



# Decomplexation Performance of Cu–EDTA and Parameter Optimization by Three-Dimensional Electro-Fenton

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The strong stability of Cu-ethylenediaminetetraacetic acid (Cu-EDTA) results in the low

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Ma Y, Huang X, Han Q, Yu J, Yu F and Zhu J (2022) Decomplexation Performance of Cu–EDTA and Parameter Optimization by Three-Dimensional Electro-Fenton. Front. Environ. Sci. 10:818142. doi: 10.3389/fenvs.2022.818142 decomplexation efficiency by the traditional Fenton process. For breaking this limitation, a three-dimensional electro-Fenton (3D-EF) system was constructed to study the decomplexation of Cu–EDTA at different pH, and the effects of Fe<sup>2+</sup> concentration, particle electrode dosage, current density, and coexisting ions on decomplexation performance were investigated. The results showed that 3D-EF exhibited high pollutant removal efficiency in a wide pH range compared with the traditional electro-Fenton process. The optimal conditions for the removal of Cu–EDTA were as follows: the pH was 7, Fe<sup>2+</sup> was 1 mmol L<sup>-1</sup>, granular activated carbon was 2 g L<sup>-1</sup>, and current density was 10 mA cm<sup>-2</sup>, and the optimum Cu–EDTA removal efficiency reached 90.95%. In addition, the presence of Cl<sup>-</sup> slightly improved the decomplexation efficiency, whereas NO<sub>3</sub><sup>-</sup> and HPO<sub>4</sub><sup>2-</sup> inhibited the removal of Cu–EDTA. The kinetics of Cu–EDTA decomplexation in all experimental groups followed the first-order kinetic equation.

Keywords: Cu-EDTA, three-dimensional electro-Fenton, decomplexation, parameter optimization, electrochemical

# INTRODUCTION

The chelator ethylenediaminetetraacetic acid (EDTA) is widely used in electroplating, metallurgical, and chemical cleaning industries to form stable complexes with heavy metals of different structures (Wang et al., 2019; Wang Y. et al., 2020). Their efficient removals remain a key challenge in the field of wastewater treatment. Cu–ethylenediaminetetraacetic acid (Cu–EDTA), a strong stability complex compound in wide pH range of wastewater, poses potential hazards to water, soil environments, and human health (Song et al., 2021), and it is difficult to remove from wastewater by chemical precipitation and other processes. Therefore, appropriate methods should be taken to overcome this problem (Hu et al., 2021; Wang and Chen, 2021; Wang and Tang, 2021).

Some promising treatment methods for removing the stable complex from wastewater have received extensive attention, such as electro-coagulation (Xie et al., 2020), nonthermal plasma oxidation (Wang et al., 2019; Liu et al., 2021), photo-electrocatalytic oxidation (He et al., 2021; Shah and Patel, 2021), ozone-based oxidation (Zhao et al., 2018a; Guan et al., 2022), and microwave-assisted Fenton reaction (Wang H. et al., 2020; Xia et al., 2021). Electrochemical advanced oxidation processes (EAOPs) are sought-after for many researchers due to their high degradation efficiency, versatility, and environmental friendliness (Wang and Zhuan, 2020; Wang and Chen, 2021; Wang

and Wang, 2021). The hydroxyl radical (•OH) produced from the electro-Fenton (EF) process by the reaction of  $Fe^{2+}$  and  $H_2O_2$ solution owns the characteristics of strong oxidation, high reactivity, easy formation, non-selectivity, and harmlessness, which has been proved to have perfect removal performance for the stable complex in wastewater (Wang and Wang, 2018; Chen and Wang, 2021). Chu et al. (2022) prepared several composite cathodes using graphite, carbon nanotube, and polytetrafluoroethylene, and the degradation efficiency of cefepime reached nearly 100% at pH 3.0. Zhang et al. (2022) synthesized a novel core-shell Fe@Fe2O3-CeO2 composite for effective degradation of the tetracycline (TC) pollutant, and TC removal efficiency reached 90.7% within 1 h at the optimum pH of 3.85. Midassi et al. (2020) used the carbon-felt cathode and boron-doped diamond anode to completely remove chloroquine at pH 3.0. Hence, three-dimensional electro-Fenton (3D-EF) is appropriate for refractory organics removal, and whether it owns the same decomplexation efficiency on Cu-EDTA needs to be further studied.

