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# Transaction strategy of virtual power plants and multi-energy systems with multi-agent Stackelberg game based on integrated energy-carbon pricing

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A virtual power plant (VPP) has the ability to aggregate numerous decentralized distributed energy resources using advanced control technology, offering a promising approach for low-carbon development. In order to enhance the VPP's contribution to reducing carbon emissions, a bi-level framework is proposed that incorporates an integrated energy-carbon price response mechanism. This model allows VPPs to participate in a multi-energy system through a multi-agent Stackelberg game framework. Initially, a transaction model is established where the power distribution system operator and the gas distribution system operator act as leaders, while the virtual power plant operator acts as a follower in the multi-energy system. Subsequently, an integrated energy-carbon pricing method, rooted in carbon emission flow theory, is introduced to encourage VPPs to proactively adjust their energy-use and trading strategies within multi-energy systems, thereby promoting multiprincipal interactive trading. To achieve a distributed solution among multiple entities while maintaining the privacy of each entity's information, the adaptive step-size alternating direction multiplier method is employed. The feasibility and effectiveness of the proposed model and method are then demonstrated through case studies.

#### KEYWORDS

virtual power plant, multiple energy systems, carbon emission flow, energy-carbon integrated price, multi-agent Stackelberg game

## **1** Introduction

The construction of a new type of power system primarily based on new energy resources is being accelerated, emphasizing both centralized and distributed energy resources. However, distributed energy resources (DERs), characterized by strong uncertainty, decentralization, and heterogeneity (Chen et al., 2021), pose significant threats to the security of grid-connected power systems due to their large numbers. Virtual power plants (VPPs) are widely employed to effectively aggregate large, dispersed, and diverse DERs through advanced control, metering, communication, and other technologies (Vasirani et al., 2013; Zhao et al., 2018; Bhuiyan et al., 2021). This facilitates accurate control of internal resources, providing a viable pathway for low-carbon

development. In the context of the interactive integration of multiple energy systems (Wang et al., 2018), VPPs participating in both the power distribution and gas distribution systems can leverage the complementary characteristics of electricity and gas. This enables the realization of synergistic operations within a multi-energy network, enhancing the economic efficiency and promoting lowcarbon objectives for all stakeholders involved.

To advance the role of VPPs in the low carbon economy, several research studies have been conducted. Previous works in (Zhang et al., 2023) examine the interactions between VPPs and the higherlevel grid based on peak and off-peak time-sharing tariffs. It also developed an operational model for VPPs under carbon trading and green certificate trading mechanisms, considering both economic and low-carbon aspects. Reference (Yi et al., 2020a) addresses power flow constraints in the distribution network by formulating a twolayer planning problem involving VPPs and the distribution network, optimizing dynamic pricing for VPPs. Reference (Yi et al., 2020b) proposes a two-layer model for VPPs and the distribution system, achieving co-optimization of multiple VPPs with the distribution network through an integrated active and reactive power pricing approach. These studies primarily focus on transaction pricing strategies for VPPs in the distribution market, with an increasing involvement of VPPs in multi-energy system transactions due to the close integration of various energy systems. Reference (Yang et al., 2021) introduces a model for energy trading in micro-energy networks that considers electricity-heat multi-energy sharing, ultimately reducing energy costs for multienergy micro-grids. Additionally, works in (Zhang and Hu, 2022) suggest an optimal scheduling model for VPPs to engage in simultaneous trading within the electricity-gas multi-energy market, considering security constraints of the natural gas network and bidirectional flow of electricity and natural gas. However, the majority of these studies view VPPs predominantly as passive recipients of energy prices, ignoring their potential for active participation in multi-energy system trading and interactions with other entities.

With the advancement of VPP technology, conflicts of interest stemming from the involvement of various entities in competitive multi-energy markets have become inevitable. Game theory is increasingly being utilized to address optimization problems related to VPPs. In (Xu et al., 2022), a VPP pricing strategy is proposed within a two-tier market structure involving multiple VPPs and distribution markets. A non-cooperative pricing game model is established to enhance the economic efficiency of multiple entities. Meanwhile, Reference (Liu, 2022) introduces a cooperative game model for VPP scheduling in the context of multiple regional integrated energy systems. This model aims to optimize multiple energy sources to meet the electricity-heat-gas demand of each integrated energy system within the VPP coordinated scheduling strategy, fostering cooperative benefit sharing among members. In analyzing the intricate interactions among providers and responders of energy prices across multiple entities in multi-energy system transactions, a master-slave game model is deemed more appropriate for understanding the sequential order of the game. The research in (Zangeneh et al., 2018) adopts a multi-leader-follower master-slave game model to describe the competition between multiple VPPs and the superior market,

determining the optimal pricing strategy for multiple parties to realize optimal transactions for each entity. The study in (Wei et al., 2017) investigates multi-energy interaction transaction strategies between multiple distributed energy stations and users by constructing an energy transaction model based on a multi-leader-multiple-follower game. A model in (Chen et al., 2023) constructs a Stackelberg game trading model involving energy retailers and VPPs, where the energy operator guides the power purchase and sale behavior of VPP through tariff optimization. Research in (Lu Q. et al., 2023) proposes a onemaster-many-slave game optimization model for community integrated energy systems, considering carbon trading mechanisms and integrated demand response, which realizes interactive equilibrium between energy suppliers and load aggregators, significantly improving the economic and lowcarbon benefits of each entity.

However, there are still research gaps in the above studies, which are mainly manifested in the following two aspects: 1) Existing studies on low-carbon operation of VPPs primarily focus on carbon emission measurement from the power supply side, with less emphasis on the demand side. This limitation hinders the ability to guide load-side low-carbon electricity consumption behavior. Carbon emission flow (CEF) theory, as an effective analytical method for the low-carbon development of power systems (Cheng et al., 2019a; Cheng et al., 2019b; Sun et al., 2023), offers new perspectives on load-side carbon emission responsibility sharing and facilitates low-carbon demand response. Studies (Lu Z. et al., 2023; Yan et al., 2023) have proposed low-carbon optimal dispatch models for multi-energy systems based on CEF theory. These models implement carbon-aware distribution locational marginal pricing (CDLMP) and stepped carbon pricing to actively guide loads in reducing system carbon emissions. 2) The measurement methods of VPP carbon emissions in existing studies are not sufficiently accurate. Most studies only consider the internal carbon emissions of VPPs, neglecting the indirect carbon emissions resulting from purchasing electricity from the higher grid and gas from the gas grid. Furthermore, the purchase and sale of energy are usually based on fixed or time-based pricing, which does not account for the significant potential of integrated energy-carbon pricing to reduce VPP carbon emissions.

This paper proposes a bi-level model that optimizes a multiagent Stackelberg game with VPP participation in multi-energy systems under an integrated energy-carbon price response mechanism. In this model, the distribution system operator (DSO) and gas system operator (GSO) act as leaders, while the VPP operator (VPPO) acts as a follower. The model focuses on VPP participation in a multi-energy system under the energycarbon integrated price response mechanism. The paper also introduces an integrated energy-carbon pricing method based on CEF theory to help VPPs adjust their energy consumption and trading strategies to reduce carbon emissions. The study includes carbon flow tracking for distributed VPP energy transactions, taking into account the carbon emission responsibilities of VPPs when purchasing electricity and natural gas. To ensure privacy, the adaptive step-size alternating direction method of multipliers (ADMM) is used for a distributed solution. The effectiveness of the proposed model and method is demonstrated through case analysis.

