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Improved unscented Kalman filter based interval dynamic state estimation of active distribution network considering uncertainty of photovoltaic and load

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State estimation of active distribution network (ADN) plays an important role in distribution energy management system. The increase penetration of distributed generations, especially the distributed photovoltaic (PV), in ADN leads to high uncertainty of ADN's operation and the state of the ADN varies with the variation of the PV output power. For the uncertainty of PV power output, an interval dynamic state estimation (IDSE) method, which estimates the interval of ADN state variables is proposed in this paper. Firstly, considering the slow computation speed of the Unscented Kalman Filter (UKF), the square root UKF is used to predict the real-time operating level of the state variables. Secondly, since the power output of PV has features of the variation randomly, the neural network-based prediction intervals is employed to predict the power output interval of PV. Finally, the normal fluctuation range of ADN state is modelled as a bilevel non-linear programming problem to perform IDSE, which in turn monitors the operating state of ADN. The proposed method is evaluated on the IEEE 33-node and IEEE 123-node systems, respectively. The test results demonstrate that the dynamic status of the ADN can be tracked accurately using the proposed method.

KEYWORDS

interval dynamic state estimation, unscented Kalman filter, active distribution network, uncertainty, prediction interval

1 Introduction

State estimation (SE) is the basis for operation and control of active distribution network (ADN), providing a reliable foundation for advanced applications such as voltage control, security assessment, reactive power optimization, etc. The weighted least squares (WLS) method is the most used algorithm for traditional static state estimation (SSE). However, the large number of distributed generators (DG) such as photovoltaics (PV) connected to ADN highlights the non-linearity problem in ADN. Traditional SSE cannot satisfy real-time requirements, especially in capturing dynamic characteristics, the

dynamic state estimation (DSE) needs to be studied to support the efficient operation of ADN (Zhao et al., 2019).

The DSE could not only estimate the current state but also predict the state of the near future (Zhao et al., 2021), which is benefit for the timely problem detection and control of ADN, such as voltage exceeding limits. The traditional DSE method mainly includes Kalman Filter (KF) (Julier and Uhlmann, 2004, 2004; Valverde and Terzija, 2011; Karimipour and Dinavahi, 2015; Massignan et al., 2020). The Kalman-based DSE method, such as Extended Kalman Filter (EKF), is implemented on the assumption that the noise follows Gaussian distribution (Massignan et al., 2020). Unscented Kalman Filter (UKF) achieves higher accuracy than EKF due to unscented transformation, it propagates the mean and covariance through unscented transformation while capturing their nature to third order [6]. However, the accuracy of the UKF is dependent on the selection of initial values and the algorithm is too time consuming (Zhao et al., 2017), so it needs further improvement. Meanwhile, the large-scale grid integration of PV to ADN makes the results of SE need to consider more uncertainty factors, and how to consider the impact of uncertainty on SE is an urgent problem (Sihag and Tاجر, 2018).

In general, the main methods of modelling uncertainty variables in ADN are probabilistic models (Valverde et al., 2013; Aien et al., 2014), fuzzy number models (Al-Othman, 2009) and interval number models (Rakpenthai et al., 2012). In (Valverde et al., 2013), the Gaussian mixture models are used to obtain the probability density function of DG and load, the result of Gaussian mixture models is introduced as input variables in state estimation of ADN. In (Aien et al., 2014), an analytical probabilistic-possibilistic tool based on the evidence theory and joint propagation of possibilistic and probabilistic uncertainties is proposed for the power flow uncertainty assessment. In (Al-Othman, 2009), the affiliation functions for loads and different DG outputs are established based on plausibility measures, and linear SE is performed by means of fuzzy analysis methods. The above methods can achieve good results, but the DSE methods based on probabilistic models and fuzzy number models need to obtain *a priori* probability density functions of uncertain variables in advance, which leads to an increase in the complexity of algorithm. In addition, the probability distribution of conventional electrical loads can be obtained from historical data in a real ADN, while the complete probability density function of PV power output is difficult to obtain. In most cases, only the upper and lower boundaries of its PV power fluctuations are known (Quan et al., 2014).

In contrast, the use of interval number model to describe uncertainty problems in SE is of greater application. Interval number model does not need to obtain specific distributions of variables, it only focuses on information about the upper and lower bounds of each uncertain variable (Khosravi et al., 2011).

At present, interval state estimator (ISE) has been initially investigated in ADN. In (Al-Othman and Irving, 2005), an optimization model is proposed for the interval SE that the measurement function is linearized as constrained formulations to estimate the upper and lower bounds on the states. In (Wang et al., 2018), an optimal solution method for interval SE is proposed to detect abnormal measurements. In (Huang et al., 2019), an optimization model of interval SE is combined with bad data identification to enhance the robustness of interval SE. In (Ngo and Wu, 2021), nonlinear measurement equation is transformed into dual inequality linear equations by mean value theorem to ensure the reliability of estimated intervals. However, the current ISE methods focus on interval static SE and there is little research on interval dynamic state estimator (IDSE).

