



# **Engineering Planning Method and Control Modes for Debris Flow Disasters in Scenic Areas**

Xing-Long Gong<sup>1,2,3</sup>, Xiao-Qing Chen<sup>1,2,3</sup>, Kun-Ting Chen<sup>4,5</sup>\*, Wan-Yu Zhao<sup>1</sup> and Jian-Gang Chen<sup>1</sup>

<sup>1</sup>Key Laboratory of Mountain Hazards and Earth Surface Processes, Institute of Mountain Hazards and Environment, Chinese Academy of Sciences, Chengdu, China, <sup>2</sup>China-Pakistan Joint Research Center on Earth Sciences, CAS-HEC, Islamabad, Pakistan, <sup>3</sup>University of Chinese Academy of Sciences, Beijing, China, <sup>4</sup>Compound Disaster Prevention Research Center, General Research Service Center, National Pingtung University of Science and Technology, Pingtung, Taiwan, <sup>5</sup>Department of Soil and Water Conservation, National Pingtung University of Science and Technology, Pingtung, Taiwan

Compared with debris flows in other areas, debris flows in scenic areas not only seriously threaten residents, tourists, roads, walkways, and other infrastructure, but also cause considerable damage to the landscapes and ecosystems of these areas. Extreme rainfall events in the future will increase the complexities and challenges involved in debris flow control in scenic areas. Currently, the systematic planning of the entire scenic area is not considered in the treatment of debris flows. It is not possible to realize the rapid planning of any debris flow gully control project in a scenic area and to quantify the volume of debris flow material retained by each engineering structure. Based on field investigations and data collected from debris flow control projects in gullies in Jiuzhaigou Valley, China, an engineering planning method for debris flow control projects in scenic areas is herein proposed, and the challenges confronting existing control projects in scenic areas are discussed. Moreover, based on the example of Jiuzhaigou Valley, corresponding control engineering schemes for debris flow gullies in Xiajijie Lake Gully, Zhuozhui Gully, Xuan Gully, Pingshitou Gully, and West-Zhuozhui Gully are formulated. Four control modes for debris flow disasters in scenic areas are proposed, namely, "blocking + deposit stopping," "deposit stopping," "blocking," and "drainage + deposit stopping," which provide a systematic control strategy for post-earthquake debris flow disaster management in Jiuzhaigou Valley and other similar scenic areas.

#### Keywords: engineering planning method, control mode, debris flow, scenic areas, climate change

### INTRODUCTION

Debris flows are mixtures of sediment and water that flow down a slope under the influence of gravity. These disasters are widespread and commonplace in mountainous areas. Steep topography, abundant loose material, and concentrated rainfall are three important factors influencing debris flow formation. Numerous studies have attempted to elucidate the debris flow formation process based on rainfall thresholds and sediment supply conditions (Takahashi, 2007; Santi et al., 2008; Tang et al., 2012; Hungr et al., 2014; Zhang et al., 2014; Fan R. L. et al., 2018; Domènech et al., 2019). In particular, post-earthquake debris flows have been widely studied owing to their significant destructive power. In general, a devastating earthquake generates an adequate supply of sediment in the form of co-seismic collapses and landslides, which indirectly reduces the rainfall threshold

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> \*Correspondence: Kun-Ting Chen kuntingchen@mail.npust.edu.tw

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Gong X-L, Chen X-Q, Chen K-T, Zhao W-Y and Chen J-G (2021) Engineering Planning Method and Control Modes for Debris Flow Disasters in Scenic Areas. Front. Earth Sci. 9:712403. doi: 10.3389/feart.2021.712403 required to trigger a debris flow (Tang et al., 2012; Ma et al., 2017); catastrophic debris flows can be triggered even by lowintensity rainfall long after an earthquake has occurred. For example, destructive debris flows are still known to occur in the areas affected by the 1999 Chi-Chi, 2008 Wenchuan, and 2015 Gorkha earthquakes (Shieh and Tsai, 2009; Zhou et al., 2016; Dahlquist and West, 2019). Post-earthquake debris flows are characterized by their high destructive power, large scale, and the ease with which they form disaster chains (e.g., debris flows block river channels, causing river diversion and flooding of surrounding areas). Therefore, they seriously threaten human safety and endanger roads, bridges, houses, and other facilities (Cui et al., 2013; Chen et al., 2015; Chen K.-T. et al., 2018; Chen et al., 2019a; Chen et al., 2019b; Xiong et al., 2020). Wenjia Gully, in Qingping Township, Mianzhu, Sichuan Province, China, was not a debris flow gully prior to the Wenchuan earthquake. However, in the three rainy seasons immediately after the earthquake, five debris flow events were recorded here. Owing to heavy rainfall on August 13, 2010, the loose material in the channel of Wenjia Gully underwent violent erosion, resulting in a debris flow disaster. The debris flow peak discharge reached 1,530 m<sup>3</sup>/s, and approximately  $33.1 \times 10^6$  m<sup>3</sup> of loose material was transported to the gully mouth. Debris flow material blocked Mianyuan River, forming a dam that was 400 m long and 820 m wide. The subsequent river diversion flooded 479 newly constructed houses across and upstream of Wenjia Gully, as a result of which 7 people died, 5 were reported missing, and 39 sustained injuries (Ni et al., 2012; Tang et al., 2012; Yu et al., 2013).

Engineering measures are an effective method to mitigate debris flow disasters. Employing stabilization measures in the formation zone, blocking and drainage measures in the transport zone, and drainage and deposit stopping measures in the deposition zone of debris flow gullies are common approaches used to control debris flow disasters (Ikeya 1989; Cui and Lin, 2013; Chen et al., 2015). Stabilization measures involve stabilizing the slope, reducing erosion of the gully bed, preventing debris flow initiation, and reducing the scale of debris flows by building check dams and bed sills (Ikeya 1989; Piton et al., 2016). For example, to control debris flow disasters in Jiangjia Gully in Yunnan Province, China, a large number of check dams were built across the upstream tributaries of the watershed in 1979. These check dams effectively control erosion, stabilize the slope on both sides, promote the restoration of vegetation, and reduce the frequency of debris flows in the gully (Zeng et al., 2009). Blocking measures refer to the construction of check dams to retain debris flow material, regulate sediment transport, and reduce the destruction of downstream objects by debris flows (Ikeya 1989; Piton and Recking 2016). For example, to control debris flow disasters in the upstream region of Joganji River, Japan, check dams with a total capacity of 5 million m<sup>3</sup> were constructed to trap debris flow material (Kanbara and Imamori 2020). Drainage measures refer to the construction of drainage channels, diversion dikes, and other projects to control gully erosion and guide debris flows along the designed path so as to realize the protection of downstream objects (Ikeya 1989; Van Dine 1996). For example, a drainage channel was constructed

downstream of the Xiaogangjian debris flow gully in Sichuan Province, China; it crosses the Hanqing Highway and channels part of the debris flow material into a nearby river, effectively preventing debris flows from directly damaging the road (Chen et al., 2015; Chen J. G. et al., 2018). Deposit stopping measures refer to the construction of retention basins or retaining walls to retain debris flow material and protect vulnerable structures and objects. For example, in Jiuzhaigou Valley, Sichuan Province, China, a retaining wall was built on the debris flow fan in Zechawa Gully to retain the debris flow material and protect tourists, highways, and plank roads in the scenic area (Gong et al., 2020).

Compared with debris flow gullies that threaten roads, villages, and towns, debris flows in scenic areas not only threaten human safety and facilities, but also damage landscape resources, cause the deterioration of the ecosystem and ecological environment, and adversely impact the sustainable development of scenic areas, which has attracted extensive attention from scholars around the world (Cui et al., 2003; Faccini et al., 2009; Chen et al., 2016; Wang 2016). For example, debris flows in Jiuzhaigou Valley severely damage scenic landscapes, cause lake siltation, and block scenic roads, which significantly impact normal operations in these areas (Cui et al., 2003; Chen X.-q. et al., 2018). To protect residents, tourists, the natural landscape, and the ecological environment in Jiuzhaigou Valley, engineering measures have been employed to treat 14 debris flow gullies in which serious disasters occurred since 1984. The principles, technical measures, and typical engineering structures used for debris flow control in Jiuzhaigou Valley have been previously discussed (Cui et al., 2003). In the Shuzheng debris flow gully, which poses a threat to Shuzheng Village and the Shuzheng Lakes area, debris flow disasters were effectively controlled by constructing check dams in the formation zone to prevent the formation of conditions conducive to debris flow initiation and to stabilize the slope and gully. In the Xiajijie Lake debris flow gully, which poses a threat to the lake landscape and a nearby highway, check dams were built in the upper reaches of the gully, and a drainage channel with an embankment was constructed in the middle reaches of the gully to divert the debris flow into the forest. Vegetation is used to block debris flow material and realize the organic combination of ecosystem and engineering projects to achieve synergistic disaster reduction (Cui et al., 2007). However, the aforementioned control projects are more than 30 years old. The M7.0 earthquake that struck Jiuzhaigou Valley on August 8, 2017 severely damaged the original control projects in the area, and their capacity to control debris flows was considerably reduced (Huang et al., 2020). Global climate change trends indicate that extreme rainfall events will become more common and that debris flow disasters will become more severe because of the complex terrain conditions in this region (Liu et al., 2020). To manage post-earthquake debris flow disasters in Jiuzhaigou Valley, it is necessary to analyze the characteristics of the disasters and implement appropriate and timely control measures. Based on the characteristics of debris flow disasters, some scholars proposed that the "blocking + deposit stopping" control mode should be adopted to manage these disasters comprehensively (Gong et al., 2020). Other

