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# Development and verification of a new nuclear data processing code AXSP

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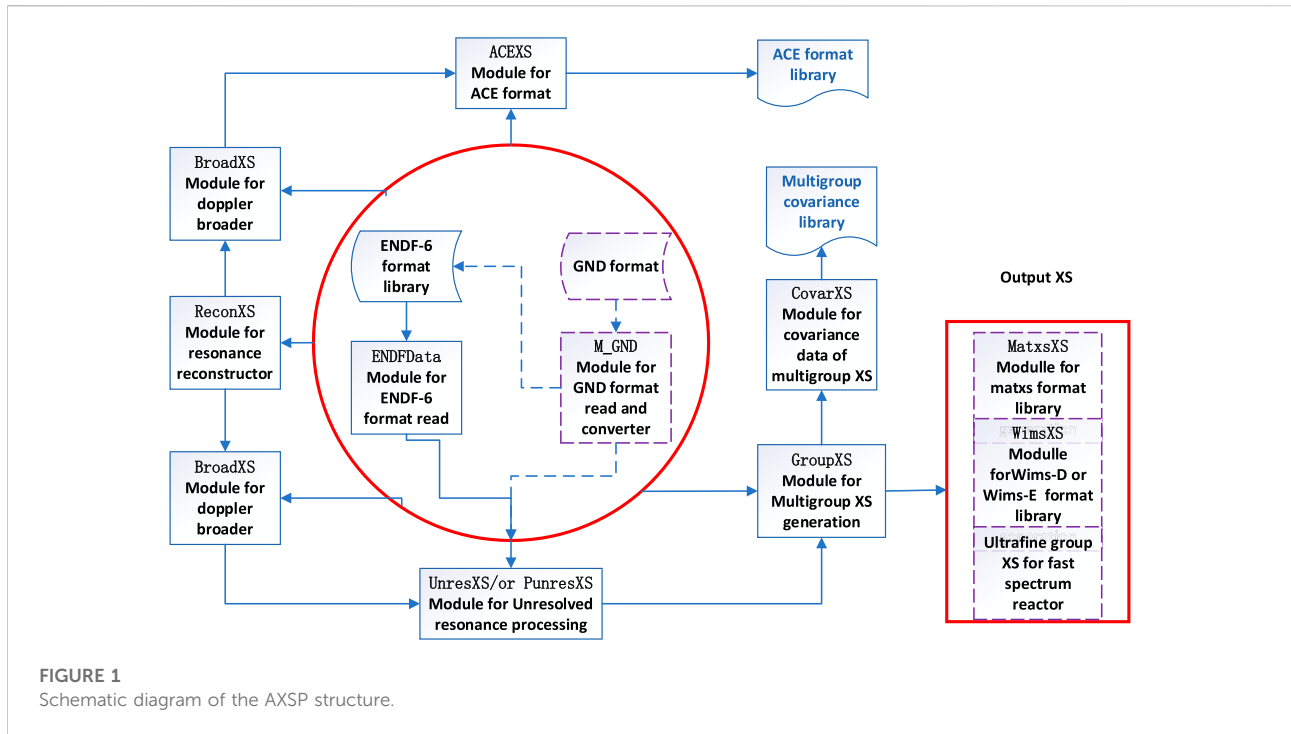
The advanced reactor design needs an accurate cross-section generation code. In this study, a new nuclear data processing code AXSP is developed, and the method and performance of which are described. Compared with the NJOY program, the precision of the unresolved resonance processing module UnresXS has been significantly improved due to the adoption of a more accurate solution method and the consideration of in-sequence overlap integrals. The time consumption of PUnresXS has been decreased significantly due to an optimized sorting algorithm. At the same time, other modules of AXSP are relatively comprehensive. The function of resolved resonance cross-section reconstruction and linearization is the ReconXS module. The Doppler broadening module is BroadXS by using Gauss–Hermite quadrature and Gauss–Legendre quadrature from 0 K temperature pointwise cross section to any temperature which is defined by the user. The shielding factor in the unresolved resonance energy region is calculated by the UnresXS or the PUnresXS module, which are developed based on the Bondarenko method and the probability table method, respectively. The ACE formatted cross sections for the Monte Carlo code is processed by the ACEXS module, and the multigroup cross sections are generated by the GroupXS module. The cross sections processed by different modules were verified by the NJOY2016 code, and the multigroup cross sections were also verified by using the critical benchmarks. The multiplication factor difference between AXSP and NJOY2016 is less than 20 pcm. In addition to this, the ZPR6/7 fast reactor is used for ACE format library verification. The results show that the criticality calculated by AXSP has a good agreement with that of NJOY2016.

## KEYWORDS

nuclear data processing code, NJOY data processing, AXSP, ENDF format, advanced reactor design

## Introduction

A total of six advanced reactor concepts have been selected for Generation IV reactor and are being investigated to meet the challenging goals of effective resource utilization and waste minimization. The cross section is one of the most fundamental quantities for the reactor design. The evaluated nuclear data files have been updated over the years with



reflecting progress on nuclear modeling, new nuclear experiment measurement, and a lot of feedback from the benchmark analysis. The cross-sections' data library of neutronics calculation codes is generated by processing the evaluated nuclear data files when it is updated. Therefore, the nuclear data processing code is very important for connecting the evaluated nuclear data file and the reactor analysis and design codes. The motivation for the development of the advanced cross-section process (AXSP) code is to establish a platform to research some new methods of nuclear processing to satisfy the demands on accurate cross sections for the advanced reactor design. For example, in the design of a mixed-spectrum reactor, it is necessary to consider not only the anisotropic scattering in the high-energy region but also the influence of the broad resonances and the upper scattering problems in the low-energy region. The problem of generating a high-precision multigroup cross section cannot be well resolved. Because if we want to better solve the problem of the hybrid spectrum reactor, we need to consider not only the anisotropic scattering in the high-energy region but also the solution of the moderation equation in the all-energy region. There are still many works to be carried out.

Currently, NJOY (Abou Jaoude, 2017), PREPRO (Cullen, 2017), and AMPX (Wiarda et al., 2016) are well-known nuclear data processing codes in the world. There are also some newly developed nuclear data processing codes. For example, RXSP (Jian-kai et al., 2013) (Li and WangKan, 2017) (Liu et al., 2020) (Li, 2012) (Yu, 2015) of Tsinghua University and FRENDY (Tada et al., 2017) of the Japan Atomic Energy Agency (JAEA) have

developed to produce an ACE format library for the Monte Carlo code. Ruller (Liu et al., 2016) of the China Institute of Atomic Energy and NECP-Atlas (Zu et al., 2019) of Xi'an Jiao Tong University have been developed to provide a multigroup library. At the same time, EXUS-F of South Korea was developed for a faster reactor multigroup cross-section generation by direct processing of the evaluated nuclear data file.

For the nuclear data processing, the open source nuclear data processing system NJOY is still not perfectly processing the evaluated nuclear data for the advanced nuclear reactor analysis when it is used to calculate the KERMA factors and DPA cross sections (Konno et al., 2016) (Wen et al., 2020) because of some bugs.

