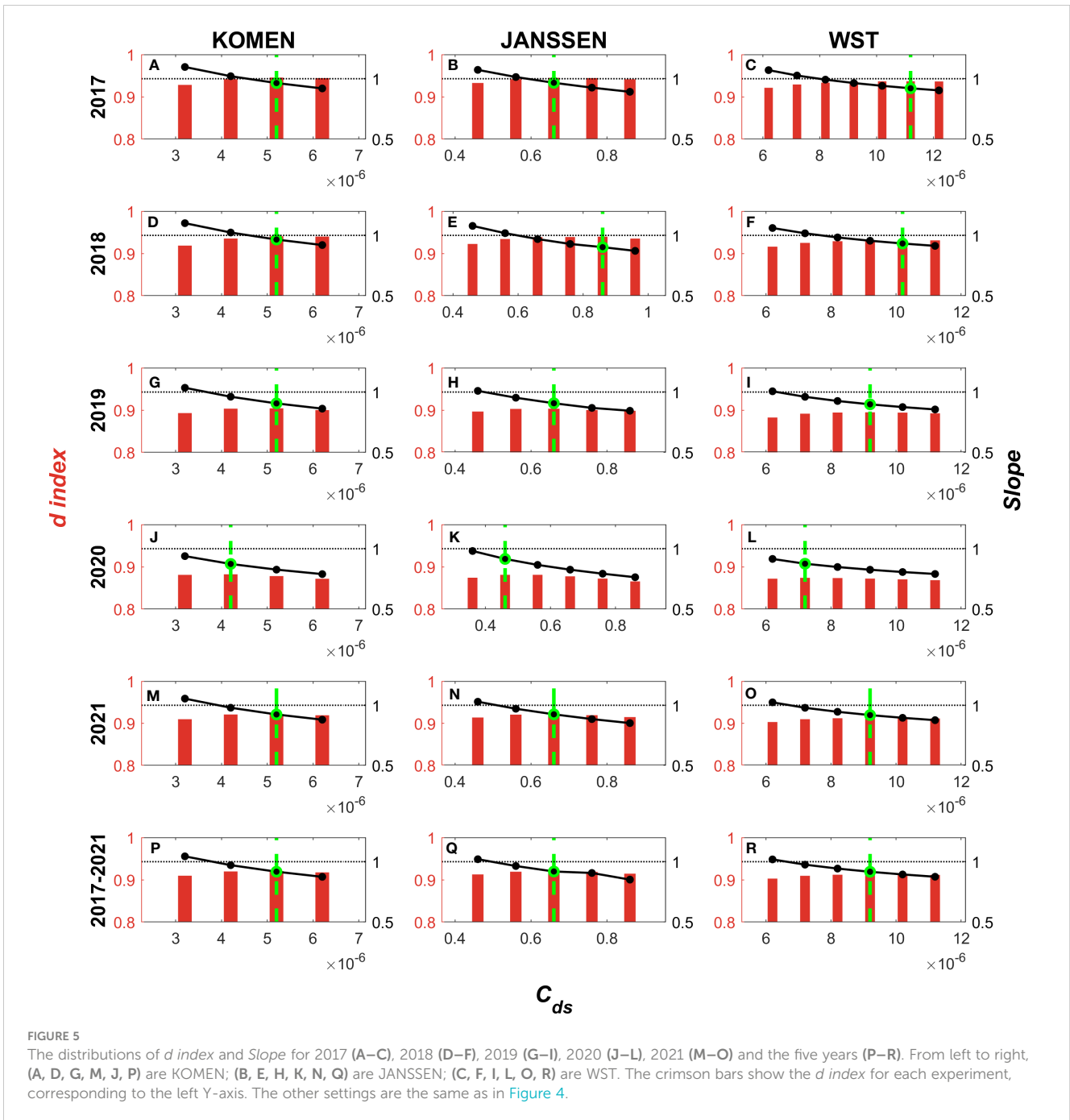
FIGURE 4
 The distributions of d index and Slope for spring (A–C), summer (D–F), autumn (G–I), and winter (J–L). From left to right, (A, D, G, J) are KOMEN; (B, E, H, K) are JANSSEN; (C, F, I, L) are WST. The purple bars show the d index for each experiment, corresponding to the left Y-axis. The solid black line shows the Slope distribution corresponding to the right Y-axis. The green dotted line indicates the experiment corresponding to the maximum value of the d index, that is, the experiment corresponding to the optimal C_{ds} . The black dashed line represents the Slope equal to 1.