scholars point to the fact that the location of debris flow control projects after an earthquake in scenic areas is limited by the functional zoning of the scenic areas; control projects can only be located within the experimental zones of scenic areas, where nature conservation and the sustainable use of resources are effectively combined. The Xiajijie Lake Gully is used as a case study to illustrate that the "blocking," "deposit stopping," and "blocking + deposit stopping" control modes should be adopted to control debris flows in Jiuzhaigou Valley (Zhao et al., 2020). Based on the foregoing analysis, the Jiuzhai Valley National Park Administration Bureau has implemented debris flow control projects in 31 debris flow gullies in the scenic area, some of which were completed in May 2019. However, on June 21, 2019, and July 22, 2019, debris flow disasters occurred in several gullies in the scenic area. The disaster reduction effect of the new control projects was found to be insufficient, and vulnerable structures were not effectively protected. The following shortcomings were noted: 1) there was a lack of planning for a debris flow disaster control system for the entire scenic area; 2) the control scheme for debris flow gullies was not appropriate; and 3) the engineering design parameters of the control scheme were inappropriate.

To overcome the aforementioned challenges, this study aimed to propose an engineering planning method for debris flow control in scenic areas using field investigations and data obtained from control projects in Jiuzhaigou Valley. This planning method consisted of the following steps: 1) The region in which the experimental zone of the scenic area overlapped with the transport and deposition zones of debris flow gullies was taken as the area in which the debris flow control projects could be constructed, so as to realize the systematic planning of debris flow disaster control for the entire scenic area. 2) Based on the objects threatened by debris flows and the topographical characteristics of the debris flow gullies, the "blocking + deposit stopping," "deposit stopping," "blocking," and "drainage + deposit stopping" control modes were adopted for different debris flow gullies in the scenic area to rapidly develop engineering measures for debris flow gullies in the scenic area. 3) The debris flow control projects were planned reasonably, the amount of debris flow material that could be retained by each project structure was quantified using parameter calculation, and the project implementation plan was determined. Based on the engineering planning method for debris flow control in the scenic area, this study discussed the challenges confronting debris flow control engineering in the scenic area, and formulated corresponding engineering schemes for debris flow control in the Xiajijie Lake, Zhuozhui, Pingshitou, Xuan, and West-Zhuozhui debris flow gullies.

### DEBRIS FLOW DISASTERS AND THEIR MITIGATION MEASURES IN JIUZHAIGOU VALLEY

### **Regional Setting of Jiuzhaigou Valley**

Jiuzhaigou Valley is located in Zhangzha Town, Jiuzhaigou County, Sichuan Province, China, approximately 440 km away from Chengdu, Sichuan Province, China. Jiuzhaigou Valley, which has a basin area of 720 km<sup>2</sup>, has a high vegetation coverage, stable surface runoff, and adequate groundwater replenishment (https:// en.jiuzhai.com/). As a result of precipitation and groundwater replenishment, a large number of lakes (commonly known as Haizi) are widely distributed in the scenic area, arranged in the form of a string of beads. The largest of these is Long Lake. The terrain of Jiuzhaigou Valley is high in the south and low in the north. The main gully has developed on the northern slope of the Gaerna watershed at the southernmost end of the basin. Water flows from south to north, and most branch gullies merge into the main gully in an east-west direction (**Figure 1**). Jiuzhaigou Valley is globally renowned for its blue and green lakes, spectacular waterfalls, and narrow conic karst landforms; it was declared a UNESCO World Heritage Site in 1992.

The study area is located between the Qinghai-Tibet Plateau and the Sichuan Basin, in a zone with a high altitude and steep slopes. There are 68 mountains with peaks higher than 4,000 m above sea level (m asl) in the area. The highest point is Gaerna in the southernmost region of the watershed, and the lowest point is Yangdong in the northernmost gully of the basin. The maximum elevation difference is 2,768 m, the horizontal distance between the highest and lowest points is approximately 46 km, and the average elevation difference of the entire basin exceeds 1,600 m. These topographic conditions are conducive to the occurrence of debris flows. The study area belongs to the Songpan-Ganzi block, which lies to the east of the Bayanhar block, and the unique geological conditions in the area are the result of the intense activity along the Tazang, Minjiang, and Huya faults. This activity led to the M7.5 Diexi earthquake in 1933, the M6.7 Zhangla earthquake in 1960, the M6.5 Huanglong earthquake in 1973, the Songpan-Pingwu earthquake cluster ( $M_S = 7.2, 6.7, and 7.2$ ) in 1976, and the M7.0 Jiuzhaigou earthquake in 2017 (Fan X. et al., 2018; Zhao et al., 2018). Frequent seismic activity leads to the fracture and collapse of the rock mass (limestone and slate with a small amount of sandstone) and induces landslides in the study area, which provides an abundant source of loose material for debris flows. In addition, the rainfall in the study area is concentrated from May to September, usually in the form of heavy rain (Gong et al., 2020). Owing to the steep terrain and abundant loose material, debris flow disasters are frequently triggered in the study area when concentrated rainfall events and rainstorms occur.

# Debris Flow Mitigation Measures in Jiuzhaigou Valley

To protect residents, tourists, the natural landscape, and the ecological environment in Jiuzhaigou Valley, engineering control has been carried out on the debris flow gully since 1984 (Cui et al., 2007). Debris flow disasters in the scenic area have recently increased owing to the 2017 Jiuzhaigou M7.0 earthquake; these disasters have damaged infrastructure, destroyed vegetation, and polluted water bodies in the scenic area (Chen X.-q. et al., 2018; Hu et al., 2019; Gong et al., 2020). After the 2017 Jiuzhaigou earthquake, the Jiuzhai Valley National Park Administration Bureau initiated phased treatment of 31 debris flow gullies; the first phase, comprising 15 debris flow gully





FIGURE 2 | Distribution of daily and hourly rainfall. (A) Daily rainfall in June 2019 recorded by the Zechawa precipitation station; (B) Hourly rainfall from 20:00 (Beijing time) on June 20 to 8:00 (Beijing time) on June 21, 2019 recorded by the Zechawa precipitation station; (C) Daily rainfall in July 2019 recorded by the Zharu Temple precipitation station; (D) Hourly rainfall from 00:00 to 12:00 (Beijing time) on July 22, 2019 recorded by the Zharu Temple precipitation station;



control projects, was completed in May 2019. From 20:00 (Beijing time) on June 20 to 08:00 (Beijing time) on June 21, 2019, heavy rainfall occurred in Jiuzhaigou Valley. Rainfall data from the Zechawa precipitation station show that the maximum 1 h rainfall was 10.8 mm, and the cumulative 6 h rainfall was 18.1 mm (**Figures 2A,B**); this rainfall intensity was almost equivalent to that of rainfall with a 2-years return period. The heavy rainfall induced simultaneous debris flows in Xiajijie Lake,

Xuan, Zhuozhui, Zechawa, Zhongjijie Lake, and West-Zhuozhui in the scenic area; the gully in the West-Zhuozhui area changed from a non-debris flow gully to a debris flow gully during this heavy rainfall event. From 00:00 to 09:00 (Beijing time) on July 22, 2019, heavy rainfall occurred again in the scenic area. Rainfall data from the Zharu Temple precipitation station show that the maximum 1 h rainfall was 15.6 mm, and the cumulative 6 h rainfall was 25 mm (**Figures 2C,D**); this rainfall intensity was



Zhuozhui. Pingshitou. Xuan. and West-Zhuozhui Debris Flow Gullies section.

almost equivalent to that of rainfall with a return period of 2–5 years. The heavy rainfall triggered a debris flow in the scenic area of Pingshitou Gully. Field investigation revealed that the new debris flow control project could not effectively control the debris flow disasters of June 21 and July 22, 2019. The inappropriate control engineering planning scheme and parameter calculation are elucidated using the examples of the Xiajijie Lake, Pingshitou, Zhuozhui, Xuan, and West-Zhuozhui debris flows.

# Blocking and Deposit Stopping to Control Debris Flow Disasters in Xiajijie Lake Gully

Xiajijie Lake Gully is adjacent to Xiajijie Lake. The straight-line distances from this gully to Nuorilang Waterfall and the entrance of Jiuzhaigou Valley are 4.6 and 16.2 km, respectively. The only scenic highway from Nuorilang Waterfall to Long Lake passes through the accumulation fan at the gully mouth (**Figure 3A**). In general, Xiajijie Lake Gully slopes from west to east; the highest point (4,120 m asl) lies on the west side of the basin and the lowest point lies near the mouth of Xiajijie Lake Gully (2,620 m asl). The watershed area of Xiajijie Lake Gully is 1.87 km<sup>2</sup>, the length of the main gully is 2.36 km, and the average longitudinal slope gradient of the gully bed is 593‰.