Recently, the nuclear data format has been considered to change from the traditional ENDF-6 format to the generalized nuclear data (GND) format (Mattoon et al., 2012) by utilizing the Extensible Markup Language. Since the GND format is completely different from the current ENDF-6 format, which was defined several decades ago, the NJOY code cannot treat such a new format without extensive modification. To solve this problem, several nuclear data processing systems, such as NJOY21 (Conlin, 2015), FUDGE (Beck and Mattoon, 2014), and AMPX-2000, are under development in a few countries.

In this study, the outline of the development, method, and capability of AXSP are described in the *Theory and processing method* section. In *Numerical calculation results* section, the verification of each module of AXSP is investigated, and the results of AXSP are compared with those of NJOY 2016. The

TABLE 1 Time consumption for the unresolved resonance processing with different codes.

Isotope	PURR/s	PUnresXS/s	PURR/PUnresXS
<sup>241</sup> Am	2,484	2,420	1.03
<sup>251</sup> Cf	2,809	2,703	1.04
<sup>239</sup> Pu	3,995	3,881	1.03
<sup>235</sup> U	2,036	1,880	1.08

critical benchmarks from the ICSBEP handbook are applied to demonstrate the accuracy of the multigroup cross section with the Bondarenko method, and ZPR6/7 was used to verify the ACE format library generated by the ACEXS module. The last section is conclusion.

## Theory and processing method

AXSP is developed to solve the problems of the current nuclear data processing systems and satisfy the demands on accurate cross sections (XS) for the advanced reactor. Therefore, modern programming techniques are utilized to make the code more maintainable, modularized, portable, and flexible; it was written in Fortran 2003 by using the object-oriented programming techniques and allocatable memory techniques. Each module has its own class, and the modification of the class does not affect the other classes. The ENDF data class can be easily reused in other modules. The schematic diagram of the AXSP structure is shown in Figure 1. The solid lined modules have already been implemented, while the dotted lined modules are still in development. The GND format is not finalized. Now, the GroupXS module is still based on the Bondarenko method, and on the other hand, the ultrafine group method and hyperfine group method for the fast reactor design will be developed in the future.

The ReconXS module is used to reconstruct resonance cross sections from resonance parameters and to reconstruct cross sections from ENDF nonlinear interpolation schemes by using a traditional inverted-stack method. The BroadXS module generates Doppler-broadened cross sections in the PENDF format from piecewise linear cross sections in the PENDF

format from 0 K temperature. To improve the calculation efficiency and maintain the calculation accuracy at the same time, the Gauss–Hermite quadrature has been used in some energy regions, and two points of Gauss–Legendre quadrature are used in other energy ranges (Li, 2012).

The UnresXS module is used to produce effective self-shielded cross sections for resonance reactions in the unresolved energy range. In the unresolved energy range, it is not possible to define precise values for the cross sections of the resonance reactions  $\sigma_x(E)$ , where  $x$  stands for the reaction type, such as total, elastic, fission, or capture. It is only possible to define average values. The average cross sections in the vicinity of  $E^*$  can be written as

$$\bar{\sigma}_{0x}(E^*) = b_x(E^*) + \frac{\bar{\sigma}I_{0x}}{1 - I_{0t}} \quad (1)$$

and

$$\bar{\sigma}_{1x}(E^*) = b_t(E^*) + \frac{\bar{\sigma}I_{1x}}{1 - I_{0t} - I_{1t}}, \quad (2)$$

where  $b_x(E^*)$  is the background cross section for the reaction type  $x$ ,  $b_t(E^*)$  is the background cross section for the total cross section, and  $I_{0x}$  and  $I_{1t}$  are the two types of “fluctuation integrals”.  $\bar{\sigma}(E^*)$  is written as

$$\bar{\sigma}(E^*) = b_t(E^*) + \sigma_0. \quad (3)$$

The background cross section  $\sigma_0$  is defined in the input file of AXSP by the user. If we assume that the resonances are widely separated and only the “self” term will be important, the fluctuation integrals become

$$I_{0x} = \sum_s A_{xs}, \quad (4)$$

$$A_{xs} = (B_{xs} - V_{0xs}) \left[ 1 - \sum_{s' \neq s} A_{ts'} \right], \quad (5)$$

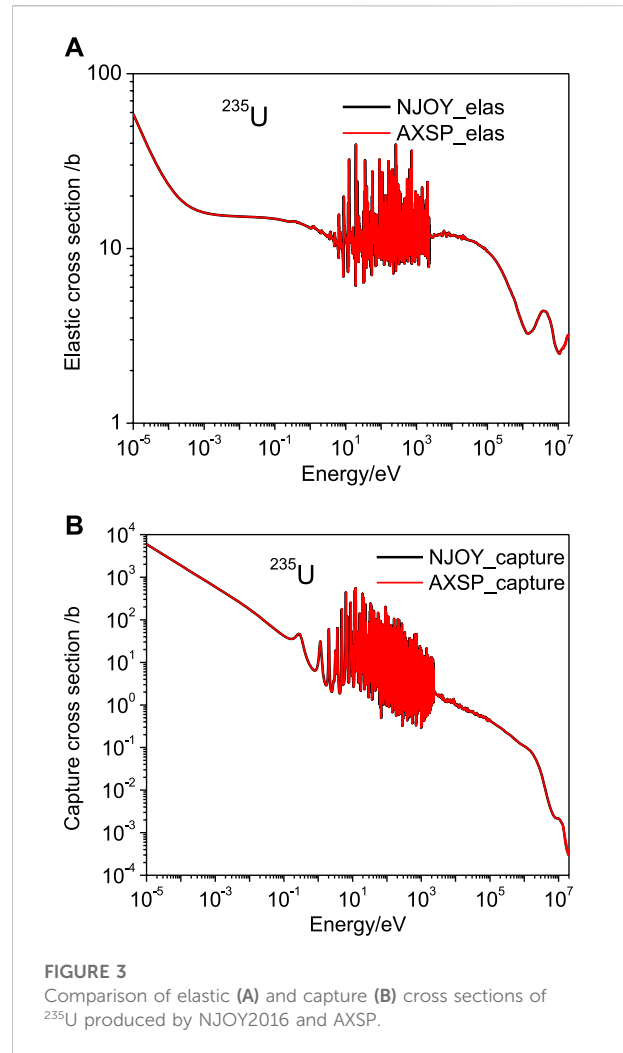
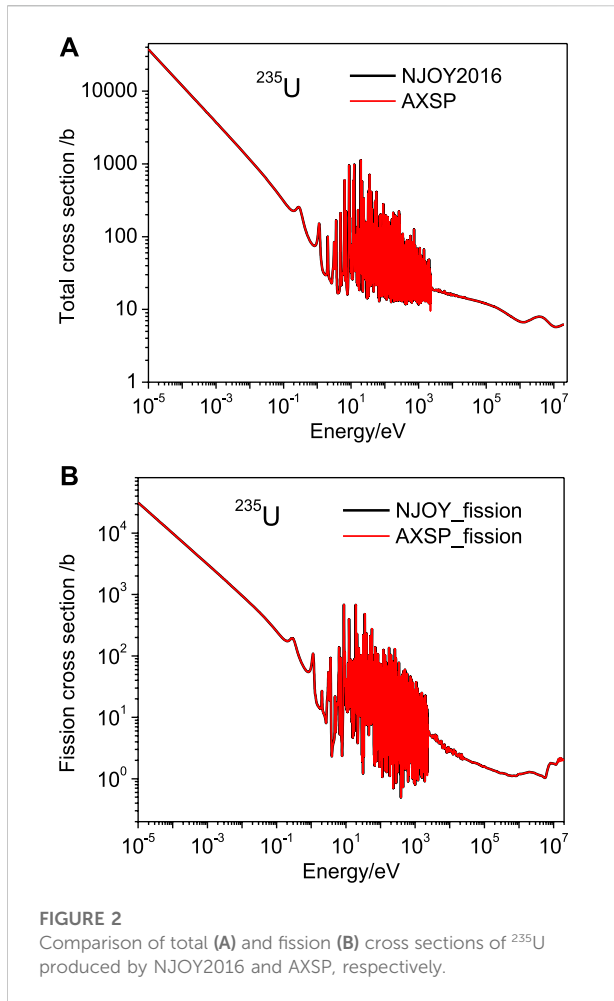
and