index of ERA5 for the five-year timeframe closely approximate those of 2021, providing further evidence of the direct relationship between wind errors and the optimal C_{ds} values. Furthermore, by comparing the d index in close proximity to the optimal C_{ds} values, we observe minimal differences among them. This finding implies that the optimal value attained for the five-year period consistently yields favorable simulation performance annually. In essence, the longer the simulation timeframe, the more accurately the main characteristics of the optimal C_{ds} can be reflected. Therefore, a simulation duration of five years will be maintained for subsequent validation experiments.

5.3 Sensitivity to different wind fields

The preceding section focused on the optimal C_{ds} characteristics when using ERA5 as the forcing wind field. In order to assess the generalizability of the optimal C_{ds} features, we conducted experiments using CCMP and FNL as alternative forcing wind fields.

As shown in Figure 3, the Slope reaches the highest when the CCMP is applied, while it is the lowest for the ERA5 winds. Figure 6 provides an illustration of the optimal C_{ds} values, showing that CCMP generally has the highest C_{ds} values among the three wind



field products, while ERA5 exhibits the lowest values. This finding provides further confirmation of the compensatory relationship between wind field errors and C_{ds} . Remarkably, for KOMEN, it is observed that the optimal C_{ds} values are identical across all three wind field products, at $0.52E-5$. The optimal C_{ds} range for JANSSEN is $[0.66, 0.76]$, while for WST, it fluctuates within the range of $[0.92E-5, 1.12E-5]$. Similar to the seasonal and interannual characteristics, the fluctuation range of the optimal C_{ds} among different wind field products is also minimal.

Figure 7 presents the differences in simulation performance between the optimal C_{ds} values and the default C_{ds} values across all experiments. The optimal C_{ds} values are represented by the black

lines in the figure, corresponding to the right y-axis. The maximum value on the right y-axis represents the default C_{ds} for each scheme. It is evident that the range of the optimal C_{ds} values for all three schemes is significantly narrower compared to the default values of the model. Specifically, for the individual whitcapping dissipation schemes, the optimal C_{ds} range is $[0.42E-5, 0.52E-5]$ for KOMEN, $[0.46, 0.86]$ for JANSSEN, and $[0.72E-5, 1.12E-5]$ for WST. From the experiments conducted above, we can conclude that the variations in wind field errors across different time scales and types indeed result in fluctuations in the optimal C_{ds} values. However, due to the overall stability of wind field errors, the optimal C_{ds} values also fluctuate within a small range. These

