



# Intelligent Prediction of Multi-Factor-Oriented Ground Settlement During TBM Tunneling in Soft Soil

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Tunneling-induced ground surface settlement is associated with many complex influencing factors. Beyond factors related to tunnel geometry and surrounding geological conditions, operational factors related to the shield machine are highly significant because of the complexity of shield-soil interactions. Distinguishing the most relevant factors can be very difficult, for all factors seem to affect tunneling-induced settlement to some degree, with none clearly the most influential. In this research, a machine learning method is adopted to intelligently select features related to tunneling-induced ground settlement based on measured data and form a robust non-parametric model with which to make a prediction. The recorded data from a real construction site were compiled and 12 features related to the operational factors were summarized. Using the intelligent method, two other features in addition to cover depth–pitching angle and rolling angle—were distinguished from among the 12 feature candidates as those most influencing the settlement trough. Another new finding is that advance rate does not emerge in the top 10 selected models from the observational data used. The generated non-parametric model was validated by comparing the measured data from the testing dataset and performance on a new dataset. Sensitivity analysis was conducted to evaluate the contribution of each factor. According to the results, engineers in general practice should attend closely to pitching angle during tunnel excavation in soft soil conditions.

**Keywords:** tunneling-induced settlement, feature selection, non-parametric, pitching angle, operational factor

## 1 INTRODUCTION

Underground tunneling is necessary for transportation in urban areas having a large population, and the shield tunnel boring machine (TBM) approach has become popular for its construction, having less effect on the surrounding environment, a relatively high construction rate and so forth. (Verruijt and Booker, 1996; Zheng et al., 2017; Zhou et al., 2017; Elbaz et al., 2018; Wu et al., 2018; Chen et al., 2019; Lin et al., 2021; Yan et al., 2021; Elbaz et al., 2022; Shen et al., 2022). Nevertheless, ground surface deformations may have destructive effects on adjacent buildings and facilities, raising

concerns for engineers and researchers (Leca and New, 2007; Marshall et al., 2010; Zhao et al., 2016; Soga et al., 2017; Zhao et al., 2017; Zhao et al., 2019a; Lu et al., 2019; Moeinossadat and Ahangari, 2019). Accordingly, engineers and researchers strive for reliable estimations of ground surface settlement and have gone to great lengths to model tunneling-induced deformation, including through use of empirical and analytical approaches (Loganathan and Poulos, 1998; Chou and Bobet, 2002; Wu et al., 2018), numerical methods (Maynar and Rodríguez, 2005; Paternesi et al., 2017; Yang et al., 2020; Lyu et al., 2022), and artificial intelligence methods (Santos and Celestino, 2008; Boubou et al., 2010; Zhang et al., 2019; Hajihassani et al., 2020; Lin et al., 2021).

Conventional empirical formulas (Attewell and Hurrell, 1985) present only a limited number of parameters for predicting ground surface settlement. For instance, Peck (Peck, 1969) adopted an inverse Gaussian probability distribution curve, which can be defined by a few parameters to describe the transverse deformation profile of tunneling-induced ground surface settlement based on field observations. Loganathan and Poulos (1998), finding these empirical solutions to lack sufficient influencing factors, introduced the concept of the “undrained gap parameter” with which to consider geometry and equivalent 3D elastic features in their proposed analytical predictions. Because their calculation method is valid only for homogeneous purely elastic clay, the observed settlement in uniform clay has mostly a narrower trough with a larger depth than in the Loganathan and Poulos method of calculation. In these analytical methods (Wu et al., 2015; Elbaz et al., 2018; 2018; Xu and Bezuijen, 2018), each input variable has its own physical meaning and changes in tunneling-induced settlement are interpretable. Nevertheless, some ideal assumptions are inevitable in these analytical methods so as to obtain a closed form solution, potentially causing deviations from practical field measurements, as ideal assumptions could eliminate certain features used to estimate the settlements and also neglect plastic deformation in the soil. Considering the complexity of tunneling-induced settlement, some researchers (Ng et al., 2013; Ibrahim et al., 2015; Soranzo et al., 2015; Zhang et al., 2017; Alagha and Chapman, 2019; Lin et al., 2019) have turned to numeric simulations that integrate complicated boundary conditions, spatial variations of stratigraphy, and elastoplastic soil behavior. Ng and Lee (2005) conducted a series of three-dimensional numerical simulations to evaluate ground deformations. Huang et al. (2015) used a simplified procedure to analyze the longitudinal performance of shield tunnels and investigated spatial variability using the finite element method. The limitation of numerical methods, however, lies in the evaluation of the input parameters involved in the constitutive models (Ninić et al., 2017). Besides, implementing all operational factors in numeric simulations simultaneously is challenging (Khisamitov and Meschke, 2018; Ren et al., 2018; Shen et al., 2019). However, these operational factors are significant for estimation of tunneling-induced ground surface settlement. Ren et al. (2018) (Ren et al., 2018) evaluated the gap area between the double-O-tube (DOT) shield

machine by considering pitching, yawing, and rolling features. Shen et al. (2019) considered pitching angle and yawing angle to investigate shield-soil interactions and proposed a prediction model. Owing to the complexity of shield-soil interactions, data-driven models were triggered using artificial intelligence methods (Cho, 2009; Ochmański et al., 2015; Chen et al., 2016; Pooya Nejad and Jaksa, 2017; Qi and Tang, 2018). Through the flexibility of machine learning methods, some scholars have generated various models with which to make predictions (Shi et al., 1998; Mahdevari et al., 2012; Chen et al., 2016; Bouayad and Emeriault, 2017; Hajihassani et al., 2019). Neaupane and Adhikari (2006) adopted a multi-layer backpropagation neural network to predict tunneling-induced ground movement. Ahangari et al. (2015) adopted Adaptive Neuro-Fuzzy Inference System (ANFIS) and Gene Expression Programming (GEP) methods to establish the relationship between possible influencing factors and tunneling-induced settlement.

In these artificial intelligence methods, the features which is to say influencing factors used to predict ground surface settlement have been summarized chiefly based on experience, which is inherently subjective. Suwansawat and Einstein (2006) classified factors affecting the surface settlement into three categories: The first is related to tunnel geometry, such as tunnel depth and tunnel diameter. The second concerns geological conditions, such as geology at the tunnel crown and invert. The third comprises shield operation factors, such as face pressure, advance rate, pitching angle, etc. Their study provided a comprehensive understanding of possible influencing factors, which they integrated to form a neural network with which to make estimations. Ahangari et al. (2015) selected the same five features adopted in Darabi et al. (2012) to predict tunneling-induced settlement. Santos and Celestino (2008) found that it was not possible to establish a clear relationship between advance rate and surface settlement. Zhang (2019) introduced global sensitivity analysis for feature selection and evaluated the importance of each input variable. Introducing irrelevant input variables can distort the Euclidean distance between different points and degrade the flexibility of prediction. However, seldom have researchers extracted significant features and eliminated irrelevant input candidates so as to obtain a robust prediction model.

In recent decades, the Bayesian inference method has been widely applied in various fields of geotechnical engineering, such as for consolidation (Kelly and Huang, 2015), braced excavation (Qi and Zhou, 2017), pile engineering (Park et al., 2012), and soil nailing (Zhou et al., 2013). One merit of this approach lies in uncertainty quantification; (Phoon and Kulhawy, 1999) an other in model selection (Gamse et al., 2018; Tan et al., 2018; Zhou et al., 2018; Jin et al., 2019a; Jin et al., 2019b). These merits allow the selection of a set of suitable input parameters from designed candidates. Yuen and Ortiz (2016) proposed a novel algorithm, Bayesian nonparametric general regression (BNGR), with which to filter out unrelated input parameters from among possible candidates. This algorithm reformulated the general regression neural network under the Bayesian framework. Except for the ability to reduce unrelated input parameters, this method can

preclude the effects of the prior distribution for the adopted regression coefficients—a common challenge in Bayesian frameworks. It provides the possibility of selecting suitable input parameters for complex problems involving many plausible input parameters, such as TBM tunneling projects.

In the present study, 12 possible input parameters potentially influencing maximum tunneling-induced settlement were selected based on engineers’ experience and concerns (Suwansawat and Einstein, 2006; Shen et al., 2019). The BNGR method was introduced to extract relevant features and form a data-driven optimal model, which was validated using the testing database. Sensitivity analysis was conducted to examine the selected inputs. The proposed model was conducted on the new introduced dataset and its performance was examined by comparison with observational measured data. Influencing factors associated with maximum ground settlement were analyzed and discussed.

## 2 METHODOLOGY AND DATABASE

### 2.1 Bayesian Nonparametric General Regression Framework

#### 2.1.1 General Regression Neural Network

The GRNN method was proposed by Specht (1991) on the basis of the probabilistic neural network. This method can establish a non-linear relationship between inputs in multi-dimensional and corresponding outputs. Moreover, it is a one-pass learning algorithm without an iterative process, in contrast to the backpropagation process seen in other artificial neural network methods. It has been widely used in geotechnical engineering in recent decades (Theodosiou, 2011; Doulati Ardejani et al., 2013; Zhao et al., 2019b), such as for spatial prediction of soil contamination (Kanevski, 1999), soil type inference (Kurup and Griffin, 2006), and static pile capacity prediction (Pal and Deswal, 2008). Chen et al. (2019) evaluated different machine learning methods for tunneling-induced settlement and indicated that the GRNN method outperforms the back-propagation neural network and radial basis neural network in prediction.