In addition to the influence of uncertainty factors, the lack of real-time measurements limits the effective application of SE. Establishing accurate pseudo-measurement models can improve data redundancy and make the SE results of ADN more accurate (Schlösser et al., 2014). The data-driven method can mine the features of high-dimensional complex data and is highly superior in improving the accuracy of pseudo-measurement models (Massaoudi et al., 2021). In (Manitsas et al., 2012; Abdel-Majeed et al., 2014), the artificial neural networks are used for pseudo-measurement modelling, but to determine the model weights, the error distribution needs to be obtained in advance. In (Zhang et al., 2019), a deep recurrent neural network based pseudo-measurement postulating module is used to learn complex nonlinear functions to improve the accuracy of measurements. However, the modelling of pseudo-measurements is also subject to uncertainty factors that leads to reduced accuracy. Inspired by (Khosravi et al., 2011; Quan et al., 2014), pseudo-measurements can be modelled using interval models.

To deal with the uncertainty factors and lack of real-time measurements in ADN, an IDSE method is proposed for ADN integrated with PVs in this paper.

- (1) In order to increase the calculation speed of the UKF without reducing accuracy, the square root of the covariance matrix is used instead of the covariance matrix in UKF and the improved UKF is used to determine the operating median values of all state variables.
- (2) Neural network based prediction interval method is used to model the uncertainty of both pseudo-measurement of node injected power and real-time measurement in the system.
- (3) The normal fluctuation range of ADN state is modelled as a bilevel non-linear programming problem to obtain the upper and lower bounds.

The simulations are carried out on IEEE 33-node and IEEE 123-node systems to evaluate the effectiveness of the proposed DSE method.

2 Dynamic state estimation based on square root unscented Kalman filter

2.1 Dynamic state estimation model

The state and measurement model of the nonlinear ADN can be written as follows (Zhao, 2018):

$$\begin{cases} x_k = f(x_{k-1}) + q_{k-1} \\ z_k = h(x_k) + r_k, \end{cases} \quad (1)$$

$$\begin{cases} q \sim N(0, Q) \\ r \sim N(0, R), \end{cases} \quad (2)$$

where, x_k is the n-dimensional state vector, state variables are chosen as the voltage magnitude and phase angle for each bus, $x_k = [v_1^k, v_2^k, \dots, v_n^k, \phi_1^k, \phi_2^k, \dots, \phi_n^k]$; z_k is the m-dimensional measurement vector, measurement variables are chosen as active and reactive power injections for each bus, $z_k = [P_1^k, P_2^k, \dots, P_n^k, Q_1^k, Q_2^k, \dots, Q_n^k]$; $f(\cdot)$ is the state transition function at $k-1$ time interval; $h(\cdot)$ is the measurement function; q_k is the system error; r_k is the measurement error, which is usually assumed to be uncorrelated Gaussian noise as Eq. 2; Q and R are system noise variance and measurement noise variance, respectively.

2.2 Square root unscented Kalman filter

2.2.1 Unscented Kalman filter

UKF is based on the basic steps of the Kalman filter, introducing the unscented transform as a sampling method to approximate the nonlinearity. The basic principle of UKF is to construct the Sigma point set with variance as the variance of the state variable around the mean point of the state variable, then perform a nonlinear transformation on each point in this point set, and finally weight the sum to obtain the state variable and variance after the nonlinear transformation, this method can achieve at least second order accuracy.

Unscented transform process: x is a random variable with mean \bar{x} and covariance P_x . Construct a Sigma point set $\{\chi_i\}$ that satisfies:

$$\bar{x} = \sum_{i=1}^L W_i^m \chi_i, \quad (3)$$

$$P_x = \sum_{i=1}^L W_i^c (\chi_i - \bar{x})(\chi_i - \bar{x})^T. \quad (4)$$

Perform a nonlinear transformation $y = f(x)$ on all Sigma points to obtain the transformed point set $\{\xi_i\}$. Once UKF has determined the sampling strategy, it also determines the number of sampling points L and weights W^m and W^c for mean and variance.

UKF consists of two main steps: time update and measurement update.

Step 1: time update

x_k is state variable at time k , P_k is the covariance of state variable at time k , the Sigma point set $\{\chi_k^i\}$ can be used to predict the state variable and variance in one step:

$$\chi_{k+1|k}^i = f(\chi_k^i) + q_k, \quad (5)$$

$$x_{k+1} = \sum_{i=1}^L W_i^m \chi_{k+1|k}^i \quad (6)$$

$$P_{k+1} = \sum_{i=1}^L W_i^c (\chi_{k+1|k}^i - x_{k+1})(\chi_{k+1|k}^i - x_{k+1})^T + Q_k, \quad (7)$$

$$y_{k+1}^i = h(\chi_{k+1|k}^i) + r_k, \quad (8)$$

$$y_{k+1} = \sum_{i=1}^L W_i^m y_{k+1}^i, \quad (9)$$

Step 2: measurement update

$$P_{y_{k+1}, y_{k+1}} = \sum_{i=1}^L W_i^c (y_{k+1}^i - y_{k+1})(y_{k+1}^i - y_{k+1})^T + R_{k+1}, \quad (10)$$

$$P_{x_{k+1}, y_{k+1}} = \sum_{i=1}^L W_i^c (\chi_{k+1|k}^i - x_{k+1})(y_{k+1}^i - y_{k+1})^T, \quad (11)$$