Up	per level: DSO	GSO Multi-Le	eader	
Power distribu	Power distribution network		Gas distribution network	
Objective function: Minimize the total o the power distribution Decision variables: LMEP, Node carbor Power purchased from	perating cost of on network n intensity, om the higher grid	Objective function: Minimize the total operating cost of the gas distribution network Decision variables: LMGP, Node carbon intensity, Gas output		
Energy-Carbon combined price	Upper ar level into Lower level: V	nd lower eraction	Electricity purchase Gas purchase	
1	Objective function: Minimize total VPP operating costs			
1	Decision variables: Purchased electricit Operating output, D	y, Purchased gas Demand response		

## 2 Electric-gas multi-energy system and VPP low-carbon operation bilevel framework

The study aims to develop a low-carbon economic operational model suitable for power distribution networks, gas distribution networks, and VPPs. Due to conflicting objective functions among the three stakeholders, i.e., DSO, GSO, and VPPO, and the presence of multiple variables, a bi-level model for the interactions between multi-energy systems and the VPP considering integrated energycarbon pricing is proposed. The transaction dynamics between DSO, GSO, and VPPO are modeled as a multi-agent Stackelberg game, where DSO and GSO are considered as the leaders and VPPO as the follower. The bi-level transaction framework is illustrated in Figure 1.

The upper level features the optimal scheduling model for the electricity-gas multi-energy system. The DSO and GSO calculate the optimal power flow (OPF) for the power distribution network and the gas distribution network based on the energy purchasing demand transmitted from the lower level. Their objective is to minimize the total operating cost for each of them. They also integrate the distribution network trends to solve the distribution of the CEF and formulate the integrated energy-carbon price. For energy pricing, this paper adopts the locational marginal electricity price (LMEP) and locational marginal gas price (LMGP). The decision information derived from this process is then provided back to the lower-level model. The follower VPP at the lower level responds to the integrated energy-carbon price information by optimizing the energy use of internal gas turbine CHP units, gas boilers, power storage equipment, and distributed wind power, with the goal of minimizing the total operating cost. The VPP develops the internal optimal scheduling strategy and uploads the power purchasing demand and gas purchasing demand information to the upper-level DSO and GSO, respectively.

In summary, the power distribution network and the gas distribution network optimize OPF and CEF based on the energy purchase demand of the VPP and its internal optimization results. They then pass the integrated energy-carbon price and node carbon intensity obtained from the solution back to the VPP. The VPP uses this information to formulate the latest internal optimization scheduling strategy and update its energy purchase demand. This iterative process continues until the transactions of each subject in the bi-level model reach a consensus and meet the convergence conditions, thus achieving the overall optimal operation of the power distribution network, gas distribution network, and VPP.

# 3 A bi-level formulation for energy transaction

Since DSOs, GSOs, and VPPOs represent different stakeholders, it is essential to establish transaction models for each party that consider the interaction of electricity and natural gas between the distribution and the VPP. This includes the energy pricing model of the upper-tier electricity-gas multi-energy system, the carbon pricing model, and the lower-level VPP energy optimization model.

# 3.1 Energy pricing modeling for electric-gas multi-energy systems

#### 3.1.1 Pricing model for power distribution networks

In this section, the LMEP pricing model for power distribution networks based on second order cone programming (SOCP) is constructed with the objective of minimizing the operating cost of power distribution networks (Xie et al., 2023; Xie et al., 2024).

#### 3.1.1.1 Objective function

The objective of the DSO is to minimize the total operating cost  $f_{\text{DSO}}$  of the power distribution network, including the cost  $C_t^{\text{b}}$  of coal-fired unit generation and the cost  $C_t^{\text{grid}}$  of purchased power from the higher grid, as presented in Eqs 1–3 as follows:

$$\min f_{\text{DSO}} = \sum_{t=1}^{T} \left( C_t^{\text{b}} + C_t^{\text{grid}} \right) \tag{1}$$

$$C_t^{\mathsf{b}} = \sum_{g \in G} \left( a_g \left( P_{g,t} \right)^2 + b_g P_{g,t} + c_g \right) \tag{2}$$

$$C_t^{\rm grid} = \lambda_t^{\rm grid} P_t^{\rm grid}$$
(3)

where *T* is the total number of scheduling hours; *G* is the set of coalfired units in the distribution network;  $a_g$ ,  $b_g$  and  $c_g$  are the generation cost coefficients of the coal-fired units *g*;  $P_{g,t}$  is the active power output of the units at the moment *t*;  $\lambda_t^{\text{grid}}$  is the selling price of the higher-level grid at the moment *t*; and  $P_t^{\text{grid}}$  is the active power purchased by the DSO from the higher-level grid at the moment *t*.

#### 3.1.1.2 Power system constraints

$$\sum_{g \in n} P_{g,t} + \sum_{w \in n} P_{w,t}^{\text{wind}} + P_t^{\text{grid}} - P_t^{\text{buy}} = P_{n,t}^{\text{L}} + \sum_{b(n,\cdot) \in n} P_{b,t}^{\text{DN}} - \sum_{l(\cdot,n) \in n} \left( P_{l,t}^{\text{DN}} - a_{l,t}r_l \right): \lambda_{n,t}^{\text{LMEP}}$$

$$n \in N_{DN}$$

(4)  
$$\sum_{g \in n} Q_{g,t} + Q_t^{\text{grid}} - \eta P_t^{\text{buy}} = Q_{n,t}^{\text{L}} + \sum_{b(n,\cdot) \in n} Q_{b,t}^{\text{DN}} - \sum_{l(\cdot,n) \in n} \left( Q_{l,t}^{\text{DN}} - a_{l,t} x_l \right)$$
(5)

$$\left(P_{b,t}^{\mathrm{DN}}\right)^2 + \left(Q_{b,t}^{\mathrm{DN}}\right)^2 \le S_l^2 \tag{6}$$

$$P^{\rm DN} = a_1 r_1^2 + (O^{\rm DN} = a_1 r_1)^2 \le S^2$$
(7)

$$(\mathbf{r}_{l,t} - u_{l,t}r_{l}) + (Q_{l,t} - u_{l,t}x_{l}) \leq S_{l}$$

$$(\mathbf{p}_{l,t}^{\text{DN}})^{2} + (\mathbf{p}_{l,t}^{\text{DN}})^{2} + U$$

$$(2)$$

$$-2(r, \mathbf{P}^{\text{DN}} + r; \mathbf{O}^{\text{DN}}) + q; (r^{2} + r^{2}) - II$$
(9)

$$U_{n',t} - 2(r_l P_{l,t}^{\rm DN} + x_l Q_{l,t}^{\rm DN}) + a_{l,t} (r_l^2 + x_l^2) = U_{n,t}$$
(9)  
$$U^2 \le U_{n,t} \le U^2$$
(10)