$$I_{1t} = \sum_s (D_{ts} - V_{1ts}) \left[ 1 - \sum_{s' \neq s} A_{ts'} \right]^2, \quad (6)$$

where  $B_{xs}$  and  $D_{ts}$  are the first kinds including the isolated resonance integrals and  $V_{0xs}$  and  $V_{1ts}$  are the in-sequence overlap

TABLE 2 Comparison time consumption between the shell sort algorithm and bubble sort algorithm.

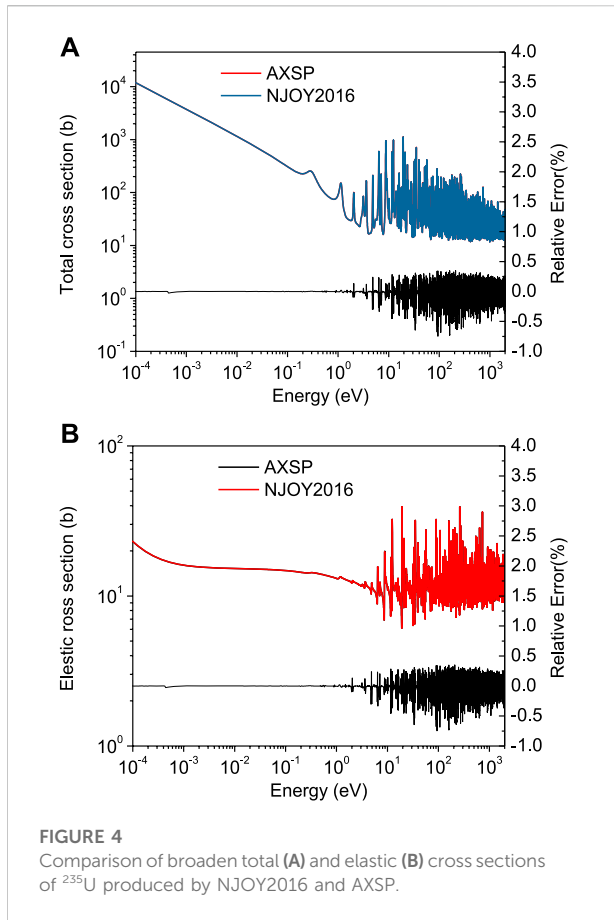
Isotope	Shell sort algorithm/s	Bubble sort algorithm/s	(Shell sort)/(bubble sort)
<sup>58</sup> Co	56.522	1,037.479	0.05
<sup>74</sup> As	584.553	4,326.493	0.14
<sup>102</sup> Ru	38.004	788.142	0.05
<sup>135</sup> Cs	104.814	1,977.199	0.05
<sup>238</sup> U	938.732	5,262.513	0.18
<sup>241</sup> Pu	779.576	2,631.492	0.30
<sup>232</sup> Th	758.535	4,271.325	0.18



integrals. In the UNRESR module of the NJOY code, the in-sequence overlap corrections  $V_{0xs}$  and  $V_{1ts}$  are neglected. This approximation is based on the assumption that resonance repulsion will reduce the overlap between resonances in different sequences as the dominant overlap effect. In the UnresXS module of AXSP, the in-sequence overlap correction  $V_{0xs}$  was calculated by using the method for computing J, which has been developed by Hang for MC<sup>2</sup>-2 (Henryson et al., 1976). The improvement of UnresXS comparison with that of UNRESR will be discussed in the *Numerical calculation results* section.

The unresolved self-shielding data generated by UnresXS are suitable for multigroup methods after processing by GroupXS based on the Bondarenko method. However, the Bondarenko method is not suitable for continuous-energy Monte Carlo codes like MCNP and RMC. Therefore, the PUnresXS module is developed by the ladder-sampling method to generate the probability table for the Monte Carlo code. On the other hand, the PUnresXS module can generate the effective self-shielded cross section which can be used for the multigroup cross-section generation. The disadvantage of PUnresXS is time

consumption. To solve this problem, we have optimized the sorting method in the program, which greatly saves the calculation time while ensuring the accuracy. Previous research (Yu, 2015) has shown that the time consumption of the PURR module is mainly related to the sorting algorithm used, and the bubble sort algorithm has been applied in the PURR module. If the bubble sort algorithm was also used in the PUnresXS module of AXSP, the time consumption for the unresolved resonance processing with different codes is shown in Table 1. As shown in Table 1, the time consumption of the PUnresXS module is almost the same as the PURR module of NJOY if the same bubble sort algorithm is used. We also compared the impact of selection sort, quicksort, heap sort, and shell sort on time; the shell sort algorithm was selected and applied in the PUnresXS module because of the better calculation speed. The time consumption with the shell sort algorithm and bubble sort algorithm in PUnresXS for different isotopes is shown in Table 2. As shown in Table 2, for most isotopes, the computation time using the shell sort algorithm is

