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Simulation of hydraulic power matching—based risk and economic evaluation among cascade hydropower stations in spot transactions

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The electricity market is evolving rapidly from pre-bid to spot markets, where the transactions between producers and consumers have become crucial and are vulnerable to safety risks. In addition, the new modes of transaction are also becoming popular and are said to have some risks. To reveal the impact of the new electricity transaction mode-spot market-on the safety risk and generation benefit, this article presents a simulation method connecting the transaction results and operation process. To verify the effectiveness of the proposed method, an actual cascade hydropower station (CHS) in the Dadu River basin, Southwestern China, which comprises eight hydropower stations, is selected. Hydraulic power matching among the CHSs is discriminated from four aspects with multiple indicators combined with the reality of a hydropowerdominated market in Sichuan, China. The dispatching decision-making process of hydropower generators is described with a multi-objective optimization model and then solved with a fast search strategy based on the classical output calculation method in hydrology. The security risks and economic damage hidden in the day-ahead market on a certain day are discovered and analyzed. The technology proposed provides support for bidding decisions in spot transactions and satisfies the reality during the transition period of electricity reform.

KEYWORDS

electricity spot market, cascade hydropower stations, hydraulic power matching, multi-objective optimization, risk and economic evaluation

1 Introduction

Hydropower is and will be playing a critical role in global carbon neutrality and climate change; its global installed capacity is 1,360 GW (Wang et al., 2022). In China, the installed capacities reached 350 GW (Wang et al., 2022). The scale continues to expand globally and in China with the increasing demand and governmental commitment to



carbon neutrality (Wang et al., 2022). Though measures have been taken, harvesting hydropower has not been uniform in all the regions for various reasons (Saini and Saini, 2019). When considering enrichment regions such as southwest Sichuan and Yunnan Province of China, harvesting hydropower remains challenging (Zhang et al., 2017). Sichuan is an important energy-producing area with 78 GW hydropower capacity to cover nearly 80% of the regional power supply (both reservoirs and runoff plants) (Luo et al., 2021). Under the constantly deepening electricity market reform, hydropower



must be brought to market in Sichuan (Khorasany et al., 2020; Nunna et al., 2020). Unfortunately, a significant number of generators are unfamiliar with spot transactions; therefore, we attempt to build a bridge between the result of spot transactions and the operational process of cascade hydropower stations (CHSs), which shows the potential risks of the transactions more clearly and helps generators in bidding decision-making.

1.1 Research problem and literature review

The power supply is surplus in the wet season but is slightly close-fitting during the rest of the periods in Sichuan, China (Tian et al., 2021). In 2016, the total energy loss of water spillage was 28.75 billion, equivalent to 8 billion CNY (approximately 1.18 billion USD) (Ye et al., 2018). As a result, interprovincial transmission is hindered by channel capacity and economic policies (Li et al., 2018). At the same time, internal absorption lacks low vitality under the current market and dispatching model (Liu et al., 2018). Therefore, there is an urgent need for a market-oriented transaction model which will guide the investment direction accurately, improve the initiative of generators, and reduce the waste of low-carbon and renewable energy (Zhang et al., 2018; Zhang Z. et al., 2021). But the power system reform that came in 2015 introduced more intense competition in the electricity market (Lei et al., 2018); since then, generators can complete medium and long-term contract transactions skillfully (Yu et al., 2019). However, since August 2017, Sichuan and the other seven provinces have been

encouraged to carry out pilot power spot transactions to provide the experience of full market development. By the end of 2022, each pilot would have been put into trial operation under the government's guidance, but the development process has been slow. As the only hydropower-dominated electricity spot pilot in China (Cai et al., 2021), both market organizers (MO) and generators are not fully prepared for the new market. System operators have habituated themselves in to generating electricity according to dispatching schedules and enjoying preferential pricing from the government (Wang J. et al., 2018; Ye et al., 2020). Subsequently, it has become a mandate to reveal the relationship between the results of spot transactions and the operational process of the reservoirs to expose risks, but research in this cognate area remains sparse. As a result, the day-ahead market has shortened the trading interval to 15 min for power generators. The traditional long-term economic dispatching strategy that aims to maximize generation capacity (Akbari-Dibavar et al., 2021; Lu et al., 2021) is being solved by largescale optimization algorithms (Niu et al., 2018), which cannot satisfy demand.

