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Multi-objective DG placement in radial distribution systems using the Ibl logic algorithm

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This paper presents a unique optimization method based on the incomprehensible but intelligible-in-time (Ibl) logic algorithm (ILA) to optimally place dispersed generators in small, medium, large, and very large (16-, 33-, 69-, and 118-bus) radial distribution power networks to reduce power losses, the total operating cost, and the voltage deviation and improve the voltage level. Two types of multiple distributed generators (DGs) are employed in this study, one working at unity power factor and the other at 0.866 p.f. The Ibl logic algorithm works by understanding concepts that are not currently recognized as logical but are expected to become logical over time. The proposed approach was used to address a multi-objective multi-DG placement problem. The results generated through this method were compared with those generated by other methods and were observed to be comparatively remarkable.

KEYWORDS

distributed generation, optimal placement of distributed generators, radial distribution network, incomprehensible but intelligible-in-time logics, load models, power loss reduction, voltage profile improvement, voltage deviation index

1 Introduction

Addressing the growing demand for power systems is challenging for the existing power line infrastructure. Distribution networks experience high I²R power losses because of low voltage and high current ratings. In addition, a low X/R ratio of the distribution level leads to more power loss and a decrease in voltage magnitude compared to the transmission level. It has a direct impact on the financial aspect, the efficiency of utilities, and the system's voltage profile, particularly in heavy load conditions. This poses severe challenges to power utilities. The problem can be solved by increasing the capacity of power systems or using distributed generators (DGs) to address the regional consumer demand (Ackermann et al., 2001). DGs can be described as small electric power-generating sources that are generally located near centers of consumption, with sizes ranging from 1 kW to 50 MW. According to El-Khattam and Salama (2004), DGs are broadly classified into traditional and non-traditional generators. Traditional generators use combustion engines such as micro-turbines and natural gas turbines, which belong to the categories of simple cycle, recuperated cycle, and combined-cycle gas turbines. Non-traditional generators can be divided into electrochemical devices, storage types, and renewable devices. Fuel cells (FCs) are primary electrochemical devices. Storage devices include batteries and flywheels. Meanwhile, renewable technologies, including PV cells and wind turbines, are presently more popular. DGs are more advantageous than conventional power-generating approaches in numerous capacities. First, they are more cost-effective and efficient because they reduce transmission losses and increase proximity to the energy

consumption points. Additionally, DGs can provide power during periods of high demand. This circumvents the need for expensive peak-load power plants. Second, distributed electricity production is decentralized and, thus, less susceptible to outages. It is more reliable than conventional power plants. Third, because DGs use pollution-free renewable energy sources such as wind, solar, and geothermal resources, these are more ecologically advantageous than conventional power plants. Large-scale power facilities can have substantial adverse effects on the environment. However, DGs may decrease the need for these facilities. Finally, auxiliary services, such as frequency control and voltage support, which improve the resilience and dependability of the grid, are additional advantages that distributed generation can provide to power systems (Selim et al., 2023).

To maximize the advantages of DGs and minimize the detrimental effects on power systems, optimizing their position and size is imperative. To optimize DG allocation, a mathematical optimization objective function is formulated and solved. This improves the capacity, performance, reliability, and longevity of the power system. Optimization techniques have been effective in computing the appropriate sizing for the best position of DGs. The advantages include a higher utilization of energy resources, improved system performance, and lower expenses and emissions. In addition to the advantages of DG technology, certain connection issues exist. These include the voltage level, system frequency variations in power flow, protection, reactive power, and power conditioning (Peperman et al., 2005).

DGs are divided into four categories based on their real and imaginary power delivery capabilities (as illustrated by Hung et al. (2010)):

- Type-1 (T-I): It has the potential of delivering only 'P' at unity p.f., such as microturbines, PV arrays, and fuel cells.
- Type-2 (T-II): It can only inject 'Q' at zero p.f., such as gas turbines.
- Type-3 (T-III): It is designed to provide both 'P' and 'Q' at p.f. from 0.8 to 0.99, such as wind, tidal, and geothermal plants.
- Type-4 (T-IV): It may provide 'P' but absorb 'Q,' such as doubly fed induction generators.

2 Literature review

To solve the optimal allocation problem of DGs, various objective functions are considered. These include real power loss, reactive power loss, voltage-profile improvement, voltage deviation, voltage stability index, power loss index, operational cost, cost of the power from the DG, and environmental and emission issues. Occasionally, these functions are considered individually. Alternatively, many of these are combined to form a multi-objective problem. Researchers have implemented different techniques to address this problem with respect to the objective function. These optimization methods were broadly classified by Viral and Khatod (2012), Pesaran et al. (2016), and Jain et al. (2017) into analytical methods, heuristic or meta-heuristic methods, hybrid methods, and the artificial intelligence approach.

Analytical methodologies use mathematical formulations to analyze the effect of DG-injected power on the power system's performance. This is exhibited by the improved analytical (IA) method and exhaustive load flow (ELF) optimization method (Hung and Mithulananthan, 2013). Several indices were developed

and calculated using an analytical method. Hung and Mithulananthan (2013) used the highly common but significant index called loss sensitivity factor based on the exact loss formula given by Elgerd (1971). Khatod et al. (2006) used analytical equations to compute different sensitivity indices such as the active power-loss, reactive power-loss, and voltage-magnitude sensitivities for a 69 bus system. Acharya et al. (2006) developed a priority list for power loss reduction using the LSF method with DGs in IEEE 30-, 33-, and 69-bus radial distribution systems (RDSs). Another analytical approach, introduced by Tah and Das (2016), used a 'p' bus to control the voltage magnitude of a 'PQV' bus for the 33- and 69-bus systems. Occasionally, the results obtained from analytical approaches are ineffective because these are dependent on network topological constraints.

Consequently, several investigators shifted to metaheuristic-based optimization strategies. Metaheuristic approaches effectively address optimization challenges without requiring a comprehensive analysis. Numerous heuristic optimization methods have been used in the power sector for DGs. These heuristic algorithms are categorized on the basis of their inspiration and involve evolutionary actions (e.g., swarm actions and food searches), physical rules, and human-related concepts. These algorithms use the exploration and exploitation phases to identify the best local solution from global options. Certain evolutionary phenomenon approaches have been employed to identify the best site and size of DG units. These include the following:

- Genetic algorithm (GA) used by Singh et al. (2019); Kashyap et al. (2017); Musa and Hashim (2019); Nezhadpashaki et al. (2020); Gopu et al. (2021); Rosado and Agustin (1998); El-Ela et al. (2010).
- Refined GA by Zhu (2002).
- Particle swarm optimization (PSO) proposed by El-Zonkolky (2011); Kansal et al. (2011, 2013); Lalitha et al. (2005), SPSO by Khalil et al. (2013), and multi-objective PSO by Ganguly et al. (2013).
- Hybrid PSO used by Aman et al. (2014).
- BAT algorithm used by Xin-She et al. (2010); Behera et al. (2015); Saxena et al. (2022).
- Whale optimization algorithm used by Prakash and Lakshminarayana (2018).
- Shark optimization used by Ali et al. (2023).
- Ant lion optimization used by Ali et al. (2018a).
- Bacterial foraging used by Devi and Geethanjali (2014); Imran et al. (2014).
- Krill herd optimization algorithm used by Sultana and Roy (2015).
- Moth flame optimizer used by Das and Srivastava (2017).
- Swine influenza optimization used by Sharma et al. (2016).
- Invasive weed algorithm used by Prabha and Jayabarathi (2016).
- Osprey and Walrus optimization algorithms used by TM et al. (2024).

Heuristic procedures based on physical rules such as slime mold optimization (Amigue et al., 2021), simulated annealing (Dharageshwari and Nayanatara, 2015), arithmetic optimization algorithm (Khan et al., 2023), and Thevenin-based impedance stability index (Talha et al., 2023) were also employed to solve multi-objective DG problem. Meanwhile, human-related concepts such as the

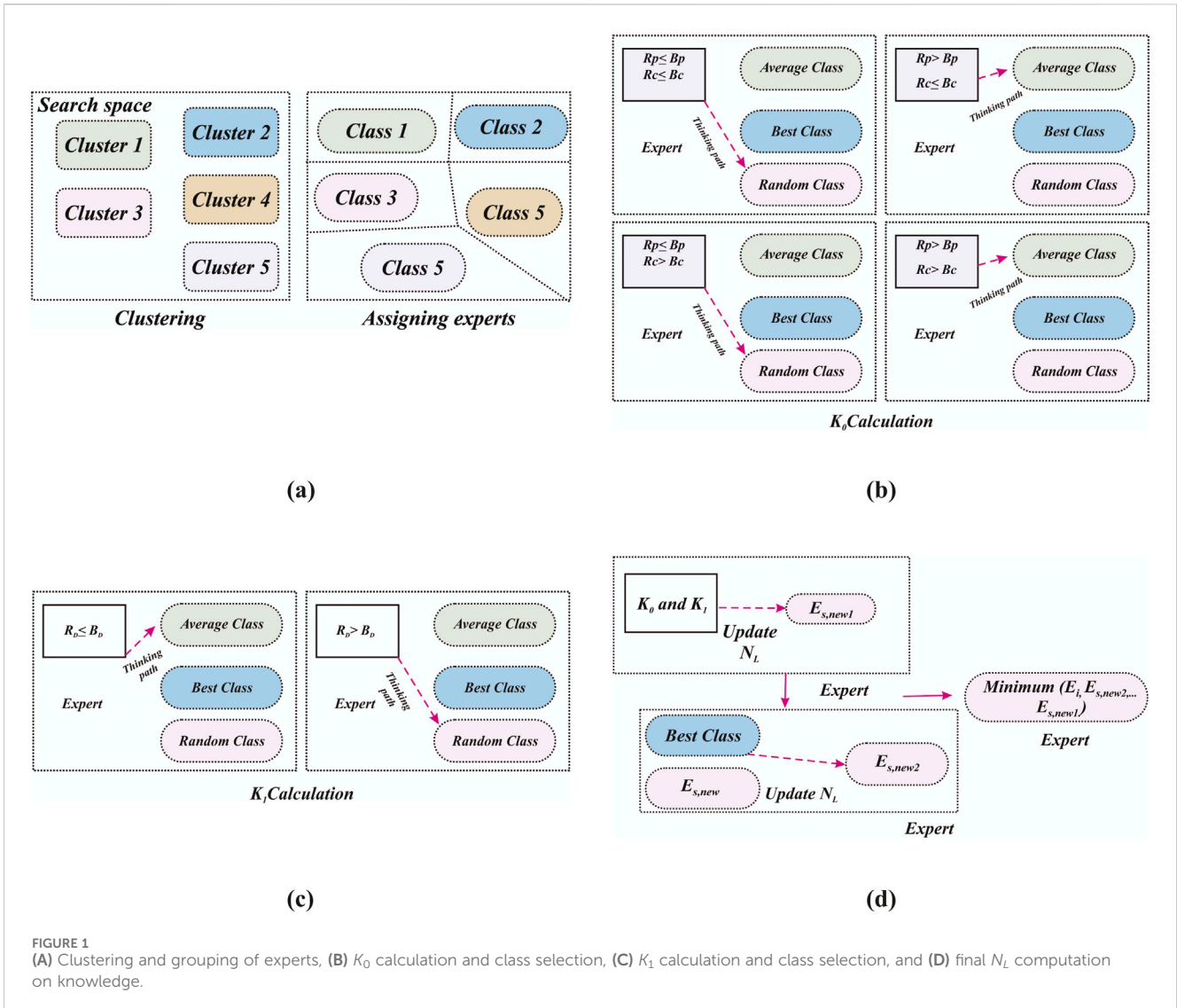


FIGURE 1 (A) Clustering and grouping of experts, (B) K_0 calculation and class selection, (C) K_1 calculation and class selection, and (D) final N_L computation on knowledge.

modified teaching–learning-based optimization algorithm (García and Mena, 2013) were used to solve single and multi-objective DG allocation. In these studies, single and multi-objective problems were addressed. In single objective functions, power-loss mitigation or voltage-level improvement are important features. Meanwhile, power loss reduction, voltage improvement, and operating cost reduction are the key factors for multi-objective functions.

