



Links of Hydrogen Sulfide Content With Fluid Components and Physical Properties of Carbonate Gas Reservoirs: A Case Study of the Right Bank of Amu Darya, Turkmenistan

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Hydrogen sulfide (H₂S) in carbonate gas reservoirs shows strong relevance with the natural gas components and has an obvious impact on reservoir types and their petrophysical properties. In this work, core and fluid samples were collected from the Right Bank of Amu Darya reservoirs, Turkmenistan. Then, fluid composition analysis and flash evaporation experiments were performed to investigate the components of reservoir fluid. Petrophysical properties, that is, porosity and permeability, and micropore structures of cores were determined by permeameter–porosimeter and scanning electron microscope (SEM) analysis, respectively. Results in this work indicate that the H₂S content shows obvious relevance to fluid components in carbonate gas reservoirs. With the increase of H₂S content, the total heavy hydrocarbons and potential condensate content decrease, while the condensate density increases. In addition, at higher H₂S content, larger pore and vug porosity was observed. However, in reservoirs with lower H₂S content, the matrix pores are relatively tight and prone to develop fractures. Furthermore, sulfate thermochemical reduction (TSR) is found to be the dominant contributor to high H₂S content in carbonate reservoirs through material and thermodynamic condition analysis. The Gibbs free energy and normalized hydrocarbon content show that the consumption of heavy hydrocarbons generally increases with carbon numbers during TSR, but reaches a minimum at the components of C₇ to C₉. Finally, the relationship between TSR and rock petrophysical properties was discussed, indicating that pore volume enlargement and the dissolution effect of acidic gases are the main mechanisms for TSR to improve carbonate reservoir property. Results in this study present comprehensive analyses of the links between H₂S content and fluid components and petrophysical properties in carbonate gas reservoirs.

Keywords: carbonate gas reservoir, hydrogen sulfide, heavy hydrocarbon, TSR, fracture

1 INTRODUCTION

Currently, carbonate gas reservoirs, accounting for about 45% of the world's total gas reserves, is one of the most significant gas field types (Skrebowski, 1996; Wei et al., 2020). Accompanied by different sizes of pores, fractures, and vugs, carbonate rocks are featured with strong reservoir heterogeneity and anisotropy (Hu et al., 2019; Zhu et al., 2019; Liu D. et al., 2020; Lan et al., 2021; Xue et al., 2021). Hence, carbonate gas reservoirs show significant differences in reservoir characteristics, flow capabilities, and production performances (Cheng et al., 2017; Liu L.-l. et al., 2020; Chen et al., 2021; Zhao et al., 2021). On the other hand, natural gas containing hydrogen sulfide (H₂S) is mostly presented in carbonate reservoirs. Fei et al. (2010) investigated 52 H₂S-bearing oil and natural gas fields all over the world, 48 of which are limestone or dolomite reservoirs. As a consequence, numerous works on the generation and distribution of H₂S and its effect on reservoir features have been done to reveal the relationship between H₂S and the carbonate reservoir (Zhang et al., 2008; He et al., 2019; Liao et al., 2020).

At present, thermal decomposition of sulfur compounds (TDS), bacterial sulfate reduction (BSR), and sulfate thermochemical reduction (TSR) have been regarded as the most significant origins of H₂S in natural gas reservoirs (Basafa and Hawboldt, 2019; Zhao et al., 2019). Due to the toxic effect of H₂S on bacteria, the amount of H₂S from the BSR process is negligible generally (Machel, 2001; Xiao et al., 2021). As for the TDS, the required sulfur compounds such as thiol, thioether, and thiophene are rather scarce in natural gas reservoirs. Besides, the temperature threshold for sufficient thermal decomposition is commonly considered to be not lower than 150°C (Shi and Wu, 2021). Therefore, TSR is regarded as the main contribution to the H₂S in carbonate gas reservoirs (Li et al., 2019; Jia et al., 2021). The favorable conditions of the TSR progress have been widely discussed. In general, the material condition and the thermodynamic condition are believed to be the fundamental preconditions to progress TSR in the underground formation. Morad et al. (2019) concluded that the existence of gypsum rock is the basic precondition to providing sufficient sulfate for TSR. Furthermore, the development of matrix pores, the content of sulfate ions in formation water, formation temperature, gas-water contact, hydrocarbon composition, and so on have been studied on the generation of H₂S (Qu et al., 2019; Liu D. et al., 2020). In addition, Liu et al. (2022) conducted a physical simulation to depict the reaction between anhydrite and organic matters for the generation process of H₂S. Tian et al. (2020) have performed TSR simulations under different temperatures in a closed system to investigate the effect of temperature on the reaction.

The impact of H₂S on the composition of natural gas has been another concerned topic. In the early 1990s, Manzano et al. (1997) noticed the effect of H₂S on oil and gas composition for the first time. Since then, to figure out the component variation of natural gas, a variety of datasets such as petrography, fluid inclusions, and stable isotopes have been used (Deng et al., 2020; Torghabeh et al., 2021). It has been declared that acidic gases like H₂S and CO₂ can increase the drying coefficient of natural gas (Alawi et al., 2020). Up to now, the consumption characteristic of hydrocarbon components during TSR

has become the bottleneck for the explanation of the relation between H₂S and hydrocarbon components. Hu et al. (2021) introduced activation energy to distinguish the hydrocarbon loss during TSR and found that the consumption of heavy hydrocarbons would increase along with the carbon numbers. However, the priorities of different hydrocarbon components during the TSR process and the relevance of H₂S content to the fluid components are still unclear.

Actually, the effect of H₂S on the reservoir property should be an integrant part of related research. Some academics have revealed the controlling function of H₂S on the reservoir types and physical properties (Zhao et al., 2019; Liu Y. et al., 2020). Zhang et al. (2005) noticed that the H₂S-rich natural gas is commonly distributed in the porous reservoirs. Cai et al. (2015) declared that the generation of H₂S requires sufficient pore space and connectivity, and the porosity should not be less than 3.5% for H₂S-bearing carbonate reservoirs. From the perspective of TSR, the positive relationship between reservoir porosity and H₂S content has been confirmed by many reports (Mayrhofer et al., 2014; Wu et al., 2022). Accordingly, the good connectedness of the matrix can facilitate the TSR progress for producing H₂S; meanwhile, the metasomatism and dissolution effect of acidic gases can promote the development of high-quality carbonate reservoirs (Lai et al., 2021). Therefore, it is legitimate to declare that TSR plays a positive role in the improvement of carbonate reservoir properties. On basis of this, the study can be furthered by performing a systemic analysis of the pore structure and petrophysical properties of carbonate reservoirs within different H₂S content and figuring out the mechanism involved.