Researchers in the literature have achieved some progress in the short-term optimization of CHSs (Sioshansi, 2015; Rasmussen et al., 2016; Apostolopoulou and McCulloch, 2019; Shafiekhani and Badri, 2019; Wang et al., 2019; Lu et al., 2020; Su et al., 2020; Zhang S. et al., 2021). However, there is significant deviation between the linearized solution and actual operation of the power stations (Sioshansi, 2015; Apostolopoulou and McCulloch, 2019). In addition, researchers have paid much attention to the bidding strategy, which directly affects the returns of the generating companies (Shafiekhani and Badri, 2019; Wang et al., 2019; Su et al., 2020). The comparison between the bidding and clearing results has been of less concern (Zhang S. et al., 2021), resulting in ignoring key factors such as unit and reservoir operating safety (Lu et al., 2020). So, turning to MOs could be a possible option, but the transition still lacks a distinct clearing model for the hydropower-dominated spot market. In some other hydropower systems, such as in Brazil and other countries, hydropower is purchased at a subsidized price to ensure adequate power supply (de Queiroz et al., 2016) where the generator can conduct self-dispatching as a pricemaker (Loschenbrand and Korpas, 2019).

On the contrary, in pool-based hydropower systems, such as in Norway and Sweden, the generation schedule and settlement price are determined with unified clearing (Pereira et al., 2017; Seljom and Tomasgard, 2017), similar to that in Sichuan, China. Meanwhile, when considering power line lock, the locational marginal price (LMP) from PJM, US market, is involved (Exizidis et al., 2019; Ali et al., 2021), and then a unique weighed clearing price is obtained. Due to the slow progress of clearing, MOs have to complete this task with security-constrained economic dispatch (SCED) in the day-ahead market (Xu et al., 2017). At the same time, real-time load balance and inflow uncertainty would be solved by bidding in a real-time market (Zhou et al., 2020). Finally, signed contracts in medium- and long-term markets are decomposed and then involved in a settlementbased "contract for difference (CFD)" to minimize bidding risk

(Douglas Foster et al., 2019). The root cause of this issue is attributed to the complex, nonlinear coupling relationship between the CHSs, which is shown in the following aspects. Firstly, inflow is the primary factor of market supply capacity, resulting in different bidding strategies (Helseth et al., 2017; Li et al., 2019). Then, the water from the upstream power station will be used as the inflow of the downstream power station, which directly affects the power generation process (Wang X. et al., 2018). When multiple owners manage a cascade system, this information is unknown. A study attempted to divide the alliance according to the hydraulic connection to overcome owners' restrictions. The rationality of alliance with the symbiosis theory was proposed by Zhu et al. (2021) which later verified alliance's stability with the game theory (Liu et al., 2020). But here comes a new problem: when there are multiple nodes in the basin, as in the Dadu River, the alliance will collapse automatically and SCED must take the power station as the unit. Last but not the least, different from thermal power (Ye et al., 2017), it is impossible to forecast inflow accurately. However, in timely checking the transaction results according to the real-time parameters and rolling bidding in the real-time market can be a good choice. For this, simulation and verification in advance are essential measures to mine and avoid risks (Huang et al., 2019). The development of intelligent systems and software packages makes this simulation and verification more convenient. Ding Q et al. developed a spot transaction decision support system (Ding et al., 2018). Zakeri et al. (2016) simulated a multiregional electricity market, which made generators respond quickly to changes in market rules and environment. More recently, such simulations and decisionmaking in the electricity market have become more popular as the power generation systems became an integral part of the smart grid systems (Ringler et al., 2016). Whereas the previous research of Ivar Skjelbred and Kong (2018) made intraday replanning after simulating the actual operation process. The study by Aliabadi et al. (2017) concluded bidding decisionmaking by simulating the bidding behaviors of generators under different market modes, such as capacity and auxiliary market. Chen et al. (2017) applied the same method in another hydro-dominated environment for the power generation system in Yunnan Province of China.

1.2 Key contributions

Considering the research problem and gap stated in Section 1.1, we re-stored the results of spot transactions for CHSs to the operation process of reservoirs and stations by fully considering the hydroelectric coupling relationship between the CHSs. Some indicators are selected to describe the mismatch between the CHSs quantitatively. The Sichuan electricity spot market is considered as the case study. The meaning and discrimination methods of hydraulic power matching

between the CHSs are described from four aspects with the help of multiple numerical indicators. We simulated the dispatching decision-making process of CHSs with a multi-objective optimization model followed by a fast search strategy for an equilibrium solution. The results provide the basis for load adjustment and bidding decision-making in the real-time market.

The key contributions of this study are as follows:

- In the transition period from the dispatching schedule to market transaction, this study puts forward a reliable risk identification and auxiliary decision-making approach that allows verification with the actual system.
- An efficient and accurate search strategy for multidimensional, nonlinear, and multi-objective problems is proposed, which expands the classical output calculation of hydrology from a single power station to the CHSs.
- The hydraulic power matching between the CHSs is quantified from multiple dimensions, providing a reference

for subsequent transaction strategy decision-making and clearing improvement in the hydro-dominated market.