The most popular evolutionary approaches amongst researchers are genetic algorithm and particle swarm optimization. Hybrid approaches primarily involve combining one of these two methods with another effective technique. These approaches have been used to obtain the best results with fast convergence. The multi-objective problem of multiple DG allocation was solved in the past by employing these techniques. The GA was combined with PSO by Moradi and Abedini (2012) to achieve better voltage regulation, reduced losses, and improved voltage profiles in 33- and 69-bus systems by optimally placing multiple DGs. The GA combined with the Tabu search algorithm was used by Gandomkar et al. (2005) for placing DG on the demand side to mitigate power losses. PSO combined with fuzzy control (Darvishi et al., 2011),

PSO integrated with the shuffled leap frog algorithm (Gitizadeh et al., 2013), and derivative techniques of combination of PSO with other algorithms, such as IPSO-Monte Carlo simulation (Abdi and Afshar, 2013) and bare bone PSO with differential evolution (Arya et al., 2012), are employed to solve the multi-DG placement problem in various test systems. Similarly, the whale optimization algorithm combined with the sine cosine algorithm was discussed by Ali et al. (2018b). A hybrid approach combining symbiotic organism search and a neural network algorithm (SOS–NNA) was proposed by Nguyen et al. (2021) for multi-objective DG and capacitor placement in 33- and 69-bus test systems. A hybrid configuration of ant colony optimization (ACO) and artificial bee colony optimization (ABO) with the point estimate method (PEM) was proposed by Kefayat et al. (2015) for the DG placement problem in 33- and 69-bus radial networks.

Other DG applications, such as PV arrays with storage facilities and the charging of electric vehicles with optimal allocation identification, were presented by Fokui et al. (2023) and Yu et al. (2024). Furthermore, hybrid and metaheuristic techniques were combined to optimally integrate PV modules with wind turbines (Avar and Ehsan, 2024).

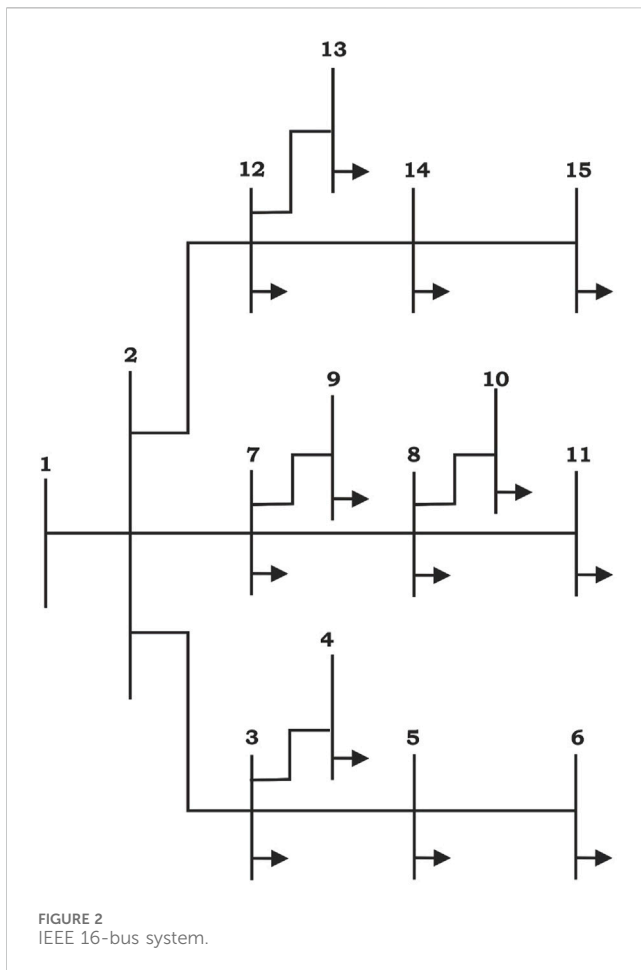


FIGURE 2
IEEE 16-bus system.

This study proposes a unique optimization theory, the incomprehensible but intelligible-in-time (IbI) logic algorithm (ILA), to optimally place dispersed generators into small, medium, large, and very large (16-, 33-, 69-, and 118-bus) radial distribution power networks to reduce power losses, minimize total operating costs, decrease voltage deviation, and improve voltage levels.

3 Problem formulation

The proposed approach aims to minimize the multi-objective function of the DG location and size within a distribution network while considering the unit and operating constraints.

3.1 Load flow in the radial network

A radial distribution network is a form of electrical power distribution network in which power is distributed radially from a single source (such as a substation) to numerous end users or distributing substations. The network comprises feeders that radiate away from the source. It is divided further into distribution networks that provide power to individual consumers.

The load flow in a radial network can be solved repeatedly by applying two distinct sets of iterative equations as follows. The first set of equations calculates the power flow from the last branch to the

root node in a backward manner. The second set of equations evaluates the voltage magnitude and angle of each node, beginning with the first node and moving to the final node. The iterative equations are evaluated as follows.

The net real power ($P_{i,i+1}$) that travels through the branch i from node i to $i+1$ can be computed in the backward direction starting from the last node. It can be expressed as in Equation 1,

$$P_{i,i+1} = P'_{i+1} + R_{i+1} \left(\frac{(P'_{i+1})^2 + (Q'_{i+1})^2}{V_{i+1}^2} \right), \quad (1)$$

where $(P'_{i+1}) = (P_{i+1,net}) + (P_{i+1})$ (P_{i+1}) = active power load connected at bus ($i+1$).

The voltage magnitude and angle for each bus are evaluated in the forward direction as follows:

$$I_i = \left(\frac{V_i * \angle \delta_i - V_{i+1} * \angle \delta_{i+1}}{R_{i,i+1} + jX_{i,i+1}} \right). \quad (2)$$

Furthermore,

$$I_i = \left(\frac{P_i - jQ_i}{V_i * \angle \delta_i} \right). \quad (3)$$

Comparing the equations of I_i given in Equations 2, 3, we obtain

$$V_{i+1} = \sqrt{\left(V_i^2 - 2(P_{i,i+1}R_{i,i+1} + Q_{i,i+1}X_{i,i+1}) + (R_{i,i+1}^2 + X_{i,i+1}^2) * \left(\frac{P_{i,i+1}^2 + Q_{i,i+1}^2}{V_i^2} \right) \right)}.$$

The active power loss of the i^{th} branch can be expressed as in Equation 4,

$$APL_{i,i+1} = R_{i+1} \left(\frac{P_{i,i+1}^2 + Q_{i,i+1}^2}{V_i^2} \right). \quad (4)$$

Hence, the total active power loss can be expressed as Equation 5,

$$TAPL = \sum_{i=1}^n APL_{i,i+1}. \quad (5)$$

3.2 Power loss with connected DGs

Optimizing the position of DGs reduces power losses, enhances voltage stability, and reduces expenditures. This, in turn, enhances supply assurance and dependability. The loss in active power when the DG is integrated into the system can be computed as follows:

$$APL_{DG,(i,i+1)} = R_{i+1} \left(\frac{P_{DG,(i,i+1)}^2 + Q_{DG,(i,i+1)}^2}{|V_i|^2} \right).$$

The total active power loss in the system connected to DGs is mentioned in Equation 6,

$$TAPL_{DG} = \sum_{i=1}^n APL_{DG,(i,i+1)}. \quad (6)$$

3.3 Reduction in power loss

The power loss should be minimized by installing a DG. The active power loss index (APLI) is calculated as the ratio of the total

TABLE 1 Performance evaluation of the IEEE 16-bus system for various load models using the Ibl logic algorithm.

Evaluation criterion	Constant power load						Constant current load		Constant impedance load	
	CP (half)		CP (full)		CP (overload)					
	W/o DG	With DG	W/o DG	With DG	W/o DG	With DG	W/o DG	With DG	W/o DG	With DG
DG size (in MW) (bus)	—	2.623 (5) 6.327 (8) 1.777 (15)	—	12.192 (8) 3.164 (15) 4.736 (5)	—	11.465 (8) 6.515 (5) 7.208 (11)	—	4.719 (5) 3.168 (15) 11.91 (8)	—	11.66 (8) 3.086 (15) 4.727 (5)
Power loss (in kW)	124.525	19.2148	511.43	80.9241	1,354.274	268.0773	487.032	77.4356	463.911	74.2639
% RL	—	84.5695	—	84.1771	—	80.2051	—	84.1005	—	83.9918
PLI	—	0.1543	—	0.1582	—	0.1979	—	0.1589	—	0.16
V _{min} (p.u.) (bus)	0.9848 (11)	0.9958 (9)	0.9687 (11)	0.9911 (9)	0.9482 (11)	0.9847 (9)	0.9696(11)	0.9913 (9)	0.9705 (11)	0.9916 (9)
VDI	0.0152	0.0042	0.0313	0.0089	0.0518	0.0153	0.03034	0.0086719	0.0295	0.0084
ROC (\$)	—	0.3743	—	0.70233	—	0.8851	—	0.69212	—	0.68071

TABLE 2 Comparative analysis of the IEEE 16-bus system.

Case	Aman et al. (2014)			Quoc and Mithulananthan (2013)						Proposed method					
	T-III DG			T-I DG			T-III DG			T-I DG			T-III DG		
No. DG	P _{LOSS} = 511.43			P _{LOSS} = 511.43			P _{LOSS} = 511.43			P _{LOSS} = 511.43			P _{LOSS} = 511.43		
1 DG	Bus	Size	P _{loss}	Bus	Size	P _{loss}	Bus	Size	P _{loss}	Bus	Size	P _{loss}	Bus	Size	P _{loss}
	8	20.77	315.02	12	10.4	193.6	9	12.82	164.02	8	12.12	170.12	8	11.99	165.6
2 DG	7	7.526	492.59	12	10.4	142.12	9	13	102.82	8	12.23	114.98	8	11.98	106.25
	8	21.38		7	5.2		6	5.84		5	4.7		5	4.86	
3 DG	11	10.93	536.56	12	10.4	106.82	9	13	69.2	8	12.12	80.92	8	11.98	73.82
	9	13.71		7	5.2		6	5.84		15	3.17		15	2.99	
	8	9.172		16	3.9		15	3.9		5	1.74		5	4.94	

active power losses including those of DG (TAPL_{DG}) to the total active power losses (TAPL) excluding it. It is given by Equation 7,

$$APLI = \frac{TAPL_{DG}}{TAPL} \tag{7}$$

By installing a DG into the system, the net power loss is reduced by minimizing APLI.

3.4 Voltage deviation index

The voltage deviation index (VDI) is also known as the voltage quality index. It is a metric used to analyze the voltage supply standards in electrical power systems. It represents the magnitude of the voltage deviations from the nominal value and is generally expressed as a percentage, as given in Equation 8. A high-voltage deviation index indicates that the voltage supplied varies significantly from the standard voltage level. This may result in equipment malfunction, low electrical device efficiency, and power quality problems.