The EF reaction could produce high activity only in a narrow pH range (may be in pH 2.5-3.5), which greatly limits the application of EF technology. In order to solve the problems, the 3D-EF system has been constructed by adding particle electrodes between the anode and cathode. It was reported that the rhodamine B removal reached 91.6% in the 3D-EF system in the presence of Fe-Cu/kaolin particle electrodes (Zhang et al., 2019). Iron foam was used as the particle electrode in a 3D-EF system in the study of Zheng et al. (2019) and found that the chemical oxygen demand (COD) and total nitrogen (TN) removal percentage in folic acid wastewater reached 43.5 and 70.4%, respectively, under the following optimal conditions: the initial COD concentration of 10 g L<sup>-1</sup>, applied current of 0.3 A, initial pH of 3, and particle electrode of 4 g. It is noteworthy that the Long's team reported that the diclofenac removal rate reached 96.3% in the presence of manganese slag-loaded active substance as a particle electrode (Long et al., 2019). Among them, it can be noted the work of Li M. et al. (2021), who prepared Cu-Fe bimetallic aerogel-like carbon as a catalytic particle electrode based on sodium alginate to remove 81.1% of fulvic acids at pH 5.4, voltage 2.5, and catalyst dosage of 4 g  $L^{-1}$ .

In the 3D-EF system, the electrode plate, pH, Fe<sup>2+</sup>, particle electrodes, current density, and coexisting ions could affect the efficiency of pollutant removal. Among them, the electrode material plays a decisive role in the generation of OH, which is a key factor in the wastewater treatment by EF (Ou et al., 2019). According to the reports, graphite electrode plates (carbon materials) have been widely examined and regarded as the most efficient electrode plates (Zhang et al., 2019; Zhang B. et al., 2019; Song et al., 2020). Graphite material plates showed better removal effect for some refractory organics, but less research was carried out on Cu-EDTA using graphite polar plates. Due to the unique functional group structure on the surface of graphite (carbon materials), organics decompose through free radical-induced pathways (Duan et al., 2018). Compared with other electrodes, graphite electrodes are easier to obtain, low-cost, nontoxic, and own a high specific surface

area, which will be cost-effective in electrochemical analysis (Le et al., 2017; Zhao K. et al., 2018). In addition, the excellent electrical conductivity of graphite makes it an ideal candidate for electrodes (Pan et al., 2020; Tasić et al., 2021).

In this study, a 3D-EF system with granular-activated carbon (GAC) as the particle electrode was used to remove Cu–EDTA. The effects of main parameters (the pH value of initial solution,  $Fe^{2+}$  concentration, particle electrode dosage, current density, and coexisting ions) on the decomplexation performance of Cu–EDTA were optimized. In addition, the reaction kinetics for all optimization processes were fitted. This study provides a new idea for the decomplexation of Cu–EDTA and other complexes, and provides a suitable way for the treatment of complex heavy metal complexes.

# MATERIALS AND METHODS

#### Chemicals

All the reagents used in this study were of analytical grade. Ethylenediaminetetraacetic acid disodium salt  $(C_{10}H_{14}N_2Na_2O_8\cdot 2H_2O)$  was purchased from Shanghai Macklin Biochemical Co., Ltd. (Shanghai, China). Copper sulfate (CuSO<sub>4</sub>·5H<sub>2</sub>O), sodium chloride (NaCl), sodium nitrate (Na<sub>2</sub>NO<sub>3</sub>), disodium hydrogen phosphate (Na<sub>2</sub>HPO<sub>4</sub>·12H<sub>2</sub>O), and sodium sulfate (Na<sub>2</sub>SO<sub>4</sub>) were purchased from Tianjin Damao Chemical Reagent Factory. (Tianjin, China). Sodium hydroxide (NaOH) was purchased from Shantou Xilong Scientific Co., Ltd. (Shantou, China). Sulfuric acid (H<sub>2</sub>SO<sub>4</sub>) was purchased from Hengyang Kaixin Chemical Reagent Co., Ltd. (Hengyang, China). GAC was obtained from Shanghai Aladdin Inc. (Shanghai, China). The particle size of GAC is approximately 0.6-2 mm. Solutions were prepared with Milli-Q water.