$$U_{\min}^2 \le U_{n,t} \le U_{\max}^2 \tag{10}$$

$$\begin{cases} P_{g,\min} \le P_{g,t} \le P_{g,\max} \\ Q_{g,\min} \le Q_{g,t} \le Q_{g,\max} \end{cases}$$
(11)

where  $g \in n$ ,  $w \in n$  denotes the coal-fired unit g and fan w connected to node n, respectively;  $b(n, \cdot) \in n$  denotes the line

injected from node *n* to other nodes, denoted as *b*;  $l(\cdot, n) \in n$ denotes the branch l injected from other nodes to node n, respectively;  $N_{\rm DN}$  is the set of nodes in the distribution network;  $P_{w,t}^{\text{wind}}$  is the active power output of fan w at the moment t;  $P_t^{\text{buy}}$  is the purchased power of VPP to the distribution network at the moment  $t; P_{nt}^{L}, Q_{nt}^{L}$  are the active and reactive power loads connected to node n at the moment t, respectively;  $P_{b,t}^{\text{DN}}$ ,  $P_{l,t}^{\text{DN}}$ ,  $Q_{b,t}^{\text{DN}}$ ,  $Q_{l,t}^{\text{DN}}$  are the active and reactive power flowing through lines b and l at time t, respectively;  $a_{l,t}$ denotes the square of the current of branch *l* at time *t*;  $r_l$ ,  $x_l$  are the resistance and reactance of branch *l*, respectively;  $\lambda_{n,t}^{\text{LMEP}}$  is the dyadic variable corresponding to the active power balance constraint;  $Q_{q,t}$  is the reactive power output of coal-fired unit g at time t;  $Q_t^{\text{grid}}$  is the reactive power purchased by the distribution network from the higherlevel grid at time t;  $\eta$  denotes the power factor of the loads;  $U_{nt}$  is the square of the magnitude of the node n at time t;  $S_l$  is the upper limit of the apparent power of line  $l; U_{\min}, U_{\max}$  are the lower and upper limit of the magnitude of the node voltage, respectively;  $P_{g, \min}$ ,  $P_{g, \max}$ ,  $Q_{g, \min}$ ,  $Q_{q, \max}$  are the lower and upper limit of the active and reactive power output of unit g, respectively. Eqs 4, 5 represent the nodal active and reactive power balance constraints. Eqs 6, 7 represent the power flow limits in each line. Eq. 8 represents convex SOC relaxation to the original equality of the apparent power. Eq. 9 is the forward voltage drop equation. Eq. 10 is the limits of the nodal voltage. Eq 11 represents the generator active and reactive output constraints.

# 3.2 Pricing model for gas distribution networks

This section constructs a SOCP-based LMEP pricing model for gas distribution networks with the objective of minimizing the gas distribution network operating costs.

#### 3.2.1 Objective function

The gas distribution network consists of the gas source, gas pipeline, air compressor, and gas load, and in this paper it is assumed that the flow of natural gas in the gas pipeline has been determined. The objective of the GSO is to minimize the operating cost  $f_{\rm GSO}$  of the gas distribution network, i.e., to minimize the cost of natural gas purchased by the GSO from the natural gas company, which is expressed in the Eq. 12 as follows:

$$\min f_{\text{GSO}} = \sum_{t=1}^{T} \left( \sum_{s \in N_s} y_{s,t}^{\text{well}} w_{s,t}^{\text{well}} \right)$$
(12)

where  $y_{s,t}^{\text{well}}$ ,  $w_{s,t}^{\text{well}}$  are the price and volume of gas purchased by the GSO from gas source s at time *t*, respectively;  $N_s$  is the set of gas sources.

#### 3.2.2 Gas system constraints

$$\sum_{s \in j} w_{s,t}^{well} + \sum_{ij \in z(j)} w_{ij,t} - \sum_{jk \in v(j)} w_{jk,t} - w_{j,t}^{load} - w_t^{buy} = 0: \lambda_{j,t}^{LMGP}$$

$$j \in N_{GN}$$
(13)

$$w_{ij,t} = sign(\pi_{i,t} - \pi_{j,t})C_{ij}\sqrt{\left|(\pi_{i,t})^2 - (\pi_{j,t})^2\right|}$$
(14)

$$w_{ij}^{\min} \le w_{ij,t} \le w_{ij}^{\max} \tag{15}$$

$$\pi_j^{\text{max}} \le \pi_{j,t} \le \pi_j^{\text{max}} \tag{16}$$

$$\pi_{j,t} \le k \pi_{i,t} \tag{17}$$

$$w_s^{\min} \le w_{s,t}^{\text{well}} \le w_s^{\max} \tag{18}$$

where  $s \in j$  denotes the natural gas source s at node j; z(j) is the set of pipelines at the end node j; v(j) is the set of pipelines at the first node *j*;  $N_{GN}$  is the set of nodes in the distribution network;  $w_{ij,t}$ ,  $w_{jk,t}$  are the amount of natural gas flowing through the pipelines ijand *jk*, respectively, at time *t*;  $w_{j,t}^{\text{load}}$  is the gas load at node *j* of the gas distribution network;  $w_t^{\text{buy}}$  is the amount of natural gas purchased from the gas distribution network by the VPP, respectively, at time *t*;  $\lambda_{i,t}^{\text{LMGP}}$  is the dyadic variable corresponding to the natural gas node flow equilibrium constraints;  $\pi_{i,t}$  and  $\pi_{j,t}$  are the pressures at nodes *i* and j at time t, respectively;  $C_{ij}$  is the pipeline transmission characteristic parameters;  $w_{ij}^{max}$ ,  $w_{ij}^{min}$  are the upper and lower bounds on the amount of natural gas to be transmitted by the pipeline;  $\pi_i^{\text{max}}$ ,  $\pi_i^{\text{min}}$  are the upper and lower bounds on the gas pressure at node j, respectively; k is the compressor coefficients;  $w_s^{\max}$ ,  $w_s^{\min}$  are the upper and lower bounds on the output of the natural gas source s, respectively. Eq 13 is the natural gas node flow balance constraint. Eq 14 is the Weymouth equation (Chen et al., 2019) for the pipeline gas flow, where  $sign(\cdot)$  is a sign function that one when  $\pi_{i,t} \ge \pi_{i,t}$  and -1 otherwise. Eq 15 is the gas network pipeline flow limit. Eqs 16, 17 denote the natural gas nodal pressure constraints. Eq. 18 denotes the gas supply constraints of gas wells.

#### 3.3 Carbon pricing model for multi-energy systems based on CEF theory

#### 3.3.1 CEF modeling for multi-energy systems

While most of the CO2 in the energy industry is generated on the source side, the ultimate driver of carbon emissions is on the load side. The focus of this paper is on how to price carbon emissions from generation to end-users so that the right incentives can be provided between electricity-gas multi-energy systems. The theory of CEF, which is based on the energy flow of the system, can intuitively characterize the flow direction of carbon emission during the system operation, and improve the new analysis perspective for the low-carbon economic dispatch (Cheng et al., 2020). In the CEF model, the carbon flow index is usually used to describe the carbon emission apportionment, this paper mainly needs to obtain the carbon intensity of each node of the electric-gas multi-energy system as a carbon signal, and through the carbon tax to establish the link between the carbon price and the node carbon intensity accessed by the VPP, and the CEF model is established as follows.