To mitigate debris flow disasters in Xiajijie Lake Gully, blocking measures were implemented in the debris flow gully in 1984. Three check dams and a drainage channel with an embankment were constructed in the transport zone of the debris flow gully (**Figure 3A**). This type of drainage channel can discharge part of the debris flow material to the forest on the left of the gully, and use vegetation to block debris flow, effectively realizing the combined use of ecological and engineering measures to achieve coordinated disaster mitigation. On August 8, 2017, the M7.0 Jiuzhaigou earthquake produced a large quantity of landslide material, which provided an abundant source of loose material for debris flow activity in Xiajijie Lake Gully. On September 25, 2017, a debris flow disaster occurred in Xiajijie Lake Gully. After the debris flow material filled the check dam, part of the debris flow material spilled out into the forest on the left side of the drainage channel, part of the material traveled rapidly along the main gully and flowed out, completely blocking the road in the area (**Figure 3B**), and part of the material entered Xiajijie Lake (**Figure 3C**). The debris flow material buried a 150 m section of the road in the scenic area, and the deposited material was up to 5 m thick.

In December 2017, the Jiuzhai Valley National Park Administration Bureau carried out treatment of the debris flow gully using the "blocking + deposit stopping" control mode. Three diversion dams were constructed in the transport zone to retain and divert the debris flow material. These dams ensure that a part of the debris flow material enters into the forest on the left and is blocked by retaining walls made of gabions, and another part of the debris flow material moves along the main gully and is blocked by a concrete retaining wall (Figure 4) (Zhao et al., 2020). Owing to heavy rainfall on June 21, 2019, a debris flow disaster occurred in Xiajijie Lake Gully. The diversion dam played an effective role during the debris flow event. A large portion of the debris flow material entered the forest on the left, and only a small portion of the material was transported along the main channel to the gully mouth, where the retaining wall effectively prevented the material from entering the Xiajijie Lake. However, owing to the tremendous destructive power of this post-earthquake debris flow, the debris flow material that was diverted to the left damaged the retaining wall made of gabions. As a result, a large amount of debris flow material was deposited on the scenic road. The length of the road section on which the debris flow material was deposited was 334 m, the width of the deposit was 12-15 m, and the thickness of the



deposit was 1.5–3.0 m (**Figure 4**). By estimating the deposition area and thickness of the debris flow material at the retaining wall, in the forest, and on the road, the total amount of debris flow material was estimated to be  $3.3 \times 10^4$  m<sup>3</sup>.

# Deposit Stopping to Control Debris Flow Disasters in Zhuozhui Gully

Zhuozhui Gully is approximately 25 km away from the exit of the scenic area. The mouth of the gully is located along the only scenic road from Zechawa village to Long Lake. In a plan view, the watershed of the debris flow gully is leaf-like. The main gully is approximately 3.3 km in length, and the basin area is about 4.14 km<sup>2</sup>. The highest point of the gully is 4,492 m asl, the elevation of the gully mouth is 2,882 m asl, the relative elevation difference between the highest point and the gully mouth is 1,610 m, and the average longitudinal slope of the gully is about 386‰. After the 2017 Jiuzhaigou earthquake, a 347 m long and 3 m high retaining wall was built in the deposition

zone of the debris flow gully to mitigate post-earthquake debris flow disasters in Zhuozhui Gully; the retaining wall had a designed storage capacity of  $1.2 \times 10^4 \text{ m}^3$  (Figure 5A). On June 21, 2019, a debris flow disaster was triggered by rainfall in Zhuozhui Gully. The debris flow material was transported to the retaining wall along the gully. Owing to the high impact of the debris flow, the retaining wall was partially damaged along the main channel of the debris flow gully (Figure 5B). Thus, a large amount of debris flow material was transported downstream, resulting in the burial of a 20 m section of scenic plank road and a 313 m section of the highway. The thickness of the debris flow material deposited on the scenic road was 2-3 m, and the debris flow continued to move downward into the forest, resulting in the destruction of approximately 3,215 m<sup>2</sup> of forest (Figure 5C). By estimating the deposition area and thickness of debris flow material in the retaining wall, road, and forest, the total amount of debris flow material was calculated to be  $2.5 \times 10^4$  m<sup>3</sup>.



FIGURE 6 Control engineering layout of Pingshitou Gully (after the debris flow event on July 22, 2019). The blue line in the figure represents the main channel. The drainage channel and the retaining wall in the figure are the proposed engineering projects described in *Application of the Planning Method for the Xiajijie Lake, Zhuozhui, Pingshitou, Xuan, and West-Zhuozhui Debris Flow Gullies* section.



FIGURE 7 | Mitigation measures in Xuan Gully. (A) Overview of the mitigation structures. (B) The debris flow material transported on June 21, 2019.

#### Blocking to Control Debris Flow Disasters in Pingshitou Gully

The mouth of Pingshitou Gully is about 2.6 km away from the entrance of the scenic area. The basin area of the debris flow gully is  $0.10 \text{ km}^2$ , and the length of the main gully is 0.90 km. The lowest point of the gully is located near the scenic road at an altitude of 2,100 m asl, and the highest point is located at an

altitude of 2,970 m asl. The relative elevation difference of the terrain is 870 m, and the average longitudinal gradient of the gully bed is 775‰. To mitigate debris flow disasters, the debris flow gully was treated using the blocking control mode in 1984; five check dams were constructed in the transport zone to retain debris flow material. After the 2017 Jiuzhaigou earthquake, the original check dams were strengthened to mitigate debris flow



disasters. Moreover, the debris flow material behind the check dams was artificially cleared, and the total storage capacity of the check dams after dredging was  $0.036 \times 10^4 \text{ m}^3$ . A debris flow disaster was triggered by heavy rainfall in Pingshitou Gully on July 22, 2019, and the debris flow material filled the check dams (**Figure 6**). Approximately  $0.2 \times 10^4 \text{ m}^3$  of debris flow material was transported to the scenic road of Pingshitou Gully, which resulted in road blockage.

# Drainage and Deposit Stopping to Control Debris Flow Disasters in Xuan Gully

Xuan Gully is located southwest of Xiajijie Lake. The only scenic highway from Nuorilang Waterfall to Long Lake passes through the accumulation fan at the gully mouth (Figure 7A). The drainage area of the debris flow gully is approximately 0.56 km<sup>2</sup>, and the length of the main gully is 1.05 km. The highest point of the gully is located in the northwest corner (elevation of 3,805 m asl), and the lowest point is located near the scenic road (elevation of 2,625 m asl). The relative elevation difference of the terrain is 1,180 m, and the average longitudinal slope is 795‰. To mitigate debris flow disasters, drainage measures were implemented in 1984. A drainage channel was constructed in the transport zone of the debris flow gully to discharge debris flow material to the right side of the mouth of the debris flow gully, to manage debris flow disasters in Xuan Gully after the 2017 Jiuzhaigou earthquake, the original drainage channel was repaired and a retention basin with a storage capacity of  $0.17 \times 10^4 \text{ m}^3$  was built in the concave area to the right of the gully mouth. On June 21, 2019, a debris flow disaster occurred in Xuan Gully, and debris flow material entered the retention basin through the drainage channel. After the retention basin was full,

about  $0.11 \times 10^4$  m<sup>3</sup> of debris flow material reached the scenic road, blocking it and causing a traffic jam (**Figures 7A,B**). The debris flow material buried a 108 m section of the road; the width of the deposit was 9–12 m and the average thickness of the deposit was 1 m.

# Debris Flow Disaster in West-Zhuozhui Gully Without Engineering Measures

West-Zhuozhui Gully is located on the left side of the road from Long Lake to Nuorilang Waterfall. The straight-line distance from this location to the mouth of Zhuozhui Gully is 600 m. The basin area of the debris flow gully is 1.33 km<sup>2</sup>, and the length of the main gully is 1.77 km. The lowest point of the gully is located near the scenic road at an altitude of 2,831 m asl, and the highest point is located at an altitude of 3,993 m asl. The relative elevation difference of the terrain is 1,162 m, and the average longitudinal gradient of the gully bed is 517‰. Prior to the 2017 Jiuzhaigou earthquake, no debris flow disaster was recorded in West-Zhuozhui Gully. On June 21, 2019, heavy rainfall triggered severe channel erosion in West-Zhuozhui Gully (Figure 8), and approximately  $0.903 \times 10^4$  m<sup>3</sup> of loose material was transported to the accumulation fan at the gully mouth and the highway in the scenic area. The debris flow material was deposited on a 120 m section of the scenic highway; the width of the deposit was 12-16 m, the thickness of the deposit was 1.5-2.5 m, and the volume of the material deposited was  $0.336 \times 10^4 \text{ m}^3$  (Figure 8).

