

Low-Carbon Robust Predictive Dispatch Strategy of Photovoltaic Microgrids in Industrial Parks

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With the flexible integration of local renewable energy with the smart distribution network system, the problems of high operating costs and power shortage can be effectively solved. However, taking the industrial park microgrid with high penetration photovoltaic as an example, due to the uncertainties and fluctuations arising from the meteorological conditions and the load demands, the safe and reliable operation of the microgrid system has been threatened significantly. Operators often need to pay additional unnecessary costs to maintain stable operations of the microgrid. Therefore, in this study, a dispatch strategy based on robust model predictive control considering low-carbon cost is designed to reduce the adverse effects of uncertainties. First, a low-carbon energy management scheme is formulated based on short-term source and load forecast information in which a two-stage robust optimization solution method is used to generate the optimal dispatch scheme under the worst scenario. Then, an intraday real-time strategy with a closed-loop feedback mechanism is formed based on the model predictive control. Finally, the feasibility of the proposed strategy is simulated and analyzed based on the measured data of the photovoltaic microgrid in the industrial park. The results show that compared with the general intraday scheduling strategy and the day-ahead robust strategy, the proposed strategy can effectively get low-carbon scheduling plans considering the uncertainty of source and load while efficiently balancing the robustness and economy of the grid-connected industrial park photovoltaic microgrid system operation.

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1 INTRODUCTION

Decentralization and low-carbon energy reformation are promoted continuously with the increasing scale and intricate operating conditions of modern power grids (Basak et al., 2012; Morstyn et al., 2018). As a single modular system, the microgrid (MG) can flexibly dispatch distributed generation (DG) such as photovoltaics (PVs) and wind turbines (WTs) to provide power for its regional load demand (Alipour et al., 2015; Zia et al., 2018). Compared with the traditional distribution network, the electrical distance between generator units and the consumers is much closer, which can increase power quality and economic benefits. Because of the plug-and-play characteristics of these distributed devices, microgrids are considered the foundation for further expansion of the power grids.

Microgrid operators are management platforms responsible for energy flow within the region, which need to consider the principles of profitability while ensuring the balance of power supply and

demand in the whole region (Zhou et al., 2021). However, due to the uncertainties of meteorological conditions and load demands, it is difficult for microgrid operators to use accurate forecast information to formulate scheduling plans (Kou et al., 2018). Therefore, microgrid operators need to use a more appropriate dispatch strategy in their energy management system (EMS) to ensure the normal and stable operation of the microgrid (Raya-Armenta et al., 2021). At the same time, to achieve the objective of low-carbon environmental protection, various regions have begun to implement carbon trading policies aiming to meet the carbon indexes. In addition to purchasing electricity from the main grid, large-scale consumers of the distribution network can also trade carbon to deal with the rest of carbon consumption apart from allocated carbon indexes (Lu et al., 2013). Therefore, the low-carbon dispatch operation of microgrids also needs further improvement.

The microgrid in the industrial park is dominated by industrial loads, which have the characteristics of large load demand and higher requirement of power supply reliability (Yu et al., 2016). To minimize the operating cost, the traditional day-ahead dispatch strategy can make an economic optimal dispatch plan based on the forecast data. However, these strategies lack consideration of uncertainty in actual operation; it is tough to make timely and rational adjustments, which leads to a higher requirement for the accuracy of the prediction model of renewable sources and load. On the other hand, operators need to pay extra costs for forecast deviations due to sudden uncertain fluctuations and tolerate the damage of power balance and the safe operation.

Therefore, in order to adapt to the dynamic characteristics of various devices in the microgrid, various types of scheduling strategies have been designed in various literature studies to cope with different uncertain information (Yang and Su, 2021). Robust optimization (RO) strategy ensures the stable operation of the microgrid in a complex operating environment by finding the worst scenario for the scheduling plan (Liu et al., 2020; Choi et al., 2019). In Liu et al. (2020), a two-stage robust model is proposed for an integrated power-heat-gas microgrid to achieve the optimal day-ahead economic scheduling considering the uncertainty of wind power scenarios. In Li et al. (2021a), a data-driven set-based robust optimization (DSRO) model considering the uncertainties of wind power and multiple demand response programs (DRPs) has been proposed, and a combined cooling, heating, and power (CCHP) microgrid with the power-to-gas (P2G) device is used to verify its feasibility. In Choi et al. (2019), the robust optimal control strategy for an energy storage system (ESS) of a grid-connected microgrid is proposed. The mixed-integer linear programming and the nonlinear efficiency map method are considered to cope with different external conditions. These aforementioned studies effectively improve the safety margin and robustness of scheduling plan through RO strategy. However, these strategies are still day-ahead scheduling strategies, which are limited by insufficient flexibility in operation. Meanwhile, on account of the requirements to consider the amount of information throughout the whole day, the computational burden on the central controller will be aggravated.