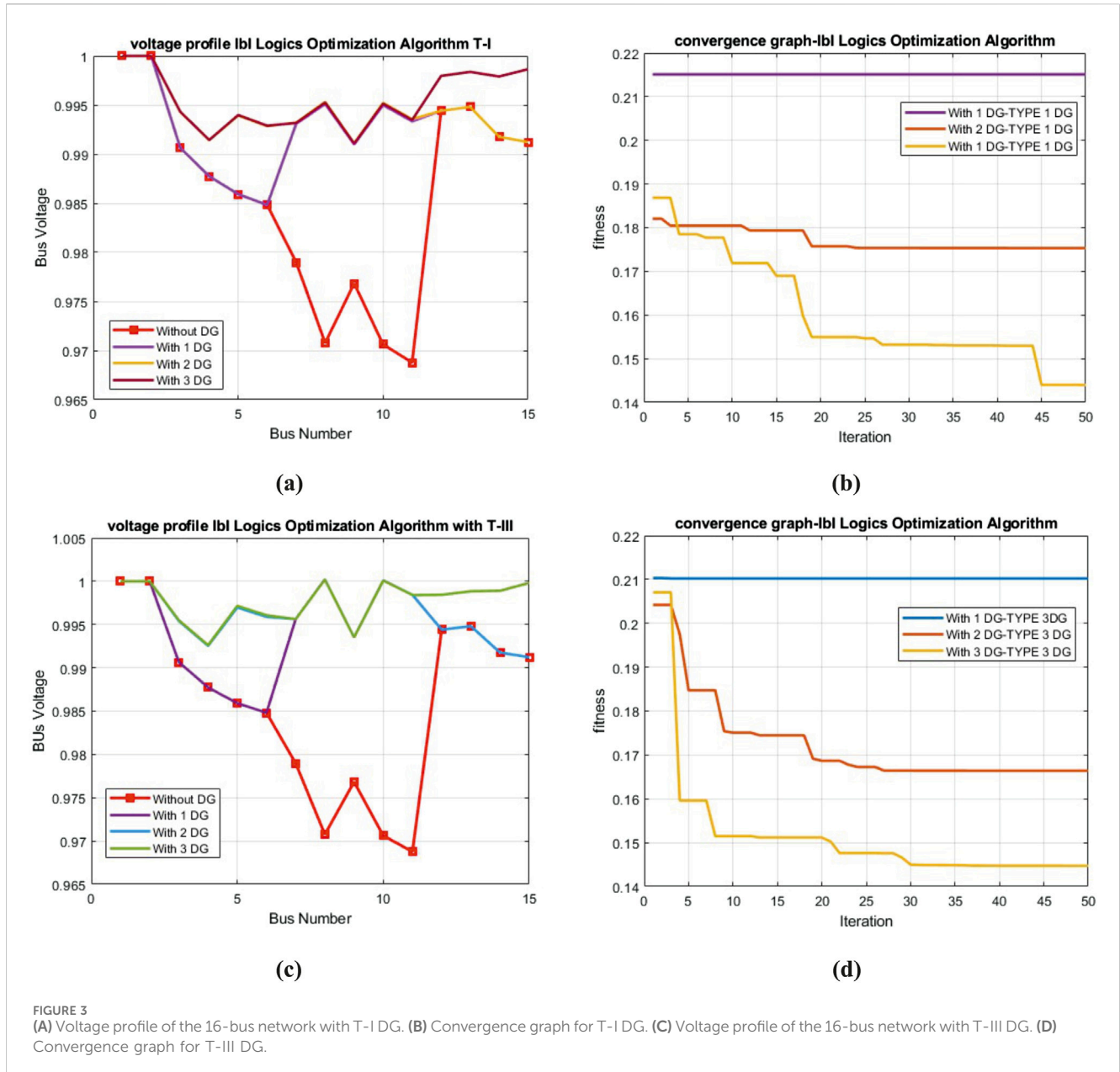
$$DI = \max\left(\frac{V_1 - V_i}{V_1}\right) \quad \forall i = 1, 2, 3, \dots, n. \tag{8}$$

By installing a DG, the proposed technique aims to minimize the VDI and bring it closer to zero. This would enhance the network performance and increase voltage stability.

3.5 Operational cost reduction

The installation of DGs helps reduce operational costs. It has two main components. One is related to the cost of active power provided by the substation. The second is the cost of the power provided by the DG. The first part can be reduced by limiting the actual power losses. Meanwhile, the second cost can be reduced by extracting less power from the DG. Hence, the total operational cost represented by Equation 9 is,

$$TOC = x * TAPL_{DG} + y * DGP_{total} \tag{9}$$



where $TAPL_{DG}$ is the total active power loss with the DG, DGP_{total} is the total rating of the DG connected, and x and y are the cost coefficients in USD/kW. The values of x and y are considered 4 USD/kW and 5 USD/kW, respectively. Thus, the reduction in operational cost is given by [Equation 10](#)

$$ROC = \frac{TOC}{c_2 DGP_{total}^{max}}, \tag{10}$$

where DGP_{total}^{max} indicates the maximum rating of the total connected DG rating.

3.6 Objective function

The proposed multi-objective optimization approach aims to reduce the power loss, voltage variation, and overall

operating costs of the distribution system. This is expressed as [Equation 11](#)

$$Minimize F(x) = \min(\alpha APLI + \beta VDI + \gamma ROC), \tag{11}$$

where $(\alpha + \beta + \gamma) = 1, \alpha, \beta, \gamma \in [0, 1]$.

The following constraints should be satisfied to optimize the objective function:

- The size and site of placement should be considered only at full load.
- The voltages at each bus should remain within the reasonable range of $\pm 5\%$, i.e., 0.95 to 1.05 p.u.

$$V_{min} \leq V \leq V_{max}.$$

- The generator operating range should lie within the permissible limit, i.e.,

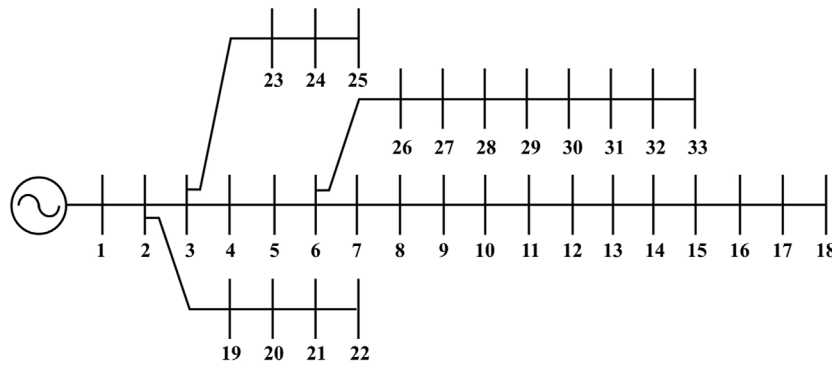


FIGURE 4 IEEE 33-bus system.

TABLE 3 Performance evaluation of the IEEE 33-bus system for various load models using the lbi logic algorithm.

Evaluation criterion	Constant power load						Constant current load		Constant impedance load	
	CP (half)		CP (full)		CP (overload)		W/ o DG	With DG	W/ o DG	With DG
	W/ o DG	With DG	W/ o DG	With DG	W/ o DG	With DG				
DG size (in MW) (bus)	—	0.367 (14) 0.371 (25) 0.529 (30)	—	0.841 (13) 0.999 (24) 0.970 (30)	—	0.996 (7) 0.321 (17) 0.756 (25)	—	0.661 (14) 0.983 (30) 0.617 (25)	—	0.603 (14) 0.652 (25) 0.907 (30)
Power loss (in kW)	47.07	17.5926	202.67	71.8924	575.36	191.4303	174.76	63.8636	151.1048	55.1885
% RL	—	62.6252	—	64.5286	—	66.7287	—	63.458	—	63.4767
PLI	—	0.3737	—	0.3547	—	0.3327	—	0.3654	—	0.3652
V _{min} (p.u.) (bus)	0.958 (18)	0.9836 (33)	0.913 (18)	0.9655 (33)	0.852 (18)	0.95 (33)	0.919 (18)	0.9680 (33)	0.926 (18)	0.9704 (33)
VDI	0.042	0.0164	0.087	0.0345	0.148	0.05	0.081	0.032	0.074	0.0296
ROC (\$)	—	0.34624	—	0.28675	—	0.55654	—	0.62489	—	0.59626

$$P_i^{min} \leq P_g \leq P_i^{max}.$$

- The current feeder capability limit should remain within the rated current capability of the branch I_i^{rated} , i.e.,

$$I_i \leq I_i^{rated} \forall_i \in \{\text{branches of network}\}.$$

4 Load models

According to Imran et al. (2014), various load models are classified on the basis of the load factor ρ , bus voltage (its magnitude and frequency), and real and imaginary power of the load. The effect of a variation in the load at any node ‘i’ is given by $P_i = \rho P_{i,actual} V_i^\xi$ and $Q_i = \rho Q_{i,actual} V_i^\psi$.

The load factor ρ is defined as the multiplying factor by which the variation in load power at any node is observed. Three load models according to the parameters were considered in this study (constant power load at half loading, full loading, and overloaded conditions; constant current load; and constant impedance load). For these loading systems, ξ is considered 0, 1, and 2, respectively. ψ

is also considered 0, 1, and 2, respectively. The load factor for all these types of loads is considered 1 only.

4.1 Incomprehensible but intelligible-in-time logic algorithm

The human brain is an exquisite albeit complex system that understands only what it observes or experiences, referring to these experiences as logic. It can be trained using various types of logic (L). Entities that fall outside the range of understanding of the common brain are rejected as illogical. However, these may be understood by an expert (E). In such cases, logic that can be understood by the common brain is called general logic (G-logic) and that which can be understood only by an expert is called special logic (S-logic). When described by an expert, G-logic can be understood by a non-expert and transformed into S-logic. However, occasionally, even experts are incapable of learning certain S-logic in the current scenario, such as the presence of wormholes in space. We call these experiences non-logics (NLs). It is likely that present NL would transform into logic over time. For example, elderly persons may not have assumed

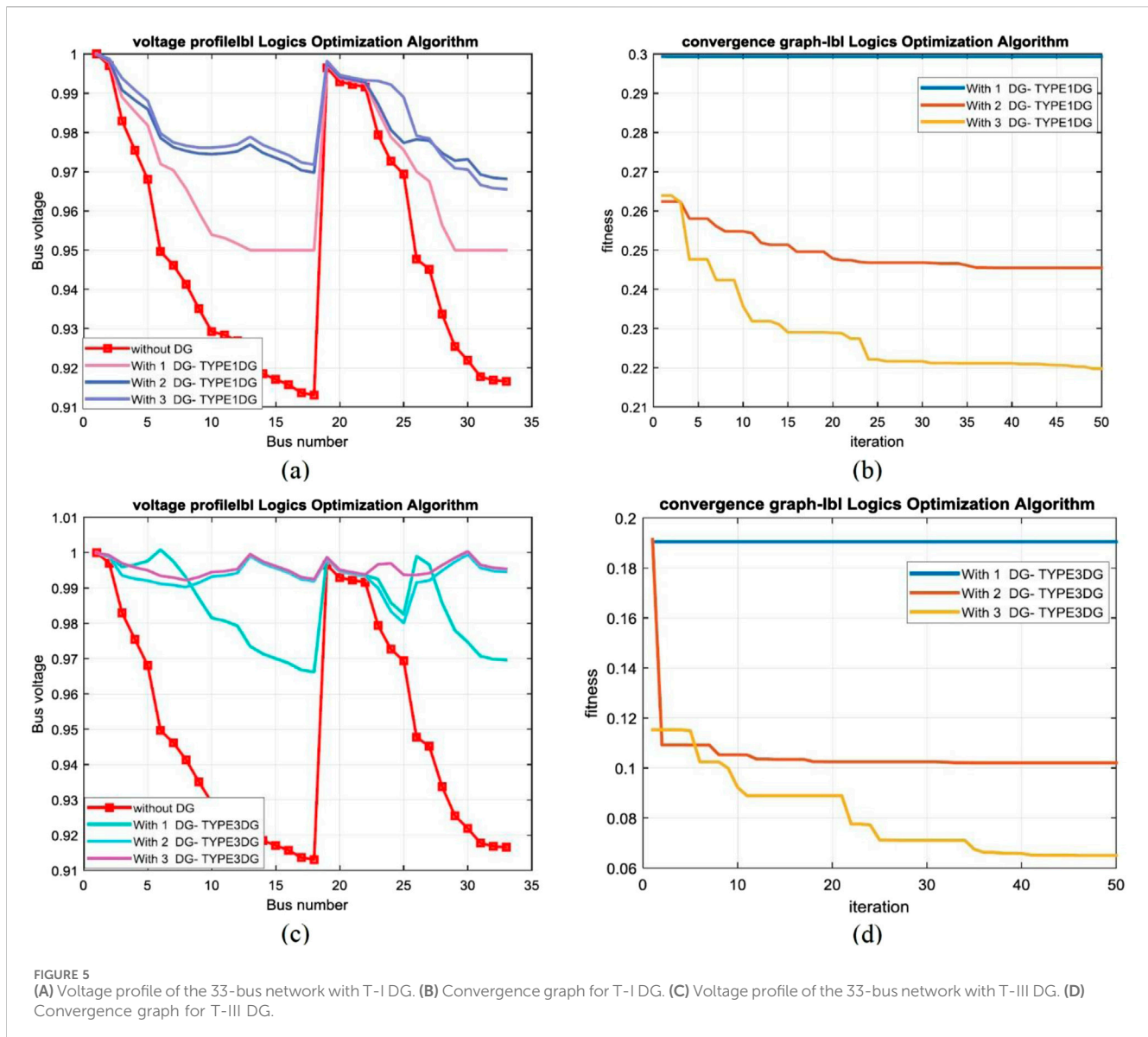
TABLE 4 Comparative analysis of the IEEE 33-bus system.