### Mitigation Effectiveness of Debris Flow Control Projects Completed in May 2019

As a consequence of the 2017 Jiuzhaigou earthquake, the scale of debris flows in Xiajijie Lake Gully, Zhuozhui Gully, Pingshitou

Debris flow gullies	Design standards	Control measures	Engineering structures	Designed capacity (m <sup>3</sup> )	Amount of transported	Whether the following were endangered in 2019?		
					debris flow material in 2019 (m <sup>3</sup> )	Tourists	Scenic road, walkways	Landscapes
Xiajijie Lake Gully	50-year return period (50-year return period)	Blocking and deposit stopping measures (Drainage and deposit stopping measures)	Check dams, drainage channel, retaining walls (Drainage channel, retaining wall)	3.0 × 10 <sup>4</sup> (3.01 × 10 <sup>4</sup> )	3.3 × 10 <sup>4</sup>	No	Yes	No
Zhuozhui Gully	20-year return period (50-year return period)	Deposit stopping measure (Deposit stopping measure)	Retaining wall (Retaining wall)	1.2 × 10 <sup>4</sup> (2.1 × 10 <sup>4</sup> )	2.5 × 10 <sup>4</sup>	No	Yes	-
Pingshitou Gully	20-year return period (50-year return period)	Blocking measure (Drainage and deposit stopping measures)	Check dams (Drainage channel, retaining wall)	0.036 × 10 <sup>4</sup> (0.32 × 10 <sup>4</sup> )	0.236 × 10 <sup>4</sup>	No	Yes	_
Xuan Gully	20-year return period (50-year return period)	Drainage and deposit stopping measures (Drainage and deposit stopping measures)	Drainage channel, retaining wall (Drainage channel, retaining wall)	0.17 × 10 <sup>4</sup> (0.72 × 10 <sup>4</sup> )	0.28 × 10 <sup>4</sup>	No	Yes	No
West- Zhuozhui Gully	(50-year return period)	None (Blocking and deposit stopping measures)	None (Check dam, retaining wall)	(1.046 × 10 <sup>4</sup> )	$0.903 \times 10^4$	No	Yes	_

#### TABLE 1 | Mitigation effectiveness of the debris flow control projects completed in May 2019.

Note: The data and content in parentheses show the results obtained using the engineering planning method for debris flow disasters in scenic areas proposed in Engineering Planning Method for Debris Flow Disasters in Scenic Areas and Application of the Planning Method for the Xiajijie Lake, Zhuozhui, Pingshitou, Xuan, and West-Zhuozhui Debris Flow Gullies sections.

Gully, and Xuan Gully increased significantly. The gully in West-Zhuozhui changed from a non-debris flow gully before the earthquake to a debris flow gully. Debris flow disasters exhibit a tendency to occur in clusters. Previous studies have shown that debris flow disasters will continue to occur for at least 5-10 years after the earthquake (Chen X.-q. et al., 2018). Therefore, it is necessary to analyze the disaster characteristics of debris flows and implement appropriate and timely control engineering measures. After the 2017 Jiuzhaigou earthquake, the "blocking + deposit stopping," "deposit stopping," "blocking," and "drainage + deposit stopping" control modes were adopted to manage the debris flow disasters in Xiajijie Lake Gully, Zhuozhui Gully, Pingshitou Gully, and Xuan Gully, respectively. The construction of the new projects was completed in May 2019. However, during the debris flow events on June 21, 2019 and July 22, 2019, the new control projects did not effectively protect the vulnerable objects, and the control project schemes and parameter calculations were found to be inappropriate. The specific considerations were as follows: 1) The main gully mouth of Xiajijie Lake exhibits conditions that are not conducive to deposit stopping; thus, it is not appropriate to construct a retaining wall at the main gully mouth. The retention conditions of the transport zone in Pingshitou Gully are poor; thus, blocking is not an appropriate control mode to manage debris flow disasters. 2) The total designed storage capacity of the debris flow control engineering project in Zhuozhui Gully, Pingshitou Gully, and Xuan Gully is far lower than the amount of transported debris flow material. Therefore, to effectively overcome these

challenges, this study combined field investigation and data collection, and proposed a method of debris flow control engineering planning in scenic areas taking into account the characteristics of different debris flow gullies and the engineering feasibility. The application of this method is illustrated in *Engineering Planning Method for Debris Flow Disasters in Scenic Areas* section, using the example of Jiuzhaigou Valley, and the mitigation effectiveness of debris flow control projects completed in May 2019 is analyzed in **Table 1**.

### ENGINEERING PLANNING METHOD FOR DEBRIS FLOW DISASTERS IN SCENIC AREAS

In China, owing to restrictions related to the functional zoning of nature reserves, debris flow control projects can only be constructed in experimental zones. The formation zones of debris flow gullies in scenic areas are usually located in the core and buffer zones of these areas. Typically, only the transport and deposition zones of debris flow gullies overlap with the experimental zones of scenic areas, which make it impossible to implement stabilization measures in the formation zones of debris flow gullies. Therefore, all types of control projects can only be implemented in the transport zones and deposition zones of debris flow gullies to realize the management of debris flow disasters in scenic areas. Based on field investigations and data collected from debris flow control



projects in scenic areas, an engineering planning method for debris flow control projects in scenic areas is proposed. The specific steps are described in **Figure 9**:

### Delimiting the Area for the Construction of Debris Flow Control Projects

Based on data related to protected objects in scenic areas, the natural environment and natural resources, social economy, and land and water utilization, the National Standard of the People's Republic of China (Cui et al., 2018) spatially divides scenic areas into core, buffer, and experimental zones (**Figure 10**). Based on field investigations and topographic surveys, debris flow gullies are divided into formation zones, transport zones, and deposition zones. Debris flow control projects can only be constructed in areas in which

the experimental zones of the natural scenic areas overlap with the transport and deposition zones of debris flow gullies.

### Obtaining Topographic Conditions and Constructing Debris Flow Control Projects

Using field investigations and topographic surveys, this study determined whether the debris flow gully mouths exhibited conditions conducive to deposit stopping, whether the channels in the transport zones exhibited material conditions conducive to debris flow retention, and whether erosion in the gullies was serious. Our study can provide the basis for the formulation of control engineering schemes.

For debris flow gullies in which conditions at the gully mouths are conducive to deposit stopping, the following



considerations should be applied. When gully erosion is severe, blocking projects should be constructed in the transport zone and deposit stopping projects should be constructed in the deposition zone of the debris flow gully within the construction area of debris flow control projects. The blocking projects and deposit stopping projects should jointly meet the following requirement: the amount of debris flow material retained by the blocking projects  $(W_{block})$  + the amount of debris flow material retained by the deposit stopping projects ( $W_{deposit}$ ) > the total volume of debris flow material under design standards ( $W_{df}$ ). When gully erosion is not severe, it is only necessary to construct deposit stopping projects in the deposition zone within the construction area of debris flow control projects. The deposit stopping projects should meet the following requirement: the amount of debris flow material retained by the deposit stopping projects  $(W_{deposit})$ > the total volume of debris flow material projected to rush out under design standards ( $W_{df}$ ).

For debris flow gullies in which conditions at the gully mouths are not conducive to deposit stopping, the following considerations should be taken into account. When the channel in the transport zone exhibits material conditions conducive to debris flow retention, it is only necessary to construct blocking projects in the transport zone in the construction area of debris flow control projects. The blocking projects should meet the following requirement: the amount of debris flow material retained by the blocking project  $(W_{block}) >$ the total volume of debris flow material projected to rush out under design standards  $(W_{df})$ . When the channel in the transport zone does not exhibit material conditions conducive to debris flow retention, drainage projects should be constructed in the transport zone in the construction area of debris flow control projects to discharge debris flow material into the recesses on both the sides of the gully; these should be accompanied by deposit stopping projects. The drainage projects should meet the following requirement: the peak discharge of the debris flow material discharged by the drainage projects  $(Q_{drainage})$  > the peak discharge of debris flow material projected to rush out under design standards  $(Q_{df})$ . The amount of debris flow material retained by the deposit stopping projects  $(W_{deposit})$  > the total volume of debris flow material projected to rush out under design standards  $(W_{df})$ . The method of calculation of all the aforementioned parameters is described in Parameter Calculation section.

#### Parameter Calculation

# Debris Flow Peak Discharge Under Different Return Periods $(Q_{df})$

The design standard of a control project determines the ability of the project to withstand debris flow disasters. Based on the risk level of the vulnerable objects or the disaster situation of the affected objects, the design standards of debris flow control projects in mountainous areas in China can be divided into 100, 50, and 20-year return periods (Chen et al., 2015; Liu et al., 2015; Gong et al., 2020). Considering the importance of scenic areas, a 50-year return period should be adopted as the design standard for debris flows. The rain-flood method is a widely used method to calculate the peak discharge of debris flows. The peak discharge  $Q_{df}$  of debris flows under different design standards can be obtained through the following steps (Zhou et al., 1991; Liu et al., 2014; Gong et al., 2020).