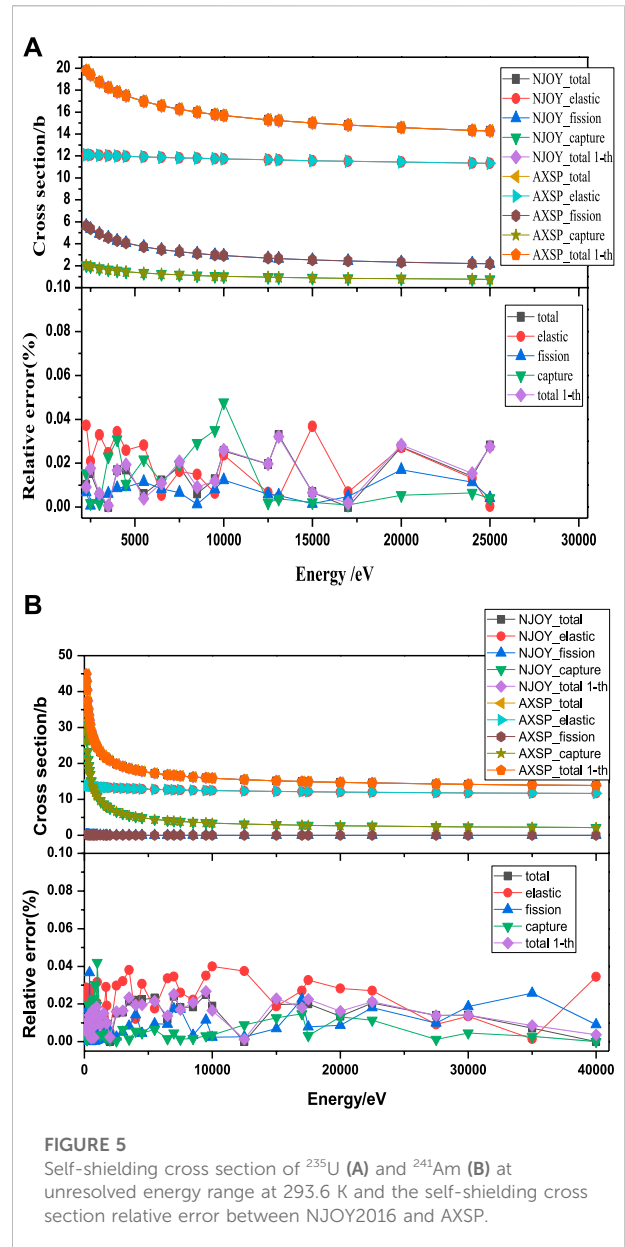


18% of the computation time of the bubble sort, or less. After using the shell sort algorithm, the calculation time is significantly reduced, and the calculation speed is significantly improved.

Multigroup constants are normally used by computer codes that calculate the distribution of neutrons and/ or photons in space and energy, and these compute various responses to these distributions. The GroupXS module in AXSP was developed to calculate the multigroup constants. The GroupXS module computes not only group average cross sections but also the group-to-group scattering matrix. The average cross sections and group-to-group scattering matrix can be represented as

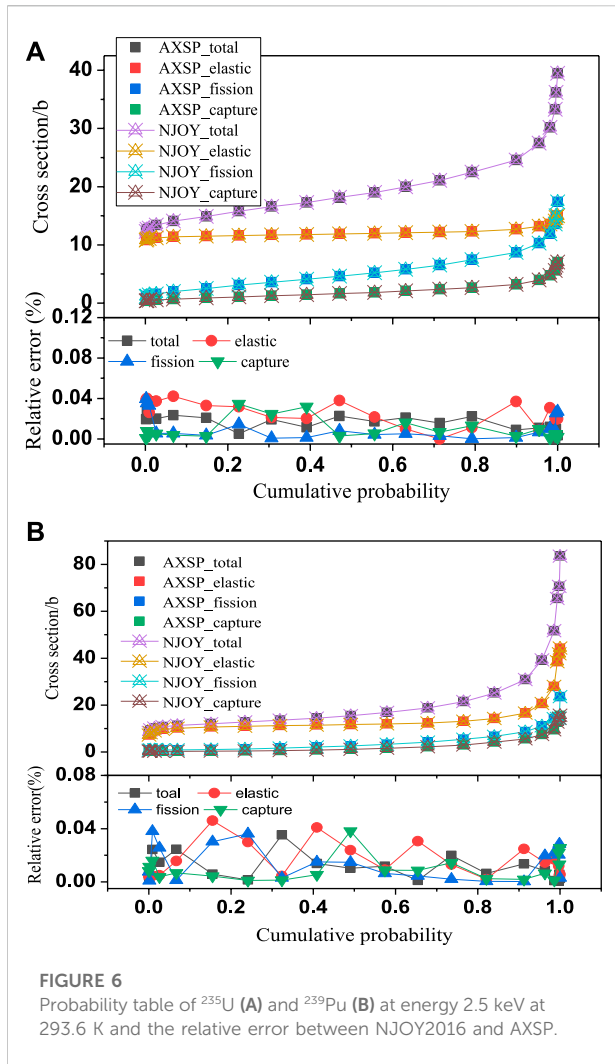
$$\bar{\sigma}_{i,x,g} = \frac{\int_{\Delta E_g} \sigma_{x,i}(E) \phi_0(E) dE}{\int_{\Delta E_g} \phi_0(E) dE}, \quad (7)$$

where i, x, and g are the indices for isotopes, reaction type, and multigroup number, respectively.  $\phi_0(E)$  is the neutron spectrum. In the group where the boundary between resolved and unresolved resonance ranges is located, both the resolved and unresolved resonances are self-shielded simultaneously. By dividing the integration interval into the resolved and unresolved resonance intervals, the self-shielding cross section is determined as



$$\bar{\sigma}_{i,x,g} = \frac{\int_{\Delta E_{resolved}} \sigma_{x,i}(E) \phi_0(E) dE + \int_{\Delta E_{unresolved}} \sigma_{x,i}(E) \phi_0(E) dE}{\int_{\Delta E_{resolved}} \phi_0(E) dE + \int_{\Delta E_{unresolved}} \phi_0(E) dE}, \quad (8)$$

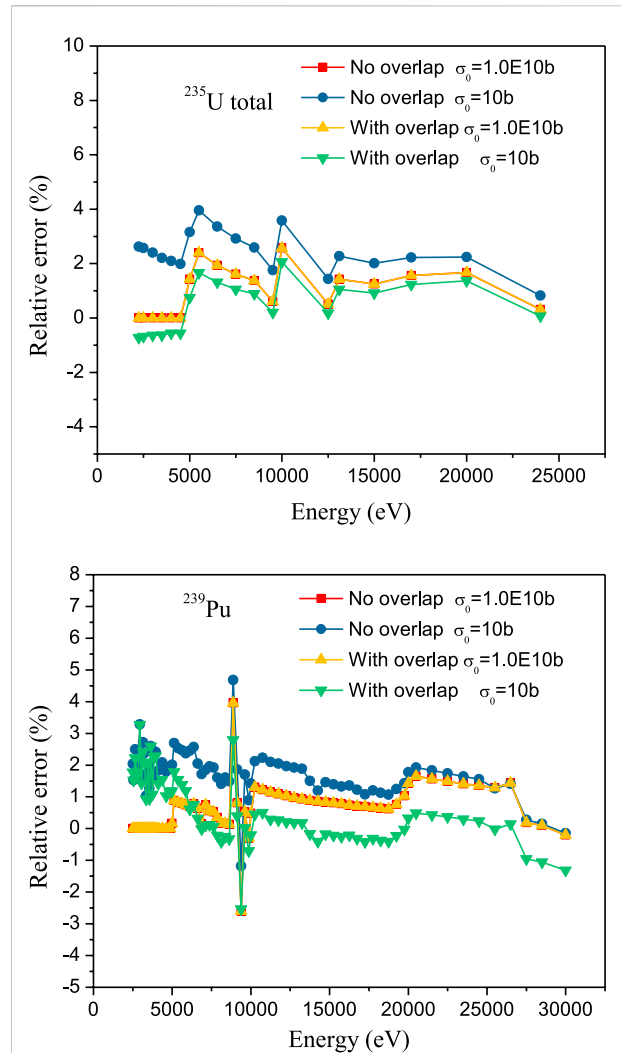
where the integrals over the resolved resonance interval are evaluated in Eq. 7. When the integrals over the unresolved interval are evaluated, the self-shielding factor generated by the UnresXS or PUnresXS module should be taken into account the self-shielding effects. The GroupXS module calculates the scattering matrix for neutron-induced scattering reactions such as elastic scattering, discrete inelastic scattering, and continuum inelastic scattering. The scattering matrix is also calculated for (n, 2n) and (n, 3n) reactions, including anisotropy