#### 3.3.1.1 CEF modeling of power distribution networks

The node carbon intensity represents the value of carbon emissions equivalent to the generation side caused by a unit of electricity consumed at that node, calculated in Eq. 19 as follows:

$$e_{n,t}^{\text{ele}} = \frac{\sum_{g \in n} P_{g,t} e_g + \sum_{l(\cdot,n) \in n} \left( P_{l,t}^{\text{DN}} - a_{l,t} r_l \right) \rho_{l,t}}{\sum_{g \in n} P_{g,t} + \sum_{w \in n} P_{w,t}^{\text{wind}} + \sum_{l(\cdot,n) \in n} \left( P_{l,t}^{\text{DN}} - a_{l,t} r_l \right)}$$
(19)

where  $e_{n,t}^{\text{ele}}$ ,  $\rho_{l,t}$  denote the nodal carbon intensity of node *n* and the carbon flow intensity of branch *l* at time *t*, respectively;  $e_g$  is the carbon emission intensity of coal-fired unit *g*.

The branch carbon intensity denotes the equivalent value of carbon emission on the generation side caused by a unit of electricity transmitted by a tributary. According to the proportional sharing principle (Kang et al., 2015), the carbon flow intensity of all transmission lines flowing from node n is equal to the carbon intensity of that node, which is expressed in Eq. 21 as follows:

$$\rho_{l,t} = e_{n,t}^{\text{ele}}, \forall l(n, \cdot) \in n$$
(20)

#### 3.3.1.2 CEF modeling of gas distribution networks

The gas distribution network CEF model is similar to that of the power distribution network, and the carbon intensity of each node and the branch carbon intensity are calculated as follows:

$$e_{j,t}^{\text{gas}} = \frac{\sum\limits_{s \in j} w_{s,t}^{\text{well}} e_s^{\text{well}} + \sum\limits_{ij \in \mathbb{Z}(j)} w_{ij,t} \rho_{ij,t}}{\sum\limits_{s \in j} w_{s,t}^{\text{well}} + \sum\limits_{ij \in \mathbb{Z}(j)} w_{ij,t}}$$
(21)

$$\rho_{ij,t} = e_{i,t}^{\text{gas}}, \forall ij \in z(j)$$
(22)

where  $e_{j,t}^{\text{gas}}$  is the carbon intensity of node *j* of the gas network at time *t*;  $\rho_{ij,t}$  is the carbon flow intensity of the gas flow into pipeline *ij* of the pipeline connected to node *j* at time *t*;  $e_s^{\text{well}}$  is the carbon emission intensity of the gas source *s* connected to node *j*.

# 3.3.1.3 An integrated energy-carbon pricing approach based on the CEF theory

As consumers, the VPP must acknowledge their carbon emission responsibility when procuring electricity and gas from the power distribution and gas distribution networks. By utilizing the CEF model to calculate the nodal carbon intensity of these networks, a connection is established between the carbon price and nodal carbon intensity through carbon tax. Subsequently, the integrated electricity/gas energy-carbon pricing method is developed by combining the LMEP/LMGP with the carbon price in Eqs 23, 24 as follows:

$$\zeta_{n,t}^{\text{ele}} = \lambda_{n,t}^{\text{LMEP}} + \tau e_{n,t}^{\text{ele}}, \forall n, t$$
(23)

$$\varsigma_{j,t}^{\text{gas}} = \lambda_{j,t}^{\text{LMGP}} + \tau e_{j,t}^{\text{gas}}, \forall j, t$$
(24)

where  $\varsigma_{n,t}^{\text{ele}}$  is the integrated electricity-carbon price at node *n* of the power distribution network at time *t*;  $\varsigma_{j,t}^{\text{gas}}$  is the integrated gascarbon price at node *j* of the gas distribution network at time *t*;  $\tau$  is the carbon tax. The integrated energy-carbon pricing system encourages VPPs to proactively adjust their energy purchases and internal scheduling strategies, leading to reduced carbon emissions and operating costs.

### 3.4 VPP energy optimization model

The operational framework of the VPP established in this study is illustrated in Figure 2. It comprises gas turbine combined heat and power (CHP) units, gas boilers, distributed wind power,



and energy storage units. The flexible loads encompass electric and thermal loads, with consideration given to demand response for both to assist users in making informed energy demand adjustments. The VPP interfaces with the power distribution network via an electric power contact line and transports natural gas through a pipeline connecting it to the gas distribution network. Notably, this paper does not address the scenario of natural gas sales to the GSOs at this time.

## 3.4.1 VPP Objective Function

The objective of the VPP energy optimization model is to minimize the total operating cost  $f_{\text{VPPO}}$  in Eqs 25–28 as follows:

$$\min f_{\text{VPPO}} = \sum_{t=1}^{T} \left( C_t^{\text{ele,buy}} + C_t^{\text{gas,buy}} + C_t^{\text{DR}} \right)$$
(25)

$$\mathcal{Q}_t^{\text{ele,buy}} = \varsigma_t^{\text{ele}} P_t^{\text{buy}} \tag{26}$$

$$C_t^{\text{gas,buy}} = \varsigma_t^{\text{gas}} w_t^{\text{buy}}$$
(27)

$$C_t^{\rm DR} = \lambda_e^{\rm cut} P_t^{\rm cut} + \lambda_e^{\rm tran} P_t^{\rm tran} + \lambda_h^{\rm cut} H_t^{\rm cut}$$
(28)

where  $C_t^{\text{ele,buy}}$  is the cost of electricity purchased by VPP interacting with the power distribution network;  $C_t^{\text{gas,buy}}$  is the cost of natural gas purchased by VPP from the gas distribution network;  $C_t^{\text{DR}}$  is the cost of integrated demand response of electricity and heat in VPP;  $P_t^{\text{tran}}$ ,  $P_t^{\text{cut}}$  denotes the amount of electric load transfer and load reduction in VPP at time t, respectively;  $H_t^{\text{cut}}$  denotes the amount of heat load reduction in VPP at time t;  $\lambda_e^{\text{cut}}$ ,  $\lambda_e^{\text{tran}}$  are the unit price of compensation for electric load reduction and transfer;  $\lambda_h^{\text{cut}}$  denotes the unit price of compensation for heat load reduction.