The purpose of this research is to illustrate the links between H₂S content on fluid components and reservoir properties of carbonate gas fields. Core and fluid samples collected from the Right Bank of Amu Darya carbonate reservoirs were used to investigate fluid compositions, microscopic pore structure, and reservoir physical property. Then, the influences of H₂S content on fluid composition and reservoir characteristics were studied in detail. Finally, based on the mechanism of TSR, the priority of hydrocarbon consumption was studied, and its effect on carbonate rock properties was discussed.

2 GEOLOGICAL SETTING

2.1 Fundamental Geological Characteristics

The gas fields of the Right Bank of Amu Darya, Turkmenistan, are located in the northeast portion of the Amu Darya Basin and close to Uzbekistan in the north. It is shaped like a narrow strip and can be divided into six different tectonic units (**Figure 1**). The Callovian–Oxfordian carbonate rocks developed in the Middle–Upper Jurassic Series are the most significant pay zone. The overlying Kimmeridgian–Tithonian Stage is regarded as the giant salt–gypsum formation, with a maximum thickness of 1,600 m (**Figure 2**). The development of salt–gypsum caprocks can provide guarantees for sufficient gas supply and preservation. The sedimentary facies of Callovian–Oxfordian carbonate rocks are

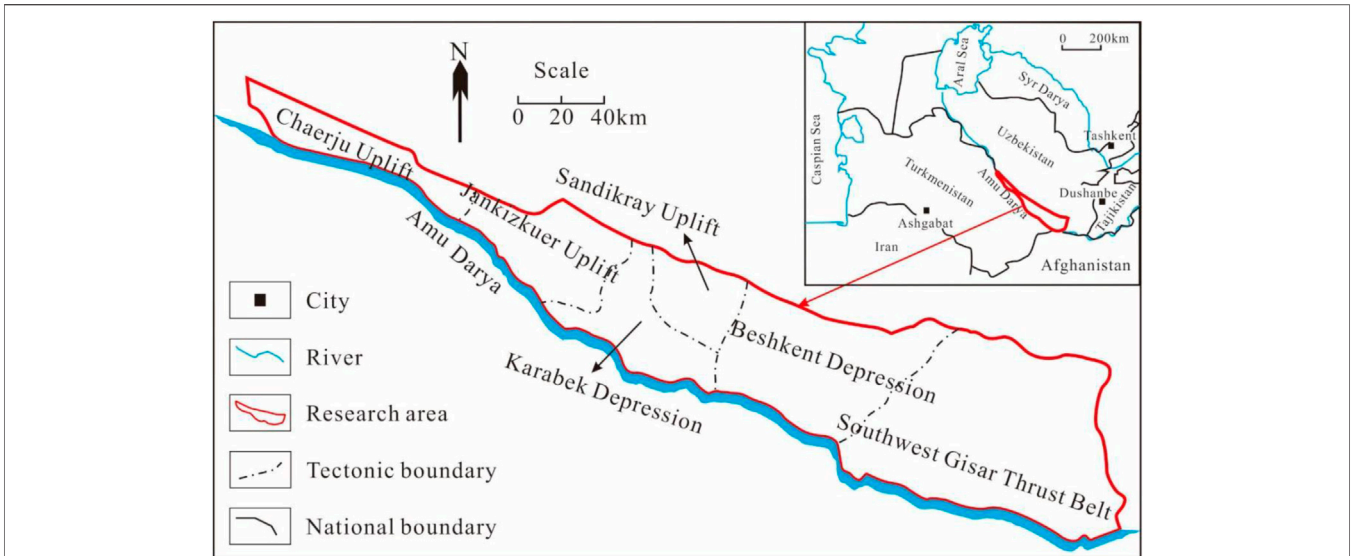


FIGURE 1 | Location of the research area.