Step one: based on topographic data, the basin area, A (km<sup>2</sup>), length of the main gully, L (km), and average longitudinal gradient of the gully bed, J, are obtained. Then, the basin characteristic parameter of the gully,  $\theta$ , is calculated using **Eq. 1** and the confluence parameter, m, is calculated using **Eq. 2**.

$$\theta = \frac{L}{J^{1/3} A^{1/4}}$$
(1)

$$m = 0.221\theta^{0.204} \tag{2}$$

Step two: the characteristic rainstorm values [1/6 h average rainfall,  $H_{1/6}$  (mm), 1 h average rainfall,  $H_1$  (mm), and 6 h average rainfall,  $H_6$  (mm)] of debris flow gullies are obtained from the rainstorm and flood calculation manual of medium-small basins in Sichuan Province. The modulus coefficients,  $K_{1/6}$ ,  $K_1$ , and  $K_6$ , corresponding to  $H_{1/6}$ ,  $H_1$ , and  $H_6$ , are obtained from the Pearson III frequency table. **Eq. 3** is used to calculate the rainstorm intensity, *S* (mm), under the design standard, and **Eq. 4** is used to calculate the rainstorm attenuation index, *n*.

$$S = H_{1}K_{1}$$
(3)  
$$n = \begin{cases} 1 + 1.285 \left( 1g \frac{H_{1/6}K_{1/6}}{H_{1}K_{1}} \right), 1/6h < t < 1h \\ , \\ 1 + 1.285 \left( 1g \frac{H_{1}K_{1}}{H_{6}K_{6}} \right), 1h < t < 6h \end{cases}$$
(4)

Step three: the confluence time, t (h), and flood peak runoff coefficient,  $\varphi$ , are calculated using **Eqs 5–8**.

$$t = t_0 \varphi^{-\frac{1}{4-n}} \tag{5}$$

$$\varphi = 1 - 1.1 \frac{\mu}{S} t_0^n \tag{6}$$

$$t_0 = \left[\frac{0.383}{mS^{1/4}/\theta}\right]^{\frac{4}{4-n}}$$
(7)

$$\mu = K_P \eta A^{-0.19} \tag{8}$$

where  $t_0$  is the basin confluence time when  $\varphi = 1$ ,  $\mu$  is the basin runoff yield parameter (mm/h), and  $\eta$  is the comprehensive

coefficient of runoff yield parameters. Based on the area in which the debris flow gully is located, the values of  $\eta$  are 6 (Qingyi River-Lutou Mountain rainstorm area), 4.8 (basin hilly area), and 3.6 (basin margin mountainous area and southwest mountainous area), respectively.  $K_p$  is the modulus ratio coefficient when the variation coefficient is 0.23, which is obtained from the Pearson III frequency table.

Step four: the peak discharge of the watershed  $Q_f$  (m<sup>3</sup>/s) is calculated using **Eq. 9**. Then, the peak discharge of the debris flow  $Q_{df}$  (m<sup>3</sup>/s) under the design standard is calculated according to **Eq. 10**.

$$Q_f = 0.278\varphi \frac{S}{t^n} A \tag{9}$$

$$Q_{df} = D_{df} \left( 1 + \psi_{df} \right) Q_f \tag{10}$$

$$\psi_{df} = \left(\gamma_{df} - \gamma_{w}\right) / \left(\gamma_{s} - \gamma_{df}\right) \tag{11}$$

where  $D_{df}$  is the blockage coefficient. The value of  $D_{df}$  varies with the degree of blockage, namely, very serious blockage ( $D_{df} = 3.0-2.6$ ), serious blockage ( $D_{df} = 2.5-2.0$ ), normal blockage ( $D_{df} = 1.9-1.5$ ), and minor blockage ( $D_{df} = 1.4-1.1$ ).  $\psi_{df}$  is the amplification coefficient of the debris flow peak discharge.  $\gamma_{df}$  is the density of the debris flow (t/m<sup>3</sup>), which is obtained *via* field investigations (Ministry of Land and Resources of the People's Republic of China, 2006).  $\gamma_w$  is the density of water (t/m<sup>3</sup>), usually taken as 1.00 t/m<sup>3</sup>.  $\gamma_s$  is the density of the solid material (t/m<sup>3</sup>), usually taken as 2.65 t/m<sup>3</sup>.

# Debris Flow Peak Discharge by Drainage Channel (Q<sub>drainage</sub>)

Based on the morphology of the cross-section of the drainage channel, the debris flow peak discharge by the drainage channel,  $Q_{drainage}$  (m<sup>3</sup>/s), can be obtained using **Eq. 12**:

$$Q_{drainage} = A_{drainage} V_{df} \tag{12}$$

where  $A_{drainage}$  is the area of the cross-section of the drainage channel (m<sup>2</sup>), and  $V_{df}$  is the average velocity of the debris flow (m/s), which can be calculated using Manning's formula (Liu et al., 2015; Gong et al., 2020):

$$V_{df} = \frac{1}{n_{drainage}} R_{df}^{2/3} I_{drainage}^{1/2}$$
(13)

where  $n_{drainage}$  is the roughness coefficient of the drainage channel, which depends on the material properties of the drainage channel, and can be obtained from (China Association of Geological Hazard Prevention 2018).  $R_{df}$  is the hydraulic radius of the debris flow (m).  $I_{drainage}$  is the longitudinal slope gradient of the drainage channel bed (m/m).

#### Total Volume of Debris Flow Material ( $W_{df}$ )

The total volume of debris flow material under the design standard,  $W_{d\beta}$  is calculated using **Equation (14)** (Zhou et al., 1991; Gong et al., 2020):

$$W_{df} = 0.264 Q_{df} T_{df}$$
 (14)

where  $Q_{df}$  is the peak discharge of the debris flow under the design standard, which can be calculated using Eq. 10.  $T_{df}$  is the duration

of the debris flow event, which can be determined by interviewing witnesses and monitoring.

# Volume of Debris Flow Material Trapped by Blocking Projects (*W*<sub>block</sub>)

Since check dams are generally used in blocking projects,  $W_{block}$  can be estimated using the following commonly used equation (Jiang 2018).

$$W_{block} = \frac{H_b^2}{I} \left( \frac{H_b}{2\tan\alpha} + b \right)$$
(15)

where  $H_b$  is the effective height of the check dam (m), I is the longitudinal slope of the gully at the project site,  $\alpha$  is the gradient of the bank slopes of check dams (degrees), and b is the average bottom width of the gully bed in the silting section of the check dam (m). I,  $\alpha$ , and b are determined based on topographic data of the debris flow gully and field investigations.

# Volume of Debris Flow Material Trapped by Deposit Stopping Projects ( $W_{deposit}$ )

Because deposit stopping projects generally adopt retaining walls, and the retaining walls are constructed in the deposition zone with gently sloping terrain,  $W_{deposit}$  can be estimated by the following commonly used equation (Jiang 2018).

$$W_{deposit} = \frac{H_d^2}{I} B_d \tag{16}$$

where  $H_d$  and  $B_d$  are the effective height (m) and length (m) of the retaining wall, respectively.

# Compatibility of Engineering Structures with the Landscape and Ecosystems

In general, debris flow control projects should be coordinated with the local landscape and ecosystem, especially in scenic areas (Cui et al., 2003; Wu and Feng 2006). To achieve this goal, the following aspects were considered in this study: 1) Optimization of the type and size of the engineering structure: Engineering structure with optimized type should be built to improve the disaster reduction effect of debris flow. Such as, slit dam and filtering dam should be built to effectively block wood debris and reduce water pollution respectively in scenic areas (Cui et al., 2007). Engineering structure with optimized size should be built to maximize the economic benefit and reduce the damage to the ecological environment due to construction. 2) Aesthetic considerations for the engineering structure: As far as possible, the engineering structure should be built out of sight of visitors to reduce the influence of the engineering structure on the aesthetic value of the scenic spot. Where this is not possible, local trees, shrubs, and grass should be spray painted using a color that blends well with that of the surrounding environment. 3) Suitable building materials: Local materials should be used to construct the engineering structures to avoid the influence of foreign materials on ecological resources, such as the pollution of local water bodies.

### **RESULTS AND DISCUSSION**

### Application of the Planning Method for the Xiajijie Lake, Zhuozhui, Pingshitou, Xuan, and West-Zhuozhui Debris Flow Gullies

Based on the basic information of Jiuzhaigou Valley, the experimental zone is determined using the method described in *Delimiting the Area for the Construction of Debris Flow Control Projects* section (Figure 10). According to the gully and distribution characteristics of loose material, the Xiajijie Lake, Zhuozhui, Pingshitou, Xuan, and West-Zhuozhui debris flow gullies can be divided into formation, transport, and deposition zones. The corresponding elevation coordinates are shown in Table 2. Debris flow control projects can be constructed in the area of overlap between the experimental zone of the scenic area and the transport and deposition zones of a debris flow gully. The elevations of the construction areas of the Xiajijie Lake, Zhuozhui, Pingshitou, Xuan, and West-Zhuozhui debris flow control projects are 2800–2620, 3025–2882, 2230–2100, 2830–2625, and 3040–2831 m asl, respectively (Table 2).