Model predictive control (MPC) utilizes the idea based on closed-loop rolling optimization to respond to the fluctuation of renewable energy and realize adaptive optimization with the time rolls (Li et al., 2018; Wu et al., 2021). In Li et al. (2018), a multitime scale-based three-layer coordination optimal scheduling system is designed. In Garcia-Torres and Bordons (2015), a control strategy using MPC for renewable energy microgrids with hybrid ESS is proposed in which the MPC is built within the market framework in different time scales to maximize the economic benefit of the microgrid. A multi-renewable-tohydrogen production method is proposed to enhance the green H₂ production efficiency in Zhang et al. (2022), and a hierarchical coordinated control strategy is also developed based on MPC to suppress high fluctuations in electrolysis current caused by uncertainty from PV and WT. In summary, the optimal scheduling strategy based on MPC intraday strategy can effectively deal with the uncertainty of renewable energy. However, the aforementioned literature is more inclined toward constructing the intraday rolling strategy, and there are few descriptions of the MPC feedback module, which is an essential means to deal with the uncertainty of renewable energy. With the increasing penetration of renewable energy, the effectiveness and the advantage of the strategy will be reduced.

An online optimal operation approach for CCHP microgrids based on MPC with feedback correction to compensate for prediction error was proposed in Gu et al. (2017a). Moreover, as a flexible framework based on the combination of multiple modules with different time scales, MPC provides the feasibility of its combination with a variety of traditional optimization strategies (Cai et al., 2020). An optimal scheduling model considering the demand responses is proposed in Zhang et al. (2021) in which a multi-time scale economic scheduling method based on day-ahead robust optimization and intraday MPC is designed. A battery/flywheel hybrid ESS stochastic model predictive control (SMPC) method is proposed in He et al. (2022) to improve the automatic generation control performance of thermal power units in which a scenario tree generation approach is proposed to simulate operation scenario. In Wu et al. (2021), the results of multiple uncertainty samplings are used to simulate the future characteristics of aggregated electric vehicles, and a two-layer strategy framework is proposed for the optimization issue. These studies provide some methods for further combating the uncertainty of renewable energy, but the analysis and processing of uncertain data are focused on the day ahead or before the optimization. Therefore, it results in the online optimization stage of MPC still aiming at the pursuit of economy alone, which has the lack of flexibility to deal with real-time changing operating scenarios.

Therefore, in order to better cope with the impact of uncertainty from high penetration of renewable energy and load demand and further flexibly balance the robustness and economy of the microgrid online dispatch plan, a dispatch strategy for the photovoltaic microgrid in an industrial park is designed based on low-carbon robust model predictive control (RMPC) in this study. First, the dynamic model and cost function of operation is built and the two-stage RO method is used to find the low-carbon scheduling scheme under the worst scenario



considering uncertainty, where the introduction of the carbon index cost target makes the environmental protection and economy of the microgrid are further comprehensively considered. Second, the feedback mechanism based on MPC is designed to respond to the fluctuation of PV in an ultra-short term time scale, which effectively combats the uncertainty of renewable energy. Finally, the MPC strategy framework is used to form the intraday scheduling plan of the microgrid, which can balance the robustness and economy of the microgrid by combining the RO and MPC strategy. Moreover, the feasibility and effectiveness of the proposed RMPC strategy are verified by simulation experiments.