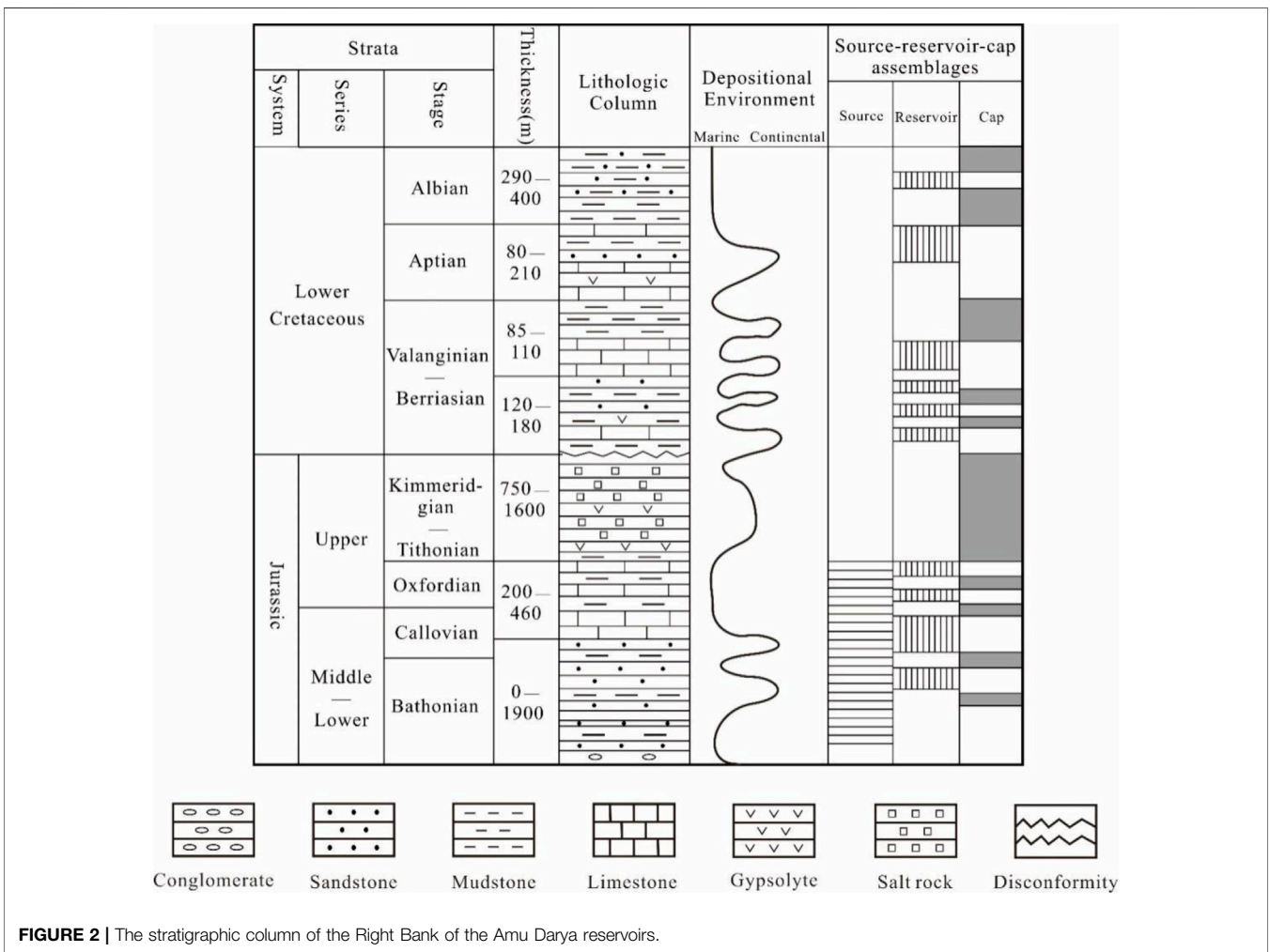
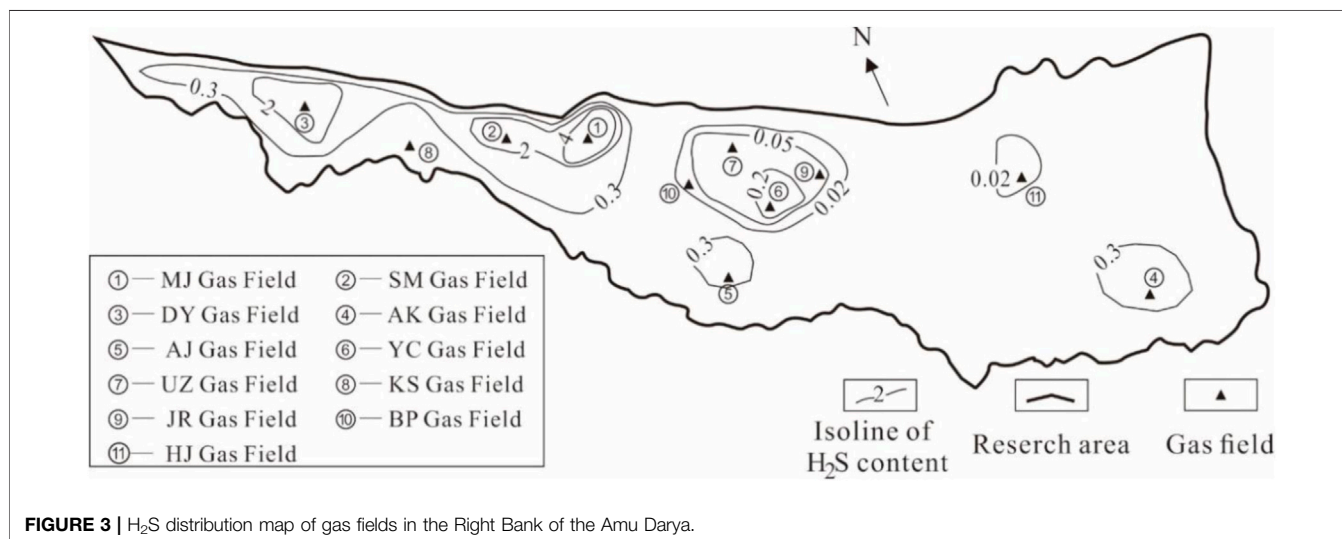


FIGURE 2 | The stratigraphic column of the Right Bank of the Amu Darya reservoirs.

TABLE 1 | H₂S content of different gas fields.

Gas field	H ₂ S content (%)	Type	Gas field	H ₂ S content (%)	Type
MJ	5.1084	High H ₂ S content	YC	0.2903	Low H ₂ S content
SM	4.2211		UZ	0.0767	
DY	2.0526	Medium H ₂ S content	KS	0.0541	
YL	0.6254		JR	0.0535	
YJ	0.5048		BP	0.0279	
JD	0.5029		HJ	0.0213	
AK	0.3586		AG	0.0178	
AJ	0.3090		JL	0.0022	



gradually transforming eastward from evaporative platform-open platform to platform margin. Dissolved pores and fractures are widely developed within the reef-shoal bodies.

Currently, sixteen gas fields are being developed in the Right Bank of Amu Darya. All gas fields involved are featured by the marine carbonate reservoir with low porosity and strong heterogeneity. According to core description results, the porosity of the gas fields is 3.43~11.27% in general and 6.37% on average, and permeability is 0.02~18.92 mD in general and 0.77 mD on average. Fractures, especially the high-angled ones, are extensively developed in the pay zone. Reservoir conditions of those gas fields vary notably with the position. Reservoirs in the western region are with large thicknesses and good physical properties with an average porosity of 10%. Conversely, formation thickness decreases for reservoirs in the middle and eastern region, and their flow capability is greatly affected by the natural fractures and vugs.

2.2 H₂S Content

H₂S content of the gas fields of the Right Bank of Amu Darya generally ranges from 0.0022% to 5.1084% (shown in **Table 1**), including classifications of a high content (>2%), medium content (0.3~2%), and low content (<0.3%). **Figure 3** plots the

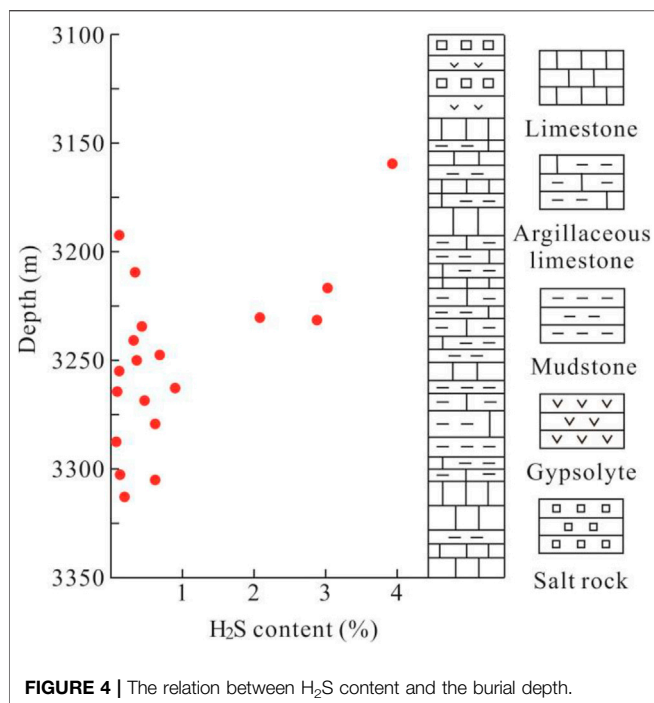
isoline of H₂S content, and it can be observed that gas fields with high H₂S content are distributed in the western regions; while H₂S content of the middle and eastern regions are mostly categorized as medium and low content, especially for reservoirs like BP, HJ, and AG, whose H₂S content are lower than 0.05% in general.