Method	PLDG (kW)	% RL	V _{min} (bus)	DG location	DG size (MW)	SDG (MVA)	p.f	TOC (\$)
GA [Moradi et al.]	106.3	49.61	0.9809 (25)	11 29 30	1.5 0.4228 1.0714	2.9942	upf	15,396.2
PSO [Moradi et al.]	105.35	50.06	0.9806 (30)	13 32 8	0.9816 0.8297 1.1768	2.9881	upf	15,361.9
GA/PSO [Moradi et al.]	103.4	50.09	0.9808 (25)	32 16 11	1.2 0.863 0.925	2.988	upf	15,353.6
SA [Injeti et al.]	82.03	61.12	0.9676 (14)	6 18 30	1.1124 0.4874 0.8679	2.4677	upf	12,666.6
BFOA [Imran et al.]	89.9	57.38	0.9705 (29)	14 18 32	0.6521 0.1984 1.0672	1.9176	upf	9,948.1
IWO [R. Prabha et al.]	85.86	57.47	0.9716 (29)	14 18 32	0.6247 0.1049 1.056	1.7856	upf	9,271.44
LSF [Hung et al.]	85.07	59.72	0.9690 (18)	18 33 25	0.72 0.81 0.9	2.43	upf	12,490.28
HPSO [Aman et al.]	84.16	60.11	0.9865 (25)	29 15 31	0.444 1.3641 1.973	3.7811	upf	19,242.14
KH [S. Sultana et al.]	75.412	64.25	0.9610 (33)	13 25 30	0.8107 0.8368 0.841	2.4885	upf	12,744.14
ILA [proposed method]	71.89	64.52	0.9655 (33)	13 24 30	0.841 0.999 0.97	2.81	upf	14,337.56
SA [Injeti et al.]	26.72	87.33	0.9826 (25)	6 18 30	1.1976 0.4778 0.9205	2.9975	0.866	13,086.3
BFOA [Imran et al.]	37.85	82.06	0.9802 (29)	14 18 32	0.6798 0.1302 1.1085	2.2153	0.866	9,743.9
IWO [R. Prabha et al.]	37.05	81.64	0.9838 (25)	14 18 32	0.5176 0.1147 1.0842	1.9821	0.866	8,730.7
LSF [Hung et al.]	23.05	89.09	0.9824 (25)	6 30 14	1.059 1.059 0.741	2.859	0.85	12,471.67
KH [S. Sultana et al.]	19.578	90.72	0.9816 (33)	13 24 30	0.853 0.9 0.899	3.062	0.866	13,336.772
ILA [proposed method]	14.49	92.85	0.9922 (8)	13 24 30	0.679 0.756 1.168	3.0057	0.866	13,072.64

that they would be able to make a video call over the internet or have considered online bank transactions. In their time, these concepts were not considered logical. However, in the present advanced world, these technologies are applied in day-to-day activities and are considered logical. A contradiction always exists between logic and non-logic in understanding and solving a particular problem. Solving problems through logic is imperative. However, there is

always a secondary plan for considering NLTs that could become logical over a period of time.

A novel optimization method based on the theory of IBI logics, introduced by [Mirrashid and Naderpour \(2023\)](#), is called IBI logic algorithm optimization. The ILA functions similarly to the human mind, which is a sophisticated biological system with special cognitive capacities. The underlying concept of the ILA is that solutions that are



presently considered illogical or indecipherable by humans may eventually develop into rational and reasonable solutions.

4.1.1 ILA parameters

1. Ibl logic and non-logic: Common understanding is logic. A set of NLs is to be considered, from which the correct NL, capable of becoming Ibl logic, must be identified.
2. Ibl probability: The likelihood of an NL transforming into Ibl logic.
3. Degree: A distance parameter calculated over a period in which NL can be transformed into Ibl logic.
4. Comprehensibility: The distance of confidence at any given time for the probability of conversion and the degree of closeness between L and N_L .

4.1.2 Ibl logic algorithm stages

The ILA comprises a preparation phase and three primary stages, namely, exploration, integration, and exploitation. The preparation phase involves the formation of a group of experts based on the

number of models and iterations required. Each stage of the optimization process has a distinct function. Additional solutions are identified within the search space during the exploration phase. Linking these new solutions and pre-existing solutions constitutes the integration step. Identifying the best solution within the search space is the ultimate objective of the exploitation phase. The capacity of ILA optimization for individually monitoring the exploration and exploitation phases provides users control over the algorithm's performance and the flexibility to modify the parameters as necessary. This is one of the significant advantages of optimization. Moreover, unlike other optimization methods, the ILA is renowned for its efficiency in identifying the best solutions while ensuring rapid computation. All of these processes are independent of characteristics. No reversal is permitted for any solution after passage through the earlier stages of the upcoming iterations. Figure 1 shows the various phases of the ILA.

4.1.2.1 Phase I—preparation

After setting the starting values of ILA parameters, the number of iterations for each model (n_m) is represented as t_m . Meanwhile,

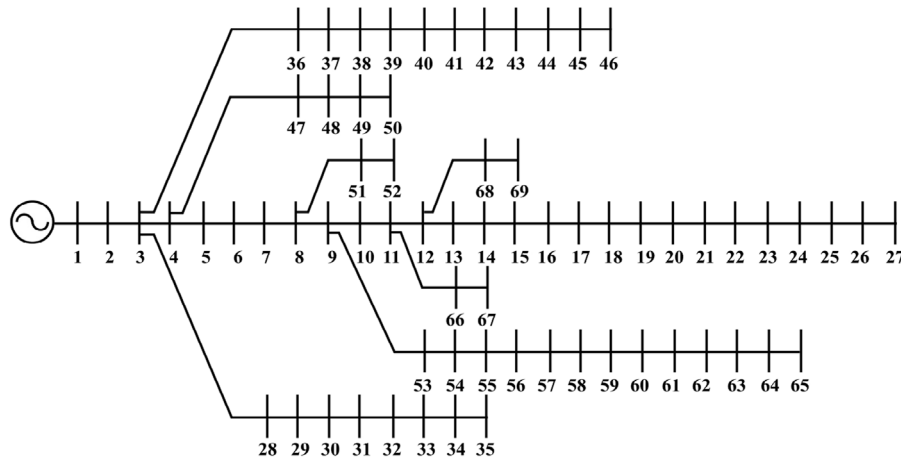


FIGURE 6 IEEE 69-bus system.

TABLE 5 Performance evaluation of the IEEE 69-bus system for various load models using the Ibl logic algorithm.

Evaluation criterion	Constant power load						Constant current load		Constant impedance load	
	CP (half)		CP (full)		CP (overload)		W/o DG	With DG	W/o DG	With DG
	W/o DG	With DG	W/o DG	With DG	W/o DG	With DG				
DG size (in MW) (Bus)	—	0.170 (12)	—	0.498 (17)	—	0.441 (21)	—	0.219 (12)	—	0.395 (18)
		0.857 (61)		0.389 (64)		1.483 (56)		1.576 (61)		0.301 (64)
		0.153 (22)		1.425 (61)		0.202 (69)		0.276 (22)		1.162 (61)
Power loss (in kW)	51.59	17.1624	224.96	71.2488	652.41	183.8777	188.6	60.7037	158.75	52.6363
% RL	—	66.7377	—	68.3283	—	71.8156	—	67.8138	—	66.8426
PLI	—	0.3326	—	0.3167	—	0.2818	—	0.3218	—	0.3315
V _{min} (p.u.) (bus)	0.9566 (65)	0.988,735 (65)	0.9090 (65)	0.981,136 (65)	0.8439 (65)	0.95 (65)	0.9172 (65)	0.97797 (65)	0.9246 (65)	0.98195 (65)
VDI	0.0433	0.011265	0.9099	0.018864	0.156	0.05	0.0827	0.02203	0.07534	0.01805
TOC (\$)	—	0.31414	—	0.2369	—	0.59818	—	0.55778	—	0.50003

the total number of iterations is represented as N_T , and the number of iterations for the first stage is represented as n_{t1} .

$$t_m = \frac{n_{t1}}{n_m},$$

$$n_{r1} = p_{s1} N_T.$$

The final observations of each model are forwarded to the next model for further optimization. This process continues until all the models are optimized. The process is then transferred to the next phase.

Before commencing the first stage, a class of experts is formed. Each class is responsible for a topic.

Here, the experts aim to identify the future logic of the topic in the search space provided. The number of classes (n_g) for a specific model is assigned a random number between 0 and a specified maximum value ($n_{g,max}$).

$$n_{g,m} = rand.(n_{g,max}).$$

4.1.2.2 Phase II—optimization

This phase includes three stages, namely, grouping, integration, and ILA logic search.

4.1.2.2.1 Stage-1 grouping.

In this step, each class focuses on every feasible option in the solution space to identify the optimal N_L . Prior to each iteration, three primary characteristics are defined. The current iteration logic (L) is the expert (E_i) that had the highest N_L value from the previous iteration ($E_{i,p}$) across all the classes. The second factor is the class's best expert E_{lg} . The third factor is the average of all the experts (E_s) denoted as A_g , achieved by each group in the previous iteration.

TABLE 6 Comparative analysis of the IEEE 69-bus system.