2 DYNAMIC MODEL OF THE PHOTOVOLTAIC INDUSTRIAL PARK MICROGRID

2.1 Typical Photovoltaic Microgrid Structure

Figure 1 shows a typical structure of the microgrid in a photovoltaic industrial park. The park is connected to the main grid through the point of common coupling (PCC); thus, stable electricity power can be purchased from the main grid to meet the large load demand. A large number of distributed PV generation units are built to obtain the renewable energy, and surplus or lack of electrical energy can be stored or released in an energy storage system (ESS). As an important auxiliary power device, ESS can handle excess renewable energy in time, which simultaneously takes into account both economy and stability of the system. Moreover, the dispatch plan and control operation of the microgrid will be formulated and sent by the control center. It should be noted that despite the existence of different devices to obtain power, renewable energy like PV is hopefully used in priority by operators meeting the load considering the electricity price and low-carbon objective.

2.2 Deterministic Dynamic Model

The deterministic power generation unit in the microgrid can provide stable and high-quality electricity power, such as generator, ESS, and the power from the main grid. The dynamic model of the devices based on the proposed background is as follows:

$$\boldsymbol{P}_{m}(t+1) = \boldsymbol{P}_{m}(t) + \Delta \boldsymbol{P}_{m}(t), \qquad (1)$$

$$E(t+1) = \begin{cases} E(t) + \eta_{ch} P_{ch}(t) \Delta t & \text{if } P_s(t) \ge 0 \\ E(t) - \frac{1}{\eta_{dis}} P_{dis}(t) \Delta t & \text{if } P_s(t) < 0 \end{cases}, \quad (2)$$

Eq. 1 represents the power transaction between the microgrid and the main grid in which the value of the traded power at t + 1is the sum of the traded power and the hope adjusted power at t; P_m and $\Delta P_m(t)$ are the purchase of power from main grid and the power should be adjusted in the next time, respectively; and tis the sampling time. Eq. 2 is the ESS model in which the remaining energy in the ESS at t + 1 is the remaining energy stored at t plus the amount of charged/discharged in this period; E represents the remaining energy of the ESS; P_{ch} and P_{dis} indicate charging and discharging power, respectively, where both cannot be present at the same time; η_{ch} and η_{dis} is the efficient factor of the charging and discharging in ESS, respectively; and Δt is the length of operation control interval.

In order to reduce integer variables during optimization, an intermediate variable δ and an auxiliary variable Z_s is used to unify the two variables of P_{ch} and P_{dis} into P_s (Parisio et al., 2014):

$$\boldsymbol{\delta} = 1 \leftrightarrow \boldsymbol{P}_{\boldsymbol{s}} \ge 0, \tag{3}$$

$$Z_{S} = \delta P_{s}, \qquad (4)$$

where P_s is the power output from the ESS. Eq. 3 means that the sufficient and necessary condition between $\delta = 1$ and $P_s \ge 0$, and the Big M method is used to guarantee the establishment of Eq. 4, in which the logical constraint will be shown later. Therefore, Eq. 2 will be transformed into Eq. 5 as follows:

$$E(t+1) = E(t) + \left[\left(\eta_{ch} - \frac{1}{\eta_{dis}} \right) Z_s(t) + \left(\frac{1}{\eta_{dis}} \right) P_s(t) \right] \Delta t. \quad (5)$$

Moreover, the operating constraints are as follows:

$$\begin{cases} P_m^{min} \le P_m \left(t+1\right) \le P_m^{max} \\ E_{min} \le E\left(t+1\right) \le E_{max} \end{cases}, \tag{6}$$

$$\begin{cases} B_{1}\delta(t) + B_{2}Z_{s}(t) \leq B_{3}P_{s}(t) + B_{4}, \\ B_{1} = \begin{bmatrix} P_{s}^{max} & -(P_{s}^{max} + \varepsilon) & P_{s}^{max} & P_{s}^{max} & -P_{s}^{max} & \end{bmatrix}, \\ B_{1} = \begin{bmatrix} 0 & 0 & 1 & -1 & 1 & -1 \\ B_{3} = B_{2}, \\ B_{4} = \begin{bmatrix} P_{s}^{max} & -\varepsilon P_{s}^{max} & P_{s}^{max} & 0 & 0 \end{bmatrix}, \end{cases}$$

(7)

$$P_s(t) = P_m(t) + V(t) - D(t), \qquad (8)$$

Eq. 6 is the limit constraints representing the PCC tie-line power limitation and the energy storage constraint, respectively. In order to ensure that the microgrid system can switch to the island operation mode at any time, P_m^{min} and P_m^{max} are used to limit the minimum and maximum power purchased from the main grid to reduce the energy dependence on the main grid and reduce certain construction costs. E_{min} and E_{max} are the upper and lower boundaries of the safety of ESS. Eq. 7 represents the logical constraints after the unification of the variables in Eq. 5 (Parisio et al., 2014). P_s^{max} is the maximum output power of the ESS and ε is a teeny error. Eq. 8 is the power balance constraint of the microgrid system, where V is the output of the PV and D is the load.