Based on field investigations and measured topographical data, the following debris flow control measures are adopted for Xiajijie Lake Gully, Zhuozhui Gully, Pingshitou Gully, Xuan Gully, and West-Zhuozhui Gully based on the considerations

TABLE 2   Topographic conditions of debris flow gulli	es.
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Parameters	Xiajijie Lake Gully	Zhuozhui Gully	Pingshitou Gully	Xuan Gully	West-Zhuozhui Gully	
Basin area (km <sup>2</sup> )	1.87	4.14	0.1	0.56	1.33	
Main gully length (km)	2.36	3.3	0.9	1.05	1.77	
Average gully gradient (‰)	593	386	775	795	517	
Highest elevation (m)	4,120	4,492	2,970	3,805	3,993	
Lowest elevation (m)	2,620	2,882	2,100	2,625	2,831	
Formation zone (m)	4,120-2,960	4,492-3,925	2,970-2,600	3,805–2,850	3,993–3,317	
Transport zone (m)	2,960-2,660	3,925–3,015	2,600-2,115	2,850-2,650	3,317-2,894	
Deposition zone (m)	2,660-2,620	3,015–2,882	2,115-2,100	2,650-2,625	2,894-2,831	
Experimental zone (m)	<2,800	<3,025	<2,230	<2,830	<3,040	
Construction area of debris flow control projects (m)	2,800-2,620	3,025-2,882	2,230-2,100	2,830-2,625	3,040-2,831	
Whether the debris flow gully mouths exhibited conditions conducive to deposit stopping	No	Yes	No	No	Yes	

described in Obtaining Topographic Conditions and Constructing Debris Flow Control Projects section. 1). After the September 25, 2017 and June 21, 2019 debris flows, large amounts of loose material were transported to the main gully mouth of Xiajijie Lake Gully. The main gully mouth does not exhibit conditions conducive to deposit stopping, and the transport zone of the gully within the construction area does not exhibit conditions conducive to blocking. Therefore, only the "drainage + deposit stopping" control mode can be adopted to treat the debris flow gully. 2) There is a large accumulation fan at the mouth of Zhuozhui Gully, which has the area required for a deposit stopping project. Gully erosion in the construction area of the debris flow control project is not serious, and the "deposit stopping" control mode can be implemented to manage debris flow disasters in Zhuozhui Gully. 3) The accumulation fan in Pingshitou Gully is small, and a scenic road has been constructed on the accumulation fan, which does not exhibit conditions conducive to deposit stopping. In the construction area of the debris flow control project, the channel in the transport zone is narrow and steep, and the storage capacity of check dams is limited. The dam was completely filled during the July 22, 2017 debris flow. There is a concave area to the right of the main gully mouth of Pingshitou Gully that exhibits conditions conducive to the construction of a retaining wall. Thus, the "drainage + deposit stopping" control mode can be adopted. The drainage channel should be constructed in the transport zone in the construction area of the debris flow control project to divert the debris flow material to the concave area, and the debris flow material should be intercepted using a retaining wall. 4) The accumulation fan at the mouth of Xuan Gully is small, and the scenic road threatened by debris flows passes the top of the accumulation fan; thus, there is not enough space for a deposit stopping project. Moreover, the transport zone of the gully does not exhibit conditions conducive to the construction of engineering structures such as check dams to intercept and hold debris flow material. Therefore, drainage projects can be constructed in the transport zone of the debris flow gully to drain the debris flow material to the concave gully mouth, and a deposit stopping project can be constructed to intercept the material. 5) The accumulation fan at the mouth of the debris flow gully in the West-Zhuozhui area is large and exhibits conditions suitable for deposit stopping. Furthermore, severe erosion occurs in the transport zone of the gully, so the "blocking + deposit stopping measures" control mode should be adopted to mitigate debris flow disasters.

Based on Eqs 1–11 in *Parameter Calculation section*, the  $W_{df}$  values in Xiajijie Lake Gully, Zhuozhui Gully, Pingshitou Gully, Xuan Gully, and West-Zhuozhui Gully were calculated as  $2.78 \times 10^4$ ,  $2.06 \times 10^4$ ,  $0.228 \times 10^4$ ,  $0.673 \times 10^4$ , and  $0.993 \times 10^4$  m<sup>3</sup>, respectively (**Table 3**). Based on the control measures proposed above, the design parameters of debris flow control projects in Xiajijie Lake Gully, Zhuozhui Gully, Pingshitou Gully, Xuan Gully, and West-Zhuozhui Gully were calculated using Eqs 12–16. The specific parameters are as follows: 1) The construction of a drainage channel with a cross-sectional area of  $6.0 \text{ m}^2$  is planned in the transport zone of Xiajijie Lake Gully (**Figure 4**). The designed peak discharge of debris flow in the drainage channel is  $61.18 \text{ m}^3$ /s, which exceeds the peak discharge of debris flow

(58.55 m<sup>3</sup>/s) under the design standard adopted. Thus, the drainage channel satisfies the  $Q_{drainage} > Q_{df}$  criterion. The construction of a retaining wall with a length of 80 m and a height of 7 m is planned in the concave area to the left of Xiajijie Lake Gully (Figure 4). The designed storage capacity of the retaining wall is  $3.01 \times 10^4$  m<sup>3</sup>, which is greater than the total amount of debris flow material that is projected to rush out  $(2.78 \times$ 10<sup>4</sup> m<sup>3</sup>) under the design standard adopted. Thus, it satisfies the  $W_{deposit} > W_{df}$  criterion. 2) The height of the original retaining wall in Zhuozhui Gully is low. The construction of a retaining wall with a length of 70 m and a height of 6 m is planned (Figure 5A). The designed storage capacity of the retaining wall is  $2.1 \times 10^4$  m<sup>3</sup>/s, which is greater than the total amount of debris flow material projected to rush out  $(2.06 \times 10^4 \text{ m}^3)$  under the design standard adopted. Thus, it satisfies the  $W_{deposit} > W_{df}$  criterion. 3) The construction of a drainage channel with a cross-sectional area of  $2.4 \text{ m}^2$  is planned in the transport zone of Pingshitou Gully (Figure 6). The designed peak discharge of debris flow in the drainage channel is 16.95 m<sup>3</sup>/s, which exceeds the peak discharge of debris flow  $(3.61 \text{ m}^3/\text{s})$  under the design standard adopted. Thus, it satisfies the  $Q_{drainage} > Q_{df}$  criterion. The construction of a retaining wall with a length of 30 m and a height of 4 m is planned in the concave area to the right of Pingshitou Gully (Figure 6). The designed storage capacity of the retaining wall is  $0.32 \times 10^4 \text{ m}^3$ , which is greater than the total amount of debris flow material that is projected to rush out  $(0.228 \times 10^4 \text{ m}^3)$  under the design standard adopted. Thus, it satisfies the  $W_{deposit} > W_{df}$  criterion. 4) The construction of a drainage channel with a cross-sectional area of  $3.0 \text{ m}^2$  is planned in Xuan Gully (Figure 7). The designed peak discharge of debris flow in the drainage channel is 32.01 m<sup>3</sup>/s, which exceeds the peak drainage of debris flow (16.99 m<sup>3</sup>/s) under the design standard adopted. Thus, it satisfies the  $Q_{drainage} > Q_{df}$ criterion. The height of the existing retaining wall is low and the storage capacity is small. The construction of a retaining wall with a length of 40.0 m and a height of 3.0 m is planned. The designed storage capacity is  $0.72 \times 10^4$  m<sup>3</sup>, which exceeds the total amount of debris flow material that is projected to rush out  $(0.673 \times 10^4 \text{ m}^3)$ under the design standard adopted. Thus, it satisfies the  $W_{deposit}$  >  $W_{df}$  criterion. 5) The construction of a check dam with a height of 4 m and a length of 20 m is proposed in the transport zone of West-Zhuozhui Gully (Figure 8). The designed storage capacity of the check dam is  $0.176 \times 10^4$  m<sup>3</sup>. At the mouth of the main gully (2,850 m asl), the construction of a retaining wall with a length of 60 m and a height of 4.0 m is proposed (Figure 8). The storage capacity of the proposed retaining wall is  $0.87 \times 10^4 \text{ m}^3$ , which satisfies the  $W_{block} + W_{deposit} > W_{df}$  criterion.

As discussed in *Compatibility of Engineering Structures with the Landscape and Ecosystems* section, the proposed control engineering structure should be coordinated with the natural landscape and ecological environment. Thus, the following measures should be adopted: 1) In Xiajijie Lake Gully, the planned retaining wall is located at the mouth of the gully, where vegetation is sparse. Therefore, construction will cause minimal damage to the vegetation in the scenic spot. However, the retaining wall is only 5 m away from the scenic road, and spruce, alpine willow shrubs, and a fire grass meadow should be transplanted to conceal it. 2) The planned retaining wall in the TABLE 3 | Parameter calculation results using the method in Engineering Planning Method for Debris Flow Disasters in Scenic Areas section.