#### **Experimental Setup**

In this study, the experimental device consists of a 5 A, -30 V DCregulated power supply (HXD-305DM), 500-ml beaker, and magnetic stirrer (IKA). The polar plates were dual graphite electrode plates ( $100 \times 50 \times 5$  mm) with a 70-mm plate spacing and GAC particle electrode. The graphite electrode plate and GAC were boiled in dilute acid and alkali for 30 min, ultrasonic cleaned for 20 min, and dried in an oven at 105°C for 10 h.

# **Experimental Procedure**

The Cu–EDTA reserve solution of 50 mg L<sup>-1</sup> was added into a 500-ml breaker with a volume of 300 ml solution for each experiment. Besides, 0.2 mol L<sup>-1</sup> NaOH and H<sub>2</sub>SO<sub>4</sub> were used to adjust the initial pH, and 0.047 mol L<sup>-1</sup> Na<sub>2</sub>SO<sub>4</sub> was used as the electrolyte. The reaction time was 120 min, and the samples were taken three times at 10, 30, 60, 90, and 120 min. After that, sample's pH were adjusted to 11 with H<sub>2</sub>SO<sub>4</sub> or NaOH to form hydroxide precipitates of heavy metal ions to remove from the supernatant and diluted 500 times for further detection. The concentration of the remaining heavy metal complex in samples was determined by inductively coupled plasma mass

spectrometry (ICP-MS) after being filtered by a 0.22- $\mu$ m membrane.

#### Cu-EDTA Degradation by 3D-EF

In order to prove the advantage of the 3D-EF system for the decomplexation of Cu–EDTA, a GAC system (pH = 3 and Fe<sup>2+</sup> = 1 mmol L<sup>-1</sup>), EF system (pH = 3, Fe<sup>2+</sup> = 1 mmol L<sup>-1</sup>, and current density 4 mA cm<sup>-2</sup>), and 3D-EF system (pH = 3, Fe<sup>2+</sup> = 1 mmol L<sup>-1</sup>, GAC 2 g L<sup>-1</sup>, and current density 4 mA cm<sup>-2</sup>) were set up. Three samples were taken at 10, 30, 60, 90 and 120 min to detect the Cu concentration.

#### Parameter Optimization of 3D-EF Degradation

The relevant factors include pH, Fe<sup>2+</sup>, particle electrodes, and current density to assess the efficiency in removing Cu-EDTA via the 3D-EF. For investigating the effect of pH on the decomplexation of Cu-EDTA, the changes of Cu-EDTA removal efficiency in different pH (pH = 3, 5, 7, and 9) were investigated. Different amounts of Fe2+ (0.5, 1.0, 1.5, and 2.0 mmol  $L^{-1}$  Fe<sup>2+</sup>) were put into the solution to study the effect of Fe<sup>2+</sup> dosages on Cu-EDTA decomplexation. This was followed up by using the most suitable pH solution obtained from the previous experiment. Subsequently, different doses of the particle electrode (doses of 1, 2, 3, 4, 5, and 6 g  $L^{-1}$ ) were added to discuss the effect of the particle electrode on the decomplexation of Cu-EDTA. The most suitable conditions such as pH, Fe<sup>2+</sup> dosages, and particle electrode were prepared. A certain current density (2, 4, 6, 8, 10, and 12 mA  $cm^{-2}$ ) was added to study its effect on Cu-EDTA decomplexation.

#### Effect of Coexisting Ions on Cu-EDTA Removal

The effects of coexisting ions (Cl<sup>-</sup>, NO<sub>3</sub><sup>-</sup>, and HPO<sub>4</sub><sup>2-</sup>) were studied in terms of the most suitable conditions such as solution pH of 7, 1 mmol L<sup>-1</sup> Fe<sup>2+</sup>, 4 g L<sup>-1</sup> GAC, and current density of 10 mA cm<sup>-2</sup>.

#### **Chemical Analytical Methods**

The solution pH was measured by a pH meter (PB-10, Sartorius). During the electrolysis, samples were collected at specific time intervals for copper ion determination. If not noted otherwise, each experiment was repeated three times to ensure the repeatability of experimental results. The concentrations of copper ions were determined by inductively coupled plasma mass spectrometry (ICP-MS, NexION 2000). The conditions for the detection of copper ions were as follows: a radio frequency power of 1500 W, plasma gas flow of  $15 \text{ L min}^{-1}$ , and auxiliary gas flow of  $1.0 \text{ L min}^{-1}$  and nebulization gas flow of  $1.0 \text{ L min}^{-1}$ .