2.3 Uncertainty Dynamic Model

Uncertain equipment in the microgrid refers to the renewable energy generation units and loads with volatility and uncertainty. In this study, the high penetration of the PV is the main reason to cause a great challenge to the safe and stable operation of the microgrid, where the dispatching scheme did not match the actual power output. The uncertainty model is described as follows:

$$\boldsymbol{u} = \begin{cases} \boldsymbol{V}(t) = \left[\bar{\boldsymbol{V}}(t) - \Delta \boldsymbol{V}(t), \bar{\boldsymbol{V}}(t) + \Delta \boldsymbol{V}(t) \right], \\ \boldsymbol{D}(t) = \left[\bar{\boldsymbol{D}}(t) - \Delta \boldsymbol{D}(t), \bar{\boldsymbol{D}}(t) + \Delta \boldsymbol{D}(t) \right], \end{cases}$$
(9)

$$\boldsymbol{e} = \begin{cases} \Delta V(t) = \boldsymbol{\eta}_V V(t) \\ \Delta D(t) = \boldsymbol{\eta}_D D(t), \end{cases}$$
(10)

Equation 9 represents the uncertainty model of the PV and load. \bar{V} and \bar{D} are the day-ahead forecast value, respectively. ΔV and ΔD are the uncertainty range. Eq. 10 is the calculation method of the uncertainty range, where η_V and η_D are the error coefficient. Thus, the uncertainty set of the microgrid is described as follows:

$$U = \begin{cases} u \\ e \\ \sum_{t=1}^{O} \frac{|V(t) - V(t)|}{\Delta V(t)} \leq \Gamma_{V}, \qquad (11) \\ \sum_{t=1}^{O} \frac{|D(t) - D(t)|}{\Delta D(t)} \leq \Gamma_{D}, \end{cases}$$

where Γ_{V} and Γ_{D} are the uncertainty degree of the PV and load, respectively. **O** is the length of the operation layer.

3 LOW-CARBON ROBUST PREDICTIVE DISPATCH STRATEGY

3.1 Low-Carbon Optimization Layer

As mentioned in the introduction, the MPC strategy incorporates the idea of rolling optimization, which can be more flexibly integrated with other algorithms reasonably. Therefore, the original optimal economic problem in MPC is transformed into a "min-max-min" robust optimization problem to obtain the robust scheduling plan under the worst scenario.

$$J = \min_{x} J_{CO2} + \max_{U} \min_{x,U} f^T y, \qquad (12)$$

$$\begin{cases} J_{CO2} = K_{CO2} (W_{CO2} - W_{ep}), \\ W_{CO2} = \sum_{t=1}^{O} \alpha + \beta P_m + \gamma P_m^2, \\ W_{ep} = \sum_{t=1}^{O} \eta_{CO2} (P_m + V), \end{cases}$$
(13)

$$\begin{cases} f = \begin{bmatrix} K_{ch} + K_{dis} & -K_{dis} & K_m & \mathbf{0} & \mathbf{0} \end{bmatrix}^T, \\ y = \begin{bmatrix} Z_S & P_s & P_m & E & \Delta P_m \end{bmatrix}^T, \end{cases}$$
(14)

$$\begin{cases} K_{ch} = a\left(\frac{E(k)}{C_s}\right) + c \\ K_{dis} = -a\left(\frac{E(k)}{C_s}\right) + b, \end{cases}$$
(15)

Equation 12 represents the objective function of the microgrid in the optimization layer; f is the set of cost coefficients for each power generation unit; y is the set of scheduling plan; and x is the set of control variables in the optimize schedule. **Eq. 12** indicates that the scheduling objective is to optimize the comprehensive cost of carbon emissions and microgrid operation. The cost of carbon emission based on carbon index J_{CO2} is shown in **Eq. 13**.

