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Au modified PrFeO₃ with hollow tubular structure can be efficient sensing material for H₂S detection

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The H₂S concentration in exhaled breath increases marginally with the progress of periodontal disease, and H₂S is considered to be one of the most important gases related to meat and seafood decomposition; however, the concentration of H₂S is low and difficult to detect in such scenarios. In this study, Au–PrFeO₃ nanocrystalline powders with high specific surface areas and porosities were prepared using an electrospinning method. Our experimental results show that loading Au on the material provides an effective way to increase its gas sensitivity. Au doping can decrease the material's resistance by adjusting its energy band, allowing more oxygen ions to be adsorbed onto the material's surface due to a spillover effect. Compared with pure PrFeO₃, the response of 3 wt% Au–PrFeO₃ is improved by more than 10 times, and the response time is more than 10 s shorter. In addition, the concentration of H₂S due to the decomposition of shrimp was detected using the designed gas sensor, where the error was less than 15%, compared with that obtained using a GC–MS method. This study fully demonstrates the potential of Au–PrFeO₃ for H₂S concentration detection.

KEYWORDS

gas sensor, Au–PrFeO₃, H₂S, moss, gas-sensing

Introduction

H₂S is a colorless, highly toxic, and acidic gas. It has a particular rotten egg smell, and even low concentrations of H₂S can impair the human sense of smell. In high concentrations, it has no smell (as high concentrations paralyze the olfactory nerve). In addition, H₂S is flammable and is typically considered a dangerous gas (Ethiraj et al., 2015; Wu et al., 2019; Kumar et al., 2021; Liu et al., 2021; Priya et al., 2021; Zheng et al., 2021; Zuo et al., 2021; Li et al., 2022a). H₂S gas is released during the breakdown of food, and is also responsible for the bad breath caused by periodontitis (Chen et al., 2017; Wu et al., 2019; Hsu et al., 2021; Lopez et al., 2021): about 0.195 ppm H₂S can be detected in the exhaled breath of periodontitis patients, while 0.105 ppm is a typical concentration in

the exhaled breath of healthy individuals (Yaegaki and Sanada, 1992). Using the nose as a means of detecting H₂S can be fatal. Therefore, the timely detection of very low concentrations of H₂S gas is very necessary and important.

In recent years, the use of MOS (metal oxide semiconductor) gas sensors to detect the concentration of target gases has become increasingly popular, such as smoke sensors in hotels, natural gas alarms in homes, and so on. It has been reported that some MOSs, as gas-sensing materials, show excellent response to gases, such as LaFeO₃ (Xiangfeng and Siciliano, 2003; Song et al., 2014; Jaouali et al., 2018; Ma et al., 2021), SmFeO₃ (Tomoda et al., 2004