Calculation content	Parameters	Unit	Debris flow gullies				
			Xiajijie Lake Gully	Zhuozhui Gully	Pingshitou Gully	Xuan Gully	West-Zhuozhui Gully
Flood peak discharge	θ	_	2.40	3.18	1.74	1.31	2.05
, c	т	_	0.26	0.28	0.25	0.23	0.26
	$H_{1/6}$	mm	7.8	7.8	7.8	7.8	7.8
	$H_1$	mm	15	15	15	15	15
	$H_6$	mm	25	25	25	25	25
	K <sub>1/6</sub>	_	2.76	2.76	2.76	2.76	2.76
	$K_1$	_	2.58	2.58	2.58	2.58	2.58
	K <sub>6</sub>	_	2.42	2.42	2.42	2.42	2.42
	K <sub>P</sub>	_	1.56	1.56	1.56	1.56	1.56
	п	_	0.75	0.75	0.75	0.67	0.75
	μ	mm/h	4.99	4.29	8.70	6.27	5.32
	to	h	1.51	1.98	1.10	0.84	1.29
	φ	_	0.81	0.80	0.73	0.84	0.82
	t	h	1.61	2.13	1.21	0.88	1.38
	Q <sub>f</sub>	m <sup>3</sup> /s	11.36	20.13	0.69	5.53	9.20
Debris flow peak discharge	Ydf	t/m <sup>3</sup>	1.93	1.68	1.71	1.63	1.73
	D <sub>df</sub>	_	2.25	1.90	3.00	1.90	1.90
	Q <sub>df</sub>	m <sup>3</sup> /s	58.55	65.05	3.61	16.99	31.33
	T <sub>df</sub>	S	1800	1,200	2,400	1,500	1,200
	W <sub>df</sub>	m <sup>3</sup>	2.78 × 10 <sup>4</sup>	2.06 × 10 <sup>4</sup>	$0.228 \times 10^4$	0.673 × 10 <sup>4</sup>	$0.993 \times 10^4$
Debris flow peak discharge by drainage channel	Adrainage	m <sup>2</sup>	6.0	_	2.4	3.0	_
(Q <sub>drainade</sub> )	n <sub>drainage</sub>	_	0.04	_	0.04	0.04	_
( aranago,	R <sub>df</sub>	m	0.81	_	0.52	0.60	_
	Idrainage	_	0.22	_	0.19	0.36	_
	Q <sub>drainage</sub>	m <sup>3</sup> /s	61.18	-	16.95	32.01	_
Volume of debris flow solid material trapped by blocking	H <sub>b</sub>	m	_	_	_	_	4
measures (W <sub>block</sub> )	1	_	_	_	_	_	0.21
	α	degrees	_	_	_	_	33
	b	m	_	_	_	_	20
	W <sub>block</sub>	m <sup>3</sup>	_	-	_	_	$0.176 \times 10^4$
Volume of debris flow solid material trapped by deposit	H <sub>d</sub>	mm	7	6	4	3	4
stopping measures (W <sub>deposit</sub> )	$B_d$	m	80	70	30	40	60
· · · · · · · · ·	Ĩ	_	0.13	0.12	0.15	0.05	0.11
	W <sub>deposit</sub>	m <sup>3</sup>	$3.01 \times 10^{4}$	2.1 × 10 <sup>4</sup>	$0.32 \times 10^{4}$	0.72 × 10 <sup>4</sup>	$0.87 \times 10^{4}$

deposition zone of Zhuozhui Gully is approximately 100 m away from the scenic road, which is far beyond the visual range of tourists. Thus, there is no need for transplantation of vegetation to conceal the retaining wall, and the outside of the retaining wall can be painted so that it blends into the surrounding environment. 3) The proposed retaining walls at the mouths of Pingshitou Gully, Xuan Gully, and West-Zhuozhui Gully are low. Only *Salix alpina* shrubs need to be transplanted to conceal the retaining wall, and the outside of the retaining wall should be painted so that it blends into the surrounding environment.

# Control Modes of Debris Flow Disasters in Jiuzhaigou Valley

Based on the control engineering planning method proposed herein, the control modes for debris flow gullies in scenic areas can be divided into four categories (**Figure 11**). 1) For debris flow gullies that demonstrate severe erosion and conditions conducive to deposit stopping, blocking projects should be constructed in the transport zone. This control mode can realize the objective of retaining and stabilizing loose material and reduce the scale of debris flows and the damage they cause. Deposit stopping projects should then be constructed in the deposition zone within the construction area of debris flow control projects. This can stop debris flow material and reduce damage to vulnerable downstream structures (Figure 11A). 2) For debris flow gullies that do not demonstrate severe erosion and exhibit conditions conducive to deposit stopping, only deposit stopping projects should be constructed in the deposition zone within the construction area of debris flow control projects (Figure 11B). 3) In debris flow gullies that do not exhibit conditions conducive to deposit stopping but in which the channels in the transport zone exhibit material conditions conducive to debris flow retention, only blocking projects should be constructed in the transport zone within the construction area of debris flow control projects. This can realize the effective interception of debris flow material and reduce damage to



downstream objects and structures (Figure 11C). 4) For debris flow gullies that do not exhibit conditions conducive to deposit stopping and for which the channel in the transport zone does not exhibit material conditions conducive to debris flow retention, drainage projects should be constructed in the transport zone of the debris flow gully to divert the debris flow material into recesses on both sides of the gully, and deposit stopping projects should be constructed to retain the diverted material (Figure 11D).

Based on the foregoing analysis, the planning method proposed in this study is used to plan engineering countermeasures for debris flow gullies in scenic areas with severe hazards, and the control mode used in various debris flow gullies is discussed (**Table 4**). According to the analysis results, the post-earthquake control modes for the debris flow gullies in Xiajijie Lake, Zhuozhui, Pingshitou, Xuan, and West-Zhuozhui are "drainage + deposit stopping," "deposit stopping," "drainage + deposit stopping," "drainage + deposit stopping," and "blocking + deposit stopping," respectively. Field investigations indicate that the existing control modes for Xiajijie Lake Gully and Pingshitou Gully have not been effective, and the engineering structures have been partially damaged. Therefore, the results of this study can provide a reference for the improvement of subsequent management project schemes, so as to mitigate post-earthquake debris flow disasters in scenic areas under the condition of future climate change.

### Differences in the Management of Debris Flows in Scenic and Mountainous Urban Areas

The management of debris flow disasters has attracted widespread attention in mountainous urban areas. For example, by comparing approaches to debris flow control in several countries in the world (including France, Italy, Austria, Switzerland, Japan, and North America), an approach involving the construction of check dams to comprehensively manage debris flow disasters at the basin scale was proposed. These check dams perform the functions of bed stabilization, hillslope consolidation, slope gradient reduction, sediment retention, and sediment transport regulation (Piton et al., 2016). Several studies on the types, regulation

#### **Recorded debris** Number Debris flow **Topographic parameters** Existed control Threat objects Proposed gullies flow event engineering control Watershed Main Average date mode area (km²) gully longitudinal length slope (‰) (km) 1 Debris flow gully 0.15 0.72 647 2013/5/5, 2013/5/17, Retaining wall Tourists and scenic Blocking and (10 km to Zechawa 2013/6/24, 2013/7/3, road deposit stopping village) 2017/6/20 2 Zechawa Gully 1.96 2.57 611 2016/8/4, 2019/6/21 Check dam, Tourists, scenic road, and walkways retaining wall З Zeduo Gully 9.6 4.4 386 2004 Check dam, bed Tourists and scenic sill, retaining wall road 4 Shuzheng Gully 4.86 2.5 404 1931, 1971, 1981, 1985, Check dams. Shuzhena village 1986, 1988, 2013/8/7, retaining wall tourists, scenic 2014/5 road, and Shuzheng Lakes 5 Rize No.2 Gully 7.9 5.2 266 2017/7/27, 2018/7/10 Check dams, Tourists and scenic retaining wall road 6 Meitan Gully 5.2 4.3 330 2017/7/27 Retaining wall Tourists and scenic road 7 Rize Gully 3 75 376 2017/7/27 Check dams, Tourists, Rize 3.73 embankment, protection station, retaining wall and scenic road 8 Arrow Bamboo 55 37 395 2008, 2017/7/27, 2017/9, Check dam. Tourists, walkways, 2018/6 Lake Gully retaining wall toilet, viewing platform, and Arrow Bamboo Lake 9 Debris flow gully 1.25 2.1 568 2016/8/4. 2017 Embankment, Tourists, scenic road, and Arrow (Arrow Bamboo retaining wall Bamboo Lake sightseeing Lake bus station) 10 Debris flow gully 1.42 2.2 501 2018/6/25, 2018/7/10 Check dams, Tourists and scenic (700 m to Guodu retaining wall road village) 11 West-Zhuozhui 1.33 1.77 517 2019/6/21 None Tourists and scenic Gully road 12 Zhuozhui Gully 4.14 3.3 386 2010, 2017/9, 2019/6/21, Retaining wall Tourists, scenic Deposit road, and walkways 2019/9/13 stopping 13 Zhongjijje Lake 6.1 3.5 338 2015/6/29, 2016/8/1, Retaining wall Tourists and scenic Gully 2017/9/13, 2017/10/4, road 2019/6/21 Debris flow Gully 14 2.69 2.06 563 2009/10, 2019/6/21 Bed sills, retaining Tourists, scenic (on the right side of wall road, and Xiajijie Xiajijie Lake) Lake 15 Debris flow gully 0.58 1.46 752 2017/9/27, 2018/6/25, Retaining wall Tourists and (1.6 km to Heye 2018/7/10 walkways village) 2013/8/7, 2016/8/10 Tourists and Panda 16 Panda Lake Gully 0.37 1.1 800 Retaining wall Lake 17 Five-color Lake 2.6 434 Bed sill, retaining Tourists, walkways, 3.5 Gully and Five-color Lake wall 18 Debris flow Gully 0.23 0.542 671 2018 Retaining wall Tourists, scenic (Mirror Lake road, bus station, sightseeing bus and Mirror Lake station) 19 Guodu Gully 1.7 2.3 554 2013/7/3, 2013/8/7, Bed sill, retaining Guodu village, 2018/6/25, 2018/7/10 tourists, and scenic wall road 19.89 1992, 2011, 2018/6/25 Check dams, Tourists, scenic 20 Keze Gully 7.2 268 Blocking embankment road, and walkways 2013, 2017/6 21 Nuorilang Gully 8.0 5.3 366 Check dams Zechawa village, tourists, and restaurant

TABLE 4 | Debris flow control mode in Jiuzhaigou Valley.