Method	PLDG (kW)	% RL	V _{min} (bus)	DG location	DG size (MW)	SDG (MVA)	pf	TOC (\$)
GA [Moradi et al.]	89	60.44	0.9936 (57)	21 62 64	0.9297 1.0752 0.9925	2.9974	upf	15,343
PSO [Moradi et al.]	83.2	63.02	0.9901 (65)	61 63 17	1.1998 0.7956 0.9925	2.9879	upf	15,272.3
GA/PSO [Moradi et al.]	81.1	63.95	0.9925 (65)	63 61 21	0.8849 1.1926 0.9105	2.988	upf	15,264.4
SA [Injeti et al.]	77.1	65.73	0.9811 (61)	18 60 65	0.4204 1.3311 0.4298	2.1813	upf	11,214.9
BFOA [Imran et al.]	75.23	66.56	0.9808 (61)	27 65 61	0.2954 0.4476 1.3451	2.0881	upf	10,741.4
IWO [R. Prabha et al.]	74.59	66.78	0.9802 (18)	27 65 61	0.2381 0.4334 1.3266	1.9981	upf	10,288.86
LSF [Hung et al.]	90.84	58.57	0.9785 (65)	65 27 61	1.36 0.51 0.51	2.38	upf	12,263.36
HPSO [Aman et al.]	87	61.32	0.9808 (28)	61 63 46	3.6525 0.0322 0.1529	3.8376	upf	19,536
KH [S. Sultana et al.]	69.563	69.04	0.9790 (65)	12 22 61	0.4962 0.3113 1.7354	2.5429	upf	12,986.75
ILA [proposed method]	71.25	68.33	0.981,136 (65)	17 64 61	0.498 0.389 1.425	2.312	upf	11,845
SA [Injeti et al.]	16.26	92.77	0.9885 (61)	18 60 65	0.5498 1.1954 0.3122	2.3757	0.866	10,352
BFOA [Imran et al.]	12.9	94.26	0.9896 (64)	27 65 61	0.3781 0.3285 1.3361	2.3587	0.866	10,265.1
IWO [R. Prabha et al.]	13.64	93.92	0.9946 (68)	27 65 61	0.3709 0.3156 1.0905	2.052	0.866	8,939.56
LSF [Hung et al.]	4.95	97.74	0.9939 (69)	61 17 50	2.073 0.622 0.829	3.5595	0.82	14,613.75
KH [S. Sultana et al.]	5.9149	97.36	0.9943 (50)	11 22 61	0.5607 0.3574 1.7738	3.1084	0.866	13,483.02
ILA [proposed method]	6.9104	96.93	0.9942 (50)	20 61 66	0.2356 0.996 0.1882	1.6395	0.866	7,126.67

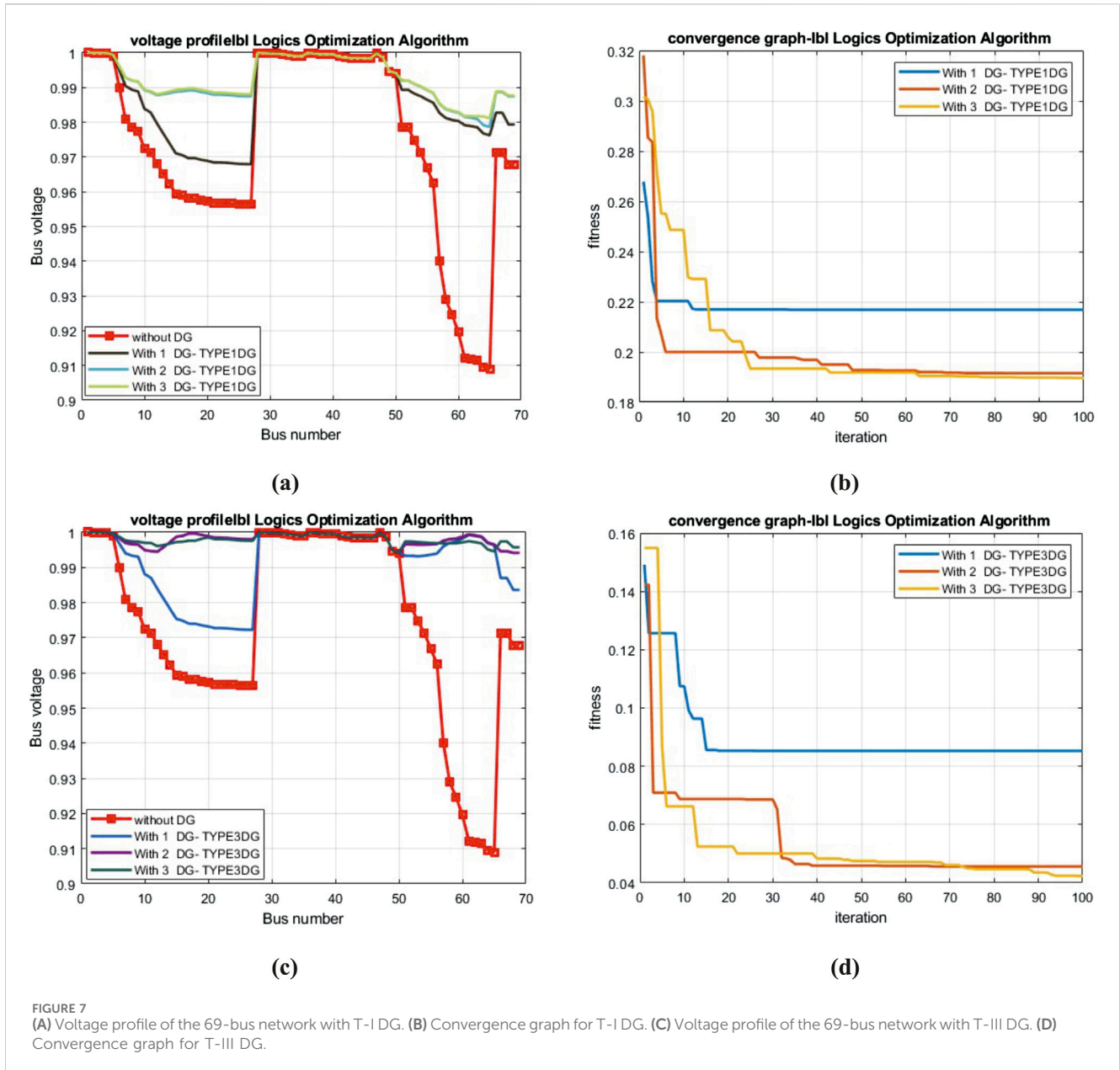
The following equations from Equation 12 to Equation 14 provide the expressions for comprehensibility, degree, and probability of any i^{th} expert E_i .

$$C_i = \sqrt{\sum_{i=1}^{n_{NL}} (E_i - L)^2}, \tag{12}$$

where $g = 1, 2, 3, \dots, n_g, m$.

$$D_i = \sqrt{\sum_{i=1}^{n_{NL}} (E_i - E_{i,p})^2}, \tag{13}$$

$$P_i = \sqrt{\sum_{i=1}^{n_{NL}} (E_i - E_{i,g})^2}, \tag{14}$$



The following equations from Equation 15 to Equation 17 are the ratios of comprehensibility, degree, and probability. These are updated at the initiation of each iteration.

$$R_{C,i} = \frac{C_i - C_{min}}{C_{max} - C_{min}}, \quad (15)$$

$$R_{D,i} = \frac{D_i - D_{min}}{D_{max} - D_{min}}, \quad (16)$$

$$R_{P,i} = \frac{P_i - P_{min}}{P_{max} - P_{min}}, \quad (17)$$

where $I = 1, 2, 3, \dots, n_{NL}$.

The first task is to update new knowledge $K_{0,i,s1}$ and $K_{1,i,s1}$. In each stage, the parameters B_p , B_c , and B_D are selected randomly between B_{min} and B_{max} . If E_i is closer to the logic of the present iteration, it can be considered in the computations. This is because it

may improve in the subsequent iterations. The knowledge of each expert should be updated according to the ratio, randomness, average value, and iterative value as specified in equations from Equation 18 to Equatio 23. Thus, the best solution can be achieved.

$$K_{0,i,s1} = R_{p,i} \frac{E_i + E_r}{2} \quad \text{for } R_{c,i} \leq B_c \text{ and } R_{p,i} \leq B_p, \quad (18)$$

$$K_{0,i,s1} = R_{p,i} \frac{E_i + E_{a,g}}{2} \quad \text{for } R_{c,i} \leq B_c \text{ and } R_{p,i} > B_p, \quad (19)$$

$$K_{0,i,s1} = R_{p,i} \frac{E_{l,g} + E_r}{2} \quad \text{for } R_{c,i} > B_c \text{ and } R_{p,i} \leq B_p, \quad (20)$$

$$K_{0,i,s1} = R_{p,i} \frac{E_{l,g} + E_{a,g}}{2} \quad \text{for } R_{c,i} > B_c \text{ and } R_{p,i} > B_p, \quad (21)$$

$$K_{1,i,s1} = c_1 E_{a,g} \quad \text{for } R_{D,i} \leq B_D, \quad (22)$$

$$K_{1,i,s1} = c_1 E_u \quad \text{for } R_{D,i} > B_D. \quad (23)$$

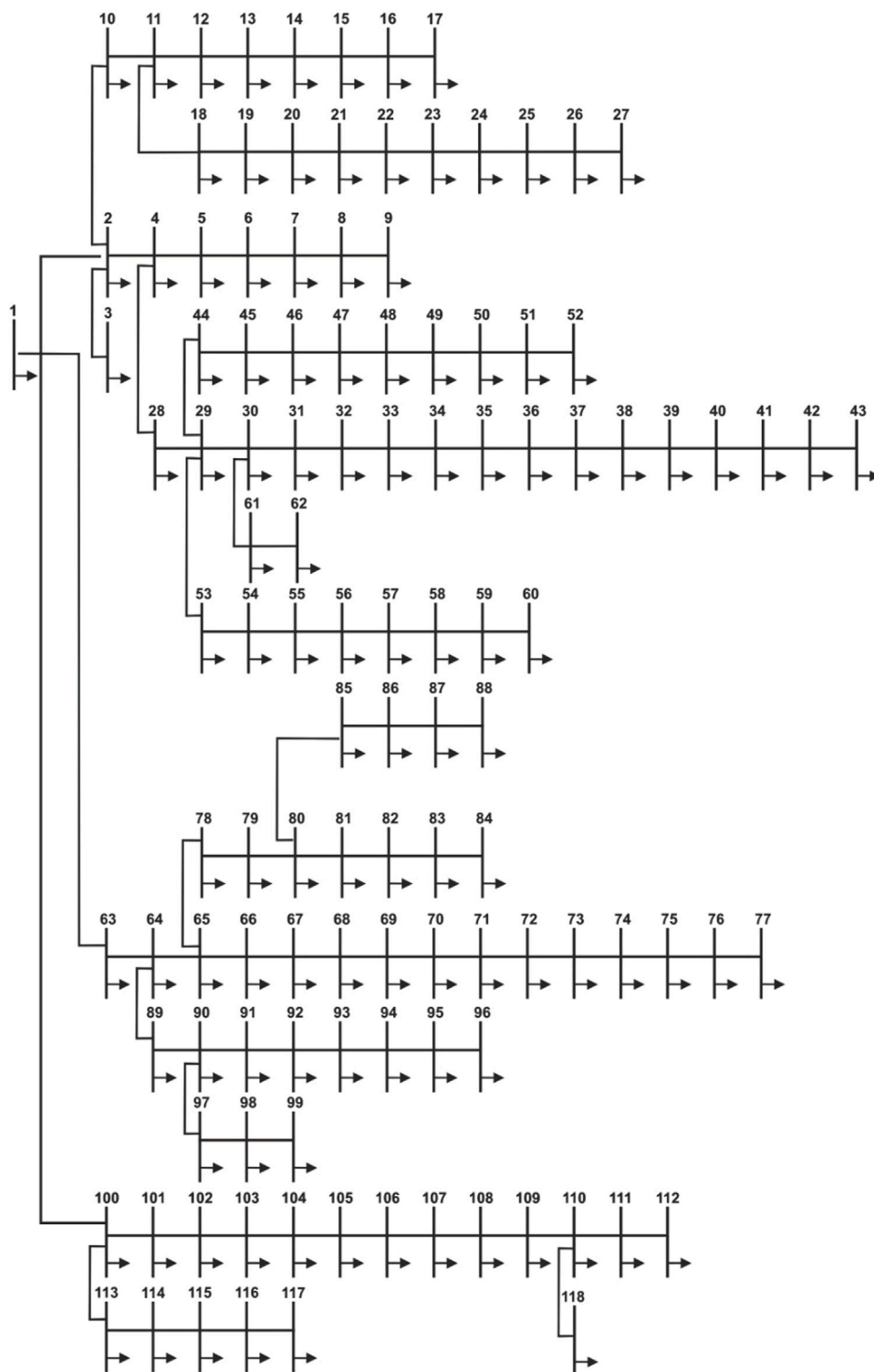


FIGURE 8
IEEE 118-bus system.