#### 3.4.2 VPP operational constraints

#### 3.4.2.1 Power balance constraints

The power balance constraints for multiple energy flows within the VPP are given in Eq. 29 as follows:

$$P_t^{\text{CHP}} + P_t^{\text{Wind}} + P_t^{\text{ES,dis}} + P_t^{\text{buy}} = P_t^{\text{ES,cha}} + P_t^{\text{load}}$$

$$H_t^{\text{CHP}} + H_t^{\text{GB}} = H_t^{\text{load}}$$

$$w_t^{\text{buy}} = w_t^{\text{GT}} + w_t^{\text{GB}}$$
(29)

where  $P_t^{\text{CHP}}$ ,  $H_t^{\text{CHP}}$  are the power supplied by the gas turbine and the heat production power at time t, respectively;  $P_t^{\text{Wind}}$  is the actual output of renewable energy at time t;  $P_t^{\text{ES,cha}}$ ,  $P_t^{\text{ES,dis}}$  are the charging and discharging power of the electrical energy storage at time t;  $P_t^{\text{load}}$ ,  $H_t^{\text{load}}$  are the amount of load after the demand response of electric and thermal loads at moment t;  $H_t^{\text{GB}}$  is the gas boiler heat power at time t;  $w_t^{\text{GT}}$ ,  $w_t^{\text{GB}}$  are the amount of natural gas input to the gas turbine and gas boiler at moment t, respectively.

#### 3.4.2.2 Gas turbine CHP unit constraints

The mathematical model and constraints for power and heat supply of CHP units are in Eq. 30 as follows:

$$P_{t}^{\text{CHP}} = \eta_{\text{P}}^{\text{CHP}} \frac{L_{\text{CH}_{4}}}{Q_{\text{EH}}} w_{t}^{\text{GT}}$$

$$P_{\text{min}}^{\text{CHP}} \leq P_{t}^{\text{CHP}} \leq P_{\text{max}}^{\text{CHP}}$$

$$H_{t}^{\text{CHP}} = \eta_{\text{H}}^{\text{CHP}} \frac{L_{\text{CH}_{4}}}{Q_{\text{EH}}} w_{t}^{\text{GT}}$$
(30)

where  $\eta_{\rm P}^{\rm CHP}$ ,  $\eta_{\rm H}^{\rm CHP}$  are the gas turbine power supply efficiency and heat production efficiency;  $L_{\rm CH_4}$  is the calorific value of natural gas per unit volume;  $Q_{\rm EH}$  is the thermal energy converted per unit of electrical energy;  $P_{\rm max}^{\rm CHP}$ ,  $P_{\rm min}^{\rm CHP}$  are the upper and lower limits of the power supply of the gas turbine.

3.4.2.3 Gas boiler output constraints

$$\begin{cases}
H_t^{GB} = \eta_{GB} \frac{L_{CH_4}}{Q_{EH}} \omega_t^{GB} \\
H_{min}^{GB} \le H_t^{GB} \le H_{max}^{GB}
\end{cases}$$
(31)

where  $\eta_{GB}$  is the electric heat conversion efficiency of the gas boiler;  $H_{\text{max}}^{\text{GB}}$ ,  $H_{\text{min}}^{\text{GB}}$  are the upper and lower limits of the heat output of the gas boiler in the VPP, respectively. Eq. 31 represents the operating constraints of GB.

#### 3.4.2.4 Energy storage unit constraints

The introduction of energy storage devices can further improve the operational flexibility of the VPP, the energy storage device is modeled in Eq. 32 as follows:

$$\begin{cases} S_t = (1 - \eta^{\text{loss}})S_{t-1} + \eta^{\text{cha}}P_t^{\text{ES,cha}} - \frac{P_t^{\text{ES,dis}}}{\eta^{\text{dis}}}\\ S_1 = S_{24}\\ 0 \le P_t^{\text{ES,cha}} \le \mu_t^{\text{ES,cha}}P_{\max}^{\text{ES,cha}}\\ 0 \le P_t^{\text{ES,dis}} \le \mu_t^{\text{ES,dis}}P_{\max}^{\text{ES,dis}}\\ \mu_t^{\text{ES,cha}} + \mu_t^{\text{ES,dis}} \le 1\\ S^{\min} \le S_t \le S^{\max} \end{cases}$$
(32)

where  $S_t$  is the capacity of the energy storage device in the VPP at time t;  $\eta^{\text{loss}}$ ,  $\eta^{\text{ES,cha}}$ ,  $\eta^{\text{ES,dis}}$  are the energy storage device energy loss coefficient, energy charging and discharging efficiency; where  $\eta^{\text{loss}} \ll 1$ ;  $P_{\max}^{\text{ES,cha}}$ ,  $P_{\max}^{\text{ES,dis}}$  are the maximum charging and discharging power of the energy storage device;  $S^{\min}$ ,  $S^{\max}$  are the minimum and maximum storage capacity of the energy storage device;  $\mu_t^{\text{ES,cha}}$ ,  $\mu_t^{\text{ES,dis}}$  are the binary variable, respectively, represents the charging and discharging state of the energy storage device at t time.

# 3.4.2.5 Electric heat integrated demand response constraints

$$\begin{cases} P_{t}^{\text{load}} = P_{t}^{0} + P_{t}^{\text{tran}} - P_{t}^{\text{cut}} \\ |P_{t}^{\text{tran}}| \leq P_{\max}^{\text{tran}} \\ \sum_{t=1}^{T} P_{t}^{\text{tran}} = 0 \\ 0 \leq P_{t}^{\text{cut}} \leq P_{\max}^{\text{cut}} \\ H_{t}^{\text{load}} = H_{t}^{0} - H_{t}^{\text{cut}} \\ 0 \leq H_{t}^{\text{cut}} \leq H_{\max}^{\text{cut}} \end{cases}$$
(33)

Eq. 33 represents the Electric heat integrated demand response constraints, where  $P_t^0$  denotes the initial load of electric load in VPP at time *t*;  $P_{\text{max}}^{\text{tran}}$  denotes the upper limit of transferable electric load;  $P_{\text{max}}^{\text{cut}}$  denotes the upper limit of curtailable electric load;  $H_t^0$  denotes the initial load of thermal load at time *t*;  $H_{\text{max}}^{\text{cut}}$  denotes the maximum curtailable thermal load.

# 4 Solution method for the muti-agent stackelberg game trading model

In the context of a multi-agent Stackelberg game transaction model involving the leader DSO, GSO, and follower VPP in an electricity-gas multi-energy system, each participant optimizes its operation state according to individual interest objectives and devises energy transaction strategies accordingly. Given the intricate internal information and substantial transaction volume, traditional centralized optimization algorithms are inadequate in meeting the information privacy needs of each participant within this model. Therefore, the proposed solution involves solving the multi-participant Stackelberg game model through a distributed approach using the adaptive ADMM algorithm.