The GRNN method involves an input layer, pattern layer, weighted layer, and output layer. Supposing that  $s$  represents tunneling-induced maximum ground settlement,  $\mathbf{w}$  is the designed inputs, and  $f(\mathbf{w}, s)$  is the joint probability density function, the regression of  $s$  given  $\mathbf{w}$  can be written as:

$$E(s|\mathbf{w}) = \frac{\int_{-\infty}^{\infty} s \cdot f(\mathbf{w}, s) ds}{\int_{-\infty}^{\infty} f(\mathbf{w}, s) ds} \tag{1}$$

$f(\mathbf{w}, s)$  is usually estimated from a sample of the measured  $\mathbf{w}$  and  $s$  using the kernel density approximation  $\hat{f}(\mathbf{w}, s)$ :

$$\hat{f}(\mathbf{w}, s) = \frac{1}{N(2\pi\sigma^2)^{(d+1)/2}} \sum_{n=1}^N \exp \left[ -\frac{(\mathbf{w} - \mathbf{w}_n)^T (\mathbf{w} - \mathbf{w}_n) + (s - s_n)^2}{2\sigma^2} \right] \tag{2}$$

where  $N$  is the number of measured samples and  $d$  is the dimension of input  $\mathbf{w}$ . The smoothing parameter,  $\sigma$ , is the only unknown to be calculated. Combining Eq. (2) and Eq. (1), the desired conditional value of  $s$  can be written as:

$$\hat{s}(\mathbf{w}) = E_{\hat{f}}(s|\mathbf{w}) = \frac{\sum_{n=1}^N s_n \exp \left[ -\frac{(\mathbf{w}_m - \mathbf{w}_n)^T (\mathbf{w}_m - \mathbf{w}_n)}{2\sigma^2} \right]}{\sum_{n=1}^N \exp \left[ -\frac{(\mathbf{w}_m - \mathbf{w}_n)^T (\mathbf{w}_m - \mathbf{w}_n)}{2\sigma^2} \right]} \tag{3}$$

To determine the appropriate value of  $\sigma^2$  and prevent possible over-fitting, the data point to be estimated is removed in the summation of Eq. 3, which can be formulated as:

$$\hat{s}(\mathbf{w}_m) = \frac{\sum_{\substack{n=1 \\ n \neq m}}^N s_n \exp \left[ -\frac{(\mathbf{w}_m - \mathbf{w}_n)^T (\mathbf{w}_m - \mathbf{w}_n)}{2\sigma^2} \right]}{\sum_{\substack{n=1 \\ n \neq m}}^N \exp \left[ -\frac{(\mathbf{w}_m - \mathbf{w}_n)^T (\mathbf{w}_m - \mathbf{w}_n)}{2\sigma^2} \right]} \tag{4}$$

Through fitting the measurements, the optimal value of  $\sigma^2$  can be obtained using Eq. 4.

The GRNN method bridges the designed inputs and the corresponding outputs. Nevertheless, the adopted designed inputs should be evaluated using experience or pre-judgment before being implemented in the GRNN method. The prior evaluation may bring uncertainties into the model inputs, which play an essential role in prediction. The ability to select models in Bayesian inferences allows selection of a suitable set of input variables from input candidates. Yuen and Ortiz (2016) proposed the innovative Bayesian nonparametric general regression (BNGR) algorithm, which can extract relevant input features for model prediction while simultaneously obtaining the non-parametric regression model. The BNGR algorithm is briefly introduced in the following section, but the detailed derivation process can be found in Yuen and Ortiz (2016).

#### 2.1.2 General Regression Under the Bayesian Framework

Assuming that  $s$  is the tunneling-induced ground surface settlement,  $C$  denotes the general regression model with a specified set of inputs, and  $\theta$  is the unknown parameter related to the smoothing parameter in GRNN method, then according to the Bayesian inference, the posterior PDF of  $\theta$  can be written as:

$$p(\theta|s, \mathbf{w}, C) = \frac{p(s|\theta, \mathbf{w}, C)p(\theta|C)}{p(s|\mathbf{w}, C)} \tag{5}$$

where  $p(s|\theta, \mathbf{w}, C)$  is the likelihood function with which to reveal fit performance based on observational data given the parameter vector,  $\theta$ .  $P(\theta|C)$  is the prior PDF of the unknown parameter,  $\theta$ .  $p(s|\mathbf{w}, C)$  indicates the normalizing constant.

The chain rule of probability is used to develop the likelihood function and the product of conditional PDFs is:

$$p(s|\theta, \mathbf{w}, C) = \prod_{m=1}^N p(s_m|s_1, \dots, s_{m-2}, s_{m-1}, \theta, \mathbf{w}, C) \quad (6)$$

where

$$p(s_m|s_1, \dots, s_{m-2}, s_{m-1}, \theta, \mathbf{w}, C) = (2\pi\sigma_{2,m}^2)^{-1/2} \exp\left[-\frac{(s_m - \hat{s}_{m|m-1}(\mathbf{w}_m))^2}{2\sigma_{2,m}^2}\right] \quad (7)$$

where  $\hat{s}_{m|m-1}(\mathbf{w}_m)$  is the estimation of  $s$  based on the first  $m-1$  observational data and can be expressed as:

$$\hat{s}_{m|m-1}(s_m) = \frac{\sum_{n=1}^{m-1} s_n \exp\left[-\frac{(w_m - w_n)^T (w_m - w_n)}{2\sigma_{1,m}^2}\right]}{\sum_{n=1}^{m-1} \exp\left[-\frac{(w_m - w_n)^T (w_m - w_n)}{2\sigma_{1,m}^2}\right]} \quad (8)$$

Yuen and Ortiz (2016) introduced the smoothing scale parameter,  $v_1$ , and the prediction error scale parameter,  $v_2$ , to integrate the smoothing parameters  $\sigma_{1,m}^2, m = 1, 2, \dots, N$ , and the prediction-error variances  $\sigma_{2,m}^2, m = 1, 2, \dots, N$ , in these conditional PDFs:

$$\sigma_{1,m}^2 = \frac{v_1}{m-1} \sum_{n=1}^{m-1} (X_m - X_n)^T (X_m - X_n) \quad (9)$$

$$\sigma_{2,m}^2 = \frac{v_2}{\sum_{n=1}^{m-1} \exp\left[-2(X_m - X_n)^T (X_m - X_n)\right]} \quad (10)$$

Then  $\theta = (v_1, v_2)$  is the generated unknown parameters in the BNGR method. The posterior PDF of this parameter can be derived as:

$$p(v_1, v_2|s, \mathbf{w}, C) \propto p(v_1, v_2)p(s|v_1, v_2, \mathbf{w}, C) \propto (v_2)^{-(N/2)} \exp\left[-\frac{1}{2v_2} \sum_{m=1}^N \Omega_m (s_m - \hat{s}_{m|m-1, v_1}(\mathbf{w}_m))^2\right] \quad (11)$$

where  $\Omega_m$  is expressed as:

$$\Omega_m = \sum_{n=1}^{m-1} \exp\left[-2(w_m - w_n)^T (w_m - w_n)\right] \quad (12)$$

The optimal value of  $v_2$  can be obtained using the following equation:

$$\frac{\partial p(v_1, v_2|s, \mathbf{w}, C)}{\partial v_2} = 0 \quad (13)$$

Based on a certain value of  $v_1$ ,

$$v_2^*(v_1) = \frac{1}{N} \sum_{m=1}^N \Omega_m (s_m - \hat{s}_{m|m-1, v_1}(\mathbf{w}_m))^2 \quad (14)$$

The parameter  $v_1^*$  can be numerically calculated by maximizing the following function:

$$g(v_1) = p(v_1, v_2^*(v_1)|s, \mathbf{w}, C) \quad (15)$$

After  $v_1$  and  $v_2$  are calculated, a general regression model is readily obtained. It should be noted that a regression model in this study means a non-parametric regression model with a subset of design variables. Suppose that  $d$  variables are included in the input domain, with different combinations of the designed variables, there will be  $N_c = (2^d - 1)$  subsets of input candidates. Bayesian model selection was applied to select the optimal model among the  $N_c$  model candidates. According to Bayes's theorem, the plausibility of a model candidate can be expressed as:

$$P(C^{(k)}|s, \mathbf{w}) = \frac{p(s|\mathbf{w}, C^{(k)})P(C^{(k)})}{\sum_{k=1}^{N_c} p(s|\mathbf{w}, C^{(k)})P(C^{(k)})} \quad (16)$$

where  $P(C^{(k)}) = 1/N_c$  is the prior plausibility for a certain model  $C^{(k)} (k = 1, 2, \dots, N_c)$  and this parameter is assumed to be the same for all models, while the evidence  $p(s|\mathbf{w}, C^{(k)})$  can be expressed as (Yuen and Ortiz, 2016):

$$p(s|\mathbf{w}, C^{(k)}) \approx \frac{2\Gamma(N/2 + 1)\sqrt{2\pi\prod_{m=1}^N (\Omega_m / |\hat{h}_k(v_1^*)|)}}{(B_{U1} - B_{L1})(B_{U2} - B_{L2})\pi^{N/2}} \times \left[\sum_{m=1}^N \Omega_m (s_m - \hat{s}_{m|m-1, v_1}(X_m))^2\right]^{-(N/2+1)} \quad (17)$$

This is the configuration of non-parametric regression under the Bayesian framework. Yuen and Ortiz (2016) identify two merits of the BNGR method. First, the variation of prior distribution in the regression coefficient,  $\theta$ , has no impact on the model selection in Eq. 16. Second, in contrast to traditional regression approaches, the proposed method dramatically decreases the number of model candidates, for the network is automatically generated based on the GRNN method and development of different function forms using the same subset of inputs is not necessary.