$$K_{k+1} = \frac{P_{x_{k+1}, y_{k+1}}}{P_{y_{k+1}, y_{k+1}}}, \quad (12)$$

$$\hat{x}_{k+1} = x_{k+1} + K_{k+1}(z_{k+1} - \bar{y}_{k+1}), \quad (13)$$

$$P_{k+1} = P_{k+1} - K_{k+1} P_{y_{k+1}, y_{k+1}} K_{k+1}^T. \quad (14)$$

The detailed steps and derivation process of UKF can be found in [6]. The traditional UKF algorithm needs to perform a non-linear transformation on each sampling point, which is a quite complex calculation and has obvious numerical errors. As a result, it will affect the non-negative characterization and symmetry of error covariance, which will affect convergence speed and stability. To improve the efficiency and accuracy of filtering algorithm, the square root of covariance matrix can be used instead of covariance matrix in traditional UKF algorithm during recursive operation process.

2.2.2 Steps of square root unscented Kalman filter

The basic idea of square root UKF (SR-UKF) is to perform a QR decomposition of state variance matrix P_k in the UKF process, so that it satisfies $P_k = A_k * A_k^T = \bar{R}_k^T * \bar{R}_k$, where \bar{R}_k is the upper triangular part of R in $A^T = QR$. The UKF filtering process is implemented by updating \bar{R}_k instead of P_k .

Thus, Eq. 7 in time update step is modified as follows:

$$S_{k+1}^- = qr \left\{ \left[\sqrt{W_1^c} (\chi_{k+1|k}^i - x_{k+1}), \sqrt{Q} \right] \right\}, \quad (15)$$

$$S_{k+1}^- = cholupdate \{ S_{k+1}^-, \chi_{k+1|k}^0 - x_{k+1}, W_0^c \}. \quad (16)$$

Eq. 10 in measurement update step is modified as follows:

$$S_{y_{k+1}, y_{k+1}} = qr \left\{ \left[\sqrt{W_1^c} (y_{k+1}^i - y_{k+1}), \sqrt{R} \right] \right\}, \quad (17)$$

$$S_{y_{k+1}, y_{k+1}} = cholupdate \{ S_{y_{k+1}, y_{k+1}}, y_{k+1}^i - y_{k+1}, W_0^c \}, \quad (18)$$

Eq. 12 and Eq. 14 are modified as follows respectively:

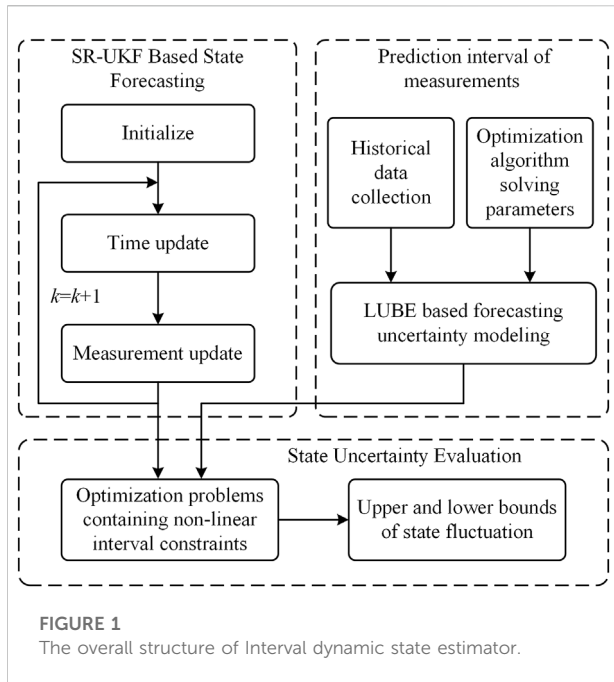


FIGURE 1
The overall structure of Interval dynamic state estimator.

$$K_{k+1} = \frac{(P_{x_{k+1}, y_{k+1}} / S_{y_{k+1}, y_{k+1}}^T)}{S_{y_{k+1}, y_{k+1}}}, \quad (19)$$

$$S_{k+1} = cholupdate\{S_{k+1}^-, K_{k+1} S_{y_{k+1}, y_{k+1}}, -1\}, \quad (20)$$

where, $qr(\cdot)$ is QR decomposition, $cholupdate(\cdot)$ is Cholesky first-order update (Jafarzadeh et al., 2011). \hat{x}_{k+1} represents the estimated optimal values for all state variables, including bus voltage magnitudes and phase angles. These values will be later used as inputs for IDSE in ADN.

3 Interval dynamic state estimator

In this section, a new generalized interval state estimator is proposed for ADN. It consists of three parts: SR-UKF, neural network (NN) and state uncertainty evaluation. SR-UKF is applied to obtain the operating states x^{k+1} of ADN (in Section 2). NN is mainly used for modeling the forecasting uncertainties of PV and load to obtain the upper and lower bounds of power. The purpose of state uncertainty evaluation is to quantify the upper and lower bounds of state fluctuation in ADN, the normal fluctuation range of ADN state is modelled as a bilevel non-linear programming problem to perform IDSE. The output parameters of the proposed state estimator are the normal fluctuation intervals for all state variables, The overall framework of IDSE is shown in Figure 1. The details of each part of the IDSE are given as follows.

