



# Research on Efficient Soft Switching Based on MPPT of PV Power Generation System

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In this paper, basic soft-switching technology is proposed based on hard switching, and then the basic soft-switching technology is optimized, and an improved soft-switching technology is proposed to improve the conversion efficiency by reducing the switching loss. The simulation results show that the conversion efficiency of hard and basic soft switching is 94.3 and 96.1%, but the conversion efficiency of improved soft switching optimized on the basis of basic soft switching is only 95.8%. To solve this problem, an innovative soft-switching technology is put forward in this paper, and its conversion efficiency is as high as 96.3%, which is superior to the basic soft-switching technology.

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## INTRODUCTION

With coal, oil, natural gas, and other fossil fuels increasingly being exhausted, the problem of energy shortage in the world has gradually emerged (Hirsch, 2008; Luo G. et al., 2021; Freeman et al., 2020), and the development of new green energy has become the only way to solve such problems (Hojnik et al., 2021). At present, the newly developed green energy sources include solar, wind, tidal, and geothermal energy and so on (Burnett and Hefner, 2021; Darwesh and Ghoname, 2021; Luo X. et al., 2021; ZOU et al., 2021). The most reliable and convenient energy among these new energy sources is solar energy. This paper includes how to use solar energy efficiently to maximize the conversion efficiency of a photovoltaic (PV) power-generation system. A solar PV power-generation system has the following advantages: pollution-free energy, a flexible application site that is not interfered with by geographical location, high power quality, low loss, and multiple policy support (Qi et al., 2021).

To improve the conversion efficiency of a PV power-generation system, soft-switching technology is proposed in this paper (Aiswariya et al., 2021; Engelkemeir et al., 2019; Genc and Koc, 2017; Yinghua et al., 2012; Pakdel and Jalilzadeh, 2016). As early as the early 1970s, foreign scholars put forward series and parallel resonance (Tkachenko and Baklanov, 2015), and soft-switching technology just uses resonance principles to make the current or voltage in the switching device change sinusoidally and implement a quick soft shutdown and soft open. Soft-switching converters can be divided into four types: ZCS-PWM, ZVS-PWM, ZCT-PWM, and ZVT-PWM. This paper mainly introduces ZVT-PWM. The reason why the ZVT-PWM converter is adopted is that the ZVT converter can avoid the problem of excessive turn-off loss caused by diode reverse recovery and greatly improves conversion efficiency (Ismail and Sebzali, 1998; Jahdi et al., 2011; Kumar et al., 2015).

In the second section, according to the physical equivalent circuit model of PV cells, the output characteristics of PV modules are simulated. The third section introduces the topological structure of basic and improved soft switching. *Simulation and Experimental Analysis* is based on Multisim to

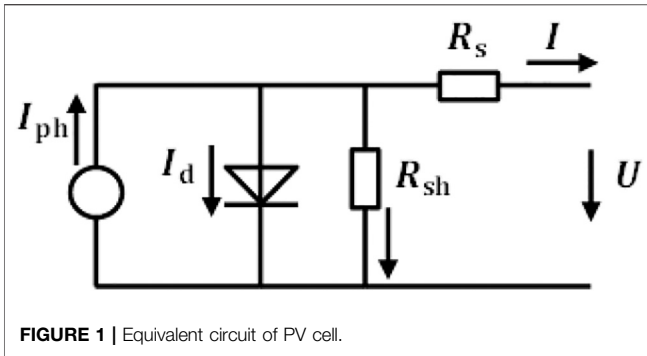


FIGURE 1 | Equivalent circuit of PV cell.

build a DC-DC BOOST circuit (Mirzaei and Rezvanyvardom, 2020; Faraji et al., 2019; Charin et al., 2013; Pahlavandust and Yazdani, 2020; Öztürk et al., 2018). First, IRFZ24N, a power switch tube suitable for a high-frequency circuit environment and a Schottky diode MBR7545 with a moderate forward voltage drop and a large reverse voltage value are selected from Multisim, and the duty ratio in the circuit is analyzed according to the maximum power point (MPP) of the PV module. Then, Proteus is used to reduce the time of tracking the MPP. Finally, to reduce the switching and conduction loss and improve the conversion efficiency, an innovative soft-switching technology is introduced and compared with the basic soft-switching technology, and the improved soft-switching technology shows the superiority and innovation of innovative soft switching in all aspects.

## SINGLE- AND MULTIPLE PEAK OUTPUT CHARACTERISTICS OF PHOTOVOLTAIC ARRAY

A PV cell is a kind of nonlinear DC power supply, which cannot be supplied at will. The equivalent circuit of a PV cell is shown in Figure 1.

The equivalent circuit model is as follows:

$$I = I_{ph} - I_0 \left( e^{\frac{q(U+IR_s)}{AKT}} - 1 \right) - \frac{U + IR_s}{R_{sh}}, \quad (1)$$

in which  $I$  is the output current of the solar panel,  $U$  is the output voltage of the solar panel,  $I_0$  is the PN junction reverse saturation current,  $I_{ph}$  is the battery photoelectric current,  $q$  is the electron charge,  $A$  is the coefficient of the diode,  $k$  is the Boltzmann constant,  $T$  is the temperature, and  $n$  is the diode factor. The current flowing through the equivalent shunt resistor  $R_{sh}$  is shown as  $I_{sh}$  as follows:

$$I_{sh} = \frac{U + IR_s}{R_{sh}}. \quad (2)$$

Because the resistance value of the equivalent series resistance is extremely small, it can be almost ignored, and the resistance value of the equivalent parallel resistance is large, so  $I_{sh}$  is very small and can be ignored. Therefore, the electrical performance characteristics of the PV cell can be simplified as follows:

$$I = I_{ph} - I_0 \left( e^{\frac{q(U+IR_s)}{AKT}} - 1 \right). \quad (3)$$

The models of the above equivalent circuits are all based on the standard  $T = 300\text{K}$ ;  $A \approx 2.8$ ;  $q = 1.6 \times 10^{-19}\text{C}$ ;  $k = 1.38 \times 10^{-23}\text{J/K}$ .