## 2.2 Description of Case History

This study investigated tunneling-induced maximum ground settlement in the construction section from Xueyuan Road Station to Gucui Road Station (Xueyuan–Gucui section) as well as from Fengtan Road Station to Gucui Road Station (Gucui–Fengtan section) of Metro Line 2 in Hangzhou, China (Figures 1, 2). A photo of the construction site is shown in Figure 2A, and the adopted Earth pressure balance (EPB) shield machine, “Shichuandao”, is presented in Figure 2B. The length of the Xueyuan–Gucui section is 975.385 m; its cover depth varies from 10.641 to 18.701 m. By contrast, the length of the Gucui–Fengtan section is 503.866 m, and its cover depth varies from 8.566 to 9.976 m. The geometries of these two sections are shown in Figure 3. The inner diameter of the tunnel is 5.5 m, and its outer diameter is 6.2 m. The thickness and width of a tunnel segment are 0.35 and 1.2 m, respectively. Extensive *in-situ* explorations and laboratory experiments were conducted in this project, whose geological profile is illustrated in Figure 4. One can observe that the tunnel mostly advanced through the muddy silty clay layer, the muddy clay layer with silt, and the muddy silty clay layer with silt. A photo of the soils is shown in

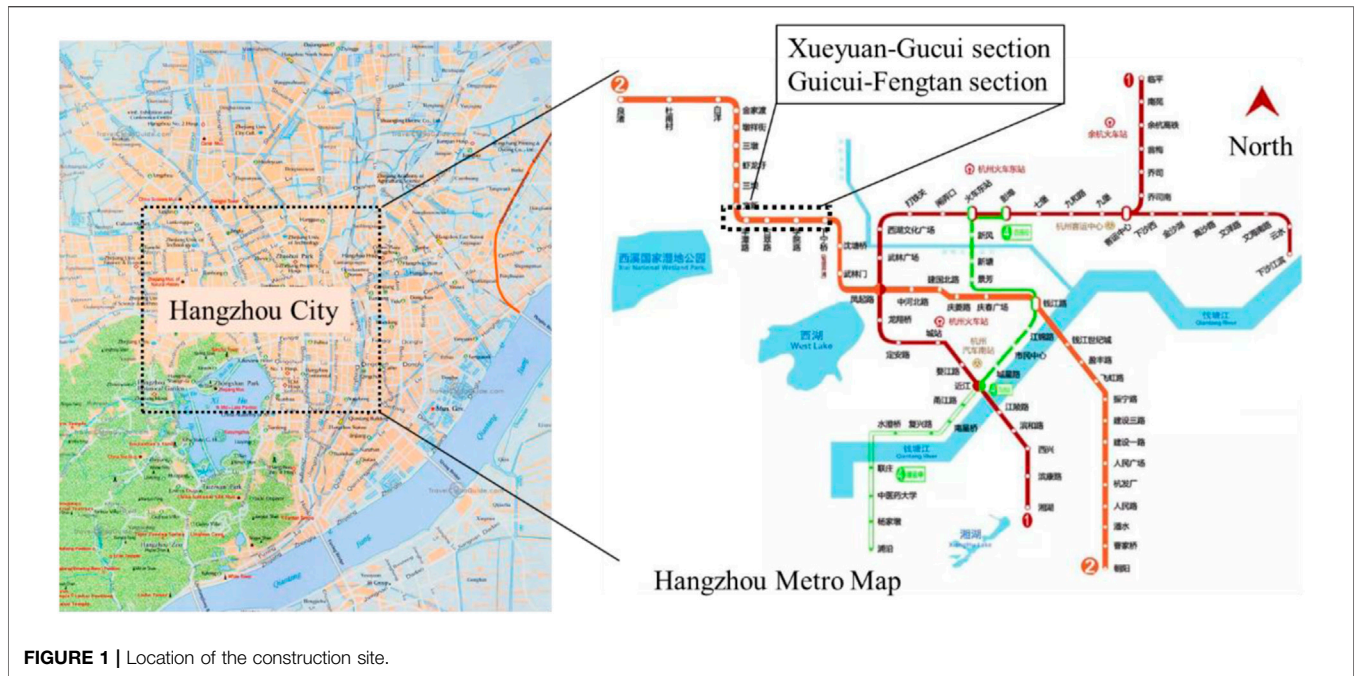


FIGURE 1 | Location of the construction site.

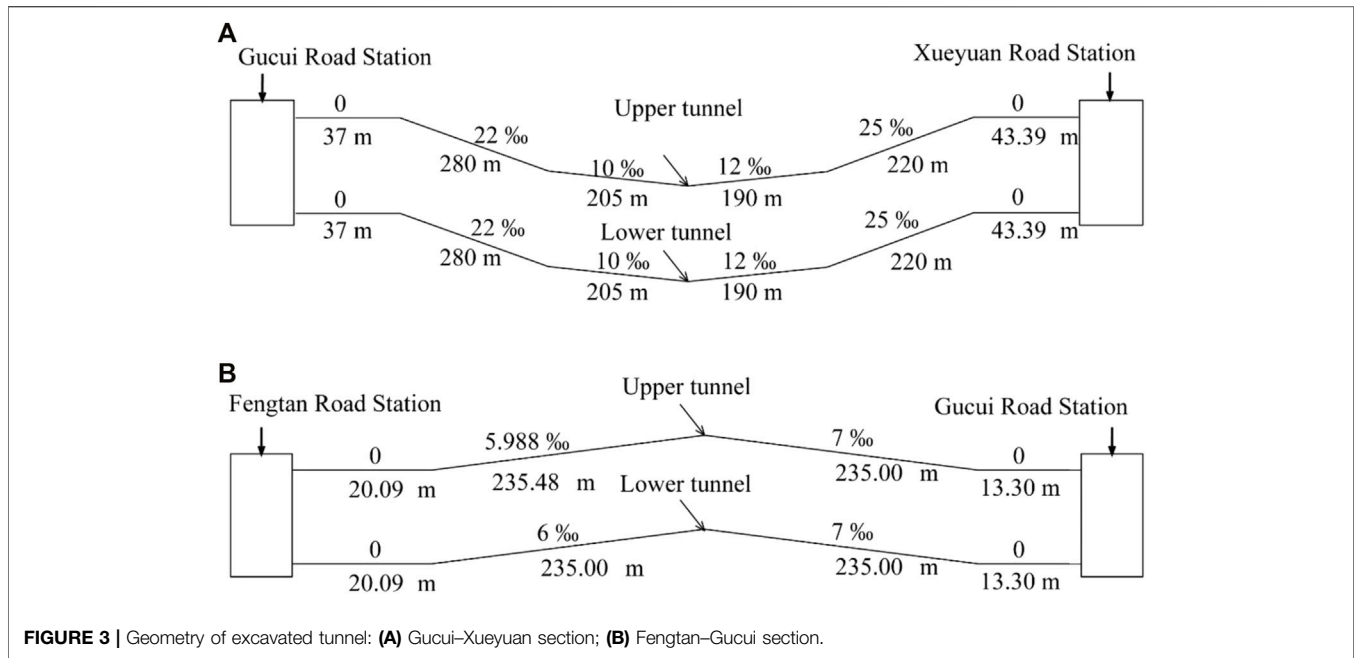


FIGURE 2 | (A) Construction site, (B) shield machine, and (C) soil sample at 10.0–15.0 m depth.

