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Pressure prediction in deep-water pipeline considering formation of natural gas hydrate

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Pressure in the deep-water pipeline is an important parameter that should be carefully predicted to control the natural gas transport in petroleum industry. However the present methods to predict pressure along the deep-water pipeline are complex and time-consuming. Some methods even ignore the formation of natural gas hydrate leading to the inaccurate pressure prediction. In this work, we proposed a model to predict the pressure along the deep-water pipeline considering the reduction of pipeline radius induced by the formation of natural gas hydrate. The model was validated by experimental data and was applied to the real deep-water pipeline in China. Results indicate that the decline of pressure in the pipeline is mainly caused by the reduction of pipeline radius due to the formation of natural gas hydrate compared with the flow resistance caused by viscous flow. The decline of pressure becomes faster against time with the 40% pressure loss at the fifth year of natural gas transport. This model enables to obtain the pressure values in the deep-water pipeline with high accuracy and good convenience.

KEYWORDS

natural gas hydrate, pressure, blockage, pipeline, deep water

Introduction

Development and transport of oil and gas are significant in petroleum industry (Xu et al., 2018, Xu et al., 2019; Mo et al., 2020; Xu et al., 2020; Wang C. et al., 2021; Wang C. et al., 2022; Mo et al., 2022). The formation of natural gas hydrate is a great threat to the transport of natural gas in the deep-water pipeline (depth of water >1000 m) (Li et al., 2016; Ren, 2018). Natural gas transport in the deep-water pipeline is under complex conditions: 1) the complicated pipeline system affected by the pipeline design, pipeline laying, pipeline management, pipeline maintenance, etc.; 2) the extreme environment, especially the low temperature and high pressure; 3) the components of gas mixture, i.e., liquid or gaseous hydrocarbons, water, etc. Natural gas hydrate is likely to form at the low temperature (lower than around 11°C) and high pressure (higher than about 2.5 MPa) (Zhang et al., 2010), which is in accordance with the temperature and pressure conditions in the deep-water environment. As a result, the natural gas hydrate can easily form and grow inside the submarine pipeline during the transport of natural gas.

The formation of natural gas hydrate causes severe problems. Natural gas hydrate adheres to the inner pipeline surface, which reduces the pipeline radius and causes the loss of pipeline pressure. And the layer of natural gas hydrate at the pipeline surface can become thicker against time. If effective treatments are not carried out promptly, the pipeline can be blocked. The blockage caused by the natural gas hydrate, on the one hand, significantly reduces gas flow rate and severely affects gas transport. On the other hand, it damages the pipelines, valves and other transportation equipment (Gao, 2018). As the formation of natural gas hydrate causes various problems during natural gas transport in deep-water pipeline, the pressure inside pipeline is worth great attention. Because the pressure affects both the formation of natural gas hydrate and the gas transport efficiency (Li et al., 2013). An accurate prediction of pressure inside deep-water pipeline is of great significance.

The pressure along the deep-water pipeline can usually be obtained by two methods: experiment and numerical simulation. Li and Dong (2019) investigated 12 experimental pipelines worldwide and found that the pressure design inside the experimental pipelines was lower than the pressure in the real deep-water pipeline systems. Among the 12 pipeline systems, the high-pressure Petreco A/S pipeline system in Norway could reach the highest pressure of about 25 MPa (Li and Dong, 2019). However, the pipeline system in laboratory is still very different from the true deep-water environment. As a result, the pressure obtained from experiments is not able to reflect the accurate pressure in the real pipeline. Numerical simulation is an effective way to predict the pressure in the submarine pipeline. In 2003, the CSMHyK model was firstly built by the Center for Hydrate Research of Colorado University of Mines (Boxall, 2009; Davies, 2009; Zerpa et al., 2012). The model is utilized to describe the formation of natural gas hydrate and is widely used in commercial software like OLGA to calculate the pressure in the real pipeline systems (Boxall et al., 2009; Davies et al., 2010; Zerpa et al., 2012). The CSMHyK model and the software OLGA are one of the most widely used methods to calculate pipeline pressure in natural gas industry (Ding et al., 2019; Wang et al., 2022). Moreover, Sonne and Pedersen (2009) used a compositional hydrate kinetics model to simulate the hydrate growth rate. Sonne and Pedersen's model was utilized to develop the software Flowasta and predict pressure in pipeline (Creek et al., 2011). There are other methods to acquire the pressure in pipeline system, i.e., neural network (Ke et al., 2021), inward and outward natural gas hydrates growth shell model (Shi et al., 2011), etc. However, Ke et al. (2021)'s method is not able to describe the formation of hydrate. Shi et al. (2011)'s model needs complex calculation, because it requires the computation of hydrate growth before obtaining the pressure values. Overall, although there are many ways to calculate the pressure inside the deep-water pipeline, the experiments differ from the real deep water environment, while the establishment and calibration of