This study is organized into six sections. Section 2 presents the matching discrimination methods for the results of spot transactions. Section 3 demonstrates the model for simulating the dispatching decision-making of the CHSs in a market transaction and its calculation strategy. Section 4 presents the case study and test system used for an investigation, followed by results and discussion in Section 5. Lastly, the conclusions and drawbacks drawn from this study are presented in Section 6.

2 Matching discrimination methods

The spot electricity market is still immature in Sichuan, mainly reflected in the single type of transaction. Currently, only the dayahead and real-time markets of electric energy have been open for

the time being. In the former, the generators submit each period's generation capacity and bidding price one day in advance (D-1). Turning to the latter, only the maximum generating capacity is submitted 1 hour in advance (T-1). The transaction results are distributed after the unified clearing of the MO. The complete process of spot transactions is illustrated in Figure 1.

Natural runoff significantly affects the supply and demand situation of the high-proportion hydroelectric power market. The supply exceeds demand during the wet season (June to October), resulting in a significant waste of hydropower resources. In the dry season, the supply is close-fitting due to the restrictions in coal supply. To promote hydropower absorption during the wet season, the waste of clean energy is reduced and sufficient power supply during the dry season is ensured, and hydropower plants only participate in spot market bidding during the wet season. The monthly hydropower generation, the power demand of Sichuan, and inflow runoff in the largest hydropower station are therein illustrated in Figure 2.

To maximize the utilization of hydropower resources in the basin, the same owner's CHSs adopt a unified method to optimize the volume and price combination process of each power station in the cascade according to the hydraulic connections therein, thereby forming a volume price and declaration plan for each power station in the cascade. However, the MO pursues minimization of expenditure during market clearing. Meanwhile, large-scale cascade hydropower clusters are often divided into multiple planning units during market clearing. Compared with the declared plan, both loads of a single power station at each time period or the load between the power stations in the same time period must have undergone significant changes. Therefore, it is necessary to simulate the load results according to the mode of organization and verify whether there is a mismatch between hydraulic and power in the cascade system.

The CHSs usually consist of one or two reservoirs connected with a series of runoff stations. The mismatch

Parameter	HZY	DGS	PBG	SXG	ZTB	SP	GZ	TJZ
Installed capacity (MW)	1700	2600	3600	660	720	345	770	700
Maximum water level (m)	1842	1130	850	660	624	554	528	474
Minimum water level (m)	1802	1120	790	655	618	550	520	469
Storage capacity (10 ⁸ m ³)	37.06	7.62	51.22	0.31	0.41	0.15	1.38	1.00
Maximum water discharge (m³/s)	1474	1834	2772	2619	2697	2825	1876	2536
Rated water head (m)	130	160	148	30	29.5	17.15	48	31
Output factor	8.5	8.5	8.29	8.38	8.34	8.5	8.5	8.5
Regulating performance	Season	Daily	Annual	Daily	Daily	Daily	Daily	Daily
Propagation time (15 min)	_	28	22	2	1	3	4	4

TABLE 1 Hydropower station parameters.

within the CHSs is described as follows: the upstream obtains less volume due to bidding failure, so they have to release less water. As for the downstream, the low running water head makes the power generation task impossible to complete when water is insufficient. This deviation may cause a loss of revenue. As the reservoir reaches the upper limit of storage capacity, all stations are forced to release water; a large amount of water spillage means clean energy wastage. Unfortunately, this mismatch occurs almost every day in the wet season.

The matching verification focuses on four aspects and has been quantified with many indicators. Firstly, output simulation ensures that the real-time output covers the transaction results and fully uses the water resources. Secondly, safety operations are checked to verify whether the hydraulic and electric constraints are damaged. Then, more attention is paid to the process of water spillage, the quantity of water, and generation of waste. Lastly, the benefit from the bidding is evaluated according to the settlement rules. When a mismatch occurs, it is advisable to strive for more capability in real-time bidding, which guarantees reservoir safety and benefits in market competition. The technology roadmap is displayed in Figure 3.

2.1 Output simulation

This part analyses the simulation results from the generation output. In addition to the apparent output deviation, the calculation results of the following four indicators can also show the effect on economic operation.