## 4.1 Stackelberg game trading model

The game model contains three elements: the set of participants, the set of strategies and the set of benefits (Li et al., 2022), and the Stackelberg game is modeled in Eq. 34 as follows:

$$G = \begin{cases} \{ \text{DSO, GSO, VPPO} \}; \\ \{ P_{g,t}, P_t^{\text{grid}}, w_{s,t}^{\text{well}}, \varsigma_{n,t}^{\text{ele}}, \varsigma_{j,t}^{\text{gas}} \}; \\ \{ P_t^{\text{buy}}, w_t^{\text{buy}} \}; \\ f_{\text{DSO}}, f_{\text{GSO}}, f_{\text{VPPO}} \end{cases} \end{cases}$$
(34)

- Participant set: {DSO, GSO, VPPO} represents the set of all participants. Where DSO and GSO are leaders and VPPO are followers.
- (2) Strategy set: the strategy of the leader DSO is the amount of electricity purchased from each distributed generator and the higher grid at each moment and the integrated electricity-carbon price set, denoted as {P<sub>g,t</sub>, P<sup>grid</sup><sub>t</sub>, s<sup>ele</sup><sub>t</sub>}; the strategy of the leader GSO is the amount of natural gas purchased from each distribution station and the integrated gas-carbon price set, denoted as {w<sup>well</sup><sub>s,t</sub>, s<sup>gas</sup><sub>j,t</sub>}; the strategy of the follower VPPO is the amount of electricity purchased with the DSO and the amount of gas purchased from the GSO, denoted as {P<sup>buy</sup><sub>t</sub>, w<sup>buy</sup><sub>t</sub>}.
- (3) Benefits: The benefits to each participant are their objective functions, which can be expressed as f<sub>DSO</sub>, f<sub>GSO</sub> and f<sub>VPPO</sub>, respectively.

# 4.2 Distributed solution of stackelberg game transaction model based on adaptive ADMM algorithm

The adaptive ADMM algorithm is utilized in this study for distributed solving of the proposed multi-agent Stackelberg game model. This approach ensures that the interaction between participating subjects does not compromise their internal privacy. Only the boundary information of each subject at the time of the transaction is required, enabling distributed and efficient solving while safeguarding the privacy of transactional information.

Based on the principle of ADMM algorithm, the auxiliary condition is introduced as shown in Eq. 35 as follows:

$$P_t^{\text{buy}} - P_t^{\text{ex}} = 0, w_t^{\text{buy}} - w_t^{\text{ex}} = 0$$
 (35)

where  $P_t^{\text{buy}}$ ,  $P_t^{\text{ex}}$  are the amount of electricity that the VPPO expects to trade with the DSO and the amount of electricity that the DSO expects to trade with the VPPO at time *t*, respectively;  $w_t^{\text{buy}}$ ,  $w_t^{\text{ex}}$  are the amount of natural gas that the VPPO expects to buy from the GSO and the amount of natural gas that the GSO expects to sell to the VPPO at time *t*, respectively.

Distributed models for optimal pricing of power distribution network, optimal pricing of gas distribution network and VPP

energy optimization are obtained based on ADMM principle, respectively.

# 4.2.1 Optimal pricing of power distribution network

$$L_{\text{DSO}} = \begin{cases} \min\left(f_{\text{DSO}} + \sum_{t=1}^{T} \left[\lambda_{t}^{\text{DSO}}\left(P_{t}^{\text{ex}} - P_{t}^{\text{buy}}\right) + \frac{\rho}{2} \|P_{t}^{\text{ex}} - P_{t}^{\text{buy}}\|_{2}^{2}\right]\right) \\ \text{s.t.} \quad (1) - (11), \quad (19) - (20), \quad (23) \end{cases}$$
(36)

The optimal pricing of power distribution network is presented in Eq. 36, where  $\lambda_t^{\text{DSO}}$  and  $\rho$  are the corresponding Lagrange multipliers and penalty factors of the DSO, respectively.

#### 4.2.2 Optimal pricing of gas distribution network

$$L_{\rm GSO} = \begin{cases} \min\left(f_{\rm GSO} + \sum_{t=1}^{T} \left[\lambda_t^{\rm GSO}(w_t^{\rm ex} - w_t^{\rm buy}) + \frac{\rho}{2} \|w_t^{\rm ex} - w_t^{\rm buy}\|_2^2\right]\right) \\ \text{s.t.} \quad (12) - (18), \quad (21) - (22), \quad (24) \end{cases}$$
(37)

The optimal pricing of gas distribution network is presented in Eq. 37, where  $\lambda_t^{\text{GSO}}$  is the Lagrangian multiplier for the GSO distribution solution.

# 4.2.3 Distributed model for VPP energy optimization

$$L_{\text{VPPO}} = \begin{cases} \min \left( f_{\text{VPPO}} + \sum_{t=1}^{T} \left[ \lambda_{t}^{1} \left( P_{t}^{\text{buy}} - P_{t}^{\text{ex}} \right) + \frac{\rho}{2} \left\| P_{t}^{\text{buy}} - P_{t}^{\text{ex}} \right\|_{2}^{2} \right] + \\ \sum_{t=1}^{T} \left[ \lambda_{t}^{2} \left( w_{t}^{\text{buy}} - w_{t}^{\text{ex}} \right) + \frac{\rho}{2} \left\| w_{t}^{\text{buy}} - w_{t}^{\text{ex}} \right\|_{2}^{2} \right] \end{cases} \\ \text{s.t.} \quad (25) - (33) \end{cases}$$
(38)

Distributed model for VPP energy optimization is presented in Eq. 38, where  $\lambda_t^1$ ,  $\lambda_t^2$  are the corresponding Lagrange multipliers when the VPPO expects to trade with the DSO and GSO, respectively.

The coupled variables and Lagrange multipliers are updated as follows:

$$\begin{bmatrix} z_t^{\text{ex},k+1} = \operatorname{argmin} L_z \left[ z_t^{\text{ex},k}, z_t^{\text{buy},k}, \lambda_t^{z,k} \right] \\ z_t^{\text{buy},k+1} = \operatorname{argmin} L_{\text{VPPO}} \left[ z_t^{\text{ex},k+1}, z_t^{\text{buy},k}, \lambda_t^{z,k} \right] \\ \lambda_t^{z,k+1} = \lambda_t^{z,k} + \rho \left( z_t^{\text{ex},k+1} - z_t^{\text{buy},k+1} \right) \end{bmatrix}$$
(39)

where z represents the energy type; k is the number of iterations for distributed solving.

The original residuals, pairwise residuals are calculated and the convergence conditions are provided in Eqs 40, 41 as follows:

$$\begin{cases} r_t^{k+1} = z_t^{\text{ex},k+1} - z_t^{\text{buy},k+1} \\ s_t^{k+1} = z_t^{\text{ex},k+1} - z_t^{\text{ex},k} \end{cases}$$
(40)

$$\begin{cases} \sum_{t=1}^{T} \left\| \boldsymbol{r}_{t}^{k+1} \right\|_{2} \leq \boldsymbol{\varepsilon}^{\text{pri}} \\ \sum_{t=1}^{T} \left\| \boldsymbol{s}_{t}^{k+1} \right\|_{2} \leq \boldsymbol{\varepsilon}^{\text{dual}} \end{cases}$$
(41)

where  $r_t^{k+1}$ ,  $s_t^{k+1}$  are the original residuals and pairwise residuals in the k + 1 iteration, respectively;  $\varepsilon^{\text{pri}}$ ,  $\varepsilon^{\text{dual}}$  are the convergence thresholds of the original and pairwise residuals, respectively.