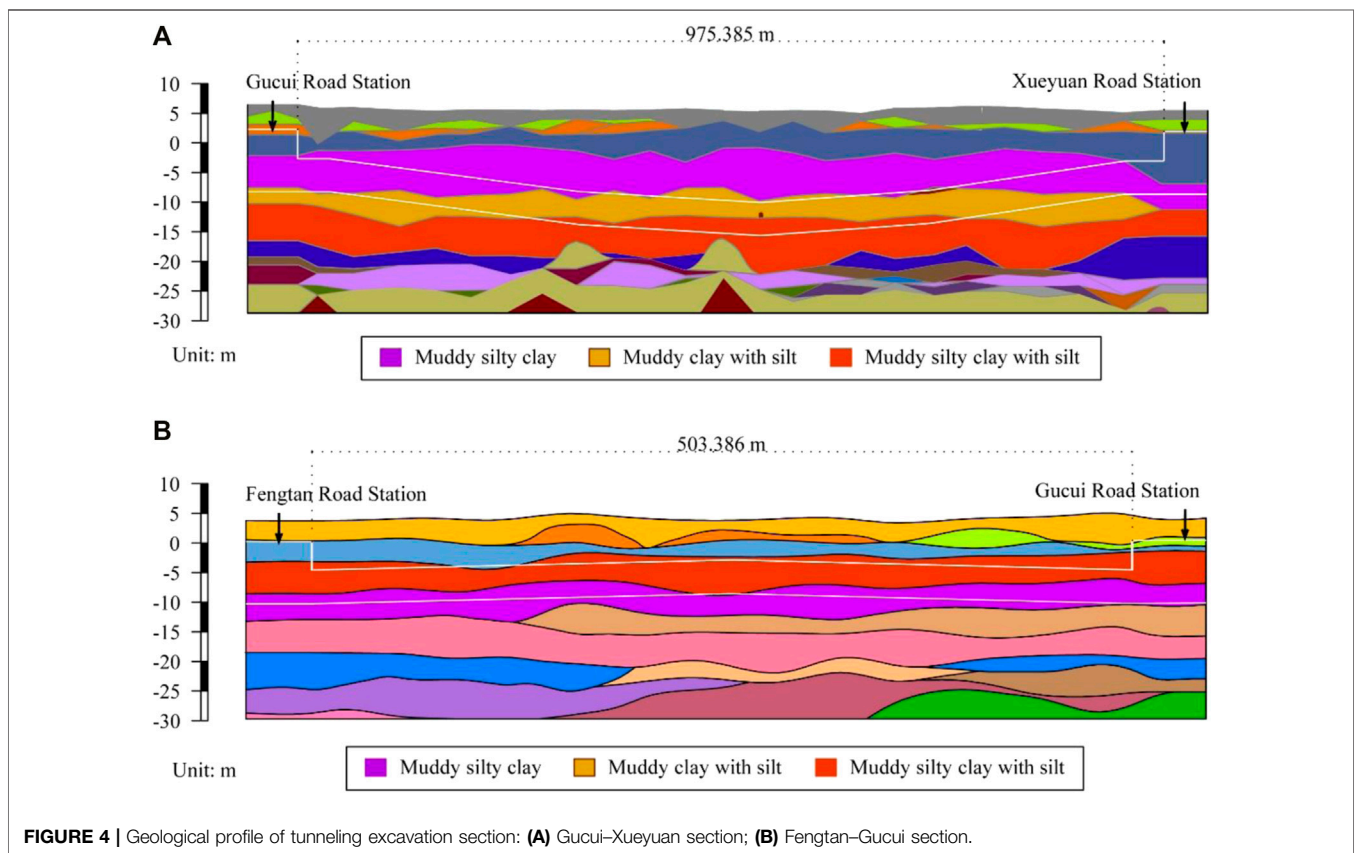
Figure 2C, and the soil properties of these three layers are presented in **Supplementary Table S1** in the supplemental data. The undrained shear strength,  $S_u$ , is obtained from the *in-situ* shear test, and the compression modulus is from the laboratory test of the remolded soil.

Along the tunnel alignment, the surface settlement markers were installed at approximately 6.0 m intervals (i.e., 5 segments)

as shown in **Figure 5**. What's more, perpendicular to the tunnel alignment, a settlement array was designed at roughly 30.0 m intervals (i.e., 25 segments), as presented in **Figure 5**. Fourteen measured points were set at each settlement array, with “Points 5” and “Point 10” positioned just above the left- and right-tunnel centerline, respectively. The measured points outside the two tunnel centerlines (left and right) were



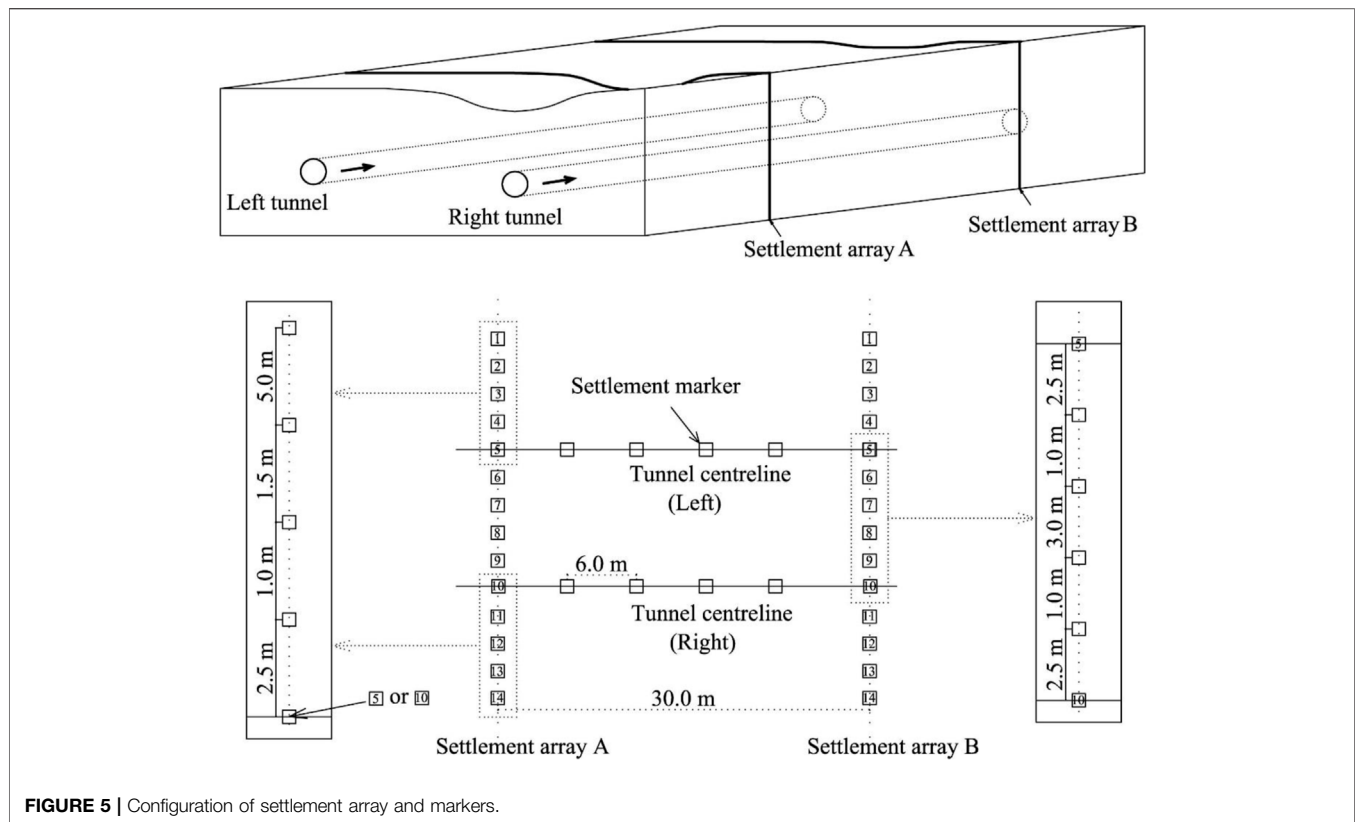
**FIGURE 3 |** Geometry of excavated tunnel: **(A)** Gucui–Xueyuan section; **(B)** Fengtan–Gucui section.



**FIGURE 4 |** Geological profile of tunneling excavation section: **(A)** Gucui–Xueyuan section; **(B)** Fengtan–Gucui section.

2.5 m, 3.5 m, 5.0 m, and 10.0 m, respectively, from the tunnel centerlines, as shown in **Figure 5**. The distances of the four measured points between the tunnel centerlines are also

presented in **Figure 5**. Settlement monitoring is conducted twice daily (8 a.m. and 3 p.m.). It should be noted that the observed ground settlement data above the right-tunnel line



**FIGURE 5** | Configuration of settlement array and markers.

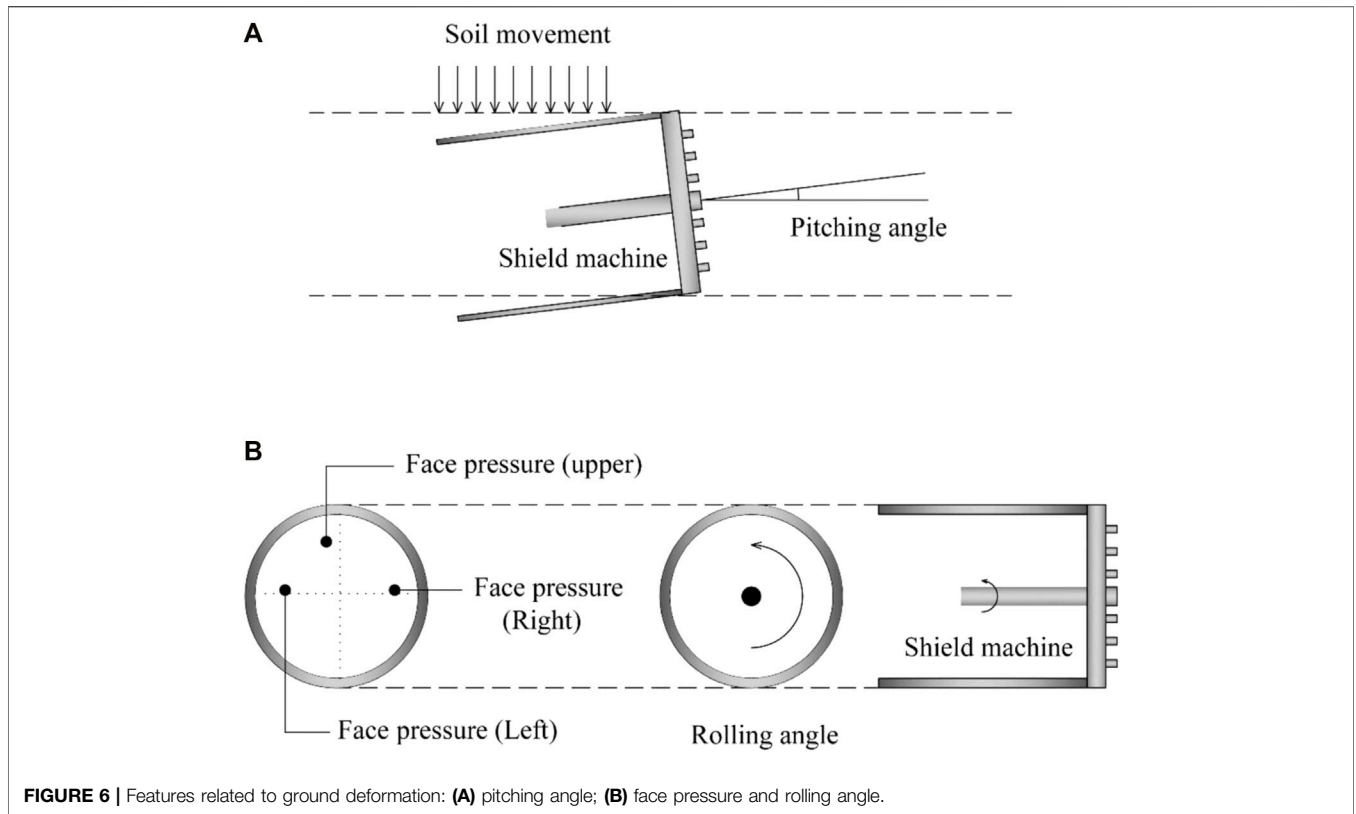
(excavated first) were applied in the present study and that data above the left-tunnel line were not introduced to prevent previously adjacent tunneling of the right-tunnel line from affecting ground settlement of the left-tunnel line. For each segment, the operational parameters, such as, face pressure, thrust, and torque, were automatically recorded. Based on the three categories of influencing factors suggested by Suwansawat and Einstein (2006), the following features may be associated with tunneling-induced maximum ground settlement:

- Advance rate ( $x_1$ ): calculated using the excavated distance over the total time in every excavation cycle;
- Cover depth ( $x_2$ ): the distance from the ground surface to the crown of the excavated tunnel;
- Pitching angle ( $x_3$ ): the discrepancy between the designed alignment and the central axial line of the shield machine (**Figure 6**);
- Rolling angle ( $x_4$ ): the slight rotation of the shield machine during the excavation process, as shown in **Figure 6**;
- Horizontal deviation ( $x_5$ ): the discrepancy between the designed tunnel alignment and the real tunnel centerline in the horizontal direction;
- Vertical deviation ( $x_6$ ): the discrepancy between the designed tunnel alignment and the real tunnel centerline in the vertical direction;
- Face pressure (upper) ( $x_7$ ): the soil pressure in the upper chamber (in this research, the face pressure was subdivided

into face pressure (upper) and face pressure (Middle), as shown in **Figure 6**);

- Face pressure (middle) ( $x_8$ ): the average face pressure of the left and right chambers, as presented in **Figure 6**—monitored using Earth pressure cells installed inside the chambers;
- Thrust ( $x_9$ ): driven by hydraulic power; used to drive the shield ahead and control the pose of shield machine;
- Torque ( $x_{10}$ ): used to cut the soil at the front of shield machine; will develop shear deformation in the soil;
- Soil removal rate ( $x_{11}$ ): used to measure how quickly the excavated soil volume is transported from the shield face;
- Soil removal volume ( $x_{12}$ ): the excavated soil volume transported from the shield face by a balanced screw conveyor.

In the present tunneling project, a new mixture composition of grouting fill was designed, as shown in **Supplementary Table S3** in the supplemental data. The lime was introduced as an additional component to accelerate the hardening and thus mitigate the uplift of the tunnel tube. Grouting pressure and filling were maintained around 0.35–0.36 MPa and 4.0–4.5 m<sup>3</sup> per segment, respectively, and features related to grouting were not considered in the present study due to the tiny variations involved. Nevertheless, the present algorithm can be used to consider the grouting pressure and filling as input candidates when the record data are available. It should be noted that grouting pressure and filling have been found to be important



**FIGURE 6 |** Features related to ground deformation: **(A)** pitching angle; **(B)** face pressure and rolling angle.

**TABLE 1 |** Model selection results.

Model	Plausibility	Likelihood	Evidence	$v_1$	$v_2$
Model-1: (2, 3, 4)	0.9702	$1.37 \times 10^{-36}$	$2.68 \times 10^{-43}$	$5.03 \times 10^{-4}$	1.2625
Model-2: (2, 3, 4, 7, 9)	0.0130	$1.56 \times 10^{-39}$	$3.57 \times 10^{-45}$	0.0080	0.5509
Model-3: (2, 3, 4, 9)	0.0097	$2.36 \times 10^{-39}$	$2.67 \times 10^{-45}$	0.0068	0.9640
Model-4: (2, 3, 4, 7)	0.0027	$3.70 \times 10^{-40}$	$7.34 \times 10^{-46}$	0.0066	0.8238
Model-5: (2, 3, 12)	0.0022	$3.63 \times 10^{-39}$	$6.00 \times 10^{-46}$	0.0018	1.7063
Model-6: (2, 3, 4, 9, 12)	0.0013	$3.43 \times 10^{-40}$	$3.46 \times 10^{-46}$	0.0043	0.7644
Model-7: (2, 3, 4, 12)	$7.47 \times 10^{-4}$	$9.49 \times 10^{-40}$	$2.06 \times 10^{-46}$	$9.35 \times 10^{-4}$	1.1320
Model-8: (2, 3, 7, 9, 12)	$1.82 \times 10^{-4}$	$2.55 \times 10^{-41}$	$5.03 \times 10^{-47}$	0.0062	0.4558
Model-9: (2, 3, 11)	$6.45 \times 10^{-5}$	$1.02 \times 10^{-40}$	$1.78 \times 10^{-47}$	0.0018	1.7382
Model-10: (2, 3, 4, 11)	$1.63 \times 10^{-5}$	$2.10 \times 10^{-41}$	$4.51 \times 10^{-48}$	$9.59 \times 10^{-4}$	1.1567

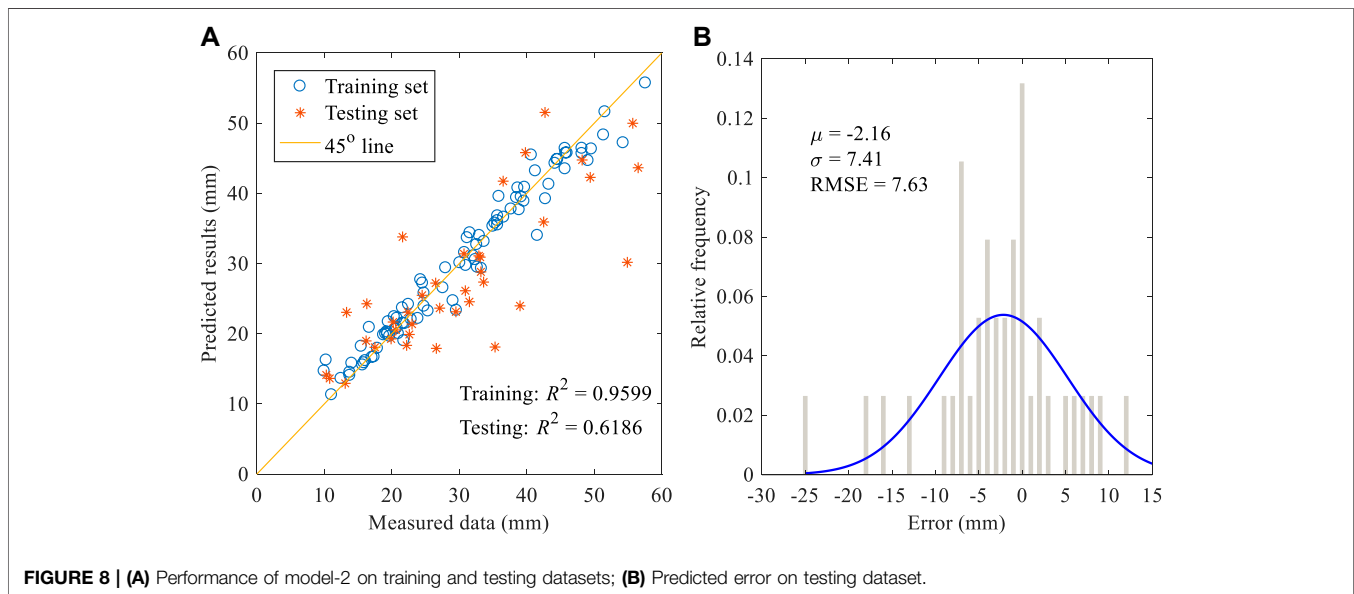
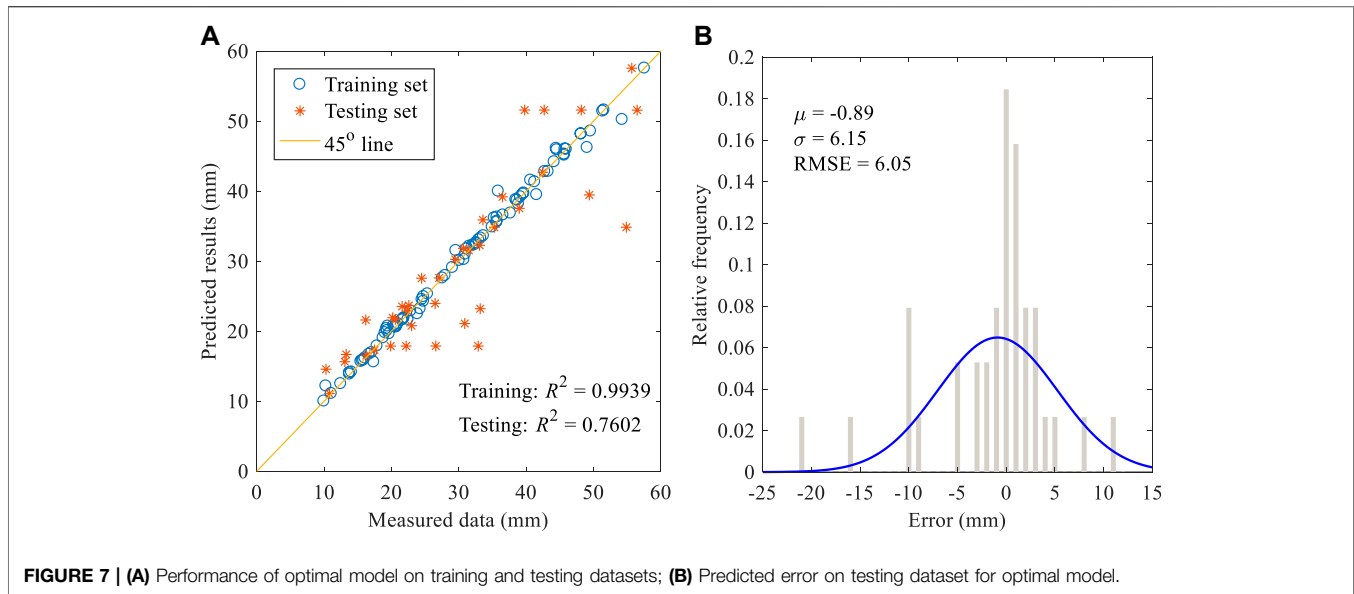
parameters in tunnel excavation with which to control maximum ground surface settlement.