2.1.1 Water resource utilization

It is a numerical indicator reflecting the runoff conversion efficiency of a hydropower plant, which is recorded as E_{wu} (%):

$$E_{wu} = \sum_{t=1}^{T} N_{k,t} / \left(\eta_k \times \sum_{t=1}^{T} R_{k,t} \times H_k^D \right), \forall k \in K, \forall t \in T.$$
(1)

2.1.2 Load rate

It is an economic indicator to measure the utilization degree of units. It is recorded as E_p (%):

$$E_p = \left(\sum_{t=1}^T N_{k,t} / T\right) / \bar{N}, \forall k \in K, \forall t \in T.$$
(2)

2.1.3 Comprehensive water consumption rate

The water consumption per unit of power generation is recorded as $Hsl_{k,t}$:

$$Hsl_{k,t} = (Q_{k,t} \times M_t \times 60)/E_{k,t}, \forall k \in K, \forall t \in T.$$
(3)

2.1.4 Generating equipment availability hours

The operating hours of power generation equipment under full load operation are recorded as Tu_k (*h*):

$$Tu_k = \sum_{t=1}^{T} E_{k,t} / \bar{N}_k, \forall k \in K, \forall t \in T.$$
(4)

In the calculated results, if the load rate and availability hours are low for the stations with reservoirs, it results in low water resource utilization or high water consumption rate, or even the load transaction task cannot be completed for other stations. This result indicates that the transaction results exhibit the risk of mismatch between upstream and downstream operations.

Indicator	HZY	DGS	PBG	SXG	ZTB	SP	GZ	TJZ
Water resource utilization (%)	30.5	62.2	131.7	88.9	72.7	42.6	44.7	71.5
Load rate (%)	19.0	44.7	74.0	77.3	58.1	52.4	75.9	81.5
Comprehensive water consumption rate	3.14	2.63	2.58	13.03	21.43	26.96	9.57	13.7
Availability hours (h)	4.6	10.7	17.8	18.6	13.9	12.6	18.2	19.6

TABLE 2 Calculated economic operation indices.

2.2 Safety risk identification

The safety of reservoirs and generating units is the basis and premise for successfully implementing transaction results. Therefore, it is necessary to reveal and warn the risks in advance when hydraulic power mismatch threatens the safe operation.

The vibration areas of each plant should be avoided as much as possible during power generation and this is determined by a ternary, implicit function containing the vibration area, real-time net head, and available status of each generation unit:

$$\begin{bmatrix} \underline{NS_{k,t}}, \overline{NS_{k,t}} \end{bmatrix} = f_{3k} \left(H_{k,t}, \mu_{n,t,k}, \begin{bmatrix} \underline{NS_{n,t,k}}, \overline{NS_{n,t,k}} \end{bmatrix} \right),$$
(5)
$$\forall k \in K, \forall t \in T, \forall n \in N.$$

The forebay elevations of reservoirs are usually limited to below the maximum in the wet season, which leaves surplus storage space for uncertain inflow. However, it is contradictory to the efficient production of electricity. It is insufficient to consider the upper and lower bounds of forebay elevations of reservoirs alone. The change speed of elevations during the dispatching period is also crucial to the safety of hydraulic structures. In particular, this constraint is indispensable for reservoirs.

Besides power generation, reservoirs usually play an important role in shipping, agricultural irrigation, and ecological landscapes. These functions put forward a series of constraints on the water release of the reservoirs.

2.3 Estimation of water spillage

When the forebay elevations of reservoirs gradually rise to the upper bound, the water spillage from the plants will naturally ensue, which implies a waste of renewable energy. The electricity loss with water spillage concerns generators, dispatching institutions, and government sectors.

This part pays attention to three aspects: firstly, time recognition to determine the time and distribution range of spillage water. Secondly, calculated natural water loss in the whole dispatching period. Finally, the conversion of water loss into generation wastage according to Eq. 6:

$$ES_k = \sum_{t=1}^{T} \eta_k \times S_{k,t} \times H_{k,t} \times 0.25, \forall k \in K, \forall t \in T.$$
(6)

where ES_k represents the generation wastage caused by water spillage (MW \cdot h).

2.4 Benefit evaluation

In the current electricity market, spot transaction, including day-ahead and real-time markets, is only a supplement to medium- and long-term contracts. The load curves after dayahead market clearing are formed by superimposing the following curves: interprovincial power-transmission curve, prior electricity generation curve, decomposition curve of medium- and long-term contracts, and the curve in the dayahead market. Each part uses a different method for settlement, and the specific mode is shown in Figure 4. The first two parts represent fixed price, while the settlement mode based on CFD leads to bidding risk, which directly determines the benefits of the bidding.