## Output Characteristics of Photovoltaic Array Without Shading

Under the condition of no shading, the single-peak characteristic curve is obtained without considering the external environmental factors. In this section, under the standard environmental conditions ( $1000\text{ W/m}^2$ ,  $25^\circ\text{C}$ ), the characteristic curves of the unshaded PV cells are simulated experimentally by Simulink Figures 2, 3.

At the same temperature, with the PV cell value changed, the PV array parameters of uniform simulation are as follows Table 1 and Table 2:

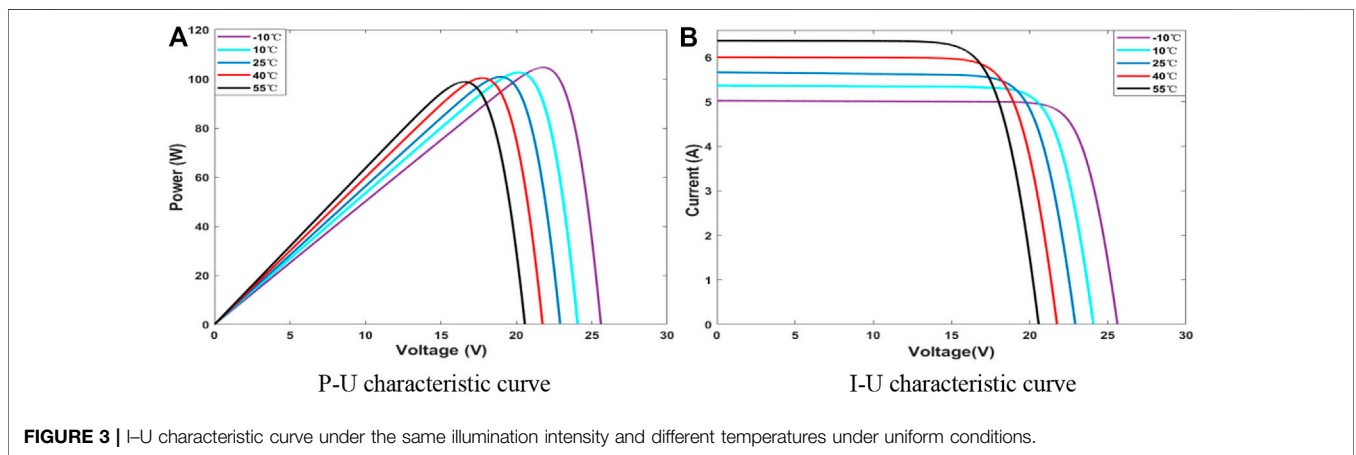
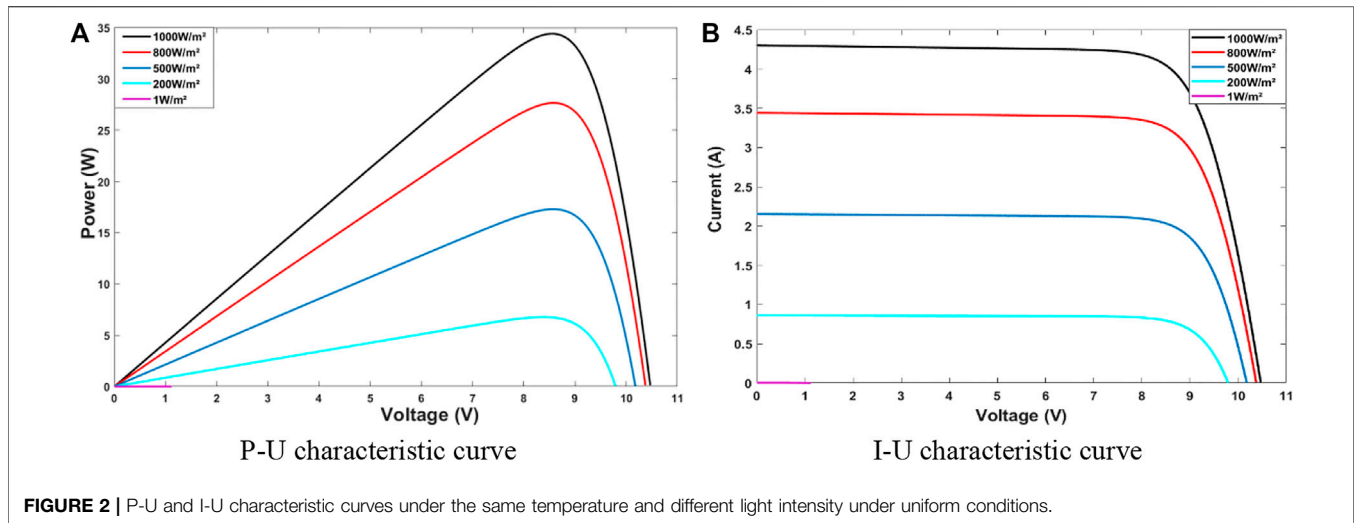
Parameters of the PV array simulated uniformly under the same illumination and changing temperature are as follows:

Through the simulation results, it can be seen that the single peak point in the P-U simulation diagram is generally on the right side, and the output power of PV modules first increases and then decreases with the increase of output voltage while the output current remains unchanged and then decreases rapidly with the increase of output voltage.

## Output Characteristics of Photovoltaic Array With Shading

This section mainly shows that, in practical engineering applications, PV modules are interfered with by various factors, such as surface dust and dark clouds, which lead to the output power of some PV modules being significantly lower than other parts and accordingly bringing about the phenomenon of multiple peaks or inflection points (Veerapen and Wen, 2016; Mirza et al., 2019; Zhou et al., 2021). Three PV panels are connected in series to form a PV array, and each PV panel is connected in reverse parallel with a bypass diode. However, due to the shunt effect of the bypass diode, the PV arrays do not match, resulting in multiple local extreme points in the P-U characteristic curve, named multi-peak characteristics. In this section, the PV array is simulated by Simulink with different illumination intensities at the standard atmospheric temperature to study the condition with shading. The parameters are shown in Table 3:

Through the simulation experiment in Figure 4, it can be concluded that the P-U characteristic curve of the PV array with different illumination intensities under the shading condition presents multi-peaks. Taking Group 2 in Table 3 as an example, there are three local MPPs in the P-U characteristic curve of the PV array when the open circuit voltage of the PV array is  $U_{oc-array} = 10.4\text{ V}$  and the open circuit voltage of the PV cell is  $U_{oc-module} = U_{oc-array}/3 \approx 3.47\text{ V}$ . The voltages corresponding to the three local MPPs are  $U_{mpp1} = 1.97\text{ V} \approx 0.75 \times U_{oc-module}$ ,  $U_{mpp2} = 5.1\text{ V} \approx 2 \times 0.75 \times U_{oc-module}$ ,  $U_{mpp3} = 8.4\text{ V} \approx 3 \times 0.75 \times U_{oc-module}$ . Thus, it can be drawn that, for an  $n \times m$  PV array, there



are only local MPPs-n, and the voltage value corresponding to each local MPP is generally  $k \times 0.75 \times U_{oc-module}$ .