by using the ENDF-formatted nuclear data library. The scattering matrix for the  $l$ -th anisotropic scattering can be resented as

$$\bar{\sigma}_{i,x,g' \rightarrow g}^l = \frac{\int_{\Delta E_g} dE \int_{\Delta E_{g'}} \sigma_{i,x} \phi_l(E') f(E' \rightarrow E, \mu_s) P_l(\mu_s) d\mu_s dE'}{\int_{\Delta E_{g'}} \phi^l(E) dE}, \quad (9)$$

where  $f(E' \rightarrow E, \mu_s)$  is the scattering transfer probability from the incident energy  $E'$  to the outgoing energy  $E$  and the cosine of the scattering angle  $\mu_s$  in the laboratory system.  $\phi_l(E)$  is the  $l$ -th moment of the neutron flux, and  $P_l(\mu_s)$  is the  $l$ -th order Legendre polynomial. With a given transfer probability, the element of the scattering transfer matrix can be determined by evaluating the integrals numerically. There are three ways to give the transfer probability, according to the data types given in nuclear data files: the angular distribution in file 4, the angular distribution in file 4 and the energy distribution in file 5, and the energy-angle distribution in file 6.



**FIGURE 7**  
In-sequence overlap integral effects to the self-shielding total cross sections of  $^{235}\text{U}$  and  $^{239}\text{Pu}$  with different background cross sections (the temperature is set as 293.6 K).

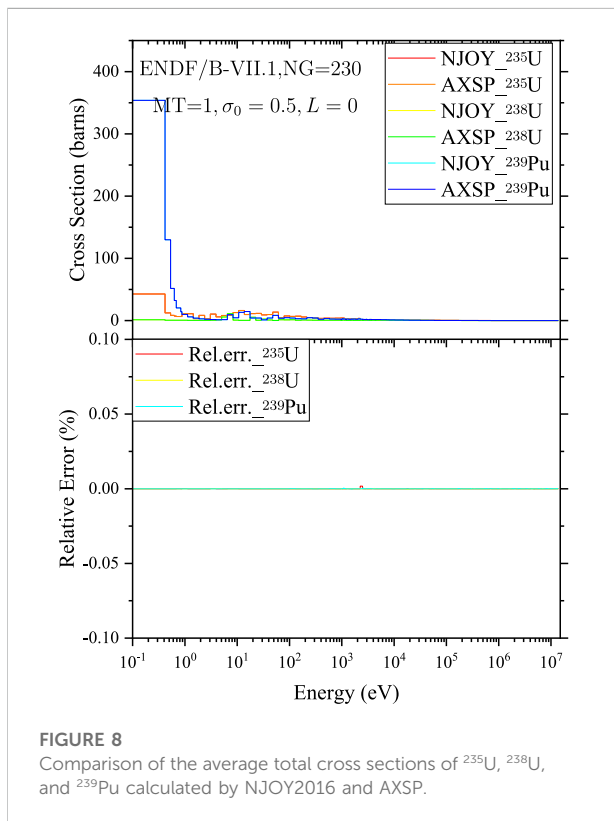
For the multigroup constant generation, it is important to select the continuum energy neutron flux and flux moment  $\phi_l(E)$ . In many cases of practical interest, the neutron flux and flux moment  $\phi_l(E)$  will contain dips corresponding to the absorption resonances of various materials, and these dips will reduce the effect of the corresponding resonance, which is also called self-shielding. If the Bondarenko narrow-resonance weight scheme (MacFarlane, 2012) is used, the flux can be written as

$$\phi_l^i(E) = \frac{C(E)}{[\sigma_i^l(E) + \sigma_0^l]^{l+1}}, \quad (10)$$

where  $\sigma_i^l(E)$  is the microscopic total cross section for the isotope  $i$ ,  $C(E)$  is the smooth function of energy, and  $\sigma_0^l$  is a constant background cross section, which represents all the other isotope

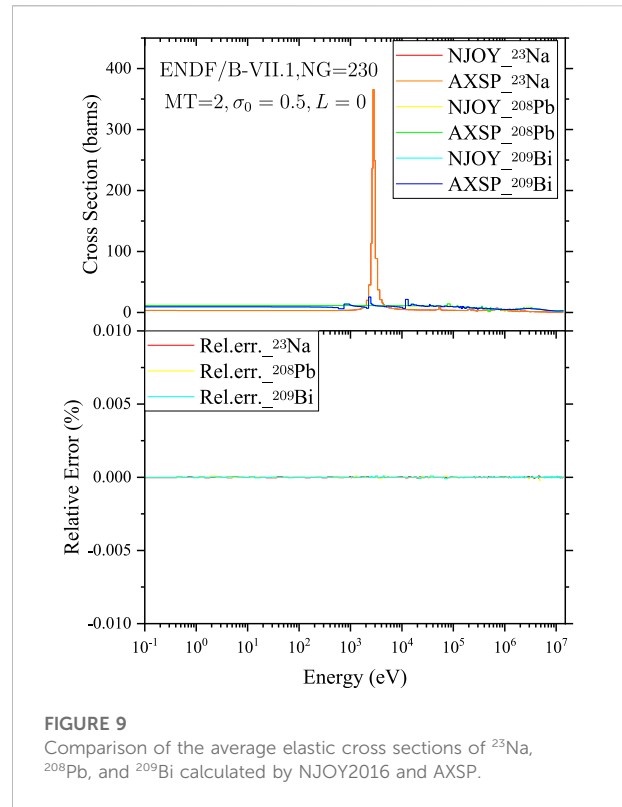
**TABLE 3** Number of materials in ENDF/B-VII.1 for specific File 5 formats for total fission, first-chance neutron-induced fission, and (n, 2n) reactions.

Reaction type MT	18	19	16
Total number of isotopes	82	3	176
LF = 1	68 ( <sup>235</sup> U)	1 ( <sup>234</sup> U)	158 ( <sup>241</sup> Pu)
LF = 7	11 ( <sup>241</sup> Pu)	2 ( <sup>236</sup> U, <sup>240</sup> U)	—
LF = 9	—	—	18 ( <sup>23</sup> Na)
LF = 11	1 ( <sup>233</sup> U)	—	—
LF = 12	2 ( <sup>241</sup> Am, <sup>243</sup> Am)	—	—