CFD is a reasonable path to reduce the loss of bidding failure in the immature market environment. Medium- and long-term contracts can avoid economic risks as far as

possible. The profit is mainly from medium- and long-term contracts and day-ahead market, then reducing power deviation in real time. The benefits under the CFD settlement method are calculated as follows:

$$W_{k} = \sum_{t=1}^{T} E_{k,t} \times P_{k,t}^{d} + \left(E_{k,t} - E_{k,t}^{l}\right) \times \left(P_{k,t}^{d} - P_{k}^{l}\right), \forall k \in K, \forall t \in T,$$
(7)

where W_k represents the total benefit (CNY) of station k settled with CFD.

3 Model and algorithm

3.1 Model description

When receiving the transaction result, generators are willing to fully use reservoirs' regulation capacity to complete tasks with low water consumption. However, the failure of hydraulic power matching causes output deviation and water spillage, especially for runoff stations. Therefore, we describe the dispatching decision-making process of CHSs with an optimization model, whose results will reflect the real power generation operation process.

Objective 1: the output of each station shall be close to the transaction result as much as possible, that is, minimizing the deviation:

$$\min\sum_{t=1}^{T} \left(N_{k,t} - N_{k,t}^{p} \right)^{2}, \forall k \in K, \forall t \in T.$$
(8)

Objective 2: improve the utilization efficiency of water resources and reduce water consumption, especially water spillage:

$$\min\sum_{k=1}^{K} \sum_{t=1}^{T} S_{k,t}.$$
 (9)

Constraint conditions:

(a) Water balance

 $V_{k,t+1} = V_{k,t} + (R_{k,t} + I_{k,t} - O_{k,t}) \times M_t \times 60, \forall k \in K, \forall t \in T,$ (10)

$$I_{k,t} = \begin{cases} \sum_{w \in \Omega_k} O_{w,t-\tau_{k-1,k}}, & \text{if} \quad t - \tau_{k-1,k} \ge 1 \\ 0, & \text{otherwise} \end{cases}, k \ge 2, \forall t \in T \\ V_{1,t} = V_{1,0} + [R_{1,t} - O_{1,t}] \times M_t \times 60, \forall t \in T \end{cases}$$
(11)

$$O_{i,t} = Q_{i,t} + S_{i,t}, \forall k \in K, \forall t \in T.$$
(12)

(b) Forebay elevation of reservoirs

$$\underline{Z}_{k,t} \leq \underline{Z}_{k,t} \leq \overline{Z}_{k,t}, \forall k \in K, \forall t \in T,$$
(13)

$$\overline{Z_{k,t}} - \underline{Z_{k,t}} \le \Delta Z_k, \forall k \in K, \forall t \in T.$$
(14)

(c) Water discharge

$$Q_k \leq Q_{k,t} \leq \overline{Q_k}, \forall k \in K, \forall t \in T.$$
(15)

(d) Water release

$$O_k \leq O_{k,t} \leq \overline{O_k}, \forall k \in K, \forall t \in T.$$
(16)

(e) Vibration areas of plants

$$\left(N_{k,t} - \underline{NS_{k,t}}\right) \times \left(N_{k,t} - \overline{NS_{k,t}}\right) \ge 0, \ \forall k \in K, \forall t \in T.$$
(17)

(f) Relationship between forebay elevation and volume

$$Z_{k,t} = f_{1k}(V_{k,t}), \forall k \in K, \forall t \in T.$$
(18)

(g) Relationship between tail-race elevation and water release

$$z_{k,t} = f_{2k}(O_{k,t}), \forall k \in K, \forall t \in T.$$
(19)

(h) Reservoir net head

$$H_{k,t} = (Z_{k,t} - z_{k,t}) \times (1 - L_k).$$
(20)

(j) Hydroelectric power generation function

$$N_{k,t} = \eta_k \times Q_{k,t} \times H_{k,t}, \forall k \in K, \forall t \in T,$$
(21)

$$N_k \leq N_{k,t} \leq \overline{N_k}, \forall k \in K, \forall t \in T.$$
(22)

(k) Types of variables

$$O_{k}(t) \ge 0, Q_{k}(t) \ge 0, S_{k}(t) \ge 0, \forall k \in K, \forall t \in T,$$

$$V_{k}(t) \ge 0, Hu_{k}(t) \ge 0, Hd_{k}(t) \ge 0, \forall k \in K, \forall t \in T,$$

$$H_{k}(t) \ge 0, \forall k \in K, \forall t \in T$$
(23)

3.2 Algorithm

The simulation model above is a complex optimization problem with multiple dimensions, stages, and objectives, whose Pareto front is almost impossible to be described thoroughly. Moreover, the time to search for the complete solution set is far more than 15 min, which is not conducive to rapid decision-making in the spot market. Decision makers determine whether there is a mismatch through a few equilibrium solutions in a short time and then formulate bidding strategies in a real-time market. Therefore, we redesigned the fast search algorithm for an equilibrium solution from the reality of decision-making.