### 2.3 Preparation of Database

According to the classification proposed by Suwansawat and Einstein (2006), the features used to estimate the maximum ground settlement were separated into three categories: geological properties, tunnel geometry, and operation factors. The geological properties are closely related to the friction between shield and soil and were investigated by many researchers (Chen et al., 2019; Bouayad and Emeriault, 2017). The geological properties were evaluated according to the friction angle and cohesion as presented in **Supplementary Table S1** in the supplemental data. The contact areas between the shield and

different soil layers were considered as the weights to evaluate the geological index. Then, the geological index can be used as one influencing factors. **Supplementary Table S1** in the supplemental data indicates that there is little variation of geological properties in the zone where the tunnel crossed, so that geological features can be neglected in the present study. Nevertheless, the geological variation is important for tunnelling induced settlement. The methodology proposed by Chen et al. (2019) is adopted to consider the geological variation. This novel approach associated the location and thickness of soil layers and the soil properties and these geological properties can be quantified using formulas. The detailed description is shown in the study of Chen et al. (2019). Furthermore, in the whole excavation section, the same shield tunnel boring machine was used, with uniform





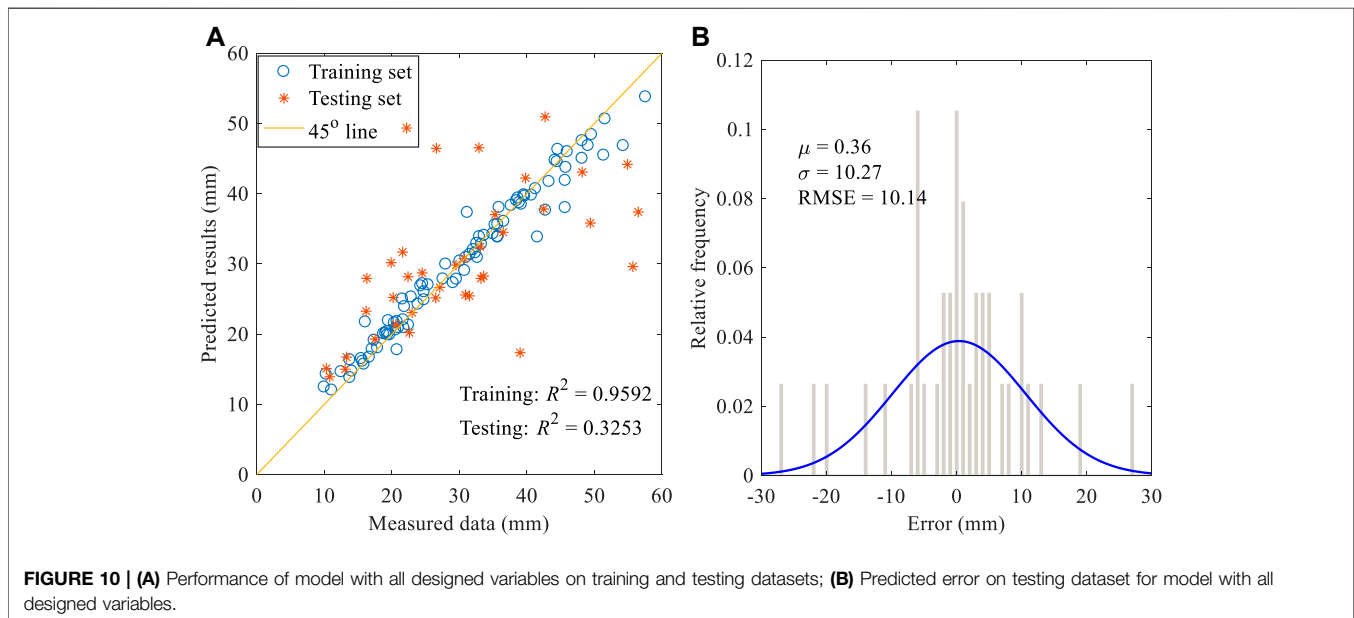
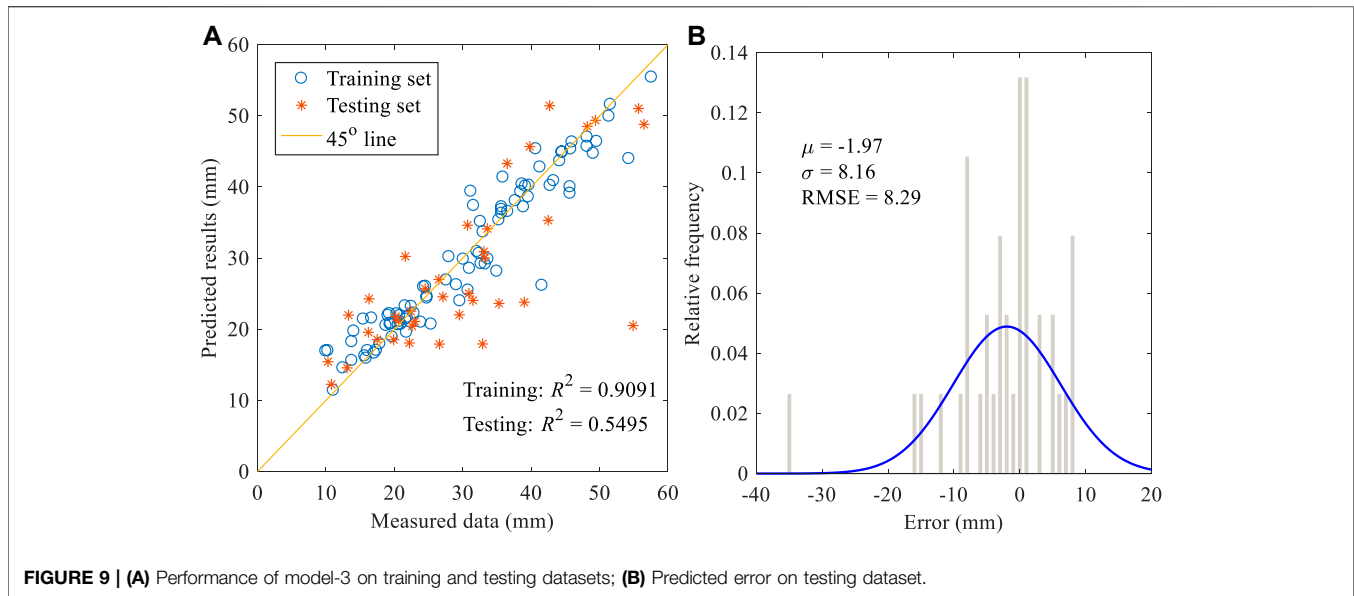
diameter maintained. Hence the cover depth is the only parameter in the category of tunnel geometry, with the overburden thickness at the middle of each segment collected to form a database of cover depth. It should be noted that the tunnel diameter is an important factors related to the ground maximum settlement. This can be a significant factors when the database contains varying diameter. Advance rate is calculated by advance distance over advance time in each segment. Average values in each segment were calculated for the other operational factors (Chen et al., 2019), with 12 features in total summarized in this tunnel project. 126 datasets were compiled, including input candidates and corresponding maximum ground surface settlement. **Supplementary Table S2** in the supplemental data illustrates the statistic characteristics of these input candidates and the related maximum ground surface settlement.