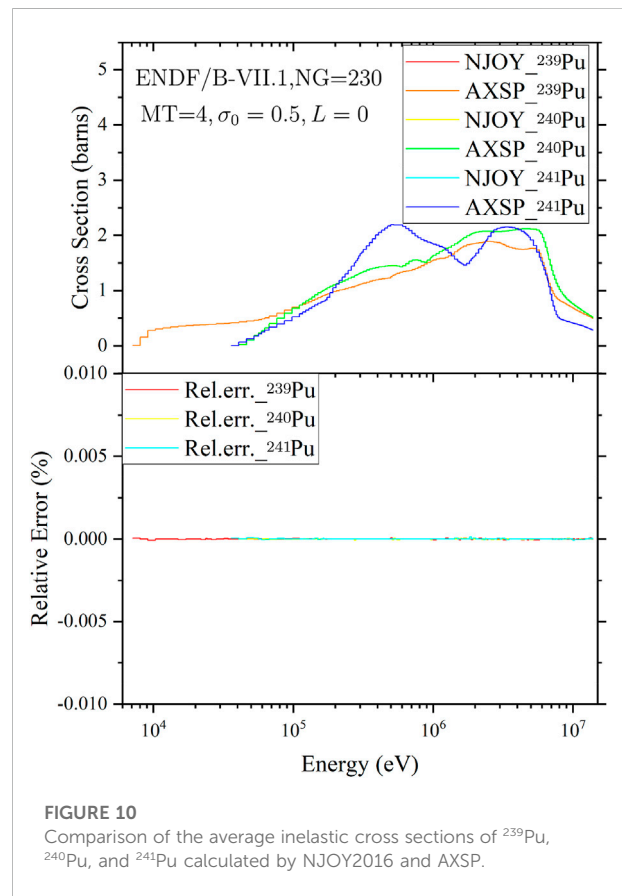


**FIGURE 8** Comparison of the average total cross sections of <sup>235</sup>U, <sup>238</sup>U, and <sup>239</sup>Pu calculated by NJOY2016 and AXSP.

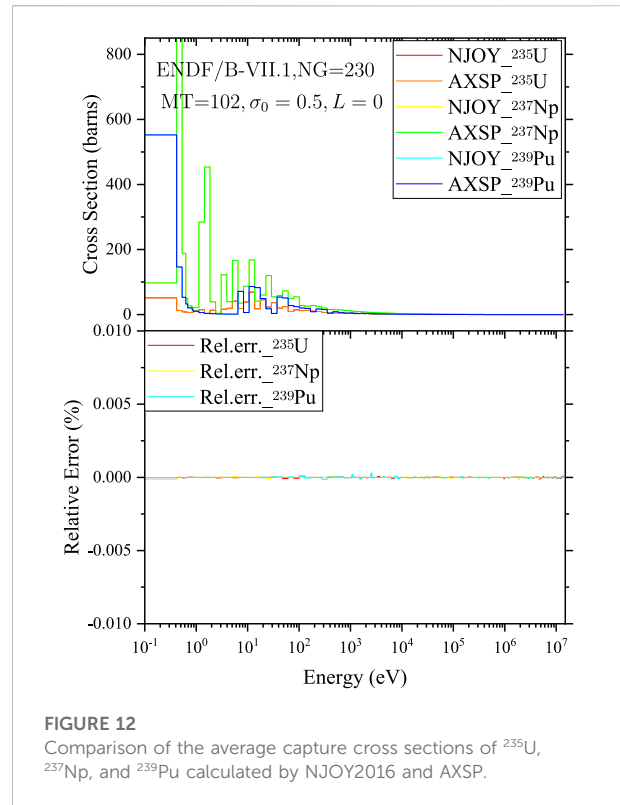
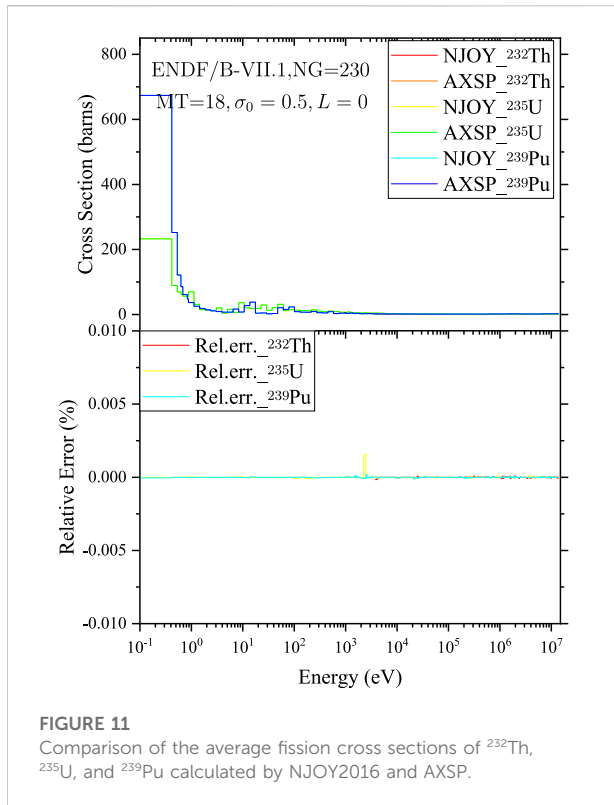
effects to the flux. However, we know that the Bondarenko method is more suitable for fast spectral reactors, and for thermal reactors, this method will introduce relatively large errors due to the need to consider the broad resonance in the low-energy region. Therefore, in the future, we will use the method of solving the continuous energy neutron transport equation to obtain the energy spectrum so that the generated multigroup cross sections will be more accurate, such as the CENTRM module (Williams and Hollenbach, 2011) in SCALE6.1 and RMET21 (Leszczynski, 2001). The disadvantage of the current version of GroupXS is that it can only handle neutron evaluated data, not yet unable to handle photon evaluated data. Therefore, there still exist some important



**FIGURE 9** Comparison of the average elastic cross sections of <sup>23</sup>Na, <sup>208</sup>Pb, and <sup>209</sup>Bi calculated by NJOY2016 and AXSP.



**FIGURE 10** Comparison of the average inelastic cross sections of <sup>239</sup>Pu, <sup>240</sup>Pu, and <sup>241</sup>Pu calculated by NJOY2016 and AXSP.



functions which need to develop in the future, such as treating the thermal neutron cross sections and produce the MATXS format library, and Wims-D and Wims-E format libraries. In the following verification, the MATXS format library was produced by using MATXS of NJOY.

## Numerical calculation results

### Cross-section comparison

The ReconXS module was verified by comparing the cross sections which were generated with AXSP with that of NJOY 2016. Almost all the isotopes in ENDF/B-VII.1 (Chadwick et al., 2011), ENDF/B-VIII.0 (Brown et al., 2018), and CENDL-3.2 (Ge et al., 2020) are used for testing. The results show that the cross sections generated by AXSP are in good agreement with those of NJOY2016. The cross sections of  $^{235}\text{U}$  for total, fission, elastic, and capture are shown in Figure 2 and Figure 3. As shown in the figures, the relative error between AXSP and NJOY2016 is all less than 0.5%, which is the maximum relative error setting for the cross-section reconstruction.

The BroadXS module was tested by using BROADR of NJOY. The Doppler-broadened cross sections of  $^{235}\text{U}$  for the total and elastic cross sections at 300 K are shown in Figure 4, and the relative errors of the cross sections between AXSP and

NJOY2016 are all less than 0.25% in all energy ranges. Therefore, the Doppler-broadened cross section calculated by AXSP is in good agreement with the calculation results of NJOY2016.