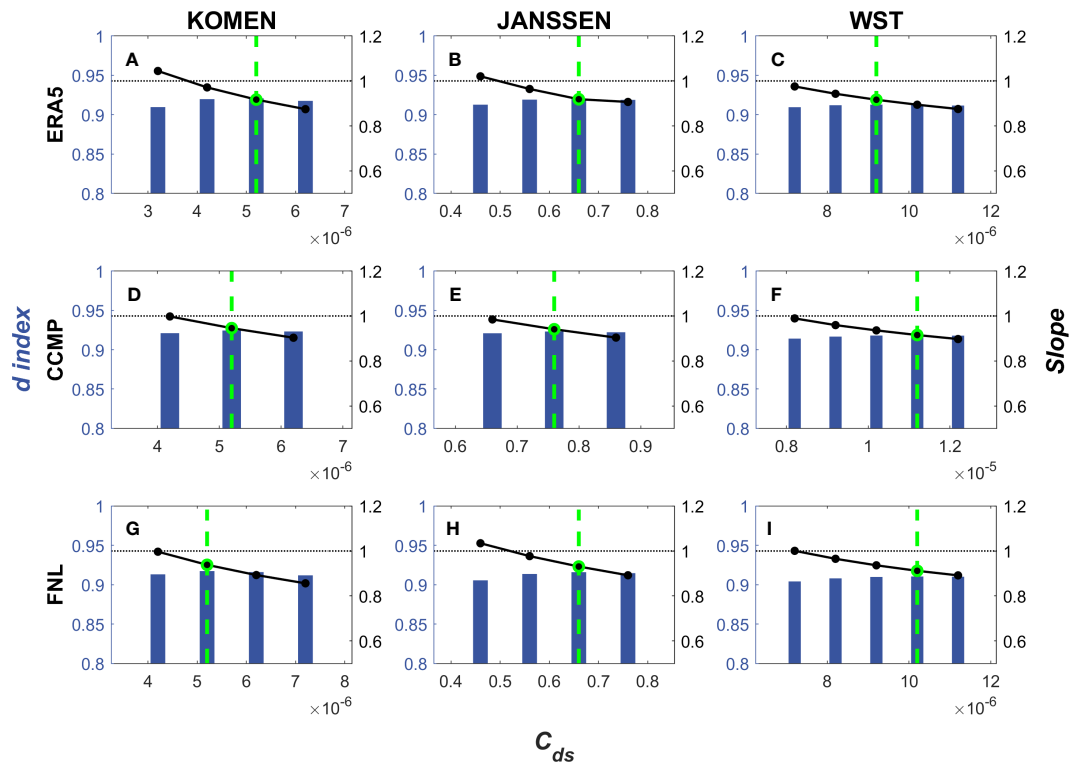


FIGURE 6
The distribution of *d index* and *Slope* of ERA5 (A–C), CCMP (D–F), and FNL (G–I). From left to right, (A, D, G) are KOMEN; (B, E, H) are JANSSEN; (C, F, I) are WST. The blue bars show the *d index* for each experiment, corresponding to the left Y-axis. The other settings are the same as in Figure 4.

results demonstrate the reliability of the theoretical basis proposed in Section 4.

The red and dark blue bars in Figure 7 represent the *d index* of the optimal C_{ds} and default C_{ds} , respectively, corresponding to the left y-axis of the figure. It can be observed that the *d index* of the optimal C_{ds} values for all three schemes is consistently around 0.90, indicating significantly improved simulation performance compared to the default values. The most notable enhancement is observed for JANSSEN with the optimal C_{ds} values, while the improvement is minimal for WST. This finding suggests that the default value of WST exhibits the best simulation performance among the three schemes. From the previous experimental results, we have discovered that C_{ds} values near the optimal C_{ds} also yield excellent simulation performance. In other words, selecting any C_{ds} value within the proposed optimal value range would result in improved simulation performance than the default value of the model.