### 3 MODEL SELECTION AND VALIDATION

The 126 observational data sets were randomly divided into a training dataset (70%), used for selecting optimal model and identifying parameters (i.e., smoothing scale parameter, and prediction error scale parameter), and a testing dataset (30%), used to examine the proposed model. All designed input candidates were normalized using the following equation:

$$\bar{w} = \frac{w - w_m}{\sigma} \quad (18)$$

where  $w_m$  stands for the mean value of designed input candidates.  $\sigma = \sqrt{\frac{1}{N-1} \sum_{i=1}^N (w - w_m)^2}$  is the standard deviation.  $N$  is the number of samples. According to the principle of the BNGR



method,  $2^{12}-1 = 4,095$  model candidates were generated on the basis of the 12 design input variables. Prior distributions of the smoothing scale factor and the prediction error scale factor were assumed to follow the uniform distribution with the range (0, 50). Choice of prior distribution for these two parameters had no effect on model selection (Yuen and Ortiz, 2016). **Table 1** presents the model selection results based on these model candidates, with the first column exhibiting the included variables for the top 10 models: 1 standing for feature  $x_1$ , 2 for feature  $x_2$  and so forth. Plausibility, maximum likelihood, and evidence are indicated in the second, third, and fourth columns. The fifth and sixth columns denote the updated smoothing scale

factor,  $v_1$ , and the prediction error scale factor,  $v_2$ . From **Table 1**, the most plausible model contains the features of cover depth, pitching angle, and rolling angle. The performance of this optimal model on the training dataset is shown in **Figure 7A** with a coefficient of determination  $R^2 = 0.9939$  and a root mean square error (RMSE) is 0.9227. This figure also presents predicted settlement versus measured data for the testing dataset, with points scattering around the perfect match line (i.e., 45° line) and a coefficient of determination  $R^2 = 0.7602$ . Model performance for the training and testing datasets for model-2 and model-3 in **Table 1** is illustrated in **Figure 8A** and **Figure 9A**, respectively. The coefficients of determination,  $R^2$ , for the top three models

diminished with declining model ranking. **Figure 10A** presents the trained model with all 12 designed input variables. The coefficient of determination,  $R^2$ , for the training dataset is acceptable, but the predictions fail on the testing dataset and  $R^2$  is 0.3253. Accordingly, when irrelevant features are introduced into the input variables, Euclidean distance is distorted and the proposed model cannot capture the relationship between inputs and output. **Figures 7B, 8B, 9B, 10** illustrate an analysis of the errors between predicted and measured ground settlements for the testing database. The standard deviation of the error expands with declining order of model ranking and reaches largest for the model having all 12 designed input variables. RMSEs are presented in these figures as well, following the trend of the standard deviation as presented in Figures 7B, 8B, 9B, 10B. This indicates that the selected optimal model is robust and exhibits acceptable performance in estimating ground settlement. It should be noted that extrapolation is not recommended when using the BNGR method. Because the data points beyond the domain of the training dataset are far from the sampling points in the GRNN algorithm, inducing a relatively large error. In practice, new datasets should be drawn outside the range of the existing training database when making new predictions.

## 4 DISCUSSION

### 4.1 Feature Selection

Based on the model selection results in **Table 1**, the overburden depth is the main feature associated with ground settlement, as has been recognized by many researchers. The pitching and rolling angles of the shield machine are included in the optimal model. Pitching angle represents the shield machine's orientation during tunneling. Changes in pitching angle, which are inevitable, may create a gap between shield machine and surrounding soil, inducing ground deformation. Rolling angle evolves from the torque of the shield machine during excavation. To provide anti-support for the cutter-head torque, self-rotation may develop in the shield machine. Shear resistance between shield machine and surrounding soil may induce ground deformation. What's more, as indicated by **Supplementary Table S1** in the supplemental data, soft soil conditions surrounding the shield machine are sensitive to tunneling-induced disturbances. Shield-soil interactions generated from the pitching and rolling angles can significantly influence ground surface settlement in such soil conditions. All this may help in interpreting the selected three input variables in the optimal model. Pitching and rolling angles as features predicting ground settlement should be considered in future studies, especially those conducted under soft soil conditions. In the second-best model (model-2), in addition to the three selected input variables in the optimal model (i.e., cover depth, pitching angle, rolling angle), thrust and face pressure (upper) were extracted from the input candidates. This indicated that thrust and face pressure (upper) could

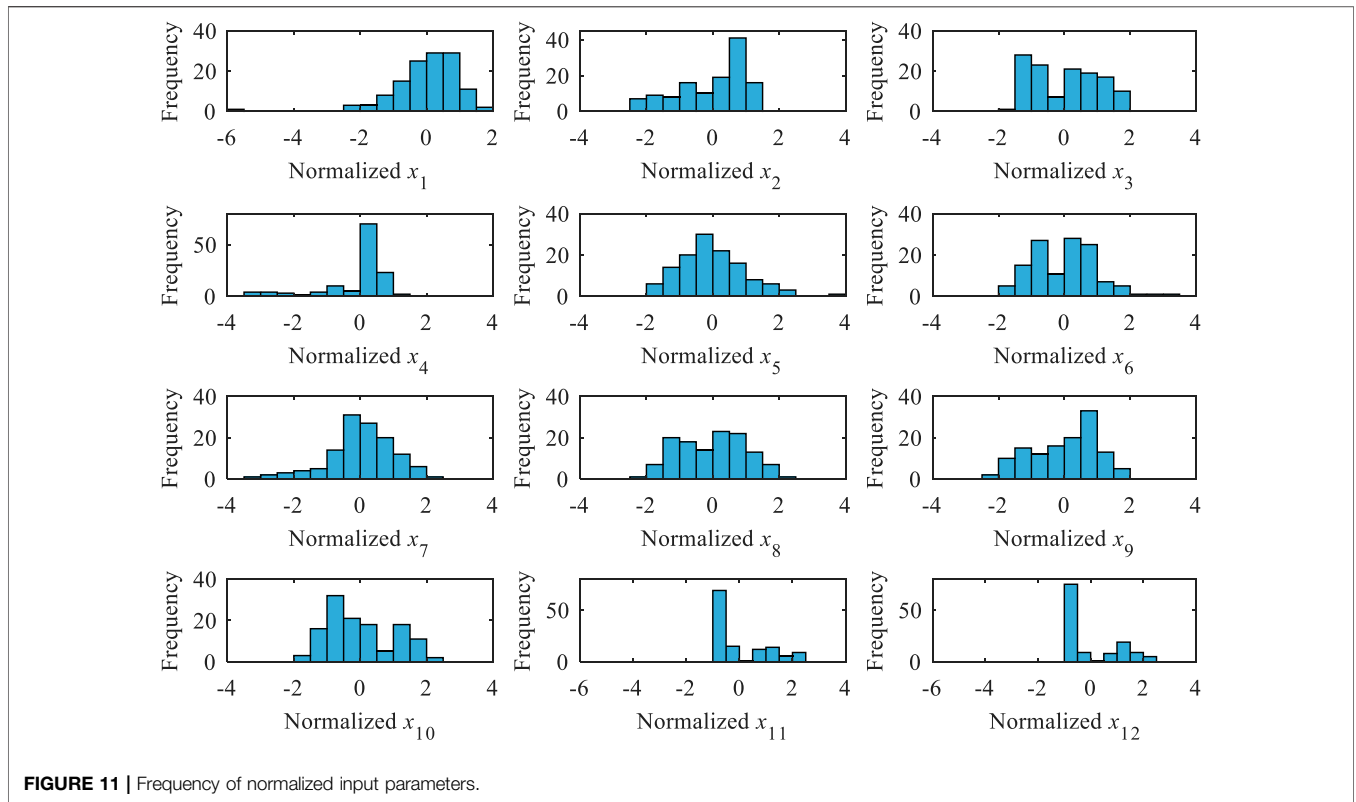
influence tunneling-induced maximum ground settlement: thrust amplitude by influencing the movement of surrounding soil and inducing ground deformation and face pressure by maintaining excavation stability, with face pressure at the upper portion closely relationship to soil movement at the shield face.

Notably, despite being an input candidate, advance rate is not among the top 10 optimal models—consistent with the findings of Zhang et al. (2019), in which advance rate ranked last among all model inputs in sensitivity analysis. In the present study, the advance rate is controlled to balance Earth pressure at the front interface of the shield machine. Undoubtedly, engineers and researchers are well aware that too small an advance rate may result in ground loss where too large a rate may generate high pressure at the front interface of the shield machine and cause ground heave. However, in this case study, advance rate is commonly carefully managed to avoid unacceptable excessive deformation. Hence advance rate may vary in a range that cannot be the dominant influencing factor for a certain project. Soil removal rate and removal volume are two factors closely related to advance rate. To maintain a desired face pressure at the front of the shield machine, soil removal rate and removal volume should be coordinated with the advance rate. As a result, these two features did not emerge in the top four models. The cutterhead torque of the shield machine can be affected by geological conditions, the opening ratio of the cutterhead, Earth pressure, tunnel diameter and the like. As a result of small variations in geological conditions, constant opening ratio, and tunnel diameter (for the same shield machine as in the present case history), the torque feature can have little impact on the ground surface settlement. Accordingly, this feature was not incorporated into the optimal model.

The relative importance of the various parameters depends on the tunneling procedure. For example, face pressure is highly determinant of the tunnel stability and settlement, as overly low face pressure may lead to collapse of the tunnel face. However, if during the period when these data sets were obtained face pressure was always sufficient, scant influence of face pressure will be evident in the data. As shown in **Figure 11**, normalized  $x_7$  (face pressure) was mostly in the range (-1, 1). Only when there is critically low face pressure in the data will this be evident as an important parameter. In general, a parameter is important in this procedure when it influences the settlement trough and is varied during the drive in a way that allows different outcomes of the settlement trough, such as the normalized  $x_2$  (cover depth) and  $x_3$  (pitching angle) illustrated in **Figure 11**, in which the frequencies in each interval are roughly equal. Important parameters that did not vary into critical ranges will not be recognized as important using this approach.