numerical model are time-consuming. A convenient method with relatively high accuracy is needed to predict the pressure along the deep-water pipeline considering the formation of natural gas hydrate.

In this work, a mathematical model to predict the pressure in the deep-water pipeline was derived considering the reduction of pipeline radius caused by the formation of natural gas hydrate. This model is able to obtain the pressure values in the deep-sea pipeline transporting the gaseous natural gas with high accuracy and good convenience.

Mathematical model

The mathematical model was established based on the following assumptions.

- (1) The deep-water pipeline is horizontally laid (Figure 1). Fluid flowing through the pipeline is the gaseous mixture consisting of methane and water vapor.
- (2) The flow of methane and water vapor mixture conforms the laminar flow.
- (3) The natural gas hydrate deposits uniformly on the pipeline inner surface and causes the reduction of pipeline radius. The hydrate grows against time. Therefore, the pipeline radius is a function of time.

The Poiseuille's law was used to describe the laminar flow of gas mixture in the horizontal pipeline:

$$Q = \frac{\pi r (t)^4 (p_0 - p_i)}{8\mu L_i}$$
(1)

where *Q* is the gas mixture flow rate in the pipeline, m³/s; r(t) is the pipeline inner radius, m, which is a function of time *t*; p_0 is the pressure at the inlet of pipeline, Pa; p_i is the pressure at the location *i*, Pa; μ is the viscosity of gas mixture, Pa·s; L_i is the distance between the inlet and the location *i*, m. Therefore, p_i can be expressed as:

$$p_{i} = p_{0} - \frac{8\mu L_{i}Q}{\pi r(t)^{4}}$$
(2)

Parameter	Value	Parameter	Value
Initial Pipeline radius r ₀ , m	0.01	Average temperature in pipeline T, K	286.6
Pressure at the inlet of the pipeline p_0 , Pa	8.6×10 ⁶	Viscosity of the gas mixture μ , Pa·s	6.8×10^{-4}
Volume factor of gas mixture $B_{\rm g}$	0.9	Flow rate of gas mixture on surface Q_s , m ³ /s	2.76×10 ⁻³
Heat transfer coefficient $F_{\rm k}$	0.5	Kinetic constant C1	3.63
Activation temperature coefficient of natural gas hydrate C_2	4,400	Molar mass of natural gas hydrate $M_{\rm g}$, kg/mol	0.16
Molar density of natural gas hydrate $\rho_g^{\ h}$, mol/m ³	44.6	Equilibrium temperature of natural gas hydrate $T_{\rm eq}$ K	292.54
Length of the pipeline L, m	39.6		

TABLE 1 Data of the parameters for model verification.

Because the formation of natural gas hydrate reduces the pipeline inner radius, the pipeline inner radius r(t) is given by:

$$r(t) = r_0 - \Delta r(t) \tag{3}$$

Where r_0 is the initial pipeline inner radius, m; $\Delta r(t)$ is the thickness of hydrate layer, m, which is also a function of time.