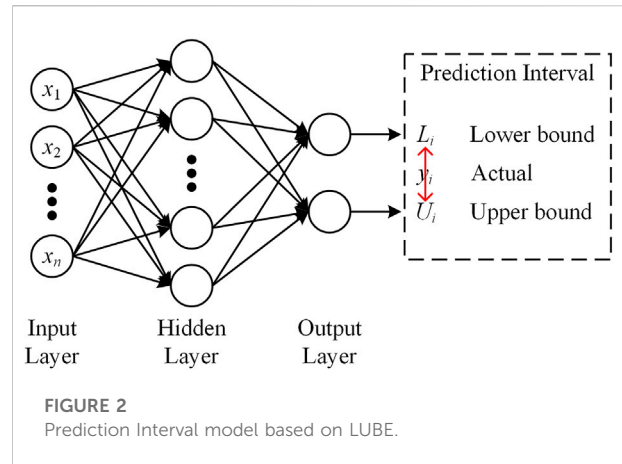


FIGURE 2
Prediction Interval model based on LUBE.

3.1 Prediction interval of measurements

Commonly used indicators for prediction interval assessment are prediction interval coverage probability (PICP), prediction interval normalized average width (PINAW) and prediction interval normalized root-mean-square width (PINRW):

$$PICP = \frac{1}{n} \sum_{i=1}^n \varepsilon_i, \quad (21)$$

where, n is the number of samples, $\varepsilon_i = 1$ if target value $y_i \in [L_i, U_i]$, otherwise $\varepsilon_i = 0$. L_i and U_i are the lower and upper bounds of the i -th prediction interval. PICP represents the probability that target value will fall within a prediction interval.

$$PINAW = \frac{1}{nR} \sum_{i=1}^n (U_i - L_i), \quad (22)$$

where, R is the range of the underlying target (maximum minus minimum), which ensures that PINAW is normalized to the interval $[0,1]$. Too wide interval leads to increased uncertainty in prediction results, reducing the predictability of the results for system scheduling. PINRW gives greater weight to wider intervals than PINAW, and practical results show that PINRW is more beneficial than PINAW for obtaining high quality intervals predictions [13].

$$PINRW = \frac{1}{R} \sqrt{\frac{1}{n} \sum_{i=1}^n (U_i - L_i)^2}. \quad (23)$$

The lower and upper boundary estimation (LUBE) theory [14] is based on a multi-layer perceptron neural network structure, which tunes the single node structure of the output layer of the back propagation neural network into a dual output node structure with lower and upper boundary values of prediction interval. Compared with traditional prediction interval schemes, LUBE avoids the limitations of data

distribution assumptions and complex calculations. The prediction interval model based on LUBE is shown in Figure 2, the number of layers and the number of nodes in each layer of neural network in LUBE can be adjusted according to actual situation.

For PV, the factors affecting the PV power output include solar radiation S , temperature T and humidity H . The inputs to the model at time i is:

$$X_i = [S_i \ T_i \ H_i]^T \tag{24}$$

The output after forward propagation is:

$$Y_i = [L_i \ U_i]^T = g(WX_i), \tag{25}$$

where, $g(\cdot)$ is activation function. As the output prediction interval of PV is related to several influencing factors, an optimization function needs to be constructed by comprehensively evaluating the interval coverage and interval width, thus transforming multi-objective optimization into single-objective optimization. The integrated evaluation function for prediction interval (loss function) selected in this paper is as follows:

$$J = \begin{cases} f = PINRW(1 + \gamma(PICP)e^{-\eta(PICP-\mu)}) \\ \gamma = \begin{cases} 0, & PICP \geq \mu \\ 1, & PICP < \mu \end{cases} \end{cases}, \tag{26}$$

where, μ is confidence level and can be set to $1 - \alpha$, η is the parameter for f and usually $\eta \in [50, 100]$. Unlike traditional back propagation (BP) neural networks which use BP to obtain network parameters, LUBE can not use BP due to the lack of targets (observations of lower and upper bound). Therefore, optimization algorithms such as particle swarm optimization (PSO) can be used to obtain the parameters of LUBE model. Load can also be modelled using LUBE method.

3.2 Operating state uncertainty evaluation

To better reflect the influence of system uncertainties on ADN state estimation results, all bus measurements in the IDSE model established in this paper are objectively quantified and described as interval numbers, resulting in the solved system state variables are also interval numbers, which can provide effective system state boundary information for dispatchers.

The interval number $[a]$ is defined as a non-empty real number set satisfying $[a] = \{a | \underline{a} \leq a \leq \bar{a}\}$ where \bar{a} and \underline{a} represent the upper and lower boundaries of the interval number $[a]$, specifically, when $\underline{a} = \bar{a}$, interval number degenerates to real number. Thus, the measurement vector z and state vector x can be expressed as:

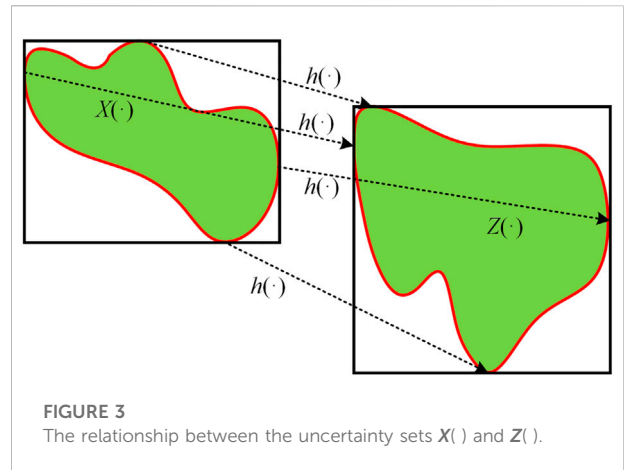


FIGURE 3 The relationship between the uncertainty sets $X(\cdot)$ and $Z(\cdot)$.