Through some references and practical research simulation experiments, this paper concludes that, for an  $n \times m$  PV array, the total number of cells is  $m$ , and the total number of different voltage differences of cells is  $n$ . The characteristics of each single cell in the PV array are basically the same, so the output characteristics have nothing to do with which specific cell is shaded and only with the overall parameters in the PV array. If the shading situation is the same, the output characteristics of the PV array must be basically the same.

## RESEARCH ON SEVERAL SOFT-SWITCHING TECHNOLOGIES

### Traditional Hard-Switching and Basic Soft-Switching Technology

The switching tubes of traditional Boost circuits generally operate in a hard-switching mode during the switching

process. Hard switching began to develop in the 1960s, and it greatly reduced the volume and weight of the device and improved the overall efficiency. However, the power switch tube of the DC-DCPWM converter, which works in a series of hard-switching conditions, is accompanied by the increase of switching frequency and produces serious electromagnetic interference (EMI), which greatly reduces efficiency (Khaled et al., 2020).

According to the power electronics textbook (Society, 1981), the integral of switching on and off loss of the switch tube under the hard-switching technology is expressed as follows.

$$\text{Open : } W_{on} = \int_0^{t_{on}} v_s i_s dt \quad (4)$$

$$\text{Turn off : } W_{off} = \int_0^{t_{off}} v_s i_s dt \quad (5)$$

The total losses of turn on and off in that cycle are

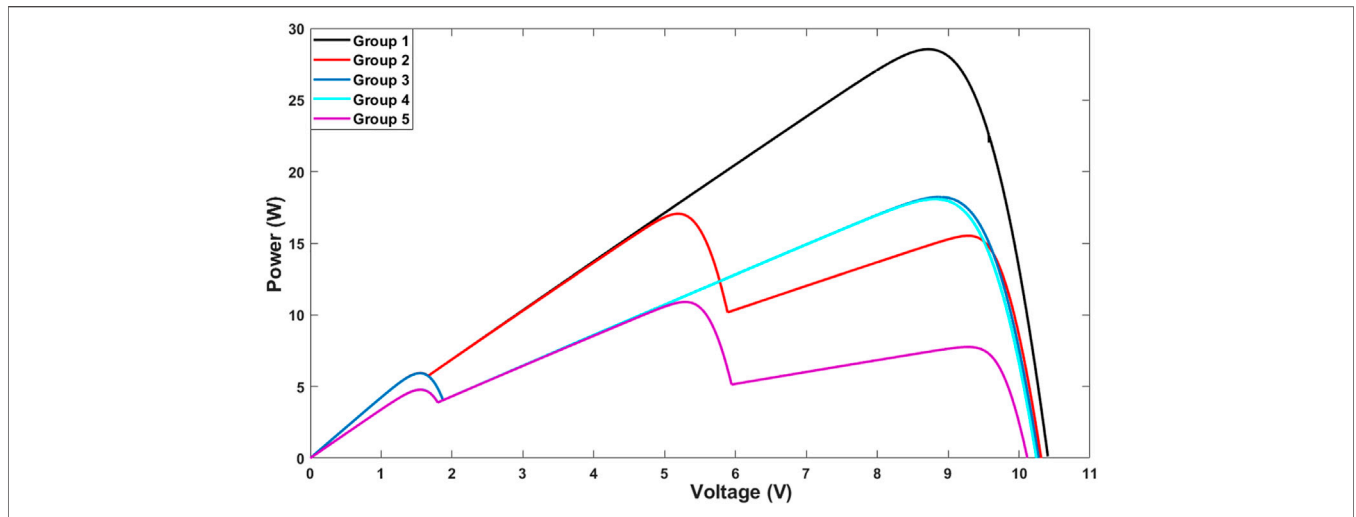


FIGURE 4 | P-U characteristic curve of different illumination intensity under shielding condition.

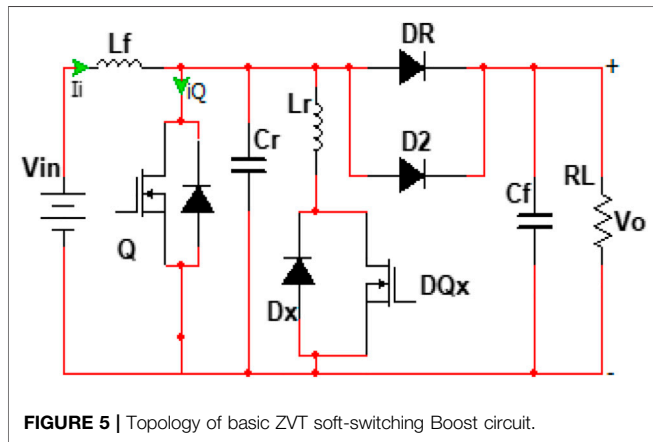


FIGURE 5 | Topology of basic ZVT soft-switching Boost circuit.

$$\text{Open : } W_{\text{on}} = \int_0^{t_{\text{on}}} v_s i_s dt \quad (6)$$

$$\text{Turn off : } W_{\text{on}} = \int_0^{t_{\text{on}}} v_s i_s dt \quad (7)$$

Among them,  $t_{\text{on}}$  is the opening time and  $t_{\text{off}}$  is the turn-off time;  $f_s$  is the switching frequency,  $v_s$  and  $i_s$  are the voltages at both ends of the switching tube and the passing current, respectively. There are still many shortcomings of hard switching, such as large switching tube loss (switching loss increases in proportion to switching frequency), poor recovery performance of diodes, capacitive on and inductive off, and serious EMI (Emami et al., 2010). As can be seen, to overcome these existing problems, scholars at home and abroad have implemented improvements on the basis of hard switching and formed soft-switching technology.