The overall updated knowledge can be expressed by Equation 24,

$$K_{s1} = \frac{|K_{0,s1} + K_{1,s1}|}{2} \tag{24}$$

A further update in the expert value is given as

$$E_{s1,new1} = E_i + c_2 K_{s1},$$

$$E_{s1,new2} = c_3 E_{s1,new1} + c_4 E_{I.g.}$$

TABLE 7 Performance evaluation of the IEEE 118 bus system with five DGs for various load models using Ibl Logic algorithm.

Evaluation criterion	Constant power load						Constant current load		Constant impedance load	
	CP (half)		CP (full)		CP (overload)		W/ o DG	With DG	W/ o DG	With DG
	W/ o DG	With DG	W/ o DG	With DG	W/ o DG	With DG				
DG size (in MW) (bus)	—	1.00(3)	—	1.919(33)	—	1.00(5)	—	1.05(3)	—	1.06(3)
		1.16(52)		1.877(70)		1.00(58)		1.20(42)		1.00(72)
		1.17(73)		1.753(91)		1.00(44)		1.15(74)		1.04(91)
		1.12(111)		2.37(110)		1.009(23)		1.39(96)		2.07(50)
		1.008(81)		1.904(80)		1.01(41)		2.89(109)		1.81(111)
Power loss (in kW)	302.66	153.948	1298.15	576.239	3795.71	1379.36	1084.08	564.89	914.48	499.2087
% RL	—	49.14	—	55.6107	—	63.66	—	47.89	—	45.4106
PLI	—	0.508	—	0.4438	—	0.3634	—	0.521	—	0.545
V _{min} (p.u.) (bus)	0.93824 (77)	0.97701 (77)	0.86881 (77)	0.95 (54)	0.76733 (77)	0.95 (77)	0.8851 (77)	0.95 (77)	0.8991 (77)	0.95 (77)
VDI	0.06176	0.2299	0.13112	0.05	0.23267	0.05	0.1149	0.05	0.1009	0.05
ROC (\$)	—	0.27986	—	0.44735	—	0.30612	—	0.40815	—	0.37012

The best value is provided by

$$E_{s1,new} = \text{minimum}(E_{s1,new1}, E_{s1,new2}).$$

In this stage, the updated value is examined using all the previous values, and the expert retains the position with superior value of fitness.

$$E_{i,s1} = \text{minimum}(E_i, E_{s1,new}).$$

4.1.2.2.2 Stage-2 integration. In this stage, all the experts are combined, and the knowledge provided in the current iteration is used to increase N_L . Initially, all the ratios R_c and R_D are computed. Then, R_p is calculated using the newly updated value of P_i .

$$P_i = \sqrt{\sum_{i=1}^{MNL} (E_i - E_I)^2} \quad g = 1, 2, 3, \dots, n_{g,m}.$$

The new knowledge updating process for experts is given by Equations 25–31 for $K_{0,s2}$ and K_{s2} , as follows:

$$K_{0,i,s2} = R_{P,i} \frac{E_i + E_R}{2} \quad \text{for } R_{c,i} \leq B_c \text{ and } R_{p,i} \leq B_p, \quad (25)$$

$$K_{0,i,s2} = R_{P,i} \frac{E_i + E_A}{2} \quad \text{for } R_{c,i} \leq B_c \text{ and } R_{p,i} > B_p, \quad (26)$$

$$K_{0,i,s2} = R_{P,i} \frac{E_I + E_R}{2} \quad \text{for } R_{c,i} > B_c \text{ and } R_{p,i} \leq B_p, \quad (27)$$

$$K_{0,i,s2} = R_{P,i} \frac{E_I + E_A}{2} \quad \text{for } R_{c,i} > B_c \text{ and } R_{p,i} > B_p, \quad (28)$$

$$K_{1,i,s2} = c_5 E_A \quad \text{for } R_{D,i} \leq B_D, \quad (29)$$

$$K_{1,i,s2} = c_5 E_u \quad \text{for } R_{D,i} > B_D, \quad (30)$$

$$K_{s2} = \frac{|K_{0,s2} + K_{1,s2}|}{2}. \quad (31)$$

When the target is the minimum value of the fitness function, the final E_i would be the result of the following equations from Equation 32 to Equation 35.

$$E_{s2,new1} = E_i + c_6 K_{s1}, \quad (32)$$

$$E_{s2,new2} = c_7 E_{s2,new1} + c_8 E_I, \quad (33)$$

$$E_{s2,new} = \text{minimum}(E_{s2,new1}, E_{s2,new2}), \quad (34)$$

$$E_{i,s2} = \text{minimum}(E_i, E_{s2,new}). \quad (35)$$

4.1.2.2.3 Stage-3 ILA logic search. The proposed strategy focuses on improving the knowledge of each expert by using the average aggregate knowledge of all the experts. It then updates the knowledge of each expert. The method is repeated until the convergence criteria are met. Before entering the next stage, the average value of the knowledge from the previous stage must be computed. These are provided from Equation 36 to Equation 41.

$$K_{i,s3} = |E_A - E_R| \quad \text{if knowledge factor} = 1, \quad (36)$$

$$K_{i,s3} = |E_A - E_I| \quad \text{if knowledge factor} = 2, \quad (37)$$

$$E_{s3,new1} = E_i + c_9 K_{s1}, \quad (38)$$

$$E_{s3,new2} = c_{10} E_{s3,new1} + c_{11} E_I, \quad (39)$$

$$E_{s3,new} = \text{minimum}(E_{s3,new1}, E_{s3,new2}), \quad (40)$$

$$E_{i,s3} = \text{minimum}(E_i, E_{s3,new}). \quad (41)$$

The ILA is different from conventional algorithms as it has a greater number of tuning parameters. The increased number of optimization phases, including all the stages with their tuning parameters, makes ILA a more controllable and faster-converging algorithm. It is also true that the major asset of the method is its main challenge. The large number of tuning parameters makes the method finely configurable, but achieving that fine configuration is an arduous task.

4.1.3 Process of the ILA for placing DGs in the RDS

The procedure for the implementation of the ILA for the placing of DG in the RDS is as follows:

TABLE 8 Comparative analysis of the IEEE 118-bus system (with five DGs).

Method	PLDG (kW)	% RL	V_{\min} (bus)	DG location	DG size (MW)	DG size (MVAr)	SDG (MVA)	pf
SA [Injeti et al.]	858.8133	33.75	0.91905 (54)	75	2.1318	—	13.4953	upf
				116	0.7501	—		
				56	1.1329	—		
				36	4.5353	—		
				103	4.9452	—		
KH [S. Sultana et al.]	576.46	55.53	0.9558 (53)	50	2.872	—	11.6869	upf
				74	2.434	—		
				81	1.8113	—		
				96	1.69	—		
				110	2.8796	—		
ILA [proposed method]	576.2388	55.61	0.95 (54)	33	1.919	—	9.827	upf
				70	1.877	—		
				91	1.753	—		
				110	2.374	—		
				80	1.904	—		
SA [Injeti et al.]	684.0282	47.23	0.93765 (54)	75	2.9296	1.6896	18.854	0.866
				116	1.5465	0.893		
				56	1.4841	0.857		
				36	4.4551	2.5725		
				103	5.9126	3.414		
KH [S. Sultana et al.]	233.383	81.99	0.9605 (46)	50	3.2112	1.8543	14.32	0.866
				74	2.3741	1.3418		
				81	1.9867	1.147		
				96	1.7109	0.9878		
				110	3.1172	1.7997		
ILA [proposed method]	230.1619	82.26	0.9605 (46)	4	2.129	1.2293	12.63	0.866
				74	2.29	1.3222		
				91	1.415	0.817		
				109	3.097	1.7882		
				50	2.012	1.1617		

1. Initialize with the basic parameters, such as the number of buses, base voltage and kVA, minimum DG size, maximum DG size, V_{\min} and V_{\max} , initial population, and number of iterations.
2. Apply the backward–forward sweep load flow method for the base case.
3. Form the BIBC-BCBV matrices and the DLF matrix.
4. The base case power losses and the bus voltage values are thus obtained.
5. Select the number of DGs to be placed (in this study, numbers could be 3, 5, or 7).
6. Identify the capacity of DGs using the ILA process.
7. Run the load flow process with the DG size selected, and check for the reduction in losses by placing the DG on suitable locations.
8. If yes, save the size for a particular bus.
9. If no, go to step 6 and repeat the cycle until the convergence is met.
10. The line losses are given as

$$PG = (dg_value (ind)) \text{ and } QG = PG * pfdata.$$
11. The reduction in power losses is calculated as

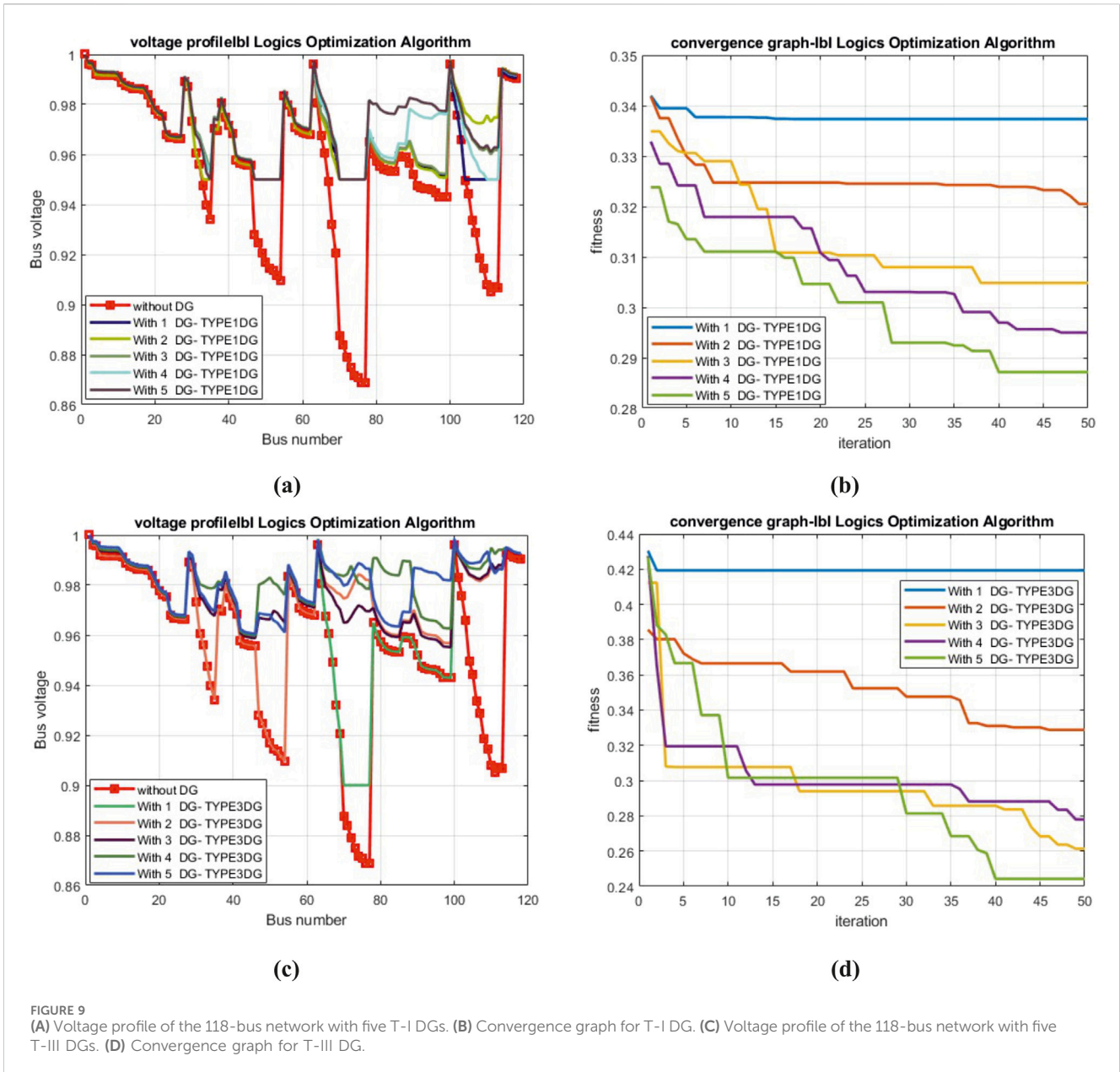


FIGURE 9 (A) Voltage profile of the 118-bus network with five T-I DGs. (B) Convergence graph for T-I DG. (C) Voltage profile of the 118-bus network with five T-III DGs. (D) Convergence graph for T-III DG.