$$\begin{cases} [z] = \{[P_i], [Q_i], [P_{ik}], [Q_{ik}]\}^T \quad i, k = 1, 2, \dots, n, \\ [x] = \{[U_i], [\theta_i]\}^T \end{cases} \tag{28}$$

where, n is the number of buses, active power P and reactive power Q are measurements, voltage magnitude U and phase angle θ are the state variables.

IDSE is to determine the state variable information of ADN based on the upper and lower bound information of measurement vector and non-linear mapping equation $z = h(x)$, which can be expressed as:

$$X(M, \underline{z}, \bar{z}) := \{x \in R^n: h(x) \in Z(M, \underline{z}, \bar{z})\}, \tag{29}$$

where, $X(\cdot)$ is the uncertainty set of system state variables, M is the set of system measurement, $Z(\cdot)$ is the uncertainty set of system measurement vector:

$$Z(M, \underline{z}, \bar{z}) := \{\hat{z} \in R^m: \underline{z}_j \leq z_j \leq \bar{z}_j, j = 1, 2, 3, \dots, m\}, \tag{30}$$

where, \hat{z} is an actual measurement vector, m is the cardinality of the system measurements set M . As the measurement vector has more dimensions than the state variable, and there is a nonlinear mapping relationship $h(\cdot)$, the geometry of the state set $X(\cdot)$ is complex, as shown in Figure 3.

It is difficult to establish uniform analytical expressions and standard analytical methods (Wang et al., 2013). However, based on the theory of unknown-but-bounded error (UBBE), the original problem can be transformed into two optimization problems containing non-linear interval constraints, where the upper and lower bounds on the variables to be solved are obtained separately (Bargiela et al., 2003). Thus, the interval state estimation model developed in this paper is expressed as follows:

Objectives:

$$\begin{aligned} \underline{x}_i &= \min x_i, \\ \bar{x}_i &= \max x_i. \end{aligned} \tag{31}$$

TABLE 1 Capacity and location of PV units.

| PV location | PV capacity (MVA) |
|-------------|-------------------|
| 15, 46, 114 | 0.6 |
| 61, 88, 105 | 0.8 |
| 25, 68, 80 | 1.0 |
| 35, 98, 121 | 1.2 |

s.t.

$$P_i + \Delta P_i^G = V_i \sum_{j=1}^n V_j (G_{ij} \cos \theta_{ij} + B_{ij} \sin \theta_{ij}), \quad (32)$$

$$Q_i + \Delta Q_i = V_i \sum_{j=1}^n V_j (G_{ij} \sin \theta_{ij} - B_{ij} \cos \theta_{ij}), \quad (33)$$

$$\Delta P_i^G = \begin{cases} \Delta P_i^{RE}, & i \in \Omega_{RE}, \\ \Delta P_i^L, & i \in \Omega_L, \end{cases} \quad (34)$$

$$\Delta P_{i,low}^{r,RE} \leq \Delta P_i^{RE} \leq \Delta P_{i,up}^{r,RE}, \quad (35)$$

$$\Delta P_{i,low}^r \leq \Delta P_i^L \leq \Delta P_{i,up}^r, \quad (36)$$

$$\Delta Q_{i,low}^r \leq \Delta Q_i \leq \Delta Q_{i,up}^r, \quad (37)$$

where, $[\underline{x}_i, \bar{x}_i]$ is the interval value of state variable of node i , including voltage magnitude V and phase angle θ , P_i and Q_i are the active and reactive power of node i , G_{ij} and B_{ij} are admittance of branch ij , ΔP_i^{RE} is PV forecasting power output interval with lower bounds $\Delta P_{i,low}^{r,RE}$ and upper bounds $\Delta P_{i,up}^{r,RE}$, ΔP_i^L and ΔQ_i are load forecasting active and reactive power interval.

The estimation of individual state variable is independent of each other, as shown in Eq. 32, subject to the same equality and inequality constraints. The equality constraint contains active and reactive power balance constraints Eqs 33–35. Inequality constraints include PV forecasting uncertainty constraints Eq. 36 and load forecasting uncertainty constraints Eqs 37, 38. The upper and lower bounds of the forecasting uncertainty are updated in real time according to NN based LUBE.

4 Case study

In order to further verify the effectiveness and feasibility of the proposed IDSE method, a simulation study on IEEE 123-bus distribution system is carried out. The test system has a rated voltage of 4.16 kV and a total load of $3620 + j1324$ kVA, with individual load capacities and network branch parameters detailed in (Chai et al., 2018). 12 PV units are installed at 12 nodes, whose capabilities and locations are listed in Table 1. In addition, some nodes are selected to arrange real-time measurement devices, whose real-time measured power value is obtained from the power flow calculation of IEEE 123-bus system, and measurement error of $\pm 0.5\%$ is superimposed on the rated value, the extended IEEE 123-bus distribution system is shown in Figure 4.