The thickness of hydrate layer (also the reduction of pipeline inner radius) $\Delta r(t)$ needs to be determined to accurately predict the pressure in the pipeline. Based on Cai (2018)'s work, the model of natural gas hydrate formation is given by:

$$\frac{\Delta V_{\rm h}}{\Delta t} = F_{\rm k} \exp\left(C_{\rm 1}\right) \exp\left(-\frac{C_{\rm 2}}{T}\right) \frac{1}{M_{\rm g}\rho_{\rm g}^{\rm h}} \left(T_{\rm eq} - T\right) A \qquad (4)$$

Where V_h is the volume of natural gas hydrate, m³; F_k is the heat transfer coefficient; C_1 is the kinetic constant, $\exp(C_1) = 37.8$; C_2 is the activation temperature coefficient of natural gas hydrate, K; T is the temperature, K; M_g is the molar mass of natural gas hydrate, kg/mol; ρ_g^{h} is the molar density of natural gas hydrate, mol/m³. T_{eq} is the equilibrium temperature of natural gas hydrate, K; A is the area of hydrate-gaseous mixture interface, m³. Using Cai (2018)'s model, the thickness of natural gas hydrate layer Δr during Δt can be written as:

$$\frac{\Delta r}{\Delta t} = F_{\rm k} \exp\left(C_1\right) \exp\left(-\frac{C_2}{T}\right) \frac{1}{M_{\rm g} \rho_{\rm g}^{\rm h}} \left(T_{\rm eq} - T\right) \tag{5}$$

Hence, the pipeline inner radius considering the formation of natural gas hydrate is given by:

$$r(t) = r_0 - F_k \exp(C_1) \exp\left(-\frac{C_2}{T}\right) \frac{1}{M_g \rho_g^h} (T_{eq} - T)t \qquad (6)$$

The pressure along the deep-water horizontal pipeline at the presence of natural gas hydrate is derived as:

$$p_{i} = p_{0} - \frac{8\mu L_{i}Q}{\pi \left[r_{0} - F_{k} \exp\left(C_{1}\right) \exp\left(-\frac{C_{2}}{T}\right) \frac{1}{M_{g}\rho_{g}^{h}} \left(T_{eq} - T\right)t\right]^{4}}$$
(7)

Eq. 7 is the model to predict the pressure in the deep-water pipeline considering formation of natural gas hydrate. This



model can be used to compute the pressure along the horizontal pipeline when natural gas hydrate forms at the inner surface of pipeline during deep-water natural gas transport.

Model verification

The model was validated using the experimental data obtained by Lorenzo et al. (2014) and the computation from Cai (2018)'s model.

Lorenzo et al. (2014)'s carried out experiments on natural gas hydrate formation in pipeline transporting gas-dominant fluids, and they measured the pressure drop inside the pipeline. The information of their experiments is exhibited in Table 1. The experimental results are plotted in Figure 2. Cai (2018) used Lorenzo et al. (2014)'s experimental data to validate her model for the formation of natural gas hydrate. The calculation of Cai (2018)'s model is also shown in Figure 2. In our work, we compared our model with the experimental data in Lorenzo et al. (2014)'s work and Cai (2018)'s computations to verify our model (Figure 2). The

Parameter	Value	Parameter	Value
Initial Pipeline radius r ₀ , m	0.1651	Average temperature in pipeline <i>T</i> , K	278.15
Pressure at the inlet of the pipeline p_0 , Pa	5×10 ⁶	Viscosity of the gas mixture μ , Pa·s	7.6×10 ⁻⁴
Volume factor of gas mixture $B_{\rm g}$	0.9	Flow rate of gas mixture on surface Q_s , m ³ /s	10.4
Heat transfer coefficient F _k	0.5	Kinetic constant C ₁	3.63
Activation temperature coefficient of natural gas hydrate C_2	6,877	Molar mass of natural gas hydrate $M_{\rm g}$, kg/mol	0.16
Molar density of natural gas hydrate $\rho_g^{\ h}$, mol/m ³	44.6	Equilibrium temperature of natural gas hydrate $T_{\rm eq}$ K	292.54
Length of the pipeline <i>L</i> , m	1,000		

TABLE 2 Data of the parameters for model application.



comparison demonstrates that the results of our model approximate the experimental data much better than Cai (2018)'s model with an average error less than 8%. Cai (2018)'s model focuses on the formation and collapse of natural gas hydrate in pipeline. In her model, the radius reduction is only considered after the collapse of natural gas hydrate. However, the loss of pipeline radius occurs at the point that the hydrate starts to form not collapse. As a result, Cai (2018)'s model overestimates the pressure along the pipeline. Because the calculation in our model is relatively simple, our model provides a more convenient and reliable way to predict the pressure in deep-water pipeline considering the pipeline radius reduction induced by natural gas hydrate.