The UnresXS module has been developed to calculate the shielding factor for the multigroup cross-section generation. To verify the UnresXS module, first, the UnresXS has been developed by the same calculation method as the UNRESR of NJOY 2016; the UNRESR module of NJOY2016 has been used to perform the comparison. The self-shielding cross section of  $^{235}\text{U}$  and  $^{241}\text{Am}$  at its unresolved energy range at 293.6 K is shown in Figure 5. As shown in Figure 5, the absolute relative error between AXSP and NJOY2016 for all the energy points is less than 0.04%. The probability table for the Monte Carlo calculation has been calculated by the PUnresXS module of AXSP, and the probability table of  $^{235}\text{U}$  and  $^{239}\text{Pu}$  at energy 2.5 KeV and temperature at 293.6 K is shown in Figure 6. The probability table calculated by AXSP is also in good agreement with PURR of NJOY2016, and the absolute relative errors are less than 0.4%. Second, we improved the UnresXS module to make it to take into account the in-sequence overlap integrals, as shown in Equation 5. The in-sequence overlap integral effects have been shown in Figure 7. In the study, the PURR module calculation results have been set as the reference results, and the relative errors with in-sequence overlap integrals and without in-sequence overlap integrals for  $^{235}\text{U}$  and  $^{239}\text{Pu}$  have been obtained. As shown in



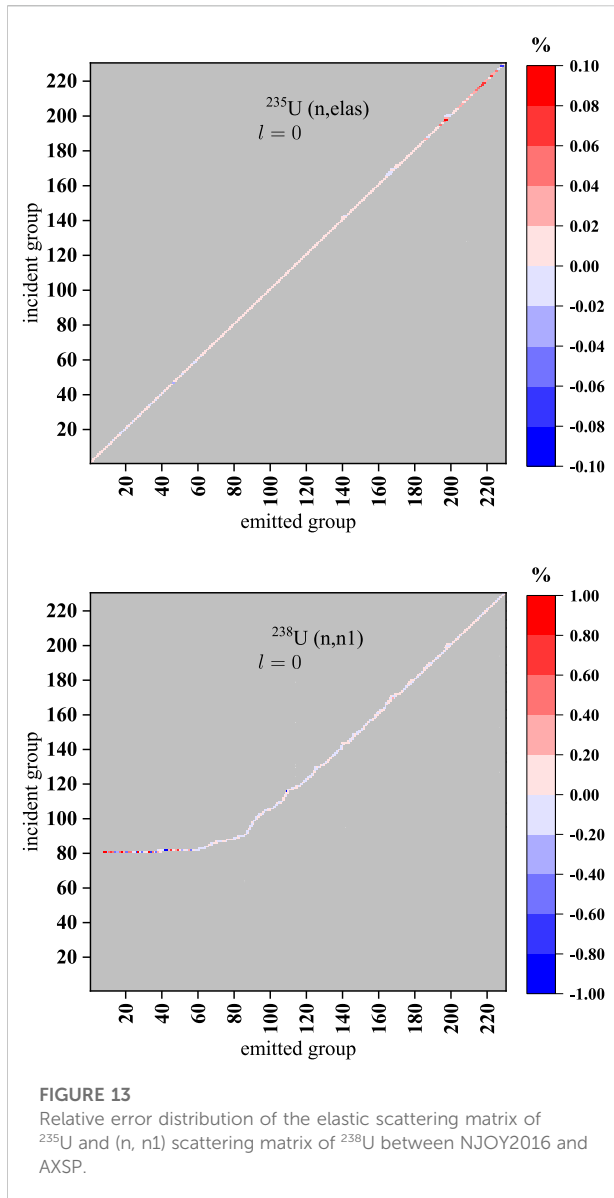
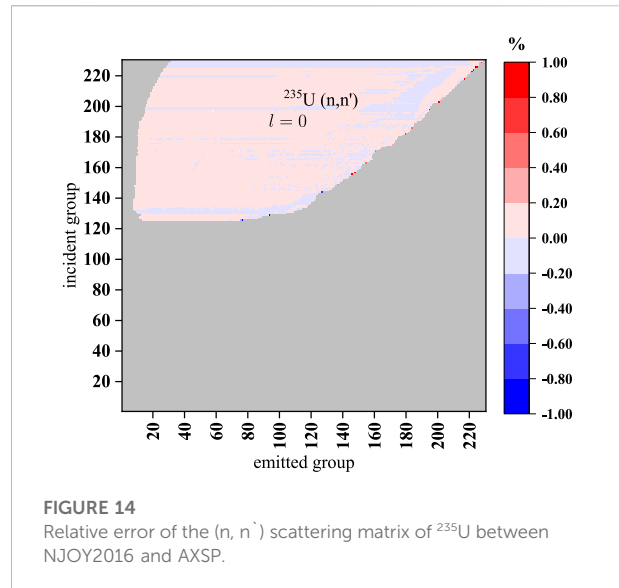


Figure 7, when the background cross section is very large, there is almost no improvement by consideration of the overlap integrals. However, the improvement is more pronounced when the background cross section is relatively small and the self-shielding effects are strong.

The calculation accuracy of the reactor physics is directly related to the calculation accuracy of the multigroup cross section. To verify the accuracy of the multigroup cross section generated by the GroupXS module and to facilitate the comparison with the calculation results of the NJOY2016 results, the ANL-230 energy group structures and the Bondarenko method were used to calculate the multigroup cross section and group-to-group matrix. The self-shielding cross section with different background cross sections was



calculated. Currently, the GroupXS module can process the average cross sections and scattering matrices of all reaction channels in the Evaluated Nuclear Data File with the ENDF-6 format. These Evaluated Nuclear Data Files mainly include ENDF/B-VII.1, ENDF/B-VIII.0, and CENDL-3.2. Taking ENDF/B-VII.1 as an example, the number of materials in ENDF/B-VII.1 for specific file 5 formats for total fission, first-chance neutron-induced fission, and  $(n, 2n)$  reactions are shown in Table 3. A total of 261 materials were given in the format of file 5, in which the number of materials given by the  $(n, 2n)$  reaction in the file 5 format is 176, and among these 176 materials, 158 of which are given in the data format of LF = 1, and the rest are given in the data format of LF = 9. Different LF numbers represent different energy distribution laws. The LF = 1 law is the arbitrary tabulated function, and the LF = 9 law is the evaporation spectrum.

The average cross sections calculated by GroupXS (Hu et al., 2022) and GROUPE for different isotopes and different reaction types are shown in Figure 8 ~ Figure 12. The average total cross sections of  $^{235}\text{U}$ ,  $^{238}\text{U}$ , and  $^{239}\text{Pu}$  with the background cross section  $\sigma_0 = 0.5\text{barn}$  and 0-th order Legendre polynomial are shown in Figure 8. The average elastic cross sections of  $^{23}\text{Na}$ ,  $^{208}\text{Pb}$ , and  $^{209}\text{Bi}$ , the average inelastic cross sections of  $^{239}\text{Pu}$ ,  $^{240}\text{Pu}$ , and  $^{241}\text{Pu}$ , the average fission cross sections of  $^{232}\text{Th}$ ,  $^{235}\text{U}$ , and  $^{239}\text{Pu}$ , and the average capture cross sections of  $^{235}\text{U}$ ,  $^{237}\text{Np}$ , and  $^{239}\text{Pu}$  with the background cross section  $\sigma_0 = 0.5\text{barn}$  are shown in Figures 9–12, respectively. In general, the value of the background cross section represents the strength of the resonance self-shielding effect. The smaller the background cross-section value, the stronger the resonance self-shielding effect is. The larger the background cross-section value, the weaker the resonance self-shielding effect is. For example, for the background section, if it is infinite, it means that there is no

TABLE 4  $k_{eff}$  results for different critical benchmarks.