There also exists a certain relation between H₂S content and the burial depth: The H₂S content showed a decreasing trend with the increase of depth. It is the distance from the overlying gypsum rock that provides the explanation for the H₂S content variation with depth. Considering the generation process of H₂S in carbonate reservoirs, the gypsum plays crucial role despite the different reaction mechanisms involved there. As a result, for gas reservoirs in the Right Bank of Amu Darya, the H₂S content experiences an obvious rise with the distance closer to the overlying gypsum rock (**Figure 4**).

3 MATERIALS AND METHODS

3.1 Materials

The gas and condensate samples from 10 reservoirs in the Right Bank of the Amu Darya were collected from the wellhead separator, with an average operating pressure and temperature



of 1.82 MPa and 32°C, respectively. All fluid samples were immediately sealed into sampling bottles to avoid component loss. Basic information and properties of the gas and condensate samples are shown in **Table 2**. To characterize the petrophysical properties and microscopic pore structure of the reservoir rocks, ten core samples were collected, with three cores from the western region and the rest from the middle and east.

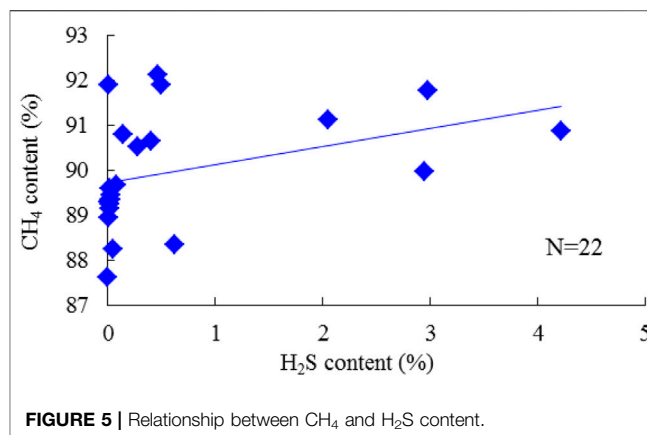
3.2 Experimental Methods

3.2.1 Fluid Composition Analysis

The composition of gas and condensate samples was analyzed by the chromatograph Agilent 7890A, abiding by the Industrial Standard “Analysis of natural gas composition: Gas chromatographic method (GB/T 13610-2014).” The hydrocarbons were determined from methane (C₁) to icosane (C₂₀) for the gas samples and from C₁ to tetratriacontane (C₃₄) for the condensate, respectively. The main nonhydrocarbon components, referring to H₂S, nitrogen (N₂), and carbon dioxide (CO₂), were also detected. Each component was expressed with its mole fraction in the gas and condensate sample.

3.2.2 Flash Evaporation Experiment

Flash evaporation experiments of the condensate samples were performed at the standard temperature and pressure using a flash



tank to separate flash gas and volatile oil from the condensate. The gas–oil ratio (GOR) and formation volume factor (FVF) of the condensate and the composition of the gas, flash gas, and volatile oil were determined. Then, the well production fluid components under formation conditions were calculated following the “Test method for reservoir fluid physical properties (GB/T 26981-2011).”

3.2.3 Core Sample Analysis

The porosity of the core samples was measured based on Boyle–Mariotte’s law *via* a Core Porosimeter OFITE 350, while, an *in situ* N₂ displacement experiment was launched to obtain the Klinkenberg permeability of the core with a core flooding device STL-II. All the test procedures abide by the “Core Analysis Method (SY/T 5336-2019).” Furthermore, the ultrahigh resolution scanning electron microscope (SEM) device QUANTA 400 was involved to characterize the structure of the pores and microfractures within the gold-coated core slice.

4 EXPERIMENTAL RESULTS

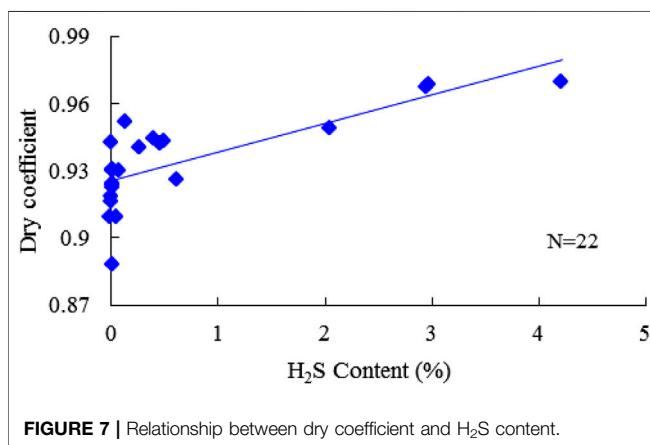
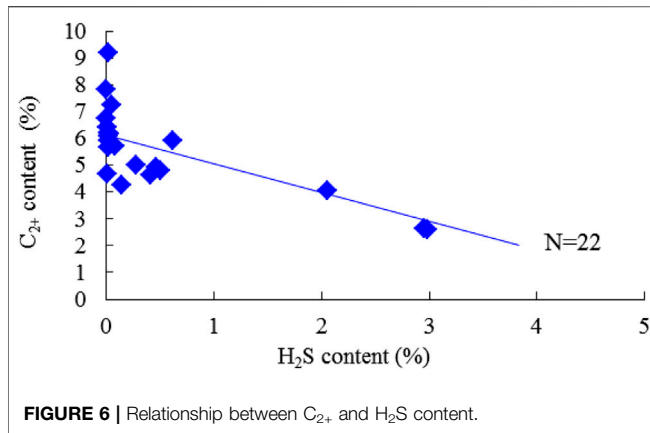
4.1 Relationships Between Fluid Component With H₂S Content

4.1.1 Hydrocarbon Components

Methane (CH₄) is the dominant component of natural gas. The measured CH₄ content varies from 87.617% to 92.779%, with an average of 95.308% in the gas phase. The cross-plot of CH₄ and H₂S content was plotted to investigate their relationships, as shown in **Figure 5**. However, the positive correlation is weak. Heavy hydrocarbons, that is, the C₂₊ component, mainly appear in the condensate phase; for gas and condensate samples, the C₂₊ content

TABLE 2 | Basic information and physical properties of samples.