Under the robust uncertainty model in **Eq. 11**, the primary goal of operation in microgrid remains economic while meeting both the supply and demand balance and a certain degree of robustness, and the microgrid operation cost is shown in **Eq. 14**, **Eq. 15**.

To be specific, **Eq. 13** indicates the carbon emission cost. In the industrial park, the microgrid needs to undertake the purchase of carbon emission quotas mainly based on CO₂. In **Eq. 13**, K_{CO2} represents the unit price of carbon trading; W_{CO2} is the carbon consumption of the microgrid, and its calculation method is shown in the literature (Saber and Venayagamoorthy, 2011); W_{ep} represents the carbon emission quota of the microgrid, and η_{CO2} represents the free carbon emission quota coefficient (Zhou et al., 2021). **Eq. 11** represents the cost coefficients and dispatch variables of the operating cost, where K_{ch} and K_{dis} are the charging/discharging cost coefficient of the ESS, respectively. K_m is the price of power in the main grid.

To mobilize the enthusiasm of all power generation units and prevent the damage to the battery caused by the excessive or low energy storage, the relationship between the charging/discharging cost coefficient and the remaining energy of the ESS is shown in **Eq. 15.** C_s is the capacity of ESS. a, b, and c are all constant coefficients.



From the aforementioned equations, after converting Eqs 1-15 into the standard form of robust optimization, Eq. 12 can be solved by a two-stage robust optimization problem based on the column constraint generation (C&CG) algorithm. The main problem is described as follows:

$$\begin{cases} \min_{x} J_{MP} \\ s.t. \quad J_{MP} \ge f^{T} \cdot y \\ Gy \le j - Hx \\ Iy \le g \\ Ly = h \\ My = u^{*}. \end{cases}$$
(16)

The constraints from **Eqs 6–8** can be written as the standard constraint expression in **Eq. 16**.

On the other hand, the strong duality theory is used to linearize the constraints in the subproblem, which the hard-to-solve "max-min" optimization problem in the subproblem is transformed into a "max" problem. This transformed Lagrange dual problem is shown in **Eq. 17**:

$$\begin{cases} F_{sp} = \max_{U} \left\{ -\lambda^{T} \left(j - Hx \right) - \mu^{T} g + \sigma^{T} h + \left(\gamma^{T} + \delta^{T} \right) u \right\} \\ \left\{ f^{T} + \lambda^{T} G + \mu^{T} I - \sigma^{T} L - \left(\gamma^{T} + \delta^{T} \right) M \right\} = 0 \\ \lambda \ge 0, \mu \ge 0. \end{cases}$$
(17)

Finally, the optimization problem iterates between the two subproblems until the optimal scheduling plan is found even in the worst scenario which is still feasible. The whole process is shown in **Figure 2**.



3.2 Robust Model Predictive Control Rolling Layer

The intraday scheduling strategy based on rolling optimization rolls forward with time in a day. The RMPC framework based on time flow is shown in **Figure 3**.

In **Figure 3**, the RMPC framework is divided into three stages. First, the time horizon for the optimization layer is from t to t + O, which is utilized to obtain the optimal scheduling plan for this period by the method we have described. However, the operator only sends the control signal from t to t + C to the system, which C represents the length of the control layer. During the time period of the control layer, the modules of the feedback layer will be continuously looped in a smaller time horizon until reaching the next sampling point t + C. After that, the sampling point t + C becomes to t, and the previous optimization process is repeated. Therefore, a real-time rolling optimization strategy based on RMPC is formed.

3.3 Low-Carbon Robust Model Predictive Control Feedback Layer

In the optimization layer, the robust optimization ensures the feasibility of the schedule plan in the worst scenario, but the problem solved without predicted data has a certain probability that it may not match the real operation conditions of the microgrid. Therefore, in a shorter time scale, the feedback mechanism of MPC is used to form a closed-loop control system that can timely forecast the predictive deviation of the uncertain information and make a response. The feedback mechanism is divided into two stages: the prediction correction and the output correction.

In the prediction correction module, the actual output value in the past is collected for feedback, and then the prediction output in an ultra-short term will be corrected. In other words, when the latest actual output is obtained at a certain feedback sampling point, the prediction module in the feedback layer will update the predicted variation of the renewable energy output at the next feedback point. At the same time, the prediction model is also revised to obtain more accurate planning in the next optimization stage. Such prediction model is generally obtained by the gray model or neural network. This study selects the wavelet



decomposition convolutional neural networks (WDCNN) to form the prediction model which is widely used in prediction research (Li et al., 2021b; Yan et al., 2021).