Model application

The model was used to predict the pressure along the real deep-water pipeline of China at the presence of natural gas hydrate. The data of the parameters in the model come from the real pipeline systems (Liang et al., 2009; Cai, 2018; Ding et al., 2019), which are exhibited in Table 2.



Influence of natural gas hydrate on pipeline pressure

Pressure along the pipeline during 5 years of natural gas transport was calculated using our model. Results are shown in Figure 3.

Figure 3 illustrates that the pressure decreases almost linearly along the pipeline. The decline of pressure is mainly caused by two aspects: laminar flow resistance in viscous flow and the reduction of pipeline radius due to the formation of natural gas hydrate. In order to compare the effects of these two aspects, we calculated the pressure along the pipelines with changeable radius and constant radius at the fifth year of natural gas transport in Figure 4. In the pipeline with changeable radius, fluid flow encounters the resistances caused by both laminar flow resistance and the reduction of pipeline radius. While in the pipeline with constant radius, fluid flow only encounters the laminar flow resistance. Results show that the reduction of pipeline radius plays a dominant role in the pressure drop inside the pipeline, because the pressure drop in the pipeline with changeable radius (1.97 MPa) is much more significant than the pipeline with constant radius (0.02 MPa). It also implies that





taking into account the formation of natural gas hydrate is important to predict the pressure in the pipeline which transports natural gas in deep sea.

Characteristics of pipeline pressure decline

The decline of pressure during the first 3 years is much slower than the fifth year based on Figure 3. In order to investigate the pressure drop against time, we plot the pressure at 200, 400, 600, 800, and 1000 m of the pipeline during 5 years of natural gas transportation in Figure 5. In the first 3 years, the maximum pressure drop is only 0.19 MPa, accounting for a 3.8% of pressure loss, which occurs at the 1000 m of the pipeline. However at the fifth year, the pressure declines drastically to around 3 MPa at 1000 m with the 1.97 MPa of pressure drop. Nearly 40% of the pressure is reduced.

The drastic pressure drop is caused by the reduction of pipeline radius due to the formation of natural gas hydrate. The average reduction of pipeline radius during 5 years is shown in Figure 6. After 5 years of natural gas transport, 66.63% of pipeline radius is occupied by natural gas hydrate. This means that the formation and deposition of natural gas hydrate significantly affect the natural gas transport by blocking the pipeline. The growth of natural gas hydrate becomes faster as time goes by. And the blockage of pipeline tends to be more serious if the transportation continues without any treatments. As a result, the natural gas hydrate inside the pipeline should be cleared in time to maintain the good transport efficiency.

Conclusion

- 1. The model considers changeable pipeline radius induced by the formation of natural gas hydrate. Therefore it provides a convenient and reliable way to predict the pipeline pressure, which is validated by the experimental data.
- 2. The decline of pressure inside the pipeline is mainly due to the reduction of pipeline radius caused by natural gas hydrate compared with the flow resistance induced by viscous flow.
- 3. The growth of natural gas hydrate becomes faster against time, and the blockage of pipeline tends to be more serious. This leads to the decline of pressure along the pipeline with a nearly 40% of pressure loss at the fifth year.

Data availability statement

The original contributions presented in the study are included in the article/supplementary material, further inquiries can be directed to the corresponding authors.

Author contributions

FM: Model establishment; Model verification; Methodology; Data analysis; Original draft preparation; Funding receiver. ZQ: Model application; Review and editing; Funding receiver. XH: Review and editing; Funding receiver. WY: Model verification; Review and editing. SW: Review and editing. QL: Data analysis; Preparation of the revised manuscript.

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Conflict of interest

Author QL was employed by the company China National Offshore Oil Corporation Research Institute Co., Ltd.

The remaining authors declare that the research was conducted in the absence of any commercial or financial

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