Type	Formation information			Sampling position	Operating condition		Sample property	
	Depth (m)	Pressure (MPa)	Temperature (°C)		Pressure (MPa)	Temperature (°C)	Numbers	Relative density
Gas	3,150–3,570	53–62	107–121	Wellhead separator	0.45–3.46; 1.82 average	24–36; 32 average	22	0.64
Condensate							22	0.78



was 4.459% and 87.984%, respectively. The C₂₊ content generally presents a negative correlation with the increase of H₂S content, especially for samples with medium and high H₂S content (Figure 6). Correspondingly, the dry coefficient, referring to the ratio of the CH₄ content to the C₂₊ content in natural gas, shows a positive trend with the H₂S content (Figure 7).

To investigate the relationship between condensate and H₂S content, the potential condensate contents were calculated from the flash evaporation results of the well production fluids. The potential content decreases and the density increases with the H₂S content as shown in Figure 8, indicating that the heavy hydrocarbons could act as reactants in the production of H₂S, but their consumption would not increase monotonously with the carbon number.

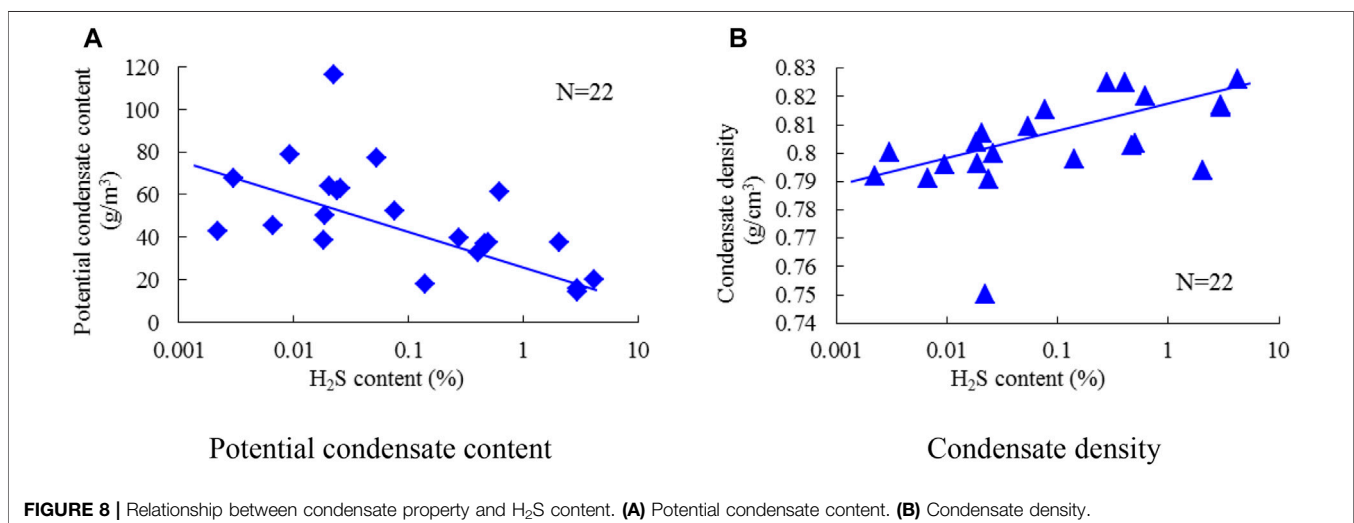
4.1.2 Nonhydrocarbon Components

N₂ is relatively scarce in the Right Bank of Amu Darya and its content varies slightly within the limit of 0.271%–0.516% in the well production fluid. The studied gas fields can be defined as medium CO₂ content reservoirs, whose content ranges from 0.917% to 4.556%, according to “The classification of the gas pool (SY/T 6168-2009).” As shown in Figure 9, CO₂ content is independent of H₂S at low and medium content ranges, while a positive correlation can be found between CO₂ and H₂S at high H₂S content. In addition, CO₂ content is greater than H₂S content within all samples despite the H₂S degree.

4.2 Reservoir Characteristics With H₂S Content

4.2.1 Porosity and Permeability

Similar to most carbonate reservoirs with fractures, the porosity and permeability of studied reservoirs do not show a clear positive correlation (Figure 10). As shown in Figure 11, the porosity increases with the increase of H₂S content, and the same trend can be found for the permeability of core samples without fractures. However, for core samples with fractures, there is no clear correlation observed between permeability and H₂S content as permeability is mainly affected by fractures. Actually, due to the lower aperture and higher permeability of fractures, the Poro-Perm Relation would somehow overturn in fractured reservoirs, which explains the differences in porosity and permeability with H₂S content. Therefore, porosity should be an intrinsic factor to figure out the effect of H₂S on reservoir physical properties.



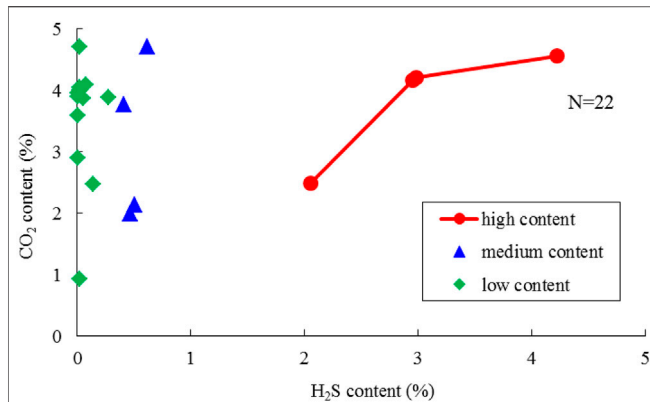


FIGURE 9 | Relationship between CO₂ and H₂S content.

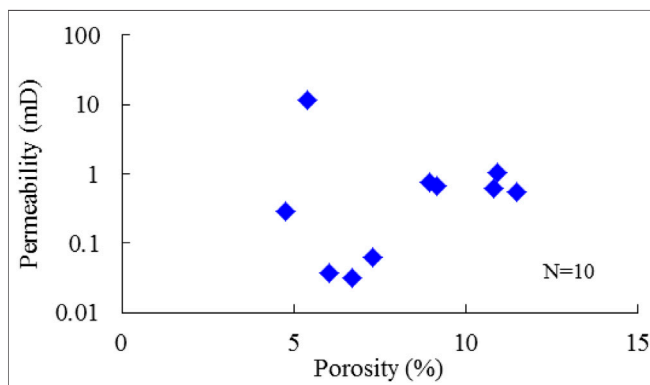


FIGURE 10 | Porosity and permeability of core samples.

4.2.2 Reservoir Types

The Right Bank of Amu Darya experienced multistage tectonic movement, and a large number of structural fractures were generated during that process. Meanwhile, the dissolution of the carbonate rocks caused by acidic gases can result in a large number of dissolved pores and vugs. As a consequence, diverse reservoir types have been discriminated in this area, among which pore, pore-fracture, pore-vug, and fracture are the most representative types.