(Continued on following page)

#### TABLE 4 | (Continued) Debris flow control mode in Jiuzhaigou Valley.

Number	Debris flow gullies	Topographic parameters			Recorded debris	Existed control	Threat objects	Proposed
		Watershed area (km <sup>2</sup> )	Main gully length (km)	Average longitudinal slope (‰)	flow event date	engineering		control mode
22	Heye Gully	25.5	8.0	186	1948, 2018/6/25, 2018/ 7/10	Check dams	Heye village, tourists, scenic road, and Penjingtan attractions	
23	Debris flow gully (community group 1 of Heve village)	3	3.3	262	1948, 2018/6/25, 2018/ 7/10	Check dams, bed sill, embankment	Heye village	
24	Debris flow gully (opposite Swan Lake sightseeing bus station)	0.3	1.5	597		Check dams	Tourists	
25	Debris flow gully (Central Panda Lake)	3.9	2.9	501		Check dams	Tourists and Panda Lake	
26	Danzu Gully	73.88	16.2	87	1984	Check dams	Mirror Lake	
27	Mirror Gully	2.55	2.9	441	2018	Check dams	Tourists, scenic road, and walkways	
28	Nadi Gully	4.68	3.8	544	2011/9/5, 2015/6/1, 2017/9/27	Check dams, embankment	Burning incense attractions and scenic road	
29	Rexi Gully	8.24	5.81	372	2018/6/25, 2018/7/10	Check dams, bed sill, embankment	Rexi village and tourists	
30	Xuan Gully	0.56	1.05	795	2013/7/3, 2013/7/28, 2013/8/3, 2013/8/7, 2015/6/28, 2019/6/21	Drainage channel, retaining wall	Tourists, scenic road, and Xiajijie Lake	Drainage and deposit stopping
31	Xiajijie Lake Gully	1.87	2.36	593	1976, 1983, 1984, 2012/ 7/21, 2013/7/3, 2013/7/ 28, 2017/9/9, 2017/9/14, 2017/9/24, 2017/9/25, 2019/6/21	Check dams, drainage channel, retaining wall	Tourists, scenic road, walkways, and Xiajijie Lake	
32	Pingshitou Gully	0.1	0.9	775	2011/9/5, 2012/8/13, 2019/7/22, 2020/5/6	Check dams	Tourists and scenic road	

Note: The occurrence time of the recorded debris flow events is taken from the annual disaster survey report of Jiuzhaigou Valley and the investigation report for the control of debris flow disasters in Jiuzhaigou Valley. The locations of all debris flow gullies in the table have been marked in **Figure 10**.

mechanisms, and disaster mitigation effects of check dams have been conducted (DeWolfe et al., 2008; Piton and Recking 2016; Cucchiaro et al., 2019a; Cucchiaro et al., 2019b; Bernard et al., 2019). In China, it is more common to implement management measures for debris flow gullies at the regional scale. The "stabilization + blocking + drainage + deposit stopping" control modes are adopted in the formation, transport, and deposition zones, respectively, with blocking measures being the most commonly implemented measures (Cui and Lin, 2013; Liu et al., 2017). This control approach is similar to that employed in Japan (Ikeya 1989; Takahashi 2007). However, after the Wenchuan earthquake, the frequency and scale of occurrence of debris flow disasters have increased significantly, and existing engineering projects have not been able to effectively mitigate these disasters. Moreover, a large number of engineering projects, particularly check dams, have been seriously damaged (Wang 2013; Chen et al., 2015). Therefore, many scholars have proposed a new approach for disaster mitigation. The proposed approach, which has proven to be effective, prioritizes the use of drainage measures, and makes full use of the transport capacity of the main river to discharge debris flow material to downstream rivers (Chen et al., 2015; Xiong et al., 2016).

The aforementioned studies have mainly focused on typical mountainous urban areas, and the proposed control methods cannot be applied to the mitigation of debris flows in the scenic area investigated herein. The reasons for this are as follows: 1) Owing to topographic conditions, no large river exists in the scenic area, and the water bodies (such as Long Lake and Nuorilang Waterfall in Jiuzhaigou Valley) distributed throughout the scenic area are important landscape resources that do not exhibit conditions conducive to the discharge of debris flow material. Thus, the control method proposed by Chen et al. (2015) is not applicable in this area. 2) Compared with the debris flow control projects in typical mountainous urban areas, debris flow control projects in scenic areas can only be implemented in the experimental zones owing to restrictions related to the functional zoning of nature reserves; it is impossible to implement large-scale engineering projects for debris flow control at the watershed scale. Therefore, the control method proposed by Piton et al. (2016) is

inappropriate for this area. The scale of debris flow disasters in scenic areas is smaller than that of disasters in typical mountainous urban areas owing to the lush vegetation and the smaller watershed area of debris flow gullies in scenic areas. Thus, the construction of small projects in the transport and deposition zones can meet the design requirements. Furthermore, these small projects are easy to integrate with the landscape and do not significantly damage the environment in scenic areas.

### Limitations of the Engineering Planning Method

This study proposed an engineering planning method for debris flow control in scenic areas, with the aim of providing guidance for relevant stakeholders to rapidly formulate control engineering plans for different debris flow gullies in scenic areas after debris flow disasters, especially mass debris flow disasters after earthquakes. However, the following limitations should be considered when this planning method is used for debris flow control engineering in scenic areas. 1) Owing to the difference of topographic conditions and threatened objects, the applicability of this planning method to debris flow control engineering planning in other scenic areas requires further verification. 2) This planning method adopts a large number of equations recommended by the code to calculate the design parameters of debris flow control engineering projects. These equations can be used to obtain the calculated values based on a small number of parameters, so they are widely used. However, the values of relevant parameters vary in different areas, so local norms should be consulted when this planning method is used to plan debris flow control projects in other scenic areas. 3) In this study, only engineering measures are considered for the control of debris flow in scenic areas. Ecological measures should also be considered for the treatment of debris flow in scenic areas. This aspect can be explored in future work.

## CONCLUSION

Based on field investigations of existing debris flow control projects in scenic areas, a planning method for debris flow control projects in scenic areas is proposed. The planning method first involves the determination of the scope of the area in which the control project can be implemented, based on the requirements related to the functional zoning of the scenic area. Then, based on the objects threatened by debris flows and the topographical features of debris flow gullies in the scenic area, the "blocking + deposit stopping," "deposit stopping," "blocking," and "drainage + deposit stopping" control modes are adopted. Finally, the amount of debris flow material that can be intercepted by the engineering structure is quantified based on parameter calculations. Based on the planning method for debris flow control engineering in the scenic area, the shortcomings of the existing control engineering projects in the scenic area are discussed. For the debris flow gullies in Xiajijie Lake, Zhuozhui, Xuan, Pingshitou, and West-Zhuozhui, the "drainage + deposit stopping," "deposit stopping," "drainage + deposit stopping," "drainage + deposit stopping," and "blocking + deposit stopping" control engineering schemes are proposed, respectively. The

proposed control engineering schemes meet the requirements of coordination with the landscape and ecosystem.

On this basis, the control mode of debris flow disasters in scenic areas is discussed: 1) For debris flow gullies with severe erosion and conditions that are conducive to deposit stopping, blocking projects should be constructed in the transport zone and deposit stopping projects should be constructed in the deposition zone within the construction area of debris flow control projects. 2) For debris flow gullies without severe erosion but which exhibit conditions conducive to deposit stopping, only deposit stopping projects should be constructed in the deposition zone within the construction area of debris flow control projects. 3) For debris flow gullies that do not exhibit conditions conducive to deposit stopping but for which the channel in the transport zone exhibits material conditions conducive to debris flow retention, only blocking projects should be constructed in the transport zone within the construction area of debris flow control projects. 4) For debris flow gullies that do not exhibit conditions conducive to deposit stopping and for which the channel in the transport zone does not exhibit material conditions conducive to debris flow retention, drainage projects should be constructed in the transport zone to discharge the debris flow material into the recesses on both the sides of the gully, and deposit stopping projects should be constructed to retain the diverted material. The results of this study are expected to provide a systematic control strategy for debris flow disaster management in scenic areas.

### DATA AVAILABILITY STATEMENT

The original contributions presented in the study are included in the article/supplementary material, further inquiries can be directed to the corresponding author.

### **AUTHOR CONTRIBUTIONS**

X-LG and K-TC contributed to the conceptualization, methodology, analysis and manuscript writing of the study. X-QC proposed the main structure of this study and approved the final version. W-YZ and J-GC participate in field investigations and helped perform the analysis with constructive discussions.

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