Benchmark	NJOY2016	AXSP	Difference/pcm
hmf1	1.00010	1.00024	14
HMF2	1.00214	1.00225	11
HMF41	1.00448	1.00459	11
IMF3	1.00312	1.00319	7
IMF4	1.00739	1.00745	6
IMF6	1.00151	1.00157	6
pmf2	0.99431	0.99430	-1
pmf5	0.99937	0.99937	0
pmf6	0.99685	0.99685	0
pmf9	1.00526	1.00539	13
pmf10	0.99623	0.99623	0
pmf23	0.99635	0.99635	0
pmf25	0.99925	0.99928	3
umf1	0.99996	1.00010	14
umf2	0.99924	0.99935	11
umf4	0.99981	0.99993	11

resonance self-shielding effect. The case where the background cross section is relatively small is selected for cross-section comparison because the cross section in this case is more difficult to calculate accurately. As shown from Figures 8–12, the results of GroupXS are in good agreement with those of GROUPR, and the maximum error is less than 0.005%. The relative error of elasticity of  $^{235}\text{U}$ , the (n, n1) scattering matrix of  $^{238}\text{U}$ , and the (n, n') scattering matrix of  $^{235}\text{U}$  are given in Figures 13, 14. As seen from the previous figures, for almost all the group-to-group scattering matrix, the relative error is less than 0.1%. Therefore, the scattering matrix calculated by GroupXS is correct, and it can be used for future reactor calculation.

## Critical benchmark verification

To verify the accuracy of the multigroup cross sections generated by AXSP, the criticality benchmarks from the International Criticality Safety Benchmark Evaluation Project (ICSBEP) are used. The reason why these critical benchmarks are selected to verify the accuracy of multigroup cross sections is that the energy spectrum of these critical devices is mostly hard, and the neutrons are mostly concentrated in the middle- and high-energy regions. In these energy regions, the cross sections generated by the Bondarenko method, which is used in AXSP and NJOY, have higher accuracy.

The effective multiplication factor  $k_{eff}$  for different critical benchmarks is shown in Table 4. As shown in Table 4, the  $k_{eff}$  results calculated by the AXSP program agree very well with the results calculated by NJOY 2016. The difference is defined as the results of AXSP minus the results of NJOY2016. The maximum

TABLE 5  $k_{eff}$  results for ZPR6/7.

	ACER	ACEXS	Difference/pcm
$k_{eff}$	0.98714	0.98708	6

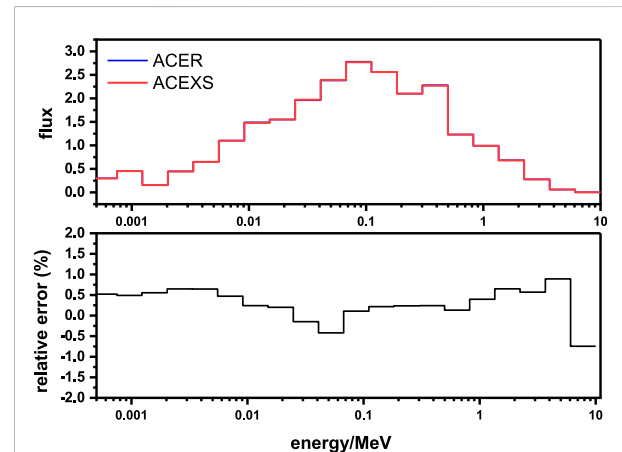


FIGURE 15  
Neutron flux of the inner core for the ZPR6/7 benchmark with a different nuclear library.

difference is 14 pcm. Compared with the experimental results, almost all the errors are less than 500 pcm, except IMF4 and pmf2 benchmarks, and the reason for the bias needs further study.

## ACE format library generation

To verify the ability of the ACEXS module to generate the ACE format section library, ZPR6/7 was selected because of its fast neutron spectrum. The loading of ZPR-6 Assembly 7 (Smith et al., 2003) began in July 1970, and experiments on this assembly continued through October 1971. The particular configuration judged most suitable for a criticality safety benchmark was Loading 12 with a fissile loading of 15.4 kg  $^{235}\text{U}$  and 1118.1 kg  $^{239}\text{Pu} + ^{241}\text{Pu}$ . The specifications of this experiment are provided in the “International Handbook of Evaluated Reactor Physics Benchmark Experiments” under the name “ZPR-LMFR-EXP-001” in the liquid metal fast reactor chapter. The homogeneous R-Z model and associated dimension are shown in Smith et al. (2003).

The ACE format nuclear library was generated based on the ENDF/B-VII.1 evaluated nuclear data file by using NJOY2016 and AXSP. In this calculation, the ACEXS module of AXSP was used to generate the library. However, the resonance reconstruction and the other module of NJOY2016 were applied. The reactor Monte Carlo RMC,

which was developed by Tsinghua University, was used to calculate the ZPR6/7 benchmark.

The  $k_{eff}$  results (Ma et al., 2022) for ZPR6/7 with different modules are shown in Table 5. As shown in Table 5, the  $k_{eff}$  results calculated by the ACEXS module are in good agreement with those of the ACER module, and the difference is only 6 pcm. The neutron flux of the inner core (Ma et al., 2022) is shown in Figure 15. As shown in Figure 15, the relative error is less than 0.5%. Therefore, the nuclear library processed by the ACEXS module is in good agreement with that of ACER of NJOY.

## Conclusion

In this study, a new nuclear process code AXSP was developed, and the basic function of the process-evaluated nuclear data file has been verified by using NJOY2016. The critical benchmarks from the ICSBEP handbook were used to verify the multigroup cross section, and the effective multiplication factor maximum difference between AXSP and NJOY2016 is 14 pcm. The ZPR6/7 benchmark was used to verify the ACE format library generation for the Monte Carlo code, and the  $k_{eff}$  results calculated by the ACEXS module are in good agreement with that of the ACER module, and the difference is only 6 pcm. Therefore, the results of AXSP are in good agreement with that of NJOY2016. Compared with the NJOY program, the precision of the unresolved resonance processing module UnresXS has been significantly improved due to the adoption of a more accurate solution method and the consideration of in-sequence overlap integrals. The improvement is more pronounced when the background cross section is relatively small and the self-shielding effects are strong. The time consumption of PUnresXS has been decreased significantly due to an optimized sorting algorithm. The computation time using the shell sort algorithm is 18% of the computation time of the bubble sort algorithm, or less. After using the shell sort algorithm, the calculation time is significantly reduced, and the calculation speed is significantly improved. In the future, we will use the method of solving the continuous energy neutron transport equation to obtain the energy spectrum in order to obtain more accurate multigroup cross sections, and the module

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of processing the MATXS format library, and Wims-D and Wims-E format libraries will also be developed (Lim et al., 2018).

## Data availability statement

The original contributions presented in the study are included in the article/Supplementary Material. Further inquiries can be directed to the corresponding author.

## Author contributions

KH: GroupXS module development and data analysis. XbM: supervision, conceptualization, methodology, and software. XaM: ACEXS module development and data analysis. YH: data analysis and check. CZ: UnresXS module development and data analysis. YC: supervision and conceptualization.

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## Conflict of interest

The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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