The algorithm design considers the following principles: firstly, objective 1 is directly related to the benefits and deserves more attention. Then, minimizing the error during calculation restores the real operation process of the stations' reservoir and runoff. Last but not the least, reasonable time consumption spares enough time for marketing decisionmaking.

In order to maintain the balance and stability of the grid, generators organize power generation in strict conformity with the transaction results such that the actual output is not greater than the expected output. Suppose the hydraulic power matching relationship is destroyed, the transaction result will be regarded as the infeasible solution of the above optimization. Considering this, we fully use the solution's information and retain the original transaction result as much as possible to reduce the output deviation. The classical output calculation method in hydrology can quickly obtain the forebay elevation and water discharge process corresponding to each result. Especially after complete iteration using binary search, it will converge to the maximum generation capacity corresponding to the current water volume.

The input of inflow in each period is the key to accurate calculation, and it is also an essential feature of CHSs. However, the propagation time of flows τ between the CHSs cannot be ignored in short-term scheduling operations. Thus, the asynchronous propagation of water energy divides the complete calculation process into three parts, as shown in Figure 5.

We discard the linearization of constraint (21) to maximize the accuracy of the calculation. Moreover, the binary search compresses the target space and ensures the stability of the solution. Finally, the solution set consists of some transaction results and the closest output. It is the dominant solution of objective 1, a Pareto equilibrium solution of the multi-objective problem. The specific steps are described as follows and shown in Figure 6.

- Step 1: The initial forebay elevation $Z_{k,0}$ and load transaction result $N_{k,t}^p$ are recorded.
- Step 2: The inflow information is unknown in both part 2 and 3; thus, the periods of each station in part 1 is first calculated with the output calculation method in hydrology and binary search. The result, including forebay elevation, water discharge, and release, is input to subsequent calculations according to time propagation as shown in Figure 5.

- Step 3: The flow propagation in Figure 5 represents the propagation direction of inflow information: the inflow of each period is calculated one by one according to eq. 11, and the output calculation repeated until the operation results of all points are obtained successively.
- Step 4: The safety risk and economic evaluation indicators are calculated with the results in Step 3 according to Section 2. Then, the matching among the CHSs is analyzed.

4 Case study: Cascade hydropower system in the Dadu River basin

This article uses an existing cascade system in the Dadu River basin, Southwestern China. The positions and configurations of the CHSs are illustrated in Figure 7, which comprise eight hydropower stations named HZY, DGS, PBG, SXG, ZTB, SP, GZ, and TJZ. Their total capacity reaches 11,095 MW, and the parameters of each station are listed in Table 1. The CHSs are all managed by Dadu River Hydropower Development Co., Ltd. and naturally adopt a consistent bidding strategy in the electricity market. In addition, the total capacity of the eight stations accounts for nearly 20% of the power supply in Sichuan,

Water level: m Generation output: MW Flow: m ³ /s												
Time	Initial water level	Final water level	Water level status	Transaction ouput	Actual ouput	Output status	Inflow	Water discharge	Water release	Flow status	Head	Vibration are
0:15	553.80	552.80		243	243		0	1733	1733		16.51	
0:30	552.80	551.65		244	244		0	1904	1904		15.08	
0:45	551.65	550.24	Lower	244	244		0	2161	2161		13.30	
1:00	550.24	550.00	Lower	245	223	Insufficient	1722	2825	2825		12.65	
1:15	550.00	550.00	Lower	243	195	Insufficient	1743	2825	2825		13.19	
1:30	550.00	550.00	Lower	246	195	Insufficient	1744	2825	2825		13.19	
1:45	550.00	550.00	Lower	243	191	Insufficient	1685	2825	2825		13.32	
2:00	550.00	550.00	Lower	244	190	Insufficient	1682	2825	2825		13.32	
2:15	550.00	550.00	Lower	214	205	Insufficient	1859	2825	2825		12.94	
2:30	550.00	550.00	Lower	210	205	Insufficient	1860	2825	2825		12.94	
2:45	550.00	550.00	Lower	216	205	Insufficient	1868	2825	2825		12.93	
3:00	550.00	550.00	Lower	219	206	Insufficient	1875	2825	2825		12.91	
3:15	550.00	550.00	Lower	212	206	Insufficient	1881	2825	2825		12.90	
3:30	550.00	550.00	Lower	217	207	Insufficient	1896	2825	2825		12.87	
3:45	550.00	550.00	Lower	215	207	Insufficient	1896	2825	2825		12.87	
4:00	550.00	550.00	Lower	236	200	Insufficient	1799	2825	2825		13.07	
4:15	550.00	550.00	Lower	243	200	Insufficient	1801	2825	2825		13.06	
4:30	550.00	550.00	Lower	242	200	Insufficient	1805	2825	2825		13.05	
4:45	550.00	550.00	Lower	241	201	Insufficient	1813	2825	2825		13.04	
5:00	550.00	550.00	Lower	235	189	Insufficient	1660	2825	2825		13.37	
5:15	550.00	550.00	Lower	236	189	Insufficient	1660	2825	2825		13.37	
5:30	550.00	550.00	Lower	235	189	Insufficient	1661	2825	2825		13.37	