#### **Statistical Analysis**

Three replicates were conducted for each sample, and average values were calculated and shown in charts. Origin 8.6 software was used for drawing figures.

The Cu-EDTA removal rate was calculated by Eq. 1.

$$R(\%) = \left(1 - \frac{C_t}{C_0}\right) \times 100\%,$$
 (1)

where R is the removal efficiency at time (t),  $C_0$  is the initial concentration, and  $C_t$  is the copper ion concentration at time (t).

The term removal rate refers to the kinetic process; the Cu–EDTA decay is followed by the first-order reaction kinetics with reaction rate constants ( $K_{obs}$ ) determined in min<sup>-1</sup> according to Eq. 2.

$$\ln\left(\frac{C_0}{C_t}\right) = kt,\tag{2}$$

where t is the electrolysis time (min).

# **RESULTS AND DISCUSSION**

# Removal of Cu–EDTA by 3D-EF

Three different reaction systems, i.e., GAC adsorption system, EF reaction system, and 3D-EF reaction system were studied to prove the advantage of the 3D-EF process for the decomplexation of Cu-EDTA, and the results were demonstrated in Figure 1. The decomplexation efficiency of Cu-EDTA increased with the reaction time extended in all experience groups (Figure 1A), and the removal rates of Cu-EDTA were 11.37, 75.46, and 86.81% in three groups, respectively. The 3D-EF reaction system owned higher removal efficiency than that of GAC adsorption and EF processes. From Figure 1B; Table 1, it is noted that the degradation of Cu-EDTA in all systems conformed to the first-order kinetic model, and the reaction rate constant  $K_{obs}$ of the 3D-EF, GAC, and EF were 0.0175, 0.0126, and 0.0012, respectively, which indicated that the 3D-EF reaction system owns a good application prospect for Cu-EDTA decomplexation. Hu et al. (2021) prepared the Ni/GO-PAC particle electrode, and Cu-EDTA degradation reached 99% at  $1 \text{ mmol } \text{L}^{-1}$  Cu-EDTA, current density of  $1.6 \text{ mA cm}^{-2}$ , and pH = 3.15. Also, Song et al. (2021) used  $RuO_2$ -IrO<sub>2</sub>/Ti and Al electrodes to treat Cu-EDTA wastewater, and the Cu removal efficiency reached 99.85%. Zhao et al. (2018b) explored the application of the EF technique by using iron-sacrificing electrodes, and the effluent could meet discharge standard (0.3 mg  $L^{-1}$  for Cu in China) under the initial pH of 2.0,  $H_2O_2$ dosage of 6 ml L<sup>-1</sup> h<sup>-1</sup>, current density of 20 mA cm<sup>-2</sup>, and sulfate electrolyte concentration of 2 g  $L^{-1}$ .

In the 3D-EF process, the additional particle electrode adsorbed pollutants, and the contaminated materials underwent electrochemical degradation on the surface of the particle electrode to achieve the efficient removal. The lower current was able to enhance the removal efficiency of pollutants, which could greatly improve the chemical reaction rate and treatment effect. Therefore, the 3D-EF reaction system exhibited better performance than the conventional EF reaction system. Theoretically, using activated carbon as the particle electrode in the EF reaction system was able to enhance Cu–EDTA removal, which was related to the particle electrode increasing the electrode specific surface area, increasing the utilization of the whole space, and improving the mass transfer effect (Zhang et al., 2018; Li H. et al., 2021), and a



FIGURE 1 (A) Removal efficiency of Cu-EDTA in different reaction systems and (B) kinetics fitting of Cu-EDTA removal in different reaction systems. (pH = 3 and  $Fe^{2+} = 1 \text{ mmol } L^{-1}$ ).

| TABLE 1   Pseudo-first-order kinetics | of Cu-EDTA removal in different reaction |
|---------------------------------------|--|
| systems.                              |  |

| Reaction system | $K_{obs}$ (min <sup>-1</sup> ) | Correlation coefficient R <sup>2</sup> |
|-----------------|--------------------------------|--|
| GAC             | 0.0012                         | 0.8722                                 |
| EF              | 0.0126                         | 0.9860                                 |
| 3D-EF           | 0.0175                         | 0.9907                                 |

synergistic strengthening effect should appear with the combination of the activated carbon and electrochemical process. However, this synergy was not obvious in this study. It might because that the adsorption of Cu-EDTA by activated carbon was presented and occupied the active sites of the particle electrodes, and with the reaction extending, the Fe<sup>2+</sup> and ·OH on the surface of the particle electrode formed the Fenton reaction, whose products ( $Fe^{3+}$  and  $Cu^{2+}$ ) took the place of these sites to inhibit the synergistic strengthening performance.