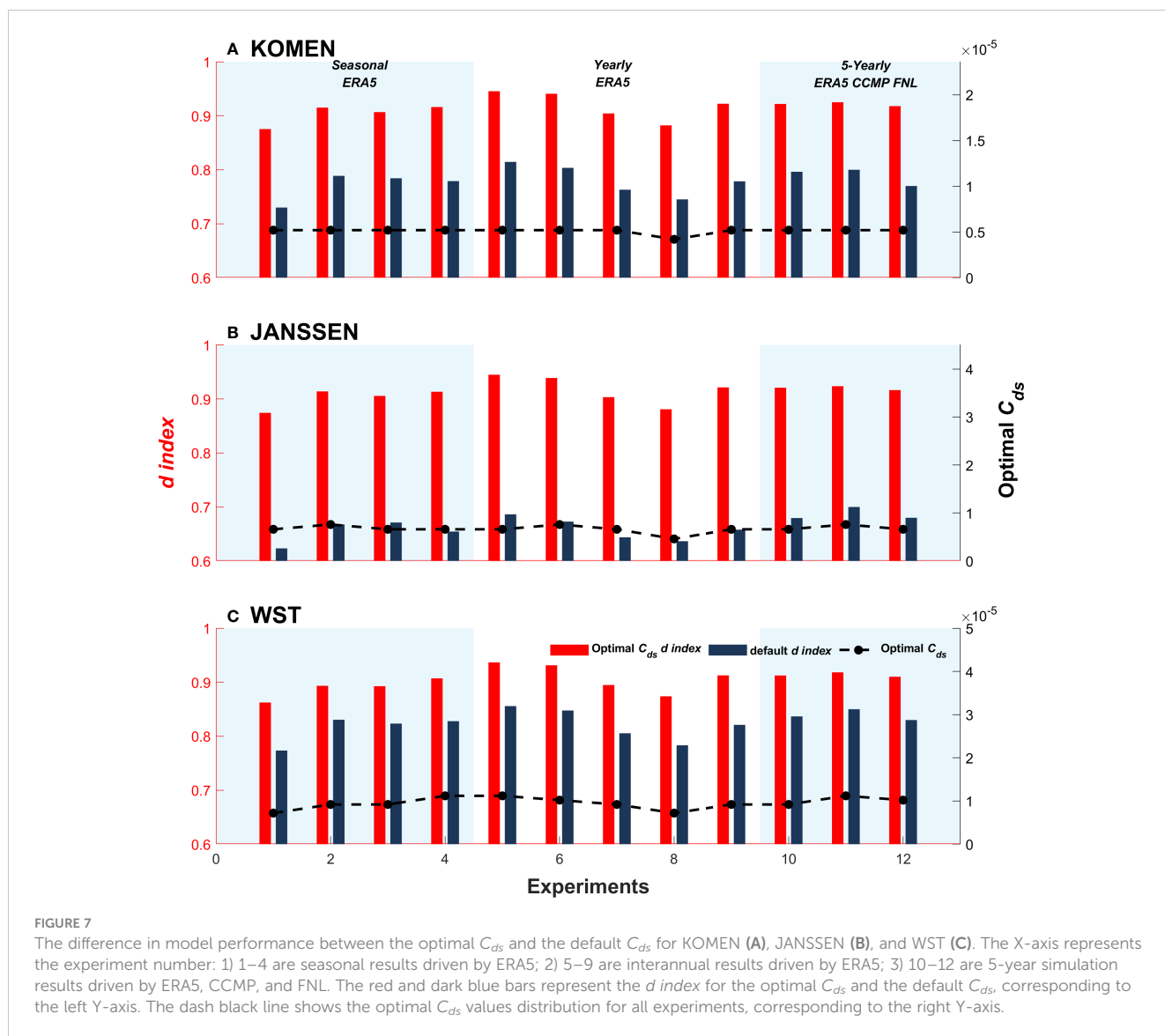
6 Discussion

This study aims to propose a general method for determining the optimal C_{ds} to enhance the accuracy of ocean wave simulation. However, the primary focus of this paper is on the SCS. Therefore, to determine the wider applicability of the optimal C_{ds} intervals, two

additional regions, namely the Gulf of Mexico (GoM; 98°W–78°W, 17°N–31°N) and the MS (8°W–37°E, 28°N–45°N), were selected as study areas. The GoM and the MS share similarities with the SCS, featuring complex topography and drastic variations in water depth. They also serve as vital maritime routes and regions rich in natural resources (Huerta and Harry, 2012; Appendini et al., 2013; Elkut et al., 2021; Beyramzadeh and Siadatmousavi, 2022). Therefore, choosing these areas as subjects of study holds heightened practical relevance. The time range, model settings, and observational data remained consistent with this study. Similarly, we filtered the raw data by excluding data points that were more than 5 kilometers away from the grid points. As a result, there were 44,756 valid data for the GoM and 84,272 valid data for the MS. To effectively utilize computational resources, we only used ERA5 to drive the model.