The SEM analysis facilitates the connections between H₂S and reservoir microstructures. As can be seen in **Figure 12**: 1) Well DY-21, whose H₂S content was measured to be 2.0526%, was classified as the pore-vug type. The porosity and permeability were 11.47% and 0.55 mD, respectively. The SEM slice can observe a distinct moldic vug associated with the primary pores. 2) Well AJ-21, whose H₂S content was measured to be 0.3090%, was classified as the pore type. The porosity and permeability were 7.31% and 0.062 mD, respectively. The pore structure showed great homogeneity and intercrystal pores were commonly distributed. 3) BL-22 well, whose H₂S content was measured to be 0.0279%, was classified as the pore-fracture type. The porosity and permeability were 6.41% and 11.64 mD, respectively. The SEM slice was penetrated by a dissolved fracture, while the surrounding pores in the matrix are rather tight. This indicates that the H₂S could be regarded as one of the evidence to characterize the reservoir property for the gas fields in the Right Bank of Amu Darya. With higher H₂S content, the porosity would be larger and the reservoir types mainly consist of pore and pore-vug. Yet, for reservoirs with low H₂S content, the matrix pore could be relatively tight and prone to develop with fractures.

To further expand this knowledge, H₂S content, porosity, and brief reservoir descriptions of 10 major gas fields from different regions of the Right Bank of Amu Darya are summarized in **Table 3**. It shows that gas fields in the western region can be characterized as high H₂S content and high porosity reservoirs. However, H₂S content rarely exceeds 0.07% in the middle and east where fractures are well developed. In particular, for gas field JL with H₂S content of 0.0022%, the porosity almost reaches the lower limit of the effective pore, and the field is thus defined as a pure fractured reservoir.

5 DISCUSSION

5.1 H₂S Origin of Gas Fields in the Right Bank of Amu Darya

With respect to the TDS and BSR, TSR has been regarded as the most significant H₂S origin. TSR refers to a series of reduction reactions between sulfates and hydrocarbons, and the sulfates are consequently reduced into acidic gases, that is,

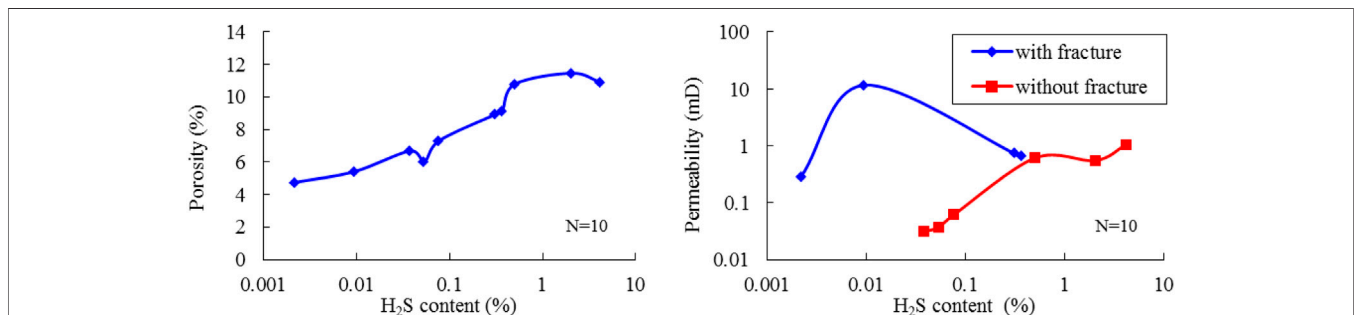


FIGURE 11 | Relationship between reservoir physical properties and H₂S contents.

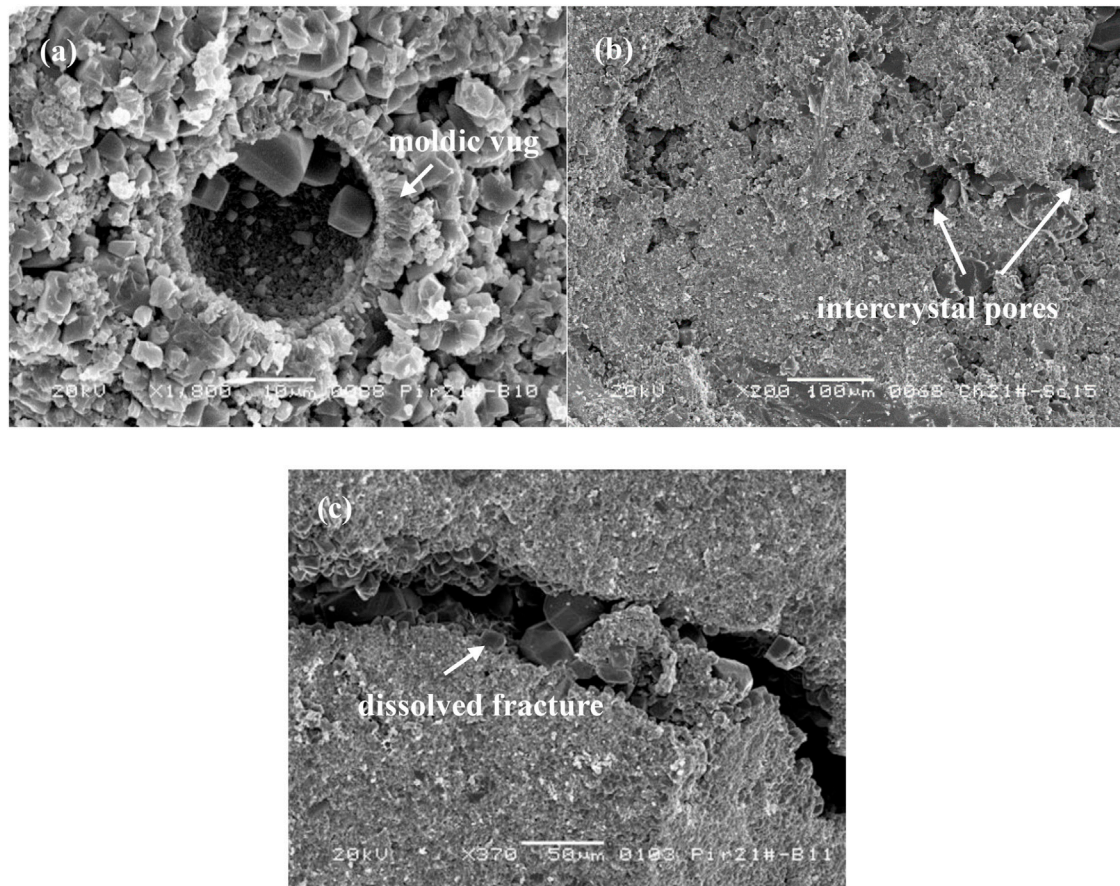
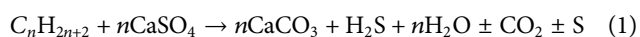


FIGURE 12 | The SEM images of core samples. **(A)** Well DY-21, showing a moldic vug; **(B)** Well AJ-21, developing with intercrystal pores; **(C)** BL-22 Well, showing a dissolved fracture.