4.1 Prediction interval of measurements

- (1) For PV power output, the ambient temperature, direct radiation, scattered radiation, and total radiation around the PV plant at various time sections during a week in a certain region are used as a source for PV power output prediction interval. The parameters of the LUBE are listed in Table 2. The resulting PV power output prediction interval based on LUBE estimates the PV power output curve at different time sections on a typical day is shown in Figure 5.
- (2) For load, historical load data from AEMO (2006–2010) in New South Wales, Australia (Qiu et al., 2018) was used as a sample for load prediction interval. The resulting load prediction interval estimates the load curve at different times sections on a typical day is shown in Figure 6.

4.2 Interval dynamic state estimation

In order to make comparison of the results of IDSE for ADN, the PV power output interval $[0, 0.1]$ kW at 01:00 a.m. and $[302, 345]$ kW at 13:00 p.m. are selected for the test, based on which the EKF and UKF are used for the IDSE analysis with SR-UKF proposed in this paper. Figures 7, 8 show the results of IDSE in ADN based on these three methods.

As can be seen from the IDSE results shown in Figures 7, 8, the interval fluctuations in injected power of node cause the voltage magnitude and phase angle to fluctuate within a certain range, and the access to PV in ADN will increase the voltage level of the system. The comparison analysis shows that at any node of the ADN, the result interval of the IDSE method used in this paper is smaller than that of the EKF and closer to the result interval of the UKF, demonstrating that the conservativeness of the uncertain DSE solution can be effectively reduced by using the DSE algorithm with high accuracy. The EKF linearizes the system through Jacobian matrix calculation, which ignore higher order terms, making the state estimation of EKF less accurate and therefore the interval range obtained through the EKF is larger. The UKF approximates the non-linear system by unscented transformation, which can be approximated to at least second order for non-Gaussian inputs. Therefore, the UKF is more accurate than the EKF and has a smaller interval range than EKF. SR-UKF reduces computational errors and improves computational efficiency by propagating the SR of matrix instead of the matrix itself, its accuracy is slightly better than that of the UKF. SR-UKF has almost the same interval range as UKF.

In order to compare the conservativeness of the above three methods more intuitively, a comparative analysis of the interval width of IDSE for node voltage magnitude and phase angle is carried out, using two indicators to assess the conservativeness:

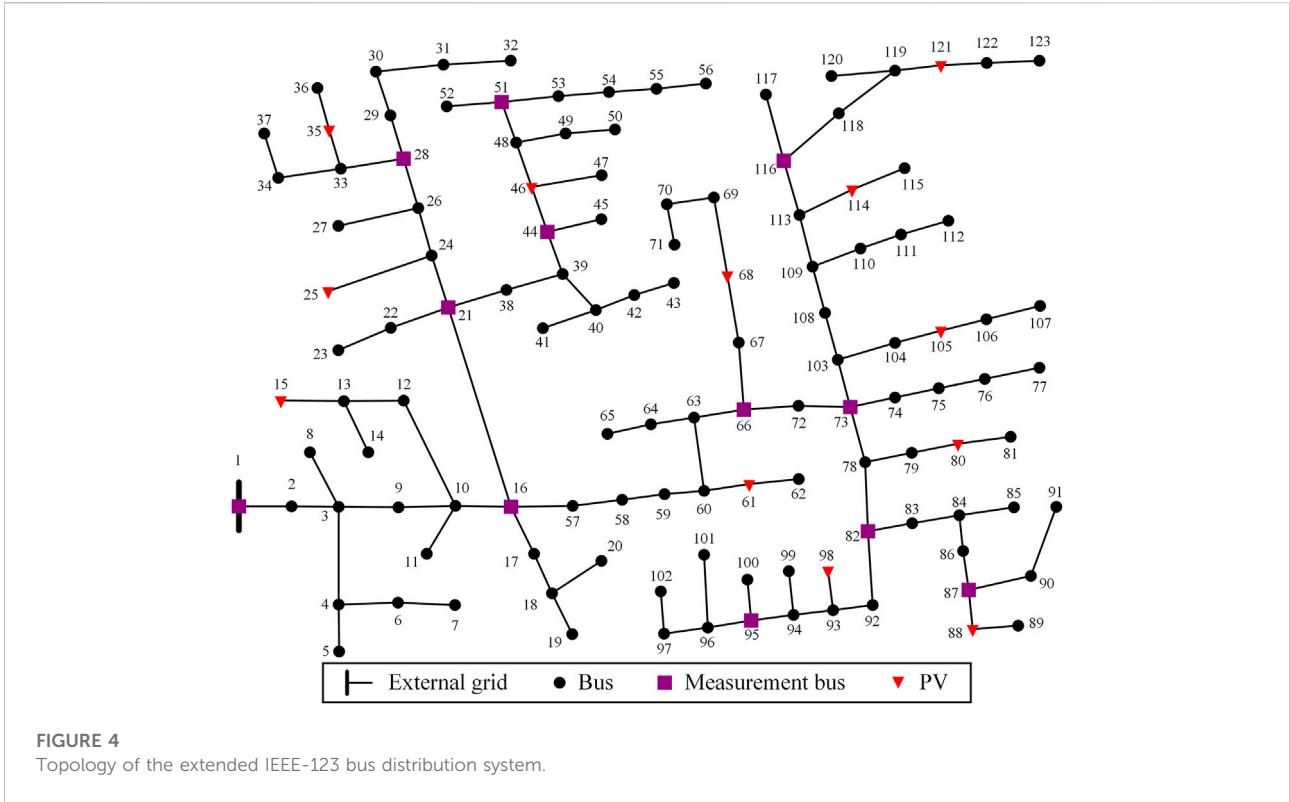
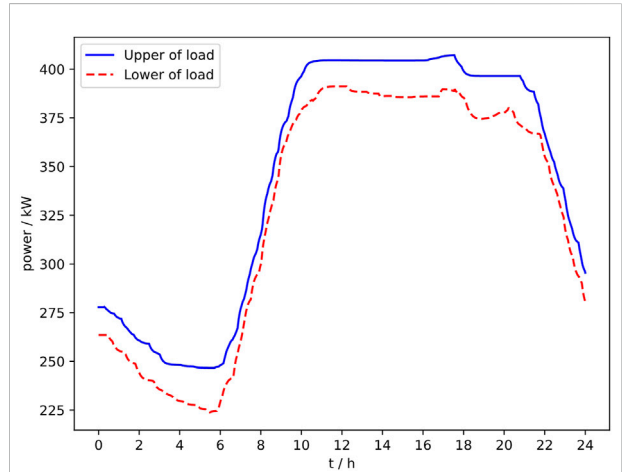
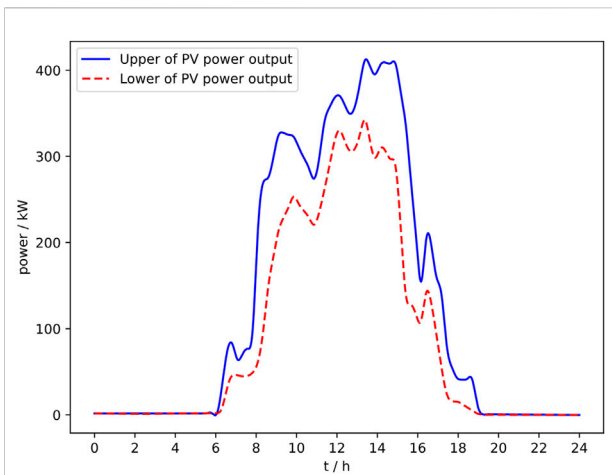