The corrected prediction output will be sent to the output correction module. Under the ultra-short time scale, the overloaded tie lines may suffer excess uncertainty fluctuations if there is no protective action in the schedule plan, and it will pose a great threat to the safe operation of the microgrid. Therefore, the redistribution principle in the output correction module is designed, which is more inclined to the safe operation than the pursuit of economy. Therefore, the minimum pressure of the remaining power generation capacity of each equipment is regard as the goal shown in **Eq. 18**, (Zhao et al., 2021). The dispatch plan will be adjusted in the ultra-short time scale based on the predicted values.

$$\Delta = \frac{\left|\Delta P_{m}^{'}\right|}{\left(P_{m}^{max} - P_{m}\left(t\right)\right)} + \frac{\left|\Delta P_{s}^{'}\right|}{\left(P_{s}^{max} - \left|P_{s}\left(t\right)\right|\right)}.$$
(18)

In Eq. 18, Δ is the predictive deviation of the corrected prediction value and the previous forecast value; $\Delta P'_m$ and $\Delta P'_s$ are the adjusted values allocated to the PCC and ESS, respectively, which both are still required to satisfy the constraints of Eqs 1–8. Finally, the updated schedule plan will be implemented when the next feedback point t + F arrives, and the feedback layer will be carried out in a loop until the sampling point of the next optimization layer t + C is reached.

4 SIMULATION RESULTS

This study takes a typical industrial park photovoltaic microgrid as an example, and the microgrid will be operated within a day through the RMPC strategy proposed. **Figure 4** shows the forecast curves of PV and load for a typical day with a time interval of 30 min. In the simulation environment with MATLAB 2019a, we set the rolling layer $\mathbf{R} = 48$, the optimization layer $\mathbf{O} =$ 8, the control layer $\mathbf{C} = 1$, and the feedback layer $\mathbf{F} = 3$. It means

TABLE 1 O	eration parameters
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Parameters	Values	Parameters	Values
P ^{max}	4 MW	P_s^{max}	5 MW
E _{max}	0.9 p.u.	E _{max}	0.1 p.u.
$\eta_{ch} \eta_{dis}$	0.9	а	1.5
b	0.85	b	-0.05
η_{co2}	0.648	α	10.33 t/h
β	–0.24444 t/MWh	y	0.00312 t/MW ² h
η_{co2}	140 RMB/t	·	



FIGURE 5 | Typical peak-valley electricity price for industrial park.



the sampling interval of the system is 30 min, the sampling interval of the feedback layer is 10 min, and the optimization time scale is 4 h. The park is equipped with PV and battery energy storage systems (BESS), with the capacity of 8 MW and 20 MWh, respectively. **Table 1** shows the operating and optimization parameters of the microgrid. **Figure 5** shows a typical

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peak-valley electricity price changing curve for the industrial park in 1 day.

4.1 Feasibility Analysis of Robust Model Predictive Control Strategy

Figure 6 shows the scheduling scheme of the photovoltaic microgrid in the industrial park using the proposed RMPC strategy. The uncertainty coefficients of photovoltaic and load in Eq. 11 are both four, which is the moderate value of robust expectation. The allowable ranges of prediction error in Eq. 10 are both 5%. The operation goal of the microgrid in industrial parks is to achieve internal supply and demand balance and can maintain stable operation even if the forecast data has errors. That is the significance of introducing a robust optimization mechanism.

As shown in **Figure 4**, although the power output from PV has a strong arch-shaped output law in a day, the shortcomings of this are also obvious. With the lack of sunlight, the PV has little output in the morning and evening. It makes the microgrid to purchase a large amount of power from the main grid and use the BESS as an auxiliary power output device to meet the large load demand.