China. Any deviation caused by hydraulic power mismatch among the CHSs will threaten the stability of the power grid.

5 Results and discussion

The total load transaction result of the test system mentioned above is 625 GW. However, the load deviation reached 10.1 GW due to mismatch, which accounts for 1.62% and almost covered all the middle and later schedule periods. Among them, the most significant deviation appears in ZTB (8433 MW), accounting for 17.4% of that station's total load transaction result. GZ and TJZ account for 1.2 and 1.8%, respectively. The load deviation time distribution is shown in Figure 8.

Changes in the water heads at some hydropower stations during the operation are plotted in Figure 9 to ascertain the reasons for failure to satisfy the transaction generation. The operating head of the power station is below the design head in ZTB, GZ, and TJZ (TJZ is lower in some periods), which can cause output attenuation among the hydropower stations.

The various economic indices of different CHSs mentioned in Section 4 are calculated and listed in Table 2. The water resource utilization and load rates of HZY, DGS, SP, and GZ are lower than those of the other four hydropower stations. The water consumption rate for ZTB and SP is higher than is for the others because there is a significant negative correlation between the rate of water consumption of hydropower stations and the head of water during the operation of such hydropower stations.

In summary, the hydraulic power mismatching among CHSs is hidden in spot transaction results; the abundant hydropower resources in the basin are not fully utilized in the wet season. HZY, DGS, ZTB, and SP should fully excavate their generation capacity and fully compete in the real-time market.

Figure 10 shows the combination and distribution of vibration zones in HZY and PBG, the two plants with reservoirs and a huge installed capacity in the test system. All CHS units were available on; the check shows that the transaction results of the various hydropower stations in all intraday time periods do not fall within the fluctuation range.

The initial forebay elevations of each station correspond to the forebay elevations at 00:15 on that day. Moreover, the daily rate of change in forebay elevations at hydropower station HZY is 0.5 m/d. In comparison, PBG presents a daily growth rate and reduced rates of 1.2 m/d and 1.5 m/d, respectively. The simulation results of the water level are shown in Figure 11.

The changes in water levels at various hydropower stations were obtained through simulation. Except for hydropower station SP, the highest water levels of the other hydropower stations do not reach the normal pool level. By contrast, the reservoir water levels satisfy the requirement of flood control safety in flood seasons. However, the hydropower station ZTB operates at a low water level for a long time and hydropower stations GZ and TJZ also operate at a low water level for some time periods. This causes the water

head at these hydropower stations to be much lower than the design head of the generating units.

In summary, 3.38 TW \cdot h of clean electricity is dissipated due to water spillage among the test CHSs, which is more than twice the actual power generation of 1.56 on the day. Nearly all power stations spill water, except PBG and ZTB. It is noticed that this situation happens in all periods in HZY and SP. The spilled water and generation wastage process of each station is illustrated in Figures 12–14. The numbers shown in Figures 12–14 denote the total intraday water loss and generation wastage caused by water spillage at various hydropower stations.

Same as the price bidding strategy, the average price transaction results among CHSs are observed to be the same. Nevertheless, the profits exhibit a noticeable difference (see Figure 15). As an objective economic law, there is a direct natural relationship between income and power generation. For example, the electricity generation at PBG is three to five times that at the other hydropower stations. However, HZY and SP separately account for 1/9 and 1/15 of the electricity generated at PBG.

Moreover, the CFD settlement method causes the loss of profits from power generation. DGS and SP do not satisfy the electrical energy generation required from medium- and longterm markets in many time periods during the bidding process. In this context, the profit margin is squeezed.

The model and technology proposed have been incorporated into the spot transaction bidding system for CHSs of CHN Energy Co., Ltd. (Figure 16). Relying on a comprehensive data collection and transmission cloud platform, the system can automatically capture inflow, water level, unit status, transaction information, and others. Adaptively rolling simulation and deduction can realize real-time transaction risk monitoring a day ahead and assist bid decision-making. Up to now, the system has been running stably for nearly 2 years. The actual risk warning of safety and economic operation results of the system on a certain day are illustrated in Figures 17, 18, respectively.