TABLE 3 | H₂S content and reservoir characteristics of typical fields.

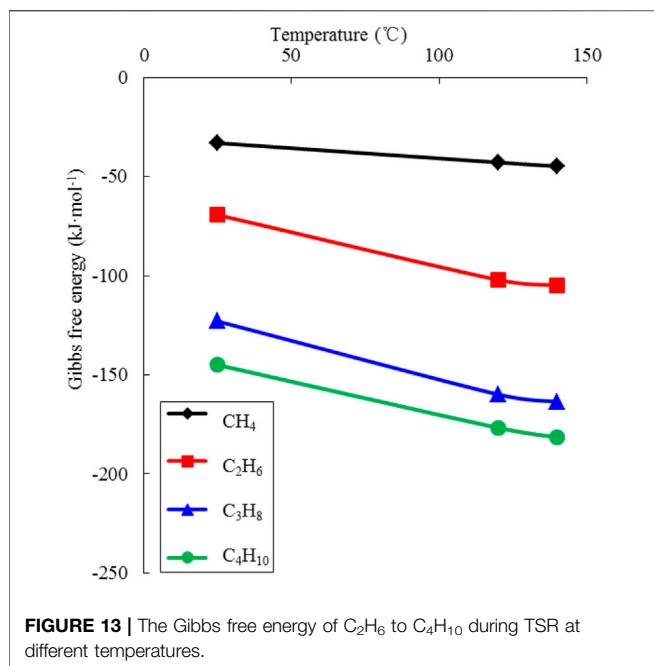
Gas field	Region	H ₂ S content (%)	Porosity (%)	Reservoir description	Reservoir type
DY	West	2.0526	9.27–13.66	Brownish gray silty limestone, light gray micritic limestone; primary pores are well developed, along with subsize vugs	Pore-vug
SM	West	4.2211	8.89–14.85	Brownish gray limestone, fine quality; the whole reservoir is of good physical properties with medium-high porosity	Pore-vug
JD	West	0.5029	9.37–12.81	Light gray silty dolomite, with good physical properties	Pore
YJ	Middle	0.5048	7.46–11.16	Light gray silty limestone; high porosity and permeability, low water saturation	Pore-vug
BP	Middle	0.0279	4.61–9.81	Dark gray and brownish gray micritic limestone, with high fracture development degree	Pore-fracture
UZ	Middle	0.0767	6.37–10.13	Grayish brown and light gray micritic limestone or silty limestone; microfractures are well developed	Pore-fracture
JR	Middle	0.0535	5.72–7.53	Brownish gray silty limestone; high angle fractures are developed	Pore-fracture
AJ	Middle	0.3090	8.62–9.93	Light gray bioclastic limestone; dissolved fracture pores and vugs are developed	Pore-vug
AG	East	0.0178	5.16–7.03	Brownish gray silty limestone; medium-scale fractures intensively are developed	Pore-fracture
JL	East	0.0022	3.53–5.04	Gray, brownish-gray micritic limestone; tight matrix pores, fractures are well developed	Fracture

H₂S and CO₂. The reaction process can be summarized in Eq. 1 (Zhang et al., 2008; He et al., 2019):



It is generally believed that the TSR requires the following preconditions: hydrocarbons, sulfate (material conditions), and

high temperature (thermodynamic condition). Because the TSR can hardly advance with the anhydrite, the reaction rate depends on the dissolution of calcium sulfate (CaSO₄) in the formation water. Therefore, higher connectivity is essential to allow adequately mixing between dissolved sulfate with hydrocarbons.



For the carbonate gas reservoirs in the Right Bank of Amu Darya, the material conditions, that is, hydrocarbons and sulfate, have undoubtedly met the requirement of TSR. Furthermore, the overlying gypsum-salt rock and the interbedded limestone-gypsum layers, dispersing in the upper section of the Callovian-Oxfordian Stage, provide direct contact for hydrocarbons and CaSO₄ to complete the reaction in the pay zone. The current formation temperature of the Amu Darya Basin ranges from 100 to 130°C. In view of the tectonic movement in the Himalayan period, the formation experienced higher temperatures. According to the inclusions homogenization temperature, the paleo-geotemperature of the reservoir had once reached 140°C, which exceeds the temperature threshold of TSR. Therefore, TSR is the dominant origin of H₂S in carbonate gas reservoirs in the Right Bank of Amu Darya. Ma et al. (2021) confirm that TSR is the principal producer of H₂S in the Right Bank of Amu Darya and also the contributor to the development of secondary pores.

5.2 Hydrocarbon Consumptions in the TSR Process

To clarify the relation between hydrocarbons and H₂S content, the priority of different hydrocarbon components involved in the TSR should be studied. According to the Van't Hoff isothermal formula (Atkins and De, 2006), the Gibbs free energy of each component can be determined with Eq. 2.

$$\Delta_r G_m = \Delta_r G_m^\ominus + RT \ln Q \quad (2)$$

where $\Delta_r G_m$ is the Gibbs free energy, kJ/mol; $\Delta_r G_m^\ominus$ is the standard formation free energy at 298.15 K, kJ/mol; R is the thermodynamic constant, 8.314 J/(mol·K); T is the reaction temperature, K; Q is the reaction quotient.

Figure 13 shows the calculated Gibbs free energy of CH₄ to C₄H₁₀ involved in TSR at different temperatures. It can be seen that: 1) The Gibbs free energy is decreasing dramatically with the increased temperature, which elucidates the necessity of high temperature for activating the reaction. 2) The Gibbs free energy of CH₄ stays at a high level despite the rising temperature, indicating that CH₄ is difficult to participate in the TSR reaction. This coincides with the statement mentioned in Section 4.1 that “no clear relation observed between CH₄ and H₂S content.” 3) For heavy hydrocarbons from C₂H₆ to C₄H₁₀, all calculated Gibbs free energy are less than -100 kJ/mol at the temperature of 120–140 °C, which demonstrates that these components are available in TSR at the reservoir conditions. In addition, the Gibbs free energy decreases with the increase of carbon numbers, indicating a rising trend of the consumption from C₂H₆ to C₄H₁₀.