Interrupt capability transformation through abrupt switching processes is called hard switching, and the soft-switching process resonates through inductance L and capacitance C. In this paper, to improve the conversion efficiency of the PV power-generation system, basic soft-switching technology is proposed first. Figures 5, 6 are the Boost circuit topology and the main power waveform diagrams of basic soft switching, respectively.

As can be seen from Figure 6, although basic soft switching has achieved great optimization compared with traditional hard switching, basic soft switching also has many disadvantages. 1) In the case of high-input voltage and light load, the zero voltage condition is almost difficult to meet. 2) Interval and circulation energy need to be dealt with in one switching cycle. 3) Although the basic soft-switching technology improves the efficiency of the main power switch device in the circuit, the auxiliary switch tube is still in the hard-switching state, which results in switching loss

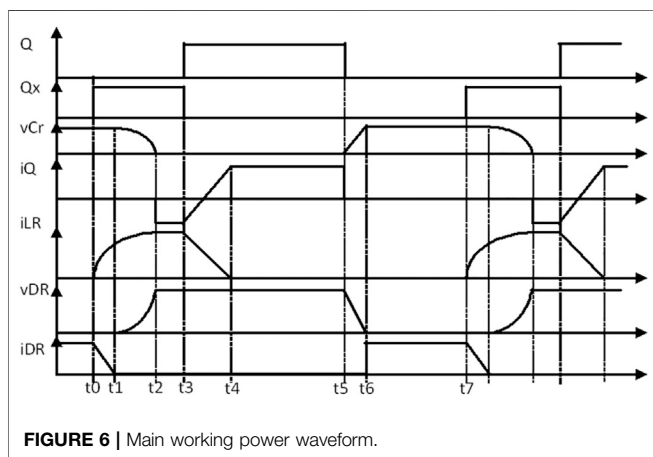
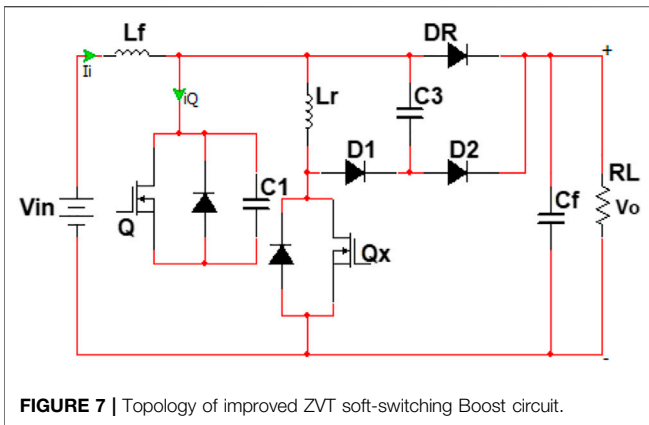


FIGURE 6 | Main working power waveform.



that cannot be ignored. Even the switching loss offsets part of the loss that is reduced due to soft switching, which gives rise to the difficulty in improving the efficiency of the whole circuit.

### Improved Soft Switching

In 2004, H. Bodur and A.F. Bakan proposed an improved soft-switching topology as is shown in **Figure 7**. Based on the basic ZVT-PWM Boost converter soft-switching topology, only by adding a diode and a capacitor to the auxiliary resonance network can both the main switch and the auxiliary switch complete soft switching and become improved soft switching (Simon and Das, 2014).

Before discussing **Figure 7**, the following assumptions should be made: All components of the circuit are ideal. The capacitance of the output filter is relatively large enough, and the  $C_f$  and  $R_L$  of one switching period can be replaced by a constant voltage source  $V_o$ . The inductance of the input filter is relatively large enough, and  $V_{in}$  and  $L_f$  of one switching cycle can be replaced by a constant current source  $I_i$ . The reverse recovery time of the diode is ignored (Kang et al., 2012; Moshksar and Ghanbari, 2018).

The first four time periods in **Figure 7** are in the resonance process, and at the end of the fourth time period, the following two modes are discussed according to whether the voltage at both ends of  $C_3$  can resonate and rise to  $V_o$ . Mode 1 represents the case in which the energy storage of the resonant inductor is small, and the duration of one complete cycle is

$$T_7 = t_7 - t_6 = \frac{I_{Lrm} Z_3 (C_1 + C_2 + C_3)}{I_i} \tag{8}$$

It satisfies the initial conditions:

$$\begin{cases} v_{C1} = V_o - I_{Lrm} Z_3 + \frac{I_i}{(C_1 + C_2 + C_3)} (t - t_6) \\ v_{C2} = V_{C3} = I_{Lrm} Z_3 - \frac{I_i}{(C_1 + C_2 + C_3)} (t - t_6), \end{cases} \tag{9}$$

$$\begin{cases} i_{C1} = \frac{C_1 I_i}{(C_1 + C_2 + C_3)} \\ i_{C2} = \frac{C_2 I_i}{(C_1 + C_2 + C_3)}, \\ i_{C3} = \frac{C_3 I_i}{(C_1 + C_2 + C_3)} \end{cases} \tag{10}$$