TABLE 2 LUBE parameters setting.

| Number of net layers | Number of neurons per layer | η | μ |
|----------------------|-----------------------------|--------|-------|
| 2 | 64 | 70 | 0.7 |



$$\begin{cases} \omega_1 = \frac{1}{n} \sum_{i=1}^n (\bar{x}_i - x_i), & i = 1, 2, \dots, n, \\ \omega_2 = \max(\bar{x}_i - x_i) \end{cases} \quad (38)$$

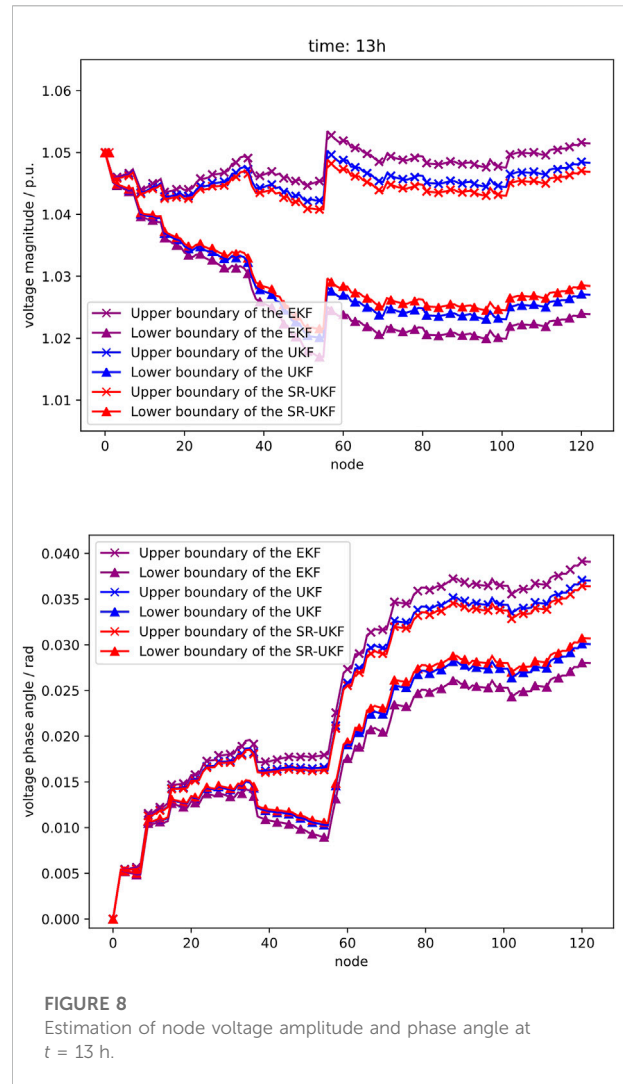
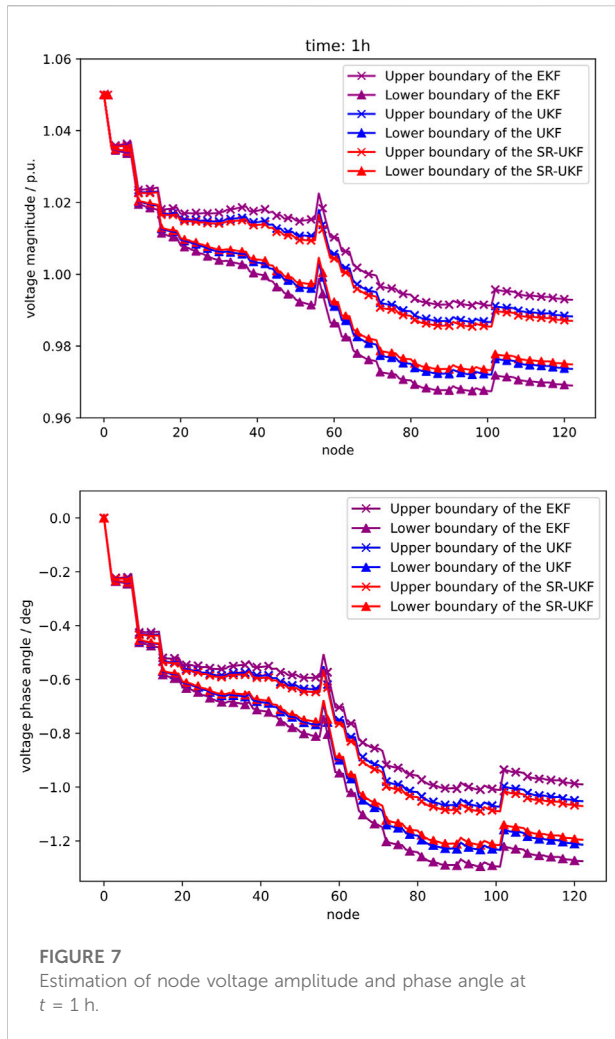