Furthermore, to investigate the relative decrement of each hydrocarbon component along with per unit H₂S content growth, the normalized hydrocarbon content was used in this study. With well production fluid composition given, regressions between the normalized content of each hydrocarbon component and the H₂S content can be established. The correlation slope can thus be employed to describe the consumption involved in TSR. Considering that the slope showed a negative value, the absolute value of the slope was adopted and named the “relative consumption.” The definition of the normalized content and the regression results for each component is attached in Supplementary Appendix.

The relative consumptions of different heavy hydrocarbon components are shown in Figure 14. It was found that there is a V-shaped relationship between relative consumption and carbon number. The consumptions reach the minimum value at C₇ and then increase with carbon numbers; as a consequence, the consumptions of C₇ to C₉ are relatively low among all heavy hydrocarbon components except for C₂. This provides a reasonable interpretation for the variation of condensate content and density with H₂S content. The decrease of potential condensate content is caused by the consumption of total heavy hydrocarbons; while the remnant of intermediate components, typified by C₇ to C₉, would lead to an increase in condensate density.

To sum up, heavy hydrocarbons act as the reactant in TSR, while CH₄ can hardly take part in the reaction. The consumption of heavy hydrocarbons generally increases with carbon numbers but reaches a minimum at C₇~C₉. The relative consumption method facilitates the reveal of hydrocarbon consumption and explains the dynamic of gas and condensate features with H₂S content.

5.3 Influence of TSR on Nonhydrocarbon Components

As mentioned earlier, inert gases like N₂ are merely affected by H₂S content, whereas the CO₂ content shows a positive correlation with H₂S content at higher concentrations. This is because CO₂ is also one of the products of TSR. In addition, H₂S dissolution in formation water can form hydrosulfuric acid, which will further react with carbonate minerals to produce CO₂. It explains the content of CO₂ is higher than that of H₂S, which can be regarded as one of the symbols of carbonate reservoirs emerging TSR.

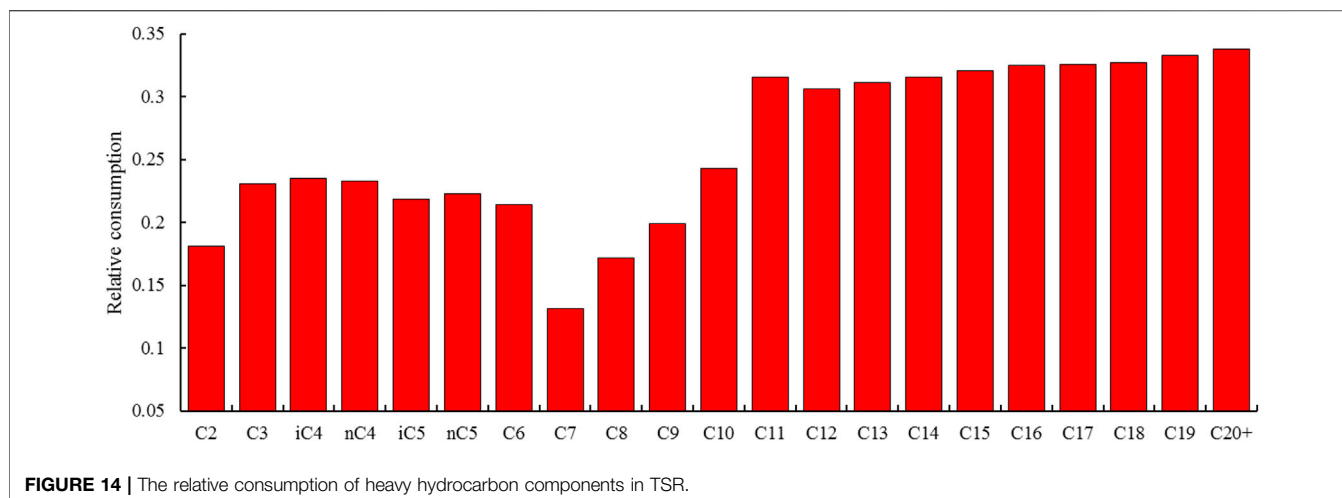


FIGURE 14 | The relative consumption of heavy hydrocarbon components in TSR.

5.4 Improvement of Reservoir Property Through TSR

From the perspective of TSR, the contribution of H₂S to the improvement of porosity can then be discerned. The controlling factor of TSR on reservoir physical properties and reservoir types can be manifested in the following aspects:

- 1) Compared to the fractured reservoirs, pore and pore-vug typed reservoirs are of higher connectedness and larger storage capacity, which not only provide space for the mutual contact of the reactants but also ensure a continuous supply of reactants and transfer of products. This prompts the TSR in the right direction. It explains why H₂S-bearing natural gas fields are generally discovered in large porous reservoirs.
- 2) It can be noticed from Eq. 1 that 1 mol of calcite (CaCO₃) can be generated with 1 mol of anhydrite (CaSO₄). The molar volume of CaCO₃ and CaSO₄ are 37 cm³/mol and 47 cm³/mol, respectively. Therefore, after 1 mol of anhydrite is involved in the reaction, the pore volume of the reservoir rock would increase by about 10 cm³. This process is usually called the “pore volume enlargement” effect of the TSR.
- 3) As the products of TSR, large amounts of H₂S and CO₂, which are acidic gases and soluble in formation water, played a significant role in the growth of secondary pores and vugs in carbonate rock. It is also an important mechanism to improve the porosity of carbonate reservoirs.

6 CONCLUSION

- 1) The H₂S content shows obvious relevance to fluid components in carbonate gas reservoirs. With the increase of H₂S content, the total content of heavy hydrocarbons decreases, causing the reduction of potential condensate content, while the condensate density is increasing with the H₂S content. In high H₂S content reservoirs, a positive correlation was observed between CO₂ content and H₂S content.

- 2) With higher H₂S content, the porosity would be larger and the reservoir rock mainly consists of pores and vugs; while for reservoirs with low H₂S content, the matrix pores could be relatively tight and prone to develop with fractures.
- 3) TSR is the dominant hydrogen sulfide origin for H₂S-rich carbonate reservoirs resembling the Right Bank of Amu Darya. The consumption of heavy hydrocarbons during TSR generally increases with carbon numbers but would reach a minimum at the components of C₇ to C₉. The pore volume enlargement and the dissolution effect of acidic gases can be regarded as the main mechanisms for the improvement of the reservoir property of TSR.

DATA AVAILABILITY STATEMENT

The raw data supporting the conclusion of this article will be made available by the authors, without undue reservation.

AUTHOR CONTRIBUTIONS

YC is responsible for the idea and writing of the manuscript; ZF, PC, CT, and HS are responsible for the experiments; CG and XL are responsible for the analysis and interpretation of data.

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SUPPLEMENTARY MATERIAL

The Supplementary Material for this article can be found online at <https://www.frontiersin.org/articles/10.3389/feart.2022.910666/full#supplementary-material>

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