The choice of step size significantly affects the speed of the ADMM solution. An inappropriate value can hinder convergence. This paper proposes an adaptive ADMM algorithm that dynamically updates the step size based on the relationship between original residuals and pairwise residuals. This approach aims to enhance algorithm convergence and reduce iteration time, as formulated in Eq. 42:

$$\rho^{k+1} = \begin{cases} \tau^{\text{incr}} \rho^{k} \|r^{k}\|_{2} > \mu \|s^{k}\|_{2} \\ \frac{\rho^{k}}{\tau^{\text{decr}}} \|s^{k}\|_{2} > \mu \|r^{k}\|_{2} \\ \rho^{k} & \text{other} \end{cases}$$
(42)

where  $\mu$  is the scaling factor between the original residuals and the pairwise residuals;  $\tau^{\text{incr}}$  and  $\tau^{\text{decr}}$  are the acceleration and deceleration factors of the step change, respectively.

The coupling variables are updated by the iterative form shown in Eq. 39 until the convergence condition in Eq. 41 is satisfied, and the specific algorithmic solution flowchart is shown in Figure 3.

# 5 Case study

## 5.1 Case description

In order to validate the models and algorithms proposed in this paper, the IEEE 33-bus power distribution network, 7node gas distribution network, and 1 VPP coupling composition are utilized. The network topology is illustrated in Figure 4, where W represents the wind turbine located at node 31 in the power distribution network. Additionally, G1 to G5 represent five coal-fired units situated at nodes 3, 9, 29, 14, and 21, with their operating parameters detailed in Supplementary Appendix Table SA1; Supplementary Appendix Figure SA1. W1 and W2 denote the gas distribution stations connected to nodes six and seven of the gas distribution network. Prediction curves for renewable energy output and load within the VPP can be found in Supplementary Appendix Figure SA2, along with unit parameters in Supplementary Appendix Table SA2.

It is assumed that the power factor  $\eta$  of the node loads in the distribution network is 0.85, and the price of power purchased from the higher-level grid is set to 160\$/MWh. The price of gas purchased by GSO from the gas source is set at 0.52\$/m3, and the carbon tax  $\tau$  is set to 45\$/tCO2. In the ADMM algorithm of adaptive step-size, the initial step-size  $\rho$  is set to 1, and the  $\mu$  is set to 10,  $\tau^{\text{incr}}$ ,  $\tau^{\text{decr}}$  are set to 2,  $\varepsilon^{\text{pri}}$  and  $\varepsilon^{\text{dual}}$  the thresholds of convergence, and are set to 10-3. In this paper, we build the simulation model based on the platform of Matlab 2018b and



the Gurobi solver is adopted to solve the simulation model. Solved using Gurobi solver.

In order to verify the impact of the multi-agent Stackelberg game on electricity-gas trading and the cost of energy purchase by each subject under the energy-carbon integrated price response mechanism, the following four energy settlement scenarios are set up.

**Case 1**: The settlement electricity price adopts fixed time-sharing electricity price, the settlement gas price adopts fixed natural gas price, the specific data are shown in Supplementary Appendix Table SA3, carbon emission flow is not considered, VPPOs completely act as the recipient of the price for the electricity-natural gas transaction, and the flexible loads in VPPs are not considered for the optimal scheduling.

**Case 2**: Based on Case 1, and the flexible loads within the VPP are considered for integrated demand response for electricity and heat.

**Case 3**: The LMEP and LMGP obtained after the game equilibrium of each subject are used for the power distribution network settlement price and the gas distribution network settlement price, respectively, without considering the carbon emission flow, and the flexible loads within the VPP are considered for optimal dispatch; Case 4: the electricity-carbon integrated price and gas-carbon integrated price obtained after the game equilibrium of each subject are adopted for the power distribution network settlement price and gas distribution network settlement price and gas distribution network settlement price and gas distribution network settlement price is considered, and optimal dispatch is considered for the flexible loads within the VPP, i.e., the model proposed in this paper.



TABLE 1 Comparison results of operating costs and carbon emissions of each subject under different scenarios.

Case	VPPO operating costs (\$)	DSO operating costs (\$)	GSO operating costs (\$)	Total cost of energy purchases (\$)	VPP carbon emissions (t)
Case 1	16118.5	8672.1	17926.5	42717.1	47.73
Case 2	12153.6	5338.9	16097.6	33590.1	32.84
Case 3	11539.2	4832.8	16817.2	33189.2	29.59
Case 4	13009.4	4776.7	18079.3	35865.4	27.43

# 5.2 Analysis of VPP simulation results

# 5.2.1 Comparative analysis of operation under different scenarios

The simulation results of the above four scenarios are shown in Table 1.

Table 1 illustrates that operating costs decrease and carbon emissions are effectively reduced when considering integrated demand response in Cases 2, 3, and 4 compared to Case 1. The dependency of VPP on power and gas distribution networks is also reduced through demand response of flexible loads, leading to decreased electricity and gas purchases. Case 3, which incorporates the interaction of VPPO with DSO and GSO master-slave game, shows a reduction in total energy purchase cost and carbon emissions by \$400.9 and 3.25 t CO2, respectively, compared to Case 2 with fixed energy settlement price. This demonstrates that settling energy prices using LMEP and LMGP can guide VPP energy optimization in a more costeffective manner, enhancing both economic and environmental aspects of VPP.

By comparing Case 3 and Case 4, it is evident that in Case 4, the integrated energy-carbon price led to a 7.29% decrease in carbon emissions from the VPP compared to Case 3. However, the energy purchase costs and total costs of the VPP increased in Case 4 due to the higher carbon price. Moreover, the inclusion of a carbon price incentivized VPPs to use more natural gas over purchased electricity, resulting in increased operating costs for GSOs and decreased costs for DSOs in Case 4. Overall, the proposed



multi-agent Stackelberg game trading strategy proves beneficial in enhancing the economic and low-carbon advantages for each agent.

#### 5.2.1.2 Analysis of price response mechanism.

The impact of different pricing methods on the power purchased by VPPs is analyzed by examining the power distribution network settlement tariffs and carbon price change curves for the nodes where the VPPs are located in Cases 3 and 4, as shown in Figure 5. Additionally, Figure 6 illustrates the carbon intensity for all nodes of the power distribution network under Case 4.

As shown in Figure 5, considering the carbon tax on VPP's electricity demand from the power distribution network



increases the purchase price. The integrated energy-carbon price is consistently higher than the LMEP, with its incremental increase varying over time. The difference between the integrated energy-carbon price and the LMEP is more pronounced at certain times (e.g., from 05:00 to 09:00) when the nodes have higher carbon emission densities. In contrast, while the combined gas-carbon price also rises, its change is minimal because the carbon intensity of each node in the gas distribution network is relatively uniform. The carbon emissions for VPPs purchasing gas from the gas distribution network depend solely on the amount of gas used. Consequently, the combined gas-carbon price remains essentially unchanged over time. In this paper, the LMGP of VPP coupled with the gas distribution network is calculated to be 0.5120 \$/m3, and the integrated gas-carbon price, considering the carbon tax, is 0.6174 \$/m<sup>3</sup>.