6 Conclusion

Considering the requirements of electricity market reform and reality in a hydro-dominated power system, a simulation approach to risk and economic evaluation among CHSs in spot transactions was proposed. Hydraulic power matching is the key, as well as a difficulty of the problem, so multiple numerical indicators from four aspects were selected to describe it. Furthermore, a model to simulate the decisionmaking process of hydropower generators was constructed and solved with an algorithm strategy that considers minimum error and reasonable time consumption. In this process, the classical output calculation of hydrology was expanded from a single power station to CHSs. Finally, a cascade system in Southwest China comprising eight hydropower stations with their real transaction results was used for verification. Through discussion, the security risks and economic damage hidden in the day-ahead market on a certain day were discovered and analyzed. The technique proposed provides support for bidding decisions in spot transactions and satisfies the reality during the transition period of electricity reform.

The proposed method's deficiency lies in regarding the propagation time of flows between the CHSs as a fixed value during calculation. However, the flow propagation time changes dynamically during a hydropower station's actual operation. Thus, the actual propagation time presents a certain difference relative to the fixed value used during calculation, which influences the calculation of the actual change of forebay elevations under corresponding outputs from hydropower stations to some extent. In subsequent research, the propagation time of flows will be introduced to calculations after being graded and calibrated to reduce the errors.

Data availability statement

The original contributions presented in the study are included in the article/supplementary material, and further inquiries can be directed to the corresponding author.

Author contributions

Conceptualization: SZ and GM; methodology: SZ; software: WH; validation: SZ, GM, and CT; formal analysis: BY and YX; resources: CT; writing—original draft preparation: SZ. All authors have read and agreed to the published version of the manuscript.

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Conflict of interest

Tao C-H was employed by the company Dadu River Hydropower Development Co., Ltd. and Yang B-Q and Xue Y-L were employed by the company Power China Hydropower Development Group Co., Ltd.

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The remaining authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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Nomenclature

 η_k Average efficiency coefficient of station k

 $\mu_{n,k,t}$ Binary constant indicating whether the unit *n* of the station *k* in period *t* is online, which is 1 when the unit is online; otherwise, it is 0.

 $P_{k,t}^d$ Clearing price of the day-ahead spot market of station k in period t

 H_k^D Design head of station k

 \varOmega_k Downstream stations of CHSs

 $E_{k,t}^l$ Electricity generation decomposed from medium- and long-term contracts of station k in period t

 $E_{k,t}$ Electricity generation of station k in period t

N Generator units

K Hydroelectric stations/reservoirs

k Index for CHSs from 1 to K

w Index for downstream stations of CHSs from 2 to \varOmega_k

 \boldsymbol{n} Index for generator units from 1 to \boldsymbol{N}

t Index for time periods from 1 to T

 $R_{k,t}$ Inflow to station k in period t

 M_t Length of the calculation period

 ΔZ_k Limit of the rate of change in the water level at reservoir k

 $N_{k,t}^p$ Load transaction result at station k in period t

 L_k Loss constant of station k

 $\underline{NS_{k,t}}, \overline{NS_{k,t}}$ Minimum/maximum fluctuations of the station k in period t

 N_k , $\overline{N_k}$ Minimum/maximum power output of station k

 $NS_{k,t,n}$, $NS_{k,t,n}$ Minimum/maximum vibration areas of the generator unit *n* at station *k* in period *t*

 V_k , $\overline{V_k}$ Minimum/maximum volume of reservoir k

 $\underline{Z_{k,t}}, \overline{Z_{k,t}}$ Minimum/maximum water level of station k in period t

 $O_{k,t}$, $\overline{O_{k,t}}$ Minimum/maximum water release from station k in period t

 $H_{k,t}$ Net head of station k in period t

T Periods

 $N_{k,t}$ Power output of station k in period t

 \boldsymbol{P}_k^l Price set by medium- and long-term contracts of station k in period t

 $f_{1k}\left(\cdot\right)$ Relationship between forebay elevation and volume of reservoir k

 $f_{2k}\left(\cdot\right)$ Relationship between tail-race elevation and water release from reservoir k

 $f_{3k}\left(\cdot\right)$ Relationship between vibration areas of the generator unit n and station k

 $z_{k,t}$ Tail level of reservoir k in period t

 $V_{k,t}$ Volume of reservoir k in period t

 $Q_{k,t}$ Water discharge from station k in period t

 $Z_{k,t}$ Water level of reservoir k in period t

 $O_{k,t}$ Water release from station k in period t

 $S_{k,t}$ Water spillage from station k in period t