$$delPLdg = PDGloss/PTloss.$$

12. The voltage index is given as

$$delvd = \max ((v1-finalvoltage)/v1).$$

13. The reduction in operating cost is expressed as

$$deltoc = TOC/(c2*PDGmax).$$

14. The complete objective function is expressed as

$$final_objective = \alpha1*delPLdg + \alpha2*delvd + \alpha3*deltoc.$$

15. Display the output.

5 Simulation and results

The proposed technique was tested on four IEEE standard test bus system (i.e., IEEE-16, IEEE-33, IEEE-69, and IEEE-118 bus radial distribution systems) to determine its efficiency on various load types and identify the optimal location of multiple DGs to minimize the objective function (which includes the minimization of the active power losses, voltage deviation index, and operational costs). MATLAB code was developed for the ILA and executed on an Intel® Core™ i7-7700 CPU @ 3.60 GHz desktop installed with 8 GB RAM. The performance of the algorithm is examined over 30 consecutive trials for each dataset, and the best minimum (in case of the power loss and the cost) and maximum (in case of the bus voltage) values are considered. The weighting factors in the objective function were set as $\alpha = 0.5$, $\beta = 0.4$, and $\gamma = 0.1$. The cost coefficients x and y were considered 4 USD/kW and 5 USD/kW, respectively. y is

TABLE 9 Performance evaluation of the IEEE-118 bus system with seven DGs for various load models using Ibl Logic algorithm.

Evaluation criterion	Constant power load						Constant current load		Constant impedance load	
	CP (half)		CP (full)		CP (overload)					
	W/o DG	With DG	W/o DG	With DG	W/o DG	With DG	W/o DG	With DG	W/o DG	With DG
DG size (in MW) (bus)	—	1.103 (5)	—	1.303 (18)	—	1.0 (2)	—	1.656 (8)	—	1.07 (30)
		1.14 (48)		1.174 (80)		1.00 (42)		1.52 (41)		1.01 (51)
		1.054 (41)		1.233 (43)		1.02 (40)		1.31 (70)		1.61 (50)
		1.062 (80)		1.765 (72)		1.00 (24)		1.55 (96)		1.06 (42)
		1.05 (111)		1.037 (35)		1.00 (35)		1.81 (110)		1.24 (80)
		1.027 (74)		2.378 (110)		1.00 (102)		1.19 (107)		2.02 (73)
		1.028 (97)		1.2 (96)		1.00 (60)		1.965 (33)		2.79 (108)
Power loss (in kW)	302.66	135.61	1,298.15	558.39	3,795.71	1,332.49	1,084.08	498.57	914.48	437.67
% RL	—	55.194	—	56.98	—	64.89	—	54.001	—	52.14
PLI	—	0.448	—	0.4301	—	0.351	—	0.46	—	0.47
V _{min} (p.u.) (bus)	0.9383 (77)	0.9721 (54)	0.8689 (77)	0.95 (54)	0.76733 (77)	0.95 (77)	0.8851 (77)	0.95 (77)	0.8991 (77)	0.9604 (99)
VDI	0.062	0.0279	0.1311	0.05	0.23267	0.05	0.1149	0.05	0.1009	0.0396
TOC (\$)	—	0.37887	—	0.52684	—	0.4052	—	0.56959	—	0.55796

generally maintained on the higher side, owing to the maintenance and installation costs of the DGs.

The performance of the ILA method depends on the selection of various input values. The number of iterations and initial population (number of experts) were set to 20 and 50, respectively. Five models were considered. B_{min} and B_{max} were set to 0.4 and 0.6, respectively. The maximum iteration percentage required for stages 1 and 2 is 33% each. The replication value for clustering (η_{rep}) was 10. The number of trials to converge the class in η_{rep} replication is considered 100. The values for ILA coefficients considered c_1 were randomly selected from the range between 0 and 1, c_2 was randomly chosen between -1.5 and 1.5, c_3 was randomly chosen between -1.5 and 1.5, c_4 and c_5 were selected randomly between 0 and 1, c_6 was selected between -0.75 and 0.75, c_7 was randomly chosen between -0.75 and 0.75, c_8 is randomly selected between 0 and 1, c_9 is a random vector selected from -0.25 and 0.25, c_{10} was randomly chosen between -0.25 and 0.25, and c_{11} was randomly chosen between 0 and 1.

The efficacy of the proposed approach was tested on various load types, such as constant power (CP) at light load (0.5), full load (1.0), heavy load (1.6), constant current (CC), and constant impedance (CI) loads. Two types of DGs were considered in this study: T-I (injects active power at unity power factor) and T-III (capable of feeding real and imaginary powers at a power factor of 0.866).

5.1 IEEE 16-bus system

Initially, to test the operation of the ILA optimization technique, a small standard test system with 16 buses was considered. The initial version of this system had 16 buses, 3 feeders, and 13 branches.

However, according to Aman et al. (2014), the earlier version was modified into the single feeder, 15-bus radial network shown in Figure 2. The bus and line data were obtained from Aman et al. (2014). The base values, load values, and losses for the 16-bus system were $V_{BASE} = 12.66$ kV, $S_{BASE} = 100$ MVA, $P_{LOAD} = 28,700$ kW, $Q_{LOAD} = 5,900$ kVAr, $P_{loss} = 511.40$ kW, and $Q_{loss} = 590.37$ kVAr. The voltage limit at all the buses was set within 0.95–1.05 p.u. The real power loss without DG inclusion was 511.43 kW, and the reactive power loss was 590.3668 kVAr. According to Behera et al. (2015), a 50% penetration of DG was considered. The base case load flow proposed by Singh and Bala (2015), without DG integration, was run. Then, DG was added to the buses.

First, the T-I DG was implemented for all types of load models. The results shown in Table 1 were found effective. Three numbers of both types of DGs, i.e., T-I and T-III were connected to the system to obtain optimum outcomes. In Table 2, these results are compared with those of previous studies conducted by Aman et al. (2014) and Quoc and Mithulanathan (2013). Compared with the results of Aman et al. (2014), which reported a loss of 536.56 kW, the proposed method displayed a remarkable loss reduction of 73.82 kW with the integration of T-III. Similarly, with the integration of T-I DG, the proposed method obtained 80.92 kW, unlike the 106.82 kW reported by Quoc and Mithulanathan (2013). Figure 3 depicts the voltage profile and convergence characteristics of both types of DGs. With no DG integrated into the system, the minimum and maximum reported voltages are 0.969 p.u. at bus 11 and 1.00 p.u. at bus 1, respectively. However, with the insertion of three T-I DGs into the network, the voltage improved by 0.991 p.u. at bus 9 and 1.00 p.u. at bus 1. Meanwhile, with the installation of three T-III DGs, the voltage limit ranged between 0.993 p.u. at bus 4 and 1.0001 p.u. at bus 8.

TABLE 10 Comparative analysis of the IEEE 118-bus system (with seven DGs).

Method	PLDG (kW)	% RL	V_{\min} (bus)	DG location	DG size (MW)	DG size (MVA)	SDG (MVA)	pf
SA [Injeti et al.]	900.19	30.56	0.93249 (111)	75	2.8246	—	22.5155	upf
				116	0.4606	—		
				56	3.6739	—		
				36	7.4673	—		
				103	5.0803	—		
				88	2.2979	—		
				48	0.7109	—		
KH [S. Sultana et al.]	574.71	55.66	0.9470 (77)	48	1.7242	—	11.5826	upf
				53	1.3356	—		
				74	1.8623	—		
				80	1.8653	—		
				96	1.6631	—		
				109	1.9473	—		
				112	1.1848	—		
ILA [proposed method]	558.39	56.98	0.95 (54)	18	1.303	—	10.09	upf
				80	1.174	—		
				43	1.233	—		
				72	1.765	—		
				35	1.037	—		
				110	2.378	—		
				96	1.2	—		
SA [Injeti et al.]	638.03	50.71	0.94689 (111)	75	2.7544	1.5904	25.2011	0.866
				116	0.5076	0.2931		
				56	4.3123	2.49		
				36	6.1109	3.5285		
				103	5.335	3.0805		
				88	0.6262	0.3616		
				48	2.1778	1.2575		
KH [S. Sultana et al.]	312.66	75.88	0.9679 (27)	43	1.9726	1.1389	13.4886	0.866
				51	1.9849	1.146		
				69	1.7929	1.0351		
				73	1.8551	1.071		
				88	1.8975	1.0955		
				108	1.9905	1.1492		
				109	1.9951	1.1519		

(Continued on following page)

TABLE 10 (Continued) Comparative analysis of the IEEE 118-bus system (with seven DGs).

Method	PLDG (kW)	% RL	V_{min} (bus)	DG location	DG size (MW)	DG size (MVAr)	SDG (MVA)	pf
ILA [proposed method]	297.98	77.04	0.9594 (46)	13	1	0.5774	12.1028	0.866
				50	1.044	0.6028		
				72	2.039	1.1773		
				84	1.175	0.6784		
				89	1	0.5774		
				110	3.091	1.7847		
				52	1.132	0.6536		