An examination of the carbon intensity of individual nodes in both Figure 6 and the IEEE 33-node system topology diagram indicates that nodes with wind turbines and their adjacent nodes have lower carbon intensity, attributed to the low carbon emissions of wind turbines. On the other hand, nodes connected to VPPs' power distribution network are situated near coal-fired units with high carbon emissions, impacting their carbon intensity. Nevertheless, the carbon intensity of these nodes aligns closely with that of thermal units. As a result, the carbon pricing of nodes linked to the power distribution network, as depicted in Figure 5, demonstrates minimal fluctuations over time.

To further investigate the impact of carbon pricing on the amount of electricity and gas purchased by VPPs, Figure 7 illustrates a comparison between the two scenarios. The results show that during the 05:00-10:00, Case 4, with carbon pricing, acquires less electricity but more natural gas compared to Case 3, without carbon pricing. This is due to the higher carbon intensity at the node connected to the power distribution network, as depicted in Figure 5. The node's carbon intensity is higher during 05:00-10:00, leading to a greater use of natural gas over electricity. Therefore, incorporating a carbon price incentivizes VPPs to utilize more natural gas and decrease electricity consumption.

In order to better understand the demand for purchased energy and carbon emissions of a VPP utilizing an integrated energycarbon price response mechanism, a comparison and analysis between Case 3 and Case 4 is conducted. The results of this comparison are illustrated in Figure 8. The visualization in Figure 8 demonstrates that, in Case 4 where carbon price is considered, natural gas becomes a more competitive option compared to Case 3 where carbon price is not a factor. Consequently, the VPP tends to procure natural gas with lower carbon intensity, leading to an increase in total gas volume purchased and a decrease in the purchase of electricity from the power distribution network with higher carbon intensity. This results in a reduction of 1.91 MWh in the total purchased electricity of the VPP. Furthermore, with the inclusion of carbon price, the total carbon emissions of the VPP decrease from 29585.8 kg to 27436.6kg, showcasing a significant reduction in carbon emissions due to the integrated energy-carbon price response mechanism. These findings suggest that the proposed multi-agent Stackelberg game energy settlement price effectively facilitates carbon emission reduction and enhances the low-carbon benefits of the VPP.



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#### 5.2.2 Analysis of VPP optimal schedule

The results of the optimization of electric power and thermal power inside the VPP are shown in Figure 9. For the VPP internal units, new energy consumption has the highest priority to minimize wind abandonment, and the VPP completes the internal optimal scheduling according to the combined energy-carbon price. The gas turbine CHP unit generates electricity and heat within the output range, and the electric energy storage is mainly charged when the energy-carbon integrated price is lower, such as 01:00-04:00 and 07: 00 moments, and discharged at 06:00 and 12:00-14:00 when the electricity-carbon integrated price is higher, so as to reduce the purchase of electricity from the power distribution network and reduce the total operating cost and carbon emissions, while the electric and heat loads are considered Comprehensive demand response can realize peak shaving and valley filling to alleviate the pressure of grid peaking; only when the internal unit output cannot meet its load demand, it purchases electricity from the power distribution network and





Algorithm	Step	Iterations/time	Solution time/s
Traditional ADMM	0.1	109	674
	1	63	402
	50	92	580
adaptive step size ADMM	0.1	68	451
	1	45	329
	50	75	483

TABLE 2 Comparison between traditional ADMM and ADMM with adaptive step size.

gas from the gas distribution network. Considering that the heat load demand within the VPP is prioritized to be met by the gas turbine CHP unit, after considering the heat load demand response, the vast majority of the moments are heat production by the gas turbine only, and only when the gas turbine is not enough to supply heat at the 23:00-24: 00 moments, the gas boiler GB unit will be powered up.

## 5.3 Algorithm convergence analysis

This section examines the iterative convergence of the proposed multi-agent Stackelberg game trading strategy. Figure 10A illustrates the converged iterations of the original and pairwise residuals in Case 4, while Figure 10B demonstrates the iterative convergence of the game interactions among DSO, GSO, and VPPO.

Based on the residual convergence analysis presented in Figure 10A, it is evident that the proposed algorithm achieves the desired level of accuracy after 45 iterations, converging within 10–3, with a computation time of 329 s. Figure 10B visually demonstrates that the cost of purchased energy for the leading DSO and GSO converges to \$4776.7 and \$18,079.3, respectively, while the cost for the follower VPPO converges to \$13009.4. This convergence indicates that the Stackelberg game between the DSO, GSO, and VPPO has reached equilibrium, where each agent cannot further reduce its operational cost by adjusting its trading strategy in isolation. These results highlight the strong convergence performance and computational efficiency of the distributed optimization algorithm proposed in this study.

In order to further validate the effectiveness of the adaptive ADMM algorithm proposed in this study, a comparative analysis with the fixed-step ADMM is conducted. The solution performance is documented in Table 2 for both fixed step size and adaptive step size ADMM. It is evident from Table 2 that the adaptive step-size ADMM, as opposed to the traditional ADMM, diminishes the reliance on the initial value selection through step size correction. This results in fewer iterations, reduced solving time, and enhanced solving efficiency.

# 6 Conclusion

This paper introduces a bi-level model and its solution method for a multi-agent Stackelberg game focused on synergistic low-carbon trading within Virtual Power Plants (VPPs) participating in multi-energy systems under an energycarbon integrated price response mechanism. The proposed trading strategy is analyzed and validated through an arithmetic example, leading to the following conclusions.

- (1) The integrated energy-carbon pricing approach, based on the CEF theory, is more effective in incentivizing VPPs to adjust their energy-use and trading strategies with multi-energy systems compared to LMEP and LMGP pricing approaches. This encourages VPPs to procure energy from both power distribution and gas distribution networks during periods of low carbon intensity, thereby reducing carbon emissions.
- (2) The proposed trading framework and multi-participant Stackelberg game model enhance energy interactions among participants, improving the economics and low-carbon benefits for each participant. Compared to traditional energy settlement methods, the integrated energy-carbon pricing method is shown to be more effective in this regard.

This study focuses on the trading of electricity and natural gas within a VPP with a multi-energy system. Future research will explore trading multiple energy sources and carbon emissions to achieve synergistic low-carbon trading. Furthermore, the impacts of renewable energy integration and load demand uncertainty in VPPs are also important areas for further investigation.

# Data availability statement

The original contributions presented in the study are included in the article/Supplementary Material, further inquiries can be directed to the corresponding author.

## Author contributions

YY: Writing-original draft, Writing-review and editing. SX: Conceptualization, Investigation, Methodology, Software, Supervision, Writing-review and editing. JT: Data curation, Funding acquisition, Methodology, Resources, Writing-review and editing. BQ: Investigation, Supervision, Visualization, Writing-original draft. XL: Software, Supervision, Validation, Writing-review and editing. FZ: Data curation, Formal Analysis, Software, Supervision, Validation, Writing-review and editing.

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# Conflict of interest

The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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## Supplementary material

The Supplementary Material for this article can be found online at: https://www.frontiersin.org/articles/10.3389/fenrg.2024.1459667/ full#supplementary-material

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