For example, as shown in **Figure 6**, from 0:00 a.m. to 6:00 a.m., there is no energy output from PV. Therefore, the load is nearly satisfied by the power purchased from the main grid considering the economy because of the lowest electricity price in the whole day, and the BESS is scheduled to contribute energy as little as possible. After that, the PV starts to generate electric power, and the electrical price of the main grid reaches the parity zone. Therefore, the power balance will be met by the BESS from 8:00 a.m. to 10:00 a.m. From 10:00 a.m. to 3:00 p.m., the PV reaches its peak period, which could promptly replenish the BESS by the surplus energy. It makes it possible to avoid the expensive period of electricity price in the afternoon while satisfying the self-sufficiency expectation of renewable energy in the industrial



park. The proposed strategy efficiently improves the economy of the photovoltaic microgrid in industrial parks.

Figure 7 shows the changing curves of the carbon index and carbon consumption in the microgrid. Due to the added carbon index in the optimization goal, the power purchased from the main grid is more restrained. Thus, the microgrid is encouraged to consider larger-scale renewable energy sources in the projecting stage to increase their advantage in the future carbon index trading market. And the application of the carbon index could also meet the environmental protection targets and low-carbon operating goals reasonably for the photovoltaic microgrid in the industrial park. Furthermore, **Figure 8** shows the change of the energy storage in the BESS. Except for periods when renewable energy is extremely abundant, the power storage in ESS can always maintain a healthy value for system operation, even it has fluctuation.

4.2 Effectiveness Analysis for Strategy Considering Uncertainty

As mentioned in **Section 3.3**, while the robust dispatch scheme satisfies the basic requirements of the economic operation, the feedback mechanism in MPC is proposed to avoid the damage to the stable operation of the microgrid caused by the error of the prediction information.

The ability to fight the uncertainty of input information depends on the accuracy of the correction model. Therefore, the proposed rolling feedback mechanism based on historical and real-time data can make the error correction curve under the ultra-short time scale closer to the actual output situation. Secondly, in the proposed output correction module, due to the setting of the redistribution objective in **Eq. 18**, the output adjustment pressure of the equipment is fairly distributed to each controllable power generation beforehand. Thereby, it could improve the safety margin of the operation (Zhao et al., 2021).



The calculation results of the average relative error of the net load (Gu et al., 2017b) are shown in **Figure 9**. It can be seen from **Figure 9** that the error calculation result based on the MPC strategy is obviously better than the rolling optimization strategy which pursues the economy completely. This is because the introduction of the feedback mechanism makes the prediction curve closer to the actual one, and the relative prediction error naturally decreases. However, it can be also found from **Figure 9** that the relative error value increases slightly with the RMPC strategy compared with the MPC strategy. This is because the worst-case scenario predicted by robust optimization is not based on the actual data, but rather on the operating state of the devices. Therefore, it does not necessarily match the actual operation scenario, which may lead to more operation errors.

Figure 10 shows the average relative error of the load under the uncertainty model compared with the day-ahead forecast value of load which $\Gamma_D = 0$. It can be seen that with the increase of the uncertainty degree, the average relative error of the load will also increase. This is because in the optimization layer, the original day-ahead forecast is forced to take into account the worst scenario due to the uncertainty set. The larger the uncertainty, means the more points are forced to deviate, and the larger result of the average relative error of the load. However, the variable weather information and flexible load are more difficult to predict in the actual operation. Therefore, for operators who need to face diverse uncertain factors, the cost of small increase error is acceptable to ensure normal operation of the microgrid. And as we described, the uncertainty degree can be adjusted timely by the operator because of the combination of MPC and RO, which can also have a better decision on the acceptance degree of this increased error.

If it is assumed that these points that are forced to deviate are called robust point, the case with the most robust points (Γ_D , Γ_V =



8) is shown in Figure 11. Due to the constraints of the load in the power balance, the power generation units in the microgrid need to supply sufficient energy to the load. Therefore, the robust point of load in the whole day is basically to increase the positive deviation as the deterioration of the operating scenario. As an important low-cost power generation unit and an important means of providing carbon indicators, photovoltaics are basically negative deviations in the worst scenario. However, at the peak of power generation, that is, at noon, a large amount of surplus power generation will challenge the storage capacity and capacity of energy storage. At this time, it is believed that larger power generation will pose a greater threat to the operation of the microgrid. In addition, the deviations of both robust points of PV and load are close to the maximum error allowable range bounded. Therefore, increasing the error coefficient is also an important means to increase the robustness of the scheduling plan.