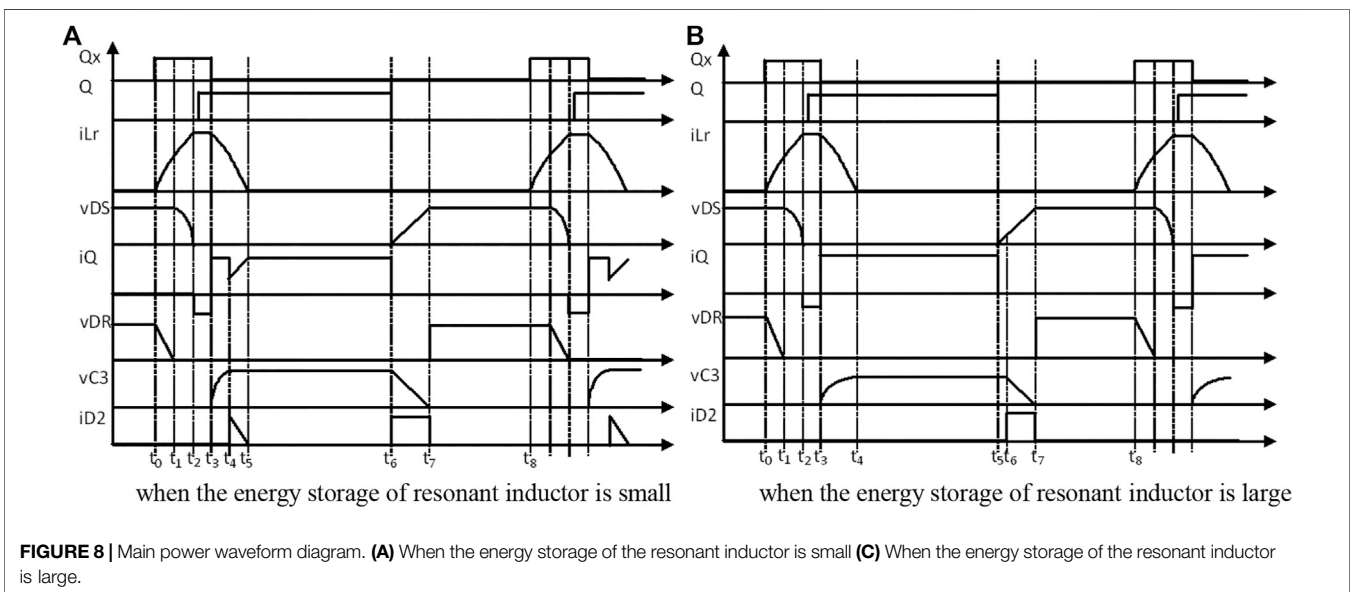
Mode 2 represents the case in which the resonant inductance is large, and the duration of a complete cycle is

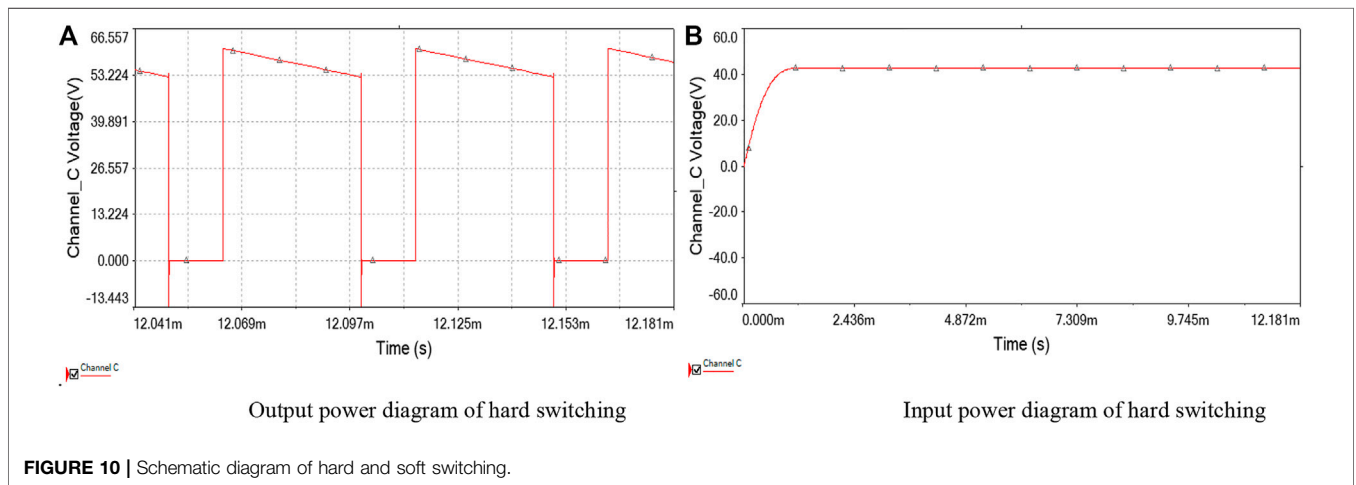
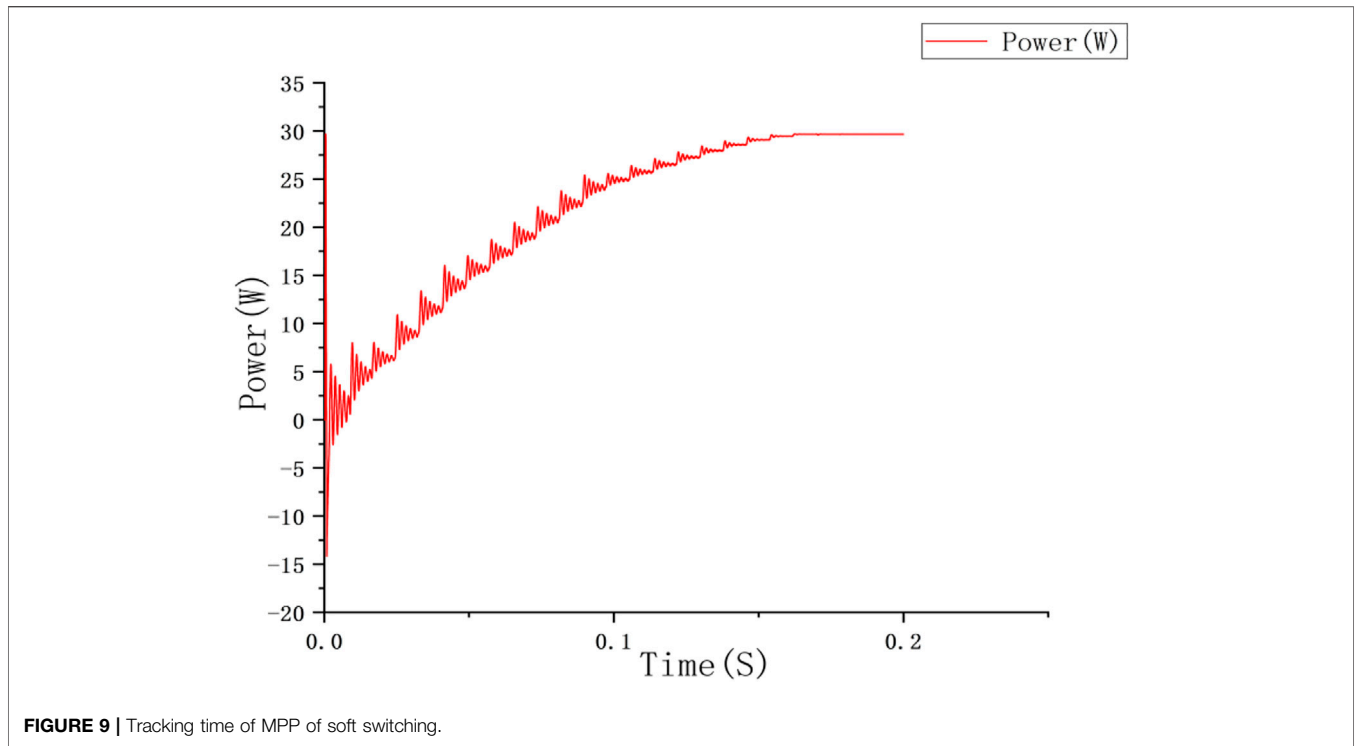
$$T_7 = t_7 - t_6 = \frac{V_o (C_1 + C_2 + C_3)}{I_i} \tag{11}$$