Figure 8A displays the bathymetry map for the GoM and the MS. For the GoM (Figures 8B, D, F), optimal C_{ds} values are determined as 0.42E-5 for KOMEN, 0.46 for JANSSEN, and 0.82E-5 for WST, respectively. Similarly, for the MS (Figures 8C, E, G), the optimal C_{ds} values for the respective schemes are 0.52E-5, 0.66, and 1.02E-5. All the optimal C_{ds} values for both regions fall within the proposed range, demonstrating the robust applicability of the proposed viewpoint across different regions.

This study primarily focuses on two wind input schemes, ST6 and YAN, in SWAN. However, SWAN offers multiple other wind input schemes to choose from. Different wind input schemes can



result in variations in the energy input to the wave model (Wang and Huang, 2004; Adcock and Taylor, 2018), potentially leading to variations in the optimal C_{ds} range. Nevertheless, the optimal C_{ds} values will always fluctuates within a very small range.

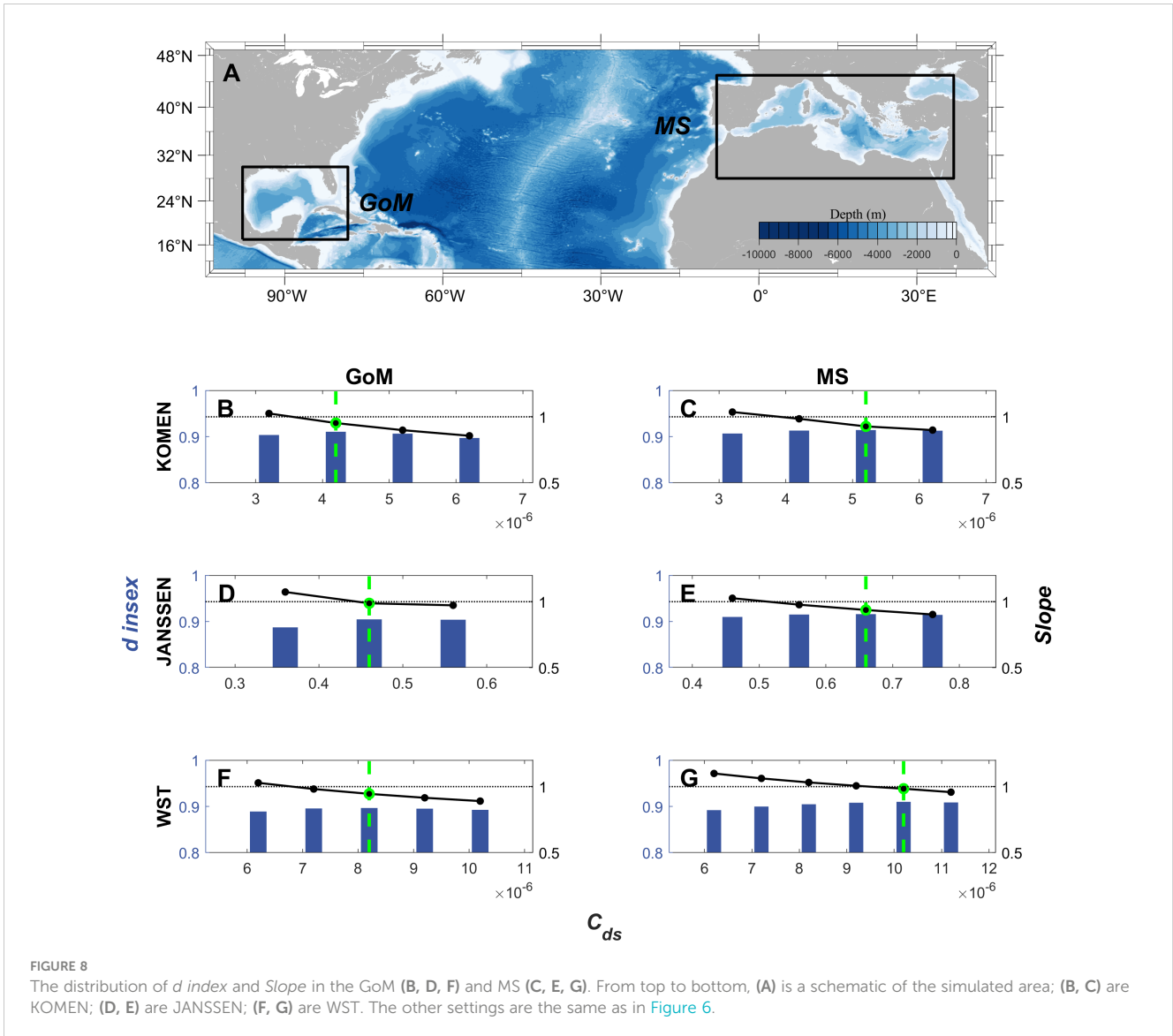
When utilizing the optimal C_{ds} range, two considerations must be taken into account. Firstly, our conclusions are based on a large volume of observational data. In cases where the validation dataset is insufficient or the simulation duration is too short, such as during typhoon events, the limited number of samples can lead to potential errors. Therefore, it's essential to exercise caution when applying the optimal C_{ds} range under these circumstances. Additionally, for nearshore wave simulations, where whitecapping dissipation no longer dominates, the contributions of bottom friction and depth-induced breaking to the dissipation process become prominent (Xu et al., 2013; Peng et al., 2023). Moreover, errors in nearshore wind fields can increase. Therefore, adjusting a single parameter alone may not yield satisfactory simulation results. In such cases, the utilization of the optimal C_{ds} range also needs to be approached with