Figure 12 shows the worst scenario for day-ahead RO and rolling RO with the same ratio of uncertainty degree. Taking Γ_D = 2 in the RMPC strategy as an example, since the length of the optimization layer is 8, the uncertainty ratio is 0.25. That means that in the optimization layer with the length of 48 in day-ahead RO, the uncertainty degree Γ_D is 12. As shown in **Figure 12B**, when the Γ_D = 12, the number of the robust point used in day-ahead RO are also 12, which most of them are used in the morning. But as shown in Figure 12A although the uncertainty ratio is the same, the number of robust points used in rolling RO is far more than day-ahead RO. That because in each rolling process, two of the sampling points in the optimization layer are always forced to be as robust points. Moreover, the robust points are gathering at the moment when the load is large in noon, which is closer to the worst case of the load for the damage operation analyzed above. Therefore, compared with the day-ahead RO, the rolling RO method used in this study will make more robust dispatch schedule in a short time of optimization layer and also has the ability to adjust flexibly in time.





4.3 Economic Analysis

Since the intraday scheduling scheme is a real-time optimization strategy that rolls with the time flow, the uncertainty degree of the system can be flexibly adjusted. Compared with the day-ahead robust optimization strategy, the worst scheduling scenario is just for the short-term period, which has greater operability and accuracy. At the same time, RO and MPC strategies can respond to the uncertainty of renewable energy at different time scales, respectively. But this ability has to pay the cost of certain economic losses, as shown in **Figure 13**, which is the comparison of the cost with different strategy and uncertainty degree. Compared with the RMPC strategy, the MPC strategy



pursues cost minimization in the short-term scheduling stage, so that the total cost can be kept lower.

And it can be seen from **Figure 13** that with the increase of uncertainty degree, the economy gradually decreases. From the change of Γ_D , $\Gamma_V = 0$ (MPC strategy) to Γ_D , $\Gamma_V = 8$, it can be found that different degrees of worst scenario have diverse degrees of influence on the operation of the microgrid, which provides an important guide for operator to select the exact uncertainty degree in real-time dispatch.

These also confirm what we discussed in the previous section, robustness and economy of the operation of the microgrid are two opposite directions that operators cannot get both at the same time. The prevention of the worst-case scenario in exchange for part of economic losses can make the microgrid with a high proportion of renewable energy access more reliable.

Moreover, if the operator wants to eliminate the impact of robust optimization on economy, they can consider increasing the benefits of microgrid operations in other aspects, such as power transactions, cooperation with other microgrids, electricity price games between operators and users, etc. In short, how to balance risks and benefits depends on the operator's thoughts and their operation goals for microgrids in the region. The proposed RMPC strategy can flexibly balance the robustness and economy of PV microgrid operation in industrial parks, which gives operators more options to achieve their desired microgrid management target.

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5 CONCLUSION

This study proposes a low-carbon robust predictive dispatch strategy for a photovoltaic microgrid in industrial parks, which combines the advantages of robust optimization strategy and MPC strategy. Based on establishing the dynamic model of power generation equipment and the uncertainty model of renewable energy and load, an energy management strategy based on RMPC is designed for the photovoltaic microgrid. The proposed strategy ensures the independent and stable operation of the microgrid and has the ability to combat the uncertainty through two-stage robust optimization method and an MPC feedback mechanism at different time scales. These two methods cooperate with each other and improve both robustness and the safe operation of the microgrid at the expense of part of the economy. At the same time, due to the characteristics of the real-time strategy, the uncertainty degree is adjustable, which allows operators to balance robustness and economy more flexibly. In addition, the introduction of the carbon index mechanism effectively increases the inhibition of the use of polluting energy. Thus, the operators have to consider the environmental cost while pursuing the operation economy so as to achieve the goal of low carbon emissions. Finally, simulations using real data are carried out to verify the effectiveness of the proposed strategy. By comparing with other strategies, the characteristics of the proposed strategy are analyzed, which provides an important reference for the application and further development of this strategy.

DATA AVAILABILITY STATEMENT

The original contributions presented in the study are included in the article/Supplementary Material, further inquiries can be directed to the corresponding author.

AUTHOR CONTRIBUTIONS

Conceptualization and methodology: ZZ; software: JG and SG; modeling: JG, and JX; formal analysis: JG and XL; validation: JG, JW and QY; writing—original draft preparation: JG and ZZ; writing review and editing: ZZ and LL; supervision: ZZ; and project administration: ZZ.

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