Initial conditions are

$$\begin{cases} v_{C1} = \frac{I_i}{(C_1 + C_2 + C_3)} (t - t_6) \\ v_{C2} = V_{C3} = V_o - \frac{I_i}{(C_1 + C_2 + C_3)} (t - t_6). \end{cases} \tag{12}$$

It can be seen from **Figure 8** that improved soft switching overcomes the fatal defect of basic soft switching; that is, the





switching loss is too large, but improved soft switching increases the conduction loss of the auxiliary switch tube, which makes it difficult to improve the overall conversion efficiency of the circuit.

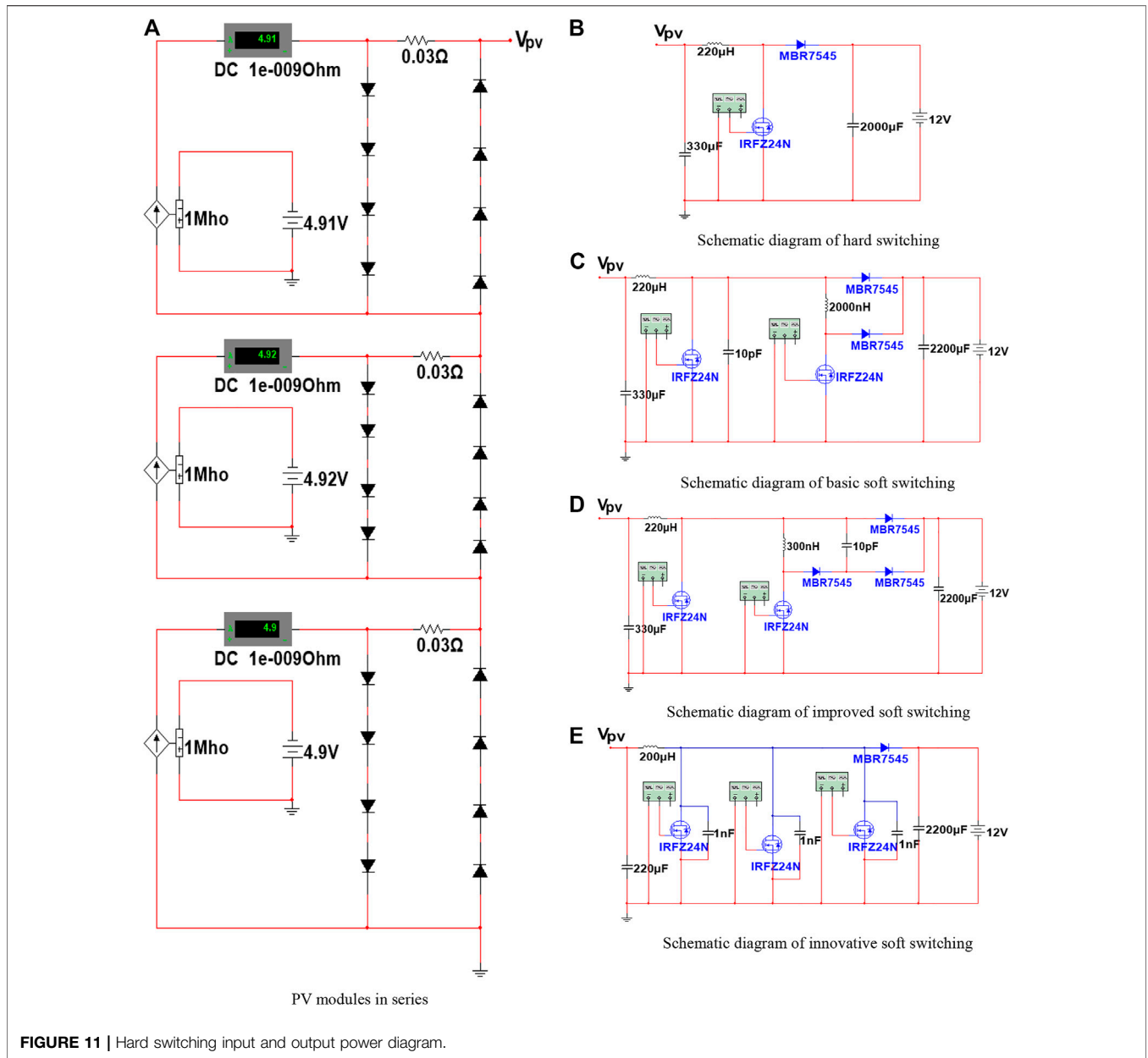
### SIMULATION AND EXPERIMENTAL ANALYSIS

The MPP of PV modules is found based on Multisim, and the duty cycle is adjusted according to the MPP. The advantages and disadvantages of basic and improved soft switches are analyzed. On this basis, an innovative soft-switching technology is proposed

to reduce the switching and conduction losses of auxiliary switch tubes. In this section, the MPP is tracked in Proteus first, and then three different methods are adopted to compare and analyze the four technologies in this paper to verify the efficiency and feasibility of the innovative soft-switching technology.

$$t_{duk} = 0.16 * (2.45 * e_k - 0.5 * e_{k1} + 0.7 * e_{k2}). \quad (13)$$

**Figure 9** uses Proteus to simulate and track the MPP. The experimental results show that the parameters in **Eq. 13** are superior to other parameters that can greatly speed up the tracking speed, there is no oscillation near the MPP, and the average tracking time is only 163 ms.