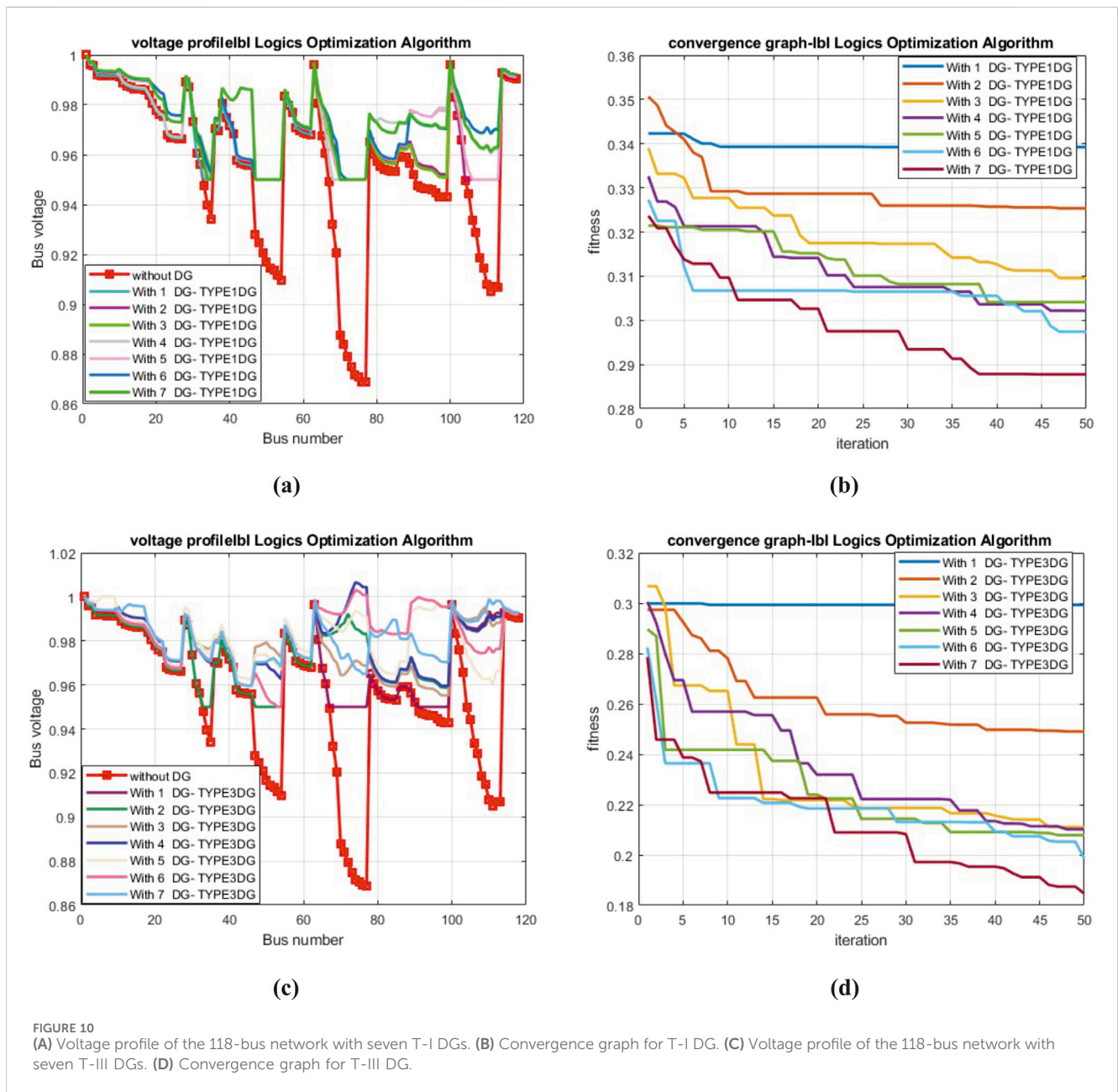


FIGURE 10 (A) Voltage profile of the 118-bus network with seven T-I DGs. (B) Convergence graph for T-I DG. (C) Voltage profile of the 118-bus network with seven T-III DGs. (D) Convergence graph for T-III DG.

TABLE 11 The worst, best, average, median, and standard deviation values of bus voltages for test systems with the implementation of T-I and T-III into all the systems under study.

Bus system	Number of DGs	Type of the DG	Minimum value (bus number)	Maximum value (bus number)	Mean value	Median	Standard deviation
16-bus	3 DGs	T-1	0.991,061 (9)	1.00 (1)	0.995574343	0.999325691	0.000674,309
		T-3	0.992610261 (4)	1.0001941 (8)	0.997674851	0.999907791	0.000092208
33-bus	3 DGs	T-1	0.965,532 (33)	1.00 (1)	0.981390851	0.982766393	0.017233607
		T-3	0.992189954 (8)	1.0003793 (30)	0.995599326	0.997724779	0.002275221
69-bus	3 DGs	T-1	0.981,136 (65)	1.00 (1)	0.992520842	0.993855028	0.006144972
		T-3	0.994246186 (50)	1.00 (1)	0.997123093	0.997873915	0.002126085
118-bus	5 DGs	T-1	0.95 (54)	1.00 (1)	0.974157367	0.99596176	0.004038241
		T-3	0.960,591 (46)	1.00 (1)	0.981,212	0.996,385	0.003615
118-bus	7 DGs	T-1	0.95 (54)	1.00 (1)	0.97483355	0.99596283	0.00403,717
		T-3	0.959,402 (46)	1.00 (1)	0.981,747	0.996,384	0.003616

5.2 IEEE 33-bus system

The second test system considered is a medium-sized radial network comprising 33 buses and 32 branches shown in Figure 4. It is completely radial in characteristic. The base values, load values, and losses for the 33-bus system were $V_{BASE} = 12.66$ kV, $S_{BASE} = 100$ MVA, $P_{LOAD} = 3,715$ kW, $Q_{LOAD} = 2,300$ kVAR, $P_{loss} = 202.67$ kW, and $Q_{loss} = 135.14$ kVAR. The bus and line data were obtained from Baran and Wu (1989a). The voltage limits at the buses were set between 0.95 and 1.05 p.u. The real and reactive power losses for this system were 202.67 kW and 135.141 kVAR, respectively. The detailed results for various load types are shown in Table 3. It includes DG capacity, power loss, percentage reduction in losses, power loss index, voltage deviation index, minimum bus voltage and its number, and operating cost.

Three DGs were connected to achieve the objective function. The results are summarized in Table 4. These are observed to be better than those achieved by the previous works from many perspectives. The results are compared with those reported by Moradi and Abedini (2012), Kumar Injeti and Kumar (2013), Imran et al. (2014), Prabha and Jayabarathi (2016), Quoc and Mithulananthan (2013), Aman et al. (2014), and Sultana and Roy (2015). The power losses obtained with the integration of the type-I DG were 71.89 kW compared with previously reported losses. Similarly, for the type-III DG, the reported loss was 14.49 kW. It was significantly lower than those achieved in these works. The voltage profiles of the type-I and type-III DGs are shown in Figures 5A, C, respectively. The convergence characteristics of the objective function with respect to the number of iterations are shown in Figures 5B, D, respectively.

5.2.1 IEEE 69-bus system

The next system considered was a large distribution network comprising 69 buses and 68 branches. The line and bus data were obtained from Baran and Wu (1989b). The single line representation is shown in Figure 6. The real and reactive power losses were 224.9606 kW and 102.147 kVAR,

respectively. The base voltage was 12.66 kV. The load on the system was set to 3,802.1 kW. The base power was 100 MVA. The voltage constraints were set between 0.95 and 1.05 p. u. The maximum permissible limit for DG penetration was set to 50%. Three DGs of type-I and type-III were connected in the system. The load flow was performed for all the load models. The results are reported in Table 5. This network involved a convergence criteria issue. Therefore, the number of iterations was increased to 100 instead of 50. Therefore, good results were obtained, compared with those reported by Moradi and Abedini (2012), Kumar Injeti and Kumar (2013), Imran et al. (2014), Prabha and Jayabarathi (2016), Quoc and Mithulananthan (2013), Aman et al. (2014), and Sultana and Roy (2015), as shown in Table 6.

The computed loss with the implementation of type-I DG was 71.25 kW using this method. This value is better than 89.0 kW obtained by the GA, 83.2 kW by PSO, and 81.1 kW by GA/PSO, as reported by Moradi and Abedini (2012). The value also shows the significance of this method compared to those of Kumar Injeti and Kumar (2013), Imran et al. (2014), Prabha and Jayabarathi (2016), Quoc and Mithulananthan (2013), and Aman et al. (2014). However, it is less effective compared to the results by Sultana and Roy (2015). Although the loss reduction by the ILA is not superior to that achieved by the KH method, the TOC is much significantly lower for the ILA method than that for the KH method. This is because the overall rating of the connected DG was less than that for the KH method.

Similarly, when the type-III DGs were optimally connected to the system using the IBI logic algorithm method, the results obtained were better than those achieved using the SA, BFOA, and IWO techniques. This is evident in Table 6. The losses were reduced less by the ILA than by the Loss Sensitivity Factor (LSF) and Krill Herd (KH) methods. However, the overall connected size of the DG was significantly smaller than those of these two superior methods. Hence, the total operating cost was significantly lower in the ILA method. The voltage profiles for type-I and type-III DGs for the 69-bus system are shown in Figures 7A, C, respectively. Meanwhile, the convergence of the objective function is shown in Figures 7B, D.

5.3 IEEE 118-bus system

The ILA was tested on a 118-bus system shown in [Figure 8](#) to demonstrate its optimal performance for a very large-scale distribution of networks. The base values, load values, and losses for the 118-bus system were $V_{BASE} = 11$ kV, $S_{BASE} = 100$ MVA, $P_{LOAD} = 22,709.72$ kW, $Q_{LOAD} = 17,041.06$ kVAr, $P_{loss} = 1,298.09$ kW, and $Q_{loss} = 978.73$ kVAr referred by [Sultana and Roy \(2015\)](#). The 118-bus radial distribution networks required seven DGs. However, the established approach was adaptable to any number. Meanwhile, the number of DG units in a test system depends on their size. However, introducing many DG units into a system can cause increased power losses. In this study, two cases were formulated for analyzing the impact of integrating five and seven DG units into the system. Both cases were tested for different load models.

5.3.1 Case 1: IEEE 118-bus system with five DGs

The real and reactive power losses for this network are 1,298.09 kW and 978.73 kVAr. The reported real power loss is 576.239 kW with the integration of type-I DG. This value is close to that reported by [Sultana and Roy \(2015\)](#) and significantly less than that obtained by [Kumar Injeti and Kumar \(2013\)](#). In addition, the TOC obtained is lower because the connected size was less.

Similarly, compared with the results of [Kumar Injeti and Kumar \(2013\)](#), the power loss is improved by 381.1619 kW, and 6.224 MVA less power was required to connect. The performance evaluation and comparative analysis for 118-bus system with five DGs are given in [Tables 7, 8](#) respectively. This reduced the operating cost. The voltage profiles and convergence characteristics for type-I and type-III are shown in [Figure 9](#).

5.3.2 Case 2: IEEE 118-bus system with seven DGs

The optimal locations of the seven type-I DGs are located at bus numbers 18, 80, 43, 72, 35, 110, and 96; with a total capacity of 10.09 MVA, these DGs reduced the loss in the 118-bus system to 558.7097 kW. This was better than that achieved by [Kumar Injeti and Kumar \(2013\)](#) and [Sultana and Roy \(2015\)](#). The type-III DG units, operating at 0.866 p. f., connected to bus numbers 13, 50, 72, 84, 89, 110, and 52 reduced the power loss to 297.9819 kW. In addition, the operating cost was lower than that in the two previous studies because the overall DG capacity connected in the ILA was 10.09 MVA for the T-I DG and 12.1028 MVA at 0.866 p. f. for the T-III DG. The performance evaluation and comparative analysis for 118-bus system with seven DGs are given in [Tables 9, 10](#) respectively. The bus voltages have been drawn for all the DG conditions. The convergence characteristics of the objective function with respect to the iterations are shown in [Figure 10](#).

The worst, best, average, median, and standard deviation values of bus voltages for test systems with the implementation of T-I and T-III into all the systems under study are given in [Table 11](#).

6 Conclusion

This study investigated the challenging mixed problem of placing and sizing DGs to minimize real power losses as the

voltage profile increases. A novel ILA method was used, for the first time, to identify the optimal size and location of DGs. To demonstrate the validity and effectiveness of the proposed technique, it was tested on very small, small, medium, and large-scale distribution networks, and hence, it shows the capability to be tuned at every size of the distribution network. Furthermore, its performance was compared with those achieved by previous published works. The recommended technique outperformed the existing algorithms in terms of single objective or as a whole, and the convergence characteristics of the objective function value. The analysis of different DG combinations to find the best possible solution to the problem, inclusion of the environmental objectives in problem formulation, and the analysis of DG performance with the 3 phase non-linear load could be the future scope for utilizing this algorithm.

Data availability statement

The original contributions presented in the study are included in the article/supplementary material; further inquiries can be directed to the corresponding author.

Author contributions

NS: Conceptualization, Data curation, Formal Analysis, Investigation, Methodology, Project administration, Resources, Software, Validation, Visualization, Writing—original draft, Writing—review and editing. MP: Supervision, Validation, Writing—review and editing. LS: Supervision, Writing—review and editing.

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Conflict of interest

The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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