caution. Typhoon and nearshore wave simulations hold significant research value, and these aspects will be the main focus of our future investigations.

7 Conclusion

Calibrating wave models is of paramount importance for simulating SWH, with C_{ds} often serving as a primary calibration parameter. Nevertheless, determining the optimal C_{ds} value is a challenging task. This study, through theoretical analysis and numerical experiments, provides a robust optimal C_{ds} range. Within this range, the accuracy of simulated SWH for any C_{ds} value is better than the model's default C_{ds} .

Specifically, we begin by revealing a direct relationship between wind errors and the optimal C_{ds} through sensitivity experiments. Through a comprehensive evaluation of high-quality wind field products using satellite observational data, we have discovered that the errors of these wind field products are stable. This mechanism



suggests that, under high-quality wind field conditions, the optimal C_{ds} values will exhibit small fluctuations.

To verify this conjecture, we conducted a five-year wave simulation in the SCS using SWAN, covering various scenarios with different time scales and wind field types. Employing two wind input schemes (ST6 and YAN) and three whitemapping dissipation schemes (KOMEN, JANSSEN, and WST), we observed that the optimal C_{ds} values for all three whitemapping dissipation schemes fluctuated within a narrow range. Specifically, the optimal C_{ds} range was [0.42E-5, 0.52E-5] for KOMEN, [0.46, 0.86] for JANSSEN, and [0.72E-5, 1.12E-5] for WST. These results demonstrate the applicability of our proposed viewpoint across different time scales and wind field types. Furthermore, compared to the model’s default C_{ds} , we found that any C_{ds} within the optimal range had better simulation performance.

To investigate the applicability of the optimal C_{ds} characteristics in different regions, we conducted similar experiments in the GoM and the MS using ERA5. The findings demonstrated that the optimal

C_{ds} values in these regions aligned with the suggested range, affirming the universality of this approach across a global scale.

Data availability statement

The original contributions presented in the study are included in the article/supplementary material. Further inquiries can be directed to the corresponding authors.

Author contributions

ZL: Formal Analysis, Methodology, Validation, Writing – original draft. WW: Data curation, Investigation, Visualization, Writing – review & editing. YG: Resources, Software, Writing – review & editing. FZ: Conceptualization, Methodology, Writing – review & editing. PL: Resources, Supervision, Writing – review & editing.

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Conflict of interest

The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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