# pH Application Window for Cu-EDTA **Decomplexation by 3D-EF**

Different initial pH conditions could affect the degradation efficiency of Cu-EDTA and is illustrated in Figure 2A. The removal efficiency of Cu-EDTA reached more than 80% at different initial pH conditions, and the removal rates of Cu-EDTA were 84.22, 88.04, 90.19, and 87.74%, when the pH ranged from 3 to 9. Among them, the Cu-EDTA removal rate reached the maximum when the pH was 7. The experimental results proved that using GAC particles as the particle electrode in a 3D-EF system broke a limitation of pH conditions, which enabled the 3D-EF reaction system to better treat various types of water quality and greatly broadened the application window of pH. The kinetics of Cu-EDTA removal at different pH conditions were fitted as shown in Figure 2B. The reaction rate constant Kobs of Cu-EDTA reaches maximum at pH 7 and reaction time 120 min. The reaction rate constant  $K_{obs}$  showed a tendency of increasing at first and then decreasing with the



| TARIE 2 | Pseudo-first-order  | kinetics of  | Cu-EDTA | removal at     | different nH |
|---------|---------------------|--------------|---------|----------------|--------------|
|         | 1 36000-11131-01061 | KII IGUGS UI | OU-LDIA | 1 CI I Oval at |              |

| рН | $K_{obs}$ (min <sup>-1</sup> ) | Correlation coefficient R <sup>2</sup> |
|----|--------------------------------|--|
| 3  | 0.0166                         | 0.9920                                 |
| 5  | 0.0187                         | 0.9916                                 |
| 7  | 0.0194                         | 0.9993                                 |
| 9  | 0.0176                         | 0.9963                                 |

increase of the initial pH, which was the same as the removal effect of Cu–EDTA (**Table 2**).

The lower pH values tend to have higher pollutant removal rates in many EF studies. Shi et al. (2021) demonstrated that the removal rate of ibuprofen could reach 90.2% in 120 min at pH 3.0 and current density of 10 mA cm<sup>-2</sup>. Also, for aniline, ciprofloxacin, and cefazolin, their removal efficiencies were more than 99, 91.30, and 95.8% under acid condition, respectively (Ma et al., 2021; Yao et al., 2021; Ghasemi et al., 2020). GAC particles, particle electrodes used in a 3D-EF system, made this system remove Cu-EDTA better under neutral conditions. The reason could be explained as follows: low pH value contributed to higher oxygen evolution potential and direct oxidation played the dominant role. However, there would be a certain side reaction of hydrogen forming in the negative area, which inevitably occupied some of the active spots (Eq. 3) (Guan et al., 2018). Under acidic conditions, the Fenton reaction occurred between Fe<sup>2+</sup> and ·OH on the electrode surface of GAC particles, which could improve the oxidation ability of the whole reaction system and enhance the removal effect of Cu-EDTA. On the contrary, with the pH increase, the side effect of oxygen forming would occur in the positive area. The decomposition of H2O2 into H2O and O2 under alkaline conditions was also occurred in a certain scavenging reaction with ·OH. In turn, the ·OH on the particle electrode surface decreased and the oxidation capacity was somewhat diminished, so that the treatment efficacy decreased at high pH values (Eqs 4-6) (Zheng et al., 2019; Zhang M.-h. et al., 2019). Therefore, the operation of the 3D-EF system with GAC particles at neutral or

**TABLE 3** | Pseudo-first-order kinetics parameters of removal effect of Cu–EDTA by  $Fe^{2+}$  dosage.

| Fe <sup>2+</sup> (mmol L <sup>-1</sup> ) | $K_{obs}$ (min <sup>-1</sup> ) | Correlation coefficient R <sup>2</sup> |
|--|--------------------------------|--|
| 0  | 0.0182                         | 0.9988                                 |
| 0.5                                      | 0.0204                         | 0.9930                                 |
| 1.0                                      | 0.0215                         | 0.9856                                 |
| 1.5                                      | 0.0169                         | 0.9924                                 |
| 2.0                                      | 0.0157                         | 0.9965                                 |

near neutral pH reduced the chemical requirements for pH regulation and reduced operating costs to achieve optimal treatment performance.