### 4.2 Sensitivity Analysis of Selected Features

Sensitivity analysis of the selected features in the optimal model was conducted to search for a dominant feature and evaluate relationships between tunneling-induced maximum ground



settlement and the selected features. The sensitivity percentage of the ground settlement related to each input parameter is calculated using the equations:

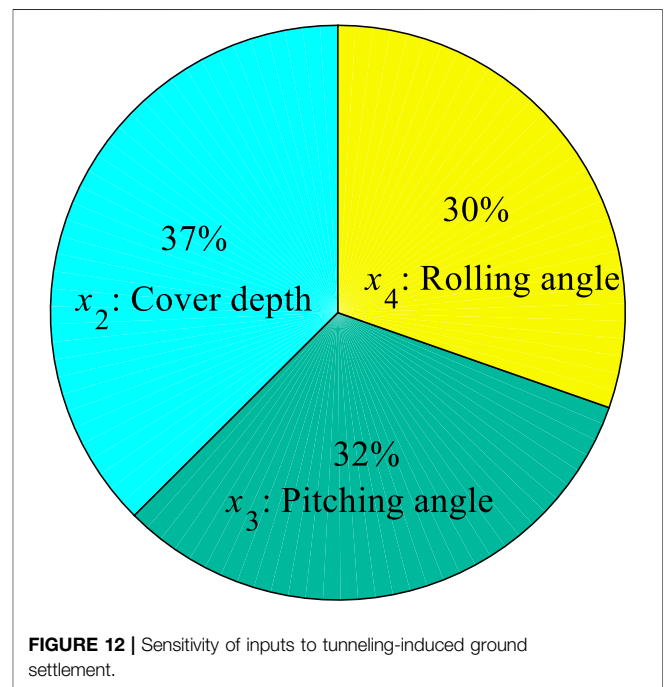
$$N_i = f_{\max}(x_i) - f_{\min}(x_i) \tag{19}$$

$$S_i = \frac{N_i}{\sum_{j=1}^n N_j} \times 100 \tag{20}$$

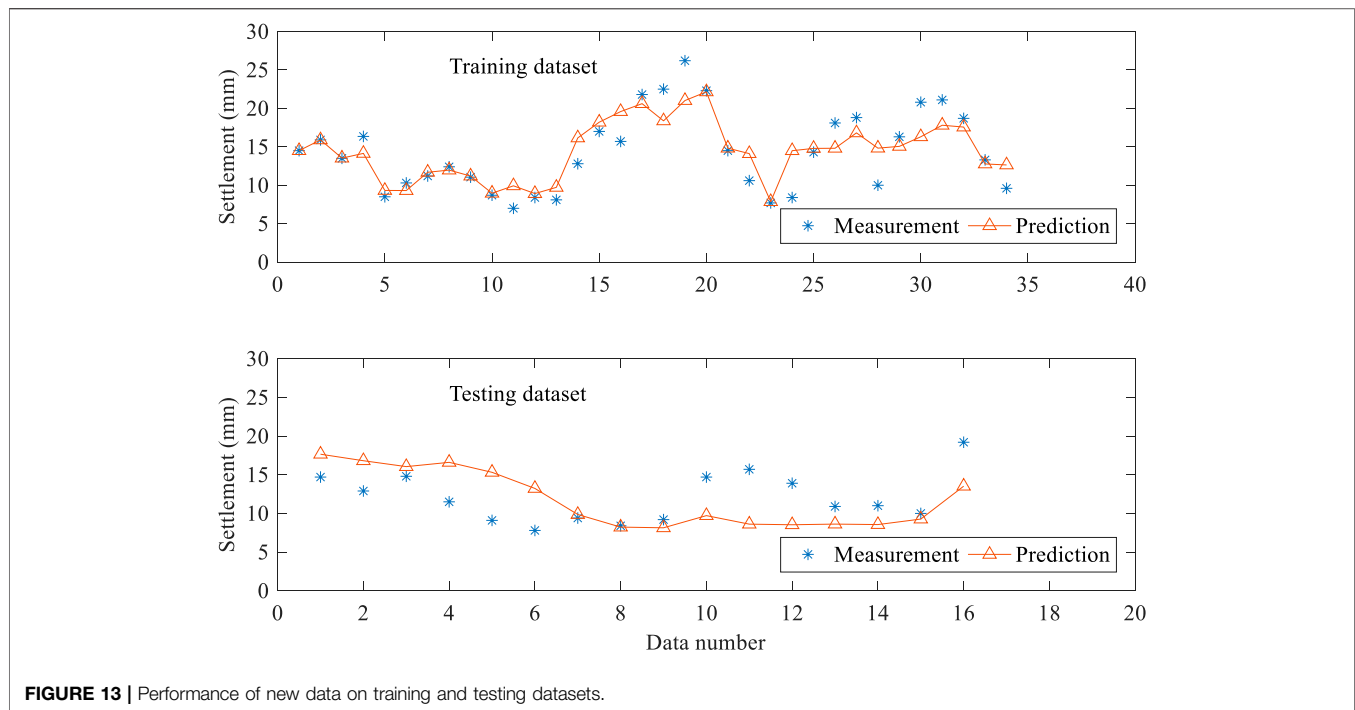
where  $x_i$  is the  $i$ th input variable and  $f_{\max}(x_i)$  and  $f_{\min}(x_i)$  denote the maximum and minimum predictions for ground settlement, respectively, by varying the  $i$ th input variable in its range while assuming other inputs to be at their mean values. **Figure 12** gives the sensitivity percentage for each input variable, showing that cover depth had the dominant impact on ground settlement and that pitching angle ranked second. Feature selection of cover depth has been recognized as one important factor by many researchers, and sensitivity analysis further illustrates the significance of pitching angle and rolling angle.

### 4.3 Maximum Settlement Prediction Using the Bayesian Nonparametric General Regression Algorithm

An additional database (50 sets of data points in total) collected from the Fengtan–Gucui section was used to assess prediction performance using the BNGR algorithm on new data. This database was manually divided into two subsets: one containing 34 data points collected from the beginning of the



Fengtan–Gucui section, incorporated into the database of the Gucui–Xueyuan section to form an extended training dataset, and another including 16 data points collected from the rest of the Fengtan–Gucui section, used to estimate maximum ground



**FIGURE 13** | Performance of new data on training and testing datasets.

settlement. Inclusion of new data points into the existing training dataset was necessary to capture the specific characteristics of the new section (Chen et al., 2019). What's more, inclusion of a new dataset can enlarge the ranges of the input variables essential for the BNGR algorithm. The geological condition of the Fengtan–Gucui section is illustrated in **Figure 4B**. Soil conditions at the site where the tunnel passes through contain mainly muddy silty clay layers, similar to those seen in the Gucui–Xueyuan section. Their properties are quite similar and are presented in **Supplementary Table S1** in the supplemental data, indicating that the geological conditions of the Fengtan–Gucui section resemble those of the Gucui–Xueyuan section. What's more, because the same shield machine was applied in these two sections, it is reasonable to combine the measured data from these two sections as a single training section. **Figure 13** illustrates both measured and predicted data for the Fengtan–Gucui section. **Figure 13A** presents tunneling-induced maximum ground settlement at the beginning of this section. This dataset is part of the training dataset, and the estimated settlements are almost identical to the measured data except for some scattering data points. **Figure 13B** shows ground settlement in the second half of the Fengtan–Gucui section. It can be observed that estimated ground settlement using the BNGR method approximates the measured data points.

## 5 CONCLUSION

Based on the collected data from a construction site in Hangzhou, China, a general regression neural network under the Bayesian framework (BNGR) was used for feature selection and prediction of tunneling-induced maximum ground settlement in soft soils.

Beyond overburden depth, two other features associated with ground settlement were selected in the optimal model: pitching angle and rolling angle. The optimal model was validated on the testing dataset and sensitivity analysis was conducted to examine the selected features. The estimation performance of the BNGR algorithm was evaluated on the new data set, with predictions found to be acceptable. Based on these findings, certain conclusions can be drawn:

- 5.1) The pitching and rolling angles of the shield machine directly control its orientation and significantly affect shield–soil interactions. In the present research, involving soft soils with lower strength and high compression, shield–soil interactions become particularly important and can cause relatively large disturbances to surrounding soil, consequently inducing ground surface settlement. Engineers should attend closely to operational factors associated with shield–soil interactions when tunneling in soft soils.
- 5.2) Thrust and face pressure (upper) emerged in the second-best model (model-2) in addition to the three features present in the optimal model. These two features, which have been discussed in the literature, play a significant role in controlling face stability during excavation process. Feature selection shows, however, that these two influencing factors are less evident than pitching angle and rolling angle for the present dataset perhaps as a result of the variation in face pressure applied within this dataset.
- 5.3) Advance rate is not selected in the top 10 models from the designed input candidates. But this does not mean the advance rate is not important and the advance rate can induce intolerant ground surface deformation when

extremely large or small. In the present study, the advance rate is carefully controlled in practice and thus varies within a range in which it can have little effect on the surrounding soil. Accordingly, compared with other features, such as overburden depth, pitching angle, and rolling angle, this operational factor might not directly influence ground surface settlement.

## DATA AVAILABILITY STATEMENT

The original contributions presented in the study are included in the article/**Supplementary Material**, further inquiries can be directed to the corresponding author.

## AUTHOR CONTRIBUTIONS

Writing: ZD, L-SZ; review and editing: W-HZ, AB.

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## SUPPLEMENTARY MATERIAL

The Supplementary Material for this article can be found online at: <https://www.frontiersin.org/articles/10.3389/fbuil.2022.848158/full#supplementary-material>

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