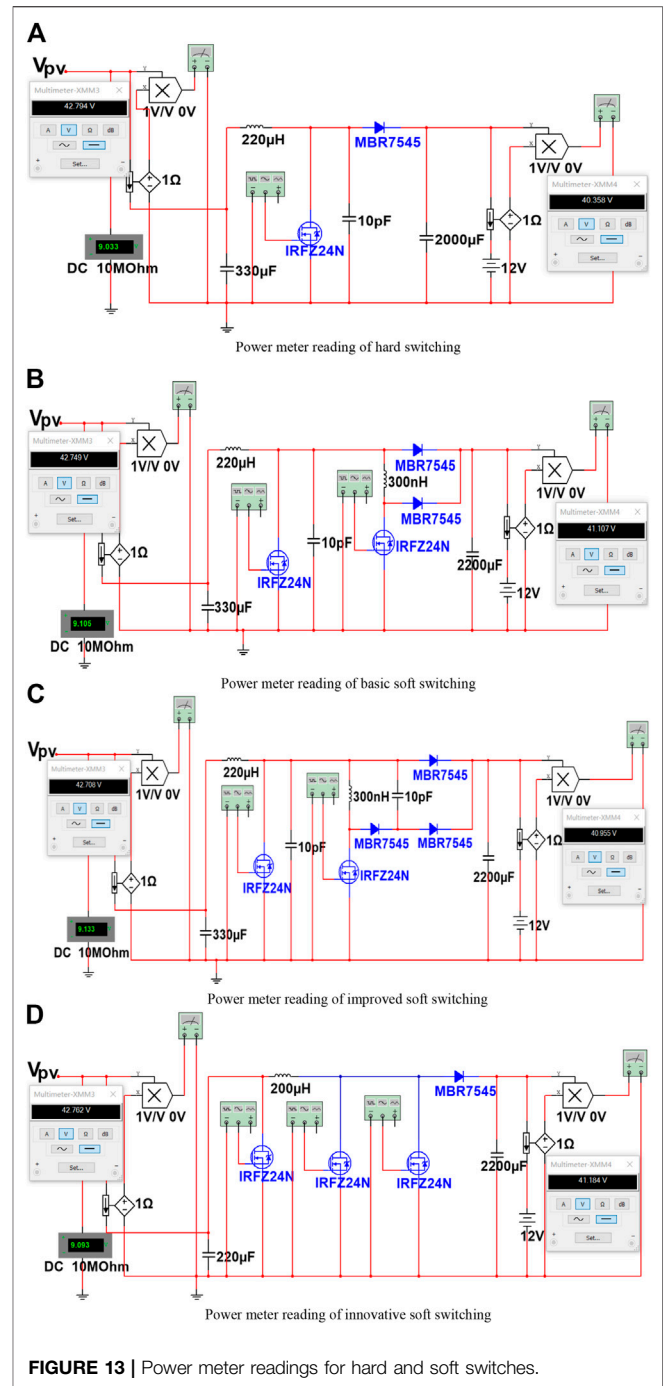
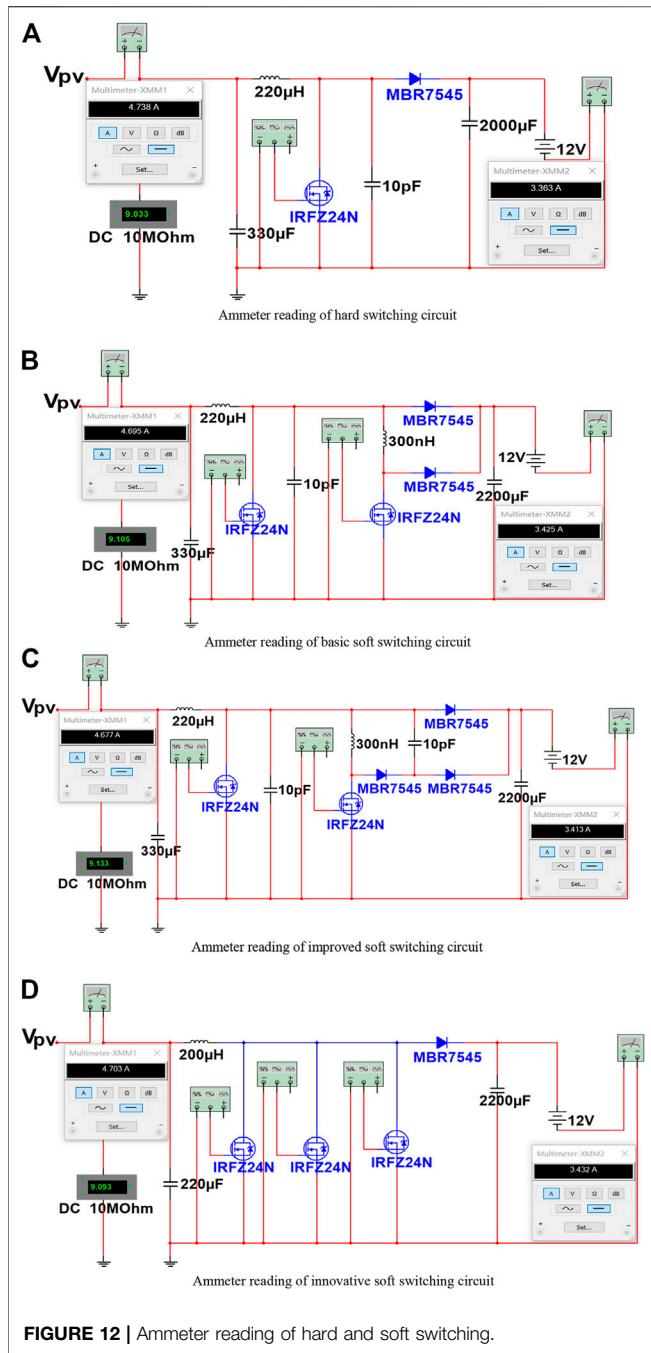
### Oscilloscope Area Method