$$2H^+ + 2e^- \to H_2; \tag{3}$$

 $2H_2O_2 \rightarrow 2H_2O + O_2; \tag{4}$ 

$$H_2O_2 \rightarrow O_2 + 2H^+ + 2e^-; \tag{5}$$

$$H_2O_2 + \cdot OH \rightarrow H_2O + \cdot HO_2.$$
 (6)

# Influencing Factors of Cu–EDTA Removal by 3D-EF

#### Fe<sup>2+</sup> Dosage

The Fe<sup>2+</sup> dosage has certain influence on Cu–EDTA removal in a 3D-EF process. As shown in **Figure 3A**, the removal rate of Cu–EDTA presented an increasing trend first and then decreased with the increase of Fe<sup>2+</sup> dosage. The highest removal efficiency could reach up to 90.95%, which was achieved at a Fe<sup>2+</sup> dosage of 1 mmol L<sup>-1</sup> after 120 min reaction. Kinetic fitting of Fe<sup>2+</sup> dosage for Cu–EDTA removal is shown in **Figure 3B** with the increase of Fe<sup>2+</sup> concentration. The reaction rate constant  $K_{obs}$  also showed a trend of increasing first and then decreasing, and the reaction rate constant  $K_{obs}$  peaked at the Fe<sup>2+</sup> dosage of 1 mmol L<sup>-1</sup>. The reaction rate constant  $K_{obs}$  reached a maximum of 0.0215 at 1 mmol L<sup>-1</sup> Fe<sup>2+</sup> (**Table 3**).

 $Fe^{2+}$  was the core of the 3D-EF reaction system. The removal of Cu–EDTA depended mainly on the reaction of the plate and





**TABLE 4** | Pseudo-first-order kinetics parameters of Cu–EDTA removal with different particle electrode dosages.

| Particle<br>electrode (g L <sup>-1</sup> ) | K <sub>obs</sub> (min⁻¹) | Correlation coefficient R <sup>2</sup> |
|--|--------------------------|--|
| 1  | 0.0152                   | 0.9910                                 |
| 2  | 0.0164                   | 0.9973                                 |
| 3  | 0.0167                   | 0.9923                                 |
| 4  | 0.0190                   | 0.9874                                 |
| 5  | 0.0168                   | 0.9897                                 |
| 6  | 0.0154                   | 0.9857                                 |

the particles without  $Fe^{2+}$  adding into this reaction system. The activity of microelectrolysis was weak with low-dosage  $Fe^{2+}$  addition, and the Cu–EDTA removal rate gradually increased with increasing  $Fe^{2+}$  dosage to generate more ·OH through the system reaction (**Eq. 7**) (Feng et al., 2010; Chu et al., 2021). Too high  $Fe^{2+}$  concentration increased the contact probability of  $Fe^{2+}$  and  $H_2O_2$  and also subsequently increased the ·OH production. However, too much of  $Fe^{2+}$  and ·OH produced side effects and formed  $Fe^{3+}$ , which consumed a large amount of ·OH, resulting in the decline of the Cu–EDTA removal rate in the 3D-EF reaction system (**Eq. 8**) (Huang et al., 2020; Zhang et al., 2020).

$$Fe^{2+} + H_2O_2 + H^+ \rightarrow Fe^{3+} + OH + H_2O; \tag{7}$$

$$Fe^{2+} + \cdot OH \rightarrow Fe^{3+} + OH^{-}.$$
 (8)

#### Particle Electrode Dosage

Particle electrode loading was also another key factor affecting the 3D-EF reaction system to treat Cu–EDTA. As seen in the inset of **Figure 4A**, the removal rate of Cu–EDTA was similar with that of the Fe<sup>2+</sup> dosage experiment group, and the highest removal rate of Cu–EDTA was 87.71% after 120 min of reaction when the particle electrode was 4 g L<sup>-1</sup> **Figure 4B**; **Table 4** showed that the removal efficiency of the Cu–EDTA reaction rate constant  $K_{obs}$  reached a maximum value of 0.0190 at the particle electrode dosage of 4 g L<sup>-1</sup>.