TABLE 3 Comparison bounds of node at $t = 1$ h

| Method | Voltage magnitude | | Phase angle | |
|--------|-------------------|------------|-------------|------------|
| | ω_1 | ω_2 | ω_1 | ω_2 |
| EKF | 0.0185 | 0.0239 | 0.0050 | 0.0071 |
| UKF | 0.0115 | 0.0147 | 0.0034 | 0.0046 |
| SR-UKF | 0.0110 | 0.0131 | 0.0030 | 0.0041 |

where, ω_1 is the average interval width, ω_2 is the maximum interval width. Larger ω_1 and ω_2 means higher conservativeness, the results are shown in Tables 3, 4.

The above results show that the SR-UKF method used for IDSE in this paper has a narrower solution interval width compared to EKF and UKF, is less comparative and has a higher

TABLE 4 Comparison bounds of node at $t = 13$ h

| Method | Voltage magnitude | | Phase angle | |
|--------|-------------------|------------|-------------|------------|
| | ω_1 | ω_2 | ω_1 | ω_2 |
| EKF | 0.0215 | 0.0284 | 0.0079 | 0.0113 |
| UKF | 0.0168 | 0.0221 | 0.0051 | 0.0072 |
| SR-UKF | 0.0162 | 0.0202 | 0.0044 | 0.0061 |

reliability of the estimation results. Meanwhile, comparing the results for $t = 1$ h and $t = 13$ h shows that the PV output increases as the light intensity becomes stronger, making the uncertainty also increasing, so that the interval width at $t = 13$ h is wider than that at $t = 1$ h.

TABLE 5 Comparison results of computing efficiency between different algorithms.

| Method | Time consuming (s) |
|--------|--------------------|
| EKF | 1.2121 |
| UKF | 0.4252 |
| SR-UKF | 0.1096 |

Next, the computing efficiency of the three methods is compared and analyzed, are shown in Table 5. From the comparison results, it can be seen that the SR-UKF method used in this paper has much better computing efficiency than EKF and UKF, and it is suitable for large-scale networks, thus making it suitable for online applications.

5 Conclusion

An interval dynamic state estimation considering the uncertainty of PV and load has been proposed in this paper.

- (1) SR-UKF is used to determine the operating median values of all state variables to improve computing efficiency.
- (2) The interval is used to analyze the measurement uncertainty of ADN, the NN based LUBE theory is used to predict the PV power output interval and the active and reactive power interval of unmeasured load.
- (3) The interval state estimation is modelled as a bilevel non-linear programming problem to obtain the upper and lower bounds. The modified test case demonstrates the feasibility and effectiveness of the proposed IDSE method.

The next step of the research will be to study the analysis of system measurement outliers (bad data), zero injection power node constraints and other factors to improve the online application of IDSE method for ADN.

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Data availability statement

The original contributions presented in the study are included in the article/supplementary material, further inquiries can be directed to the corresponding author.

Author contributions

JW, KL, and FW contributed to the conception and design of the study. ZW are responsible for providing experimental design and data analysis. LS and YL are responsible for providing code implementation. All authors contributed to the manuscript writing revision, read, and approved the submitted version.

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Conflict of interest

The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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