Under the frequency of 20 KHZ and standard experimental conditions, the hard switches and various types of soft switches are simulated, respectively, and their areas are calculated. The conversion efficiency is obtained by dividing the output area by the input area. To make the calculation result more accurate, this paper adopts the average value of 30 calculation results.

In a period of 0.00005 s, around the MPP voltage of 9.067 V, adjust the duty cycle of the hard soft switching so that the input voltage of the hard soft switching is close to the MPP voltage. Read at this time. The simulation results in **Figure 10** show that the conversion efficiency of the hard switching is about 94.382%. Similarly, the other three soft-switching technologies are

measured with this method. The simulation results show that the conversion efficiency of basic soft switching is about 96.181%, that of improved soft switching is about 95.950%, and that of innovative soft switching is about 96.398%.

The improved soft switching adds a capacitor and a diode based on basic soft switching, and they can improve the conversion efficiency by reducing the switching loss in theory. However, the increased Schottky diode greatly increases the diode conduction loss while reducing the switching loss, so the conduction loss is far greater than the switching loss. Innovative soft switching is improved on the basis of these two types of soft switches. Simulation results show that the conversion efficiency is the highest, which proves the high efficiency of innovative soft switching. To verify the accuracy



of this method, two other different methods are applied to calculate the conversion efficiency and compared with this method to obtain accurate values.

### Product Method of Ammeter and Voltmeter

In this section, the product methods of ammeter and voltmeter are used to compare with the oscilloscope area method and verify the accuracy of the conversion efficiency. On the basis of the schematic diagram in Figure 11, the input and output terminals are connected in series with a multimeter and then adjusted to the current level, and the corresponding power is calculated

**TABLE 1 |** PV arrays under the same temperature and different voltage values (illumination intensity).

G	S <sub>1</sub> W/m <sup>2</sup>	S <sub>2</sub> W/m <sup>2</sup>	S <sub>3</sub> W/m <sup>2</sup>	Result (Figure 2)
1	1,000	1,000	1,000	Black
2	800	800	800	Red
3	500	500	500	Blue
4	200	200	200	Cyan
5	1	1	1	Purple



**TABLE 2** | PV arrays at different temperatures with the same voltage (light intensity).

G	T(°C)	Result (Figure 3)
1	-10	Black
2	10	Red
3	25	Blue
4	40	Cyan
5	55	Purple

**TABLE 3** | PV array under shielding condition.

Group	S <sub>1</sub> W/m <sup>2</sup>	S <sub>2</sub> W/m <sup>2</sup>	S <sub>3</sub> W/m <sup>2</sup>	Verification result (Figure 4)
1	1,000	800	800	Black
2	1,000	800	400	Red
3	1,000	500	500	Blue
4	800	500	500	Cyan
5	800	500	200	Purple

**TABLE 4** | Statistics on conversion efficiency.

method category	Oscilloscope area (%)	Product method of ammeter and voltmeter (%)	Multimeter direct reading (%)
HS	94.382	94.293	94.308
BSS	96.181	96.145	96.159
ImSS	95.950	95.882	95.895
InSS	96.398	96.305	96.310

according to the values of the input and output current at this time.

According to the method of MPP in *Oscilloscope Area Method*, the simulation results show that the conversion efficiency of hard switching in **Figure 12** is about 94.293%, that of basic soft switching is about 96.145%, that of improved soft switching is about 95.882%, and that of innovative soft switching is about 96.305%.

### Multimeter Direct Reading Method

To verify which method, 4.1 or 4.2, is more accurate, this section connects a multimeter to the input and output ends, respectively, based on the schematic diagrams of various types of hard and soft switches. Unlike the second method, there is no specific current source in Multisim, so this method uses a current-controlled voltage source to convert the voltage signal and then connects the multiplier to the multimeter and finally adjusts the multimeter to the voltage level.

Under the experimental conditions in *Oscilloscope Area Method* and *Product Method of Ammeter and Voltmeter*, the conversion

efficiency of hard switching in **Figure 13** is about 94.308%, that of basic soft switching is about 96.159%, that of improved soft switching is about 95.895%, and that of innovative soft switching is about 96.310% **Table 4** is the data summation.

## CONCLUSION

The innovative soft switching proposed in this paper can effectively optimize the dynamic and steady-state performance of MPPT and greatly shorten its average tracking time. In addition, this method is simple, convenient, and has little efficiency loss. The fourth section uses Multisim to calculate the conversion efficiency of four kinds of hard and soft switches with three different measuring methods. The experimental results show that the measured results are almost equal, and the error is only within 0.1%. Second, it also verifies that improved soft switching optimizes the shortcomings of basic soft switching, but it also has a more fatal problem. To solve this problem, innovative soft switching is proposed in this paper. Simulation results show that the conversion efficiency of innovative soft switching can reach 96.3%, and its tracking speed is also the most efficient. It can be seen from **Figure 9** that MPP can be tracked in only 162 ms.

To sum up, innovative soft switching technology can greatly improve the conversion efficiency and average tracking time and promote the rapid development of the PV industry (Zhao and Wang, 2020).

## DATA AVAILABILITY STATEMENT

The original contributions presented in the study are included in the article/Supplementary Material, further inquiries can be directed to the corresponding author.

## AUTHOR CONTRIBUTIONS

PT: As the first author of the paper, I conducted simulation experiments and data modification, and completed the writing of the paper YC: Give guidance and provide literature JL: Check your paper for errors and Modify the format of the paper.

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