The particle electrode was distributed throughout the reaction system and formed microelectrode particles under the action of an electric field, which increased the specific surface area of the electrode, shortened the electrode spacing, greatly improved the mass transfer rate and current utilization efficiency, and improved the treatment capacity of pollutants (Dargahi et al., 2021). As the particle electrode increased, the surface area and the adsorption sites on the electrode increased, and then the Cu-EDTA removal efficiency increased accordingly (Wang et al., 2021). With the continuous increase of the particle electrode, the excess particle electrode occupied more space in the reaction system, which made the reaction system overloaded. In turn, the current and mass efficiencies will also be affected, such as leading to the short circuiting of the particle electrode and inhibiting the removal of contaminants (Zheng et al., 2016; Ghanbarlou et al., 2020).

#### **Current Density**

**Figure 5A** shows the removal effect of Cu–EDTA at different current densities. The worst removal effect of Cu–EDTA was 71.52% after 120 min at a current density of 2 mA cm<sup>-2</sup>. With the increase of current density to 10 mA cm<sup>-2</sup>, the best removal efficiency of Cu–EDTA was obtained with the removal rate of 87.26%. However, Cu–EDTA removal efficiency showed a decreasing trend as the current density continued to increase to 12 mA cm<sup>-2</sup> within the reaction system. In **Figure 5B**, the reaction rate constants  $K_{obs}$  at a current density of 10 mA cm<sup>-2</sup> were much larger than those at other current densities. From **Table 5**, the reaction rate constant  $K_{obs}$  reached a maximum of 0.0180 at a current density of 10 mA cm<sup>-2</sup>.

As the current density increased within the reaction system, the electron density and  $H_2O_2$  production on the electrode also gradually increased, and Fe<sup>2+</sup> reacted with  $H_2O_2$  to generate ··OH (Eq. 9). Moreover, the removal of Cu–EDTA gradually increased because the electron transfer between electrodes increased and accelerated the progress of its direct oxidation reaction on the electrode surface (Barhoumi et al., 2016; Moreira et al., 2019). Further increasing current density did not significantly improve



FIGURE 5 | (A) Effects of current density on the removal efficiency of Cu-EDTA and (B) kinetic fitting of removal effect of Cu-EDTA.

**TABLE 5** | Pseudo-first-order kinetics parameters of Cu–EDTA removal with different current density.

| Current<br>density (mA cm <sup>-2</sup> ) | K <sub>obs</sub> (min⁻¹) | Correlation coefficient R <sup>2</sup> |
|---|--------------------------|--|
| 2   | 0.0115                   | 0.9706                                 |
| 4   | 0.0142                   | 0.9759                                 |
| 6   | 0.0156                   | 0.9905                                 |
| 8   | 0.0159                   | 0.9817                                 |
| 10  | 0.0180                   | 0.9823                                 |
| 12  | 0.0160                   | 0.9872                                 |

the removal efficiency of Cu–EDTA because excess  $H_2O_2$  was a scavenger of  $\cdot$ OH. The high current density would accelerate the decomposition of  $H_2O_2$  and promote the occurrence of competitive side reactions such as hydrogen evolution (**Eq. 3**) and oxygen evolution (**Eq. 10**) resulting in the decrease of the concentration of  $\cdot$ OH (Zhang et al., 2020; Zhang et al., 2022).

$$Fe^{2+} + H_2O_2 \rightarrow Fe^{3+} + OH^- + OH;$$
(9)

$$2H_2O \rightarrow O_2 + 4H^+ + 4e^-.$$
 (10)

## **Coexisting Ions**

The efficiency of the 3D-EF reaction system was affected by all kinds of ions in wastewater, which could accelerate the decomposition rate of  $H_2O_2$  through competitive adsorption. The images as shown in **Figure 6A** further supported that the coexistent Cl<sup>-</sup> could promote the removal of pollutions in the 3D-EF reaction system. After 120 min, the Cu–EDTA removal rate reached 87% in the control group, and the experiment group after adding Cl<sup>-</sup> could achieve 87.55% removal efficiency, which was slightly improved by 0.55% compared with that of the control group. Hence, it can be concluded that Cl<sup>-</sup> owned a certain promoting effect on the removal of Cu–EDTA was 85.45 and 82.90%, respectively, when NO<sub>3</sub><sup>-</sup> and HPO<sub>4</sub><sup>2-</sup> were added into the reaction system for 120 min, which was 1.55 and 4.1%



**TABLE 6** | Pseudo-first-order kinetics parameters of Cu–EDTA removal with coexisting ions.

| Coexisting ions    | $K_{obs}$ (min <sup>-1</sup> ) | Correlation coefficient R <sup>2</sup> |
|--------------------|--------------------------------|--|
| Control group      | 0.0178                         | 0.9955                                 |
| CI-                | 0.0186                         | 0.9930                                 |
| NO3                | 0.0167                         | 0.9953                                 |
| HPO4 <sup>2-</sup> | 0.0157                         | 0.9942                                 |

lower than that of the control group. This phenomenon reflected that  $\rm NO_3^{-}$  and  $\rm HPO_4^{\ 2^-}$  could inhibit the removal of Cu–EDTA.

From **Figure 6B**, the slope of the reaction system with the addition of the Cl<sup>-</sup> group was larger than that of the control group, while the slopes of the reaction system with the addition of  $NO_3^-$  and  $HPO_4^{2-}$  groups were smaller than those of the control group. The reaction rate constant  $K_{obs}$  of 0.0186 for the addition of the Cl<sup>-</sup> group was larger than that of the control group (0.0178) and so as the addition of  $NO_3^-$  and  $HPO_4^{2-}$  groups (0.0167 and 0.0157, respectively) (**Table 6**).

It was noticed that a certain promotion of Cu-EDTA removal was found after the addition of Cl<sup>-</sup>, which was related to the reactive chlorine species generated in this reaction system. Because the active species generated after the addition of Clexhibited a higher lifetime than .OH, the diffusion of active species played a promoting role for Cu-EDTA removal (Rommozzi et al., 2020; Mandal et al., 2020). Cl- involved in the hydrogen evolution reaction in the anode region to form Cl<sub>2</sub> and underwent further hydrolysis to form highly oxidized ClOpromoting the removal of Cu-EDTA (Eqs 11-13). NO<sub>3</sub><sup>-</sup> and HPO<sub>4</sub><sup>2-</sup> would have a competitive electronic effect with Cu-EDTA, and  $NO_3^-$  and  $HPO_4^{2-}$  were also able to scavenge a certain ·OH, which in turn generated more reactive NO3·and H<sub>2</sub>PO<sub>4</sub>·leading to a decrease in Cu-EDTA removal effect (Eqs 14, 15) (Cheng et al., 2017; Teng et al., 2021). Therefore, NO<sub>3</sub><sup>-</sup> and HPO<sub>4</sub><sup>2-</sup> would inhibit Cu–EDTA removal in the 3D-EF reaction system.

$$2\mathbf{C}\mathbf{l}^{-} \to \mathbf{C}\mathbf{l}_{2} + 2\mathbf{e}^{-}; \tag{11}$$

$$Cl_2 + H_2O \leftrightarrow HOCl + Cl^- + H^+;$$
 (12)

$$HOCl \leftrightarrow H^+ + OCl^-; \tag{13}$$

$$NO_3^- + \cdot OH \rightarrow NO_3 \cdot + OH^-;$$
 (14)

$$H_2 PO_4^- + \cdot OH \to OH^- + H_2 PO_4^-$$
(15)

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#### CONCLUSION

In this study, the 3D-EF reaction system using GAC particles as particle electrodes could effectively achieve the goal of Cu–EDTA decomplexation. The performance of Cu–EDTA decomplexation by 3D-EF was better than that by the GAC and EF with a decomplexation efficiency of 90.95%, which broke the pH limit of the traditional EF reaction system and widened the application window of pH. Cu–EDTA was optimally treated at an initial pH of 7, 1 mmol L<sup>-1</sup> Fe<sup>2+</sup>, 4 g L<sup>-1</sup> GAC, and current density of 10 mA cm<sup>-2</sup>. In addition, Cl<sup>-</sup> promoted the removal of Cu–EDTA in the 3D-EF reaction system; however, NO<sub>3</sub><sup>-</sup> and HPO<sub>4</sub><sup>2-</sup> inhibited Cu–EDTA removal.

# DATA AVAILABILITY STATEMENT

The original contributions presented in the study are included in the article/supplementary material, further inquiries can be directed to the corresponding authors.

## AUTHOR CONTRIBUTIONS

YM contributed to data curation, methodology, writing-original draft, and writing-review and editing; XH designed all experiments and revised and examined the manuscript; JY contributed to review and editing; FY contributed to data curation and investigation; and JZ interpreted the data and resources. All authors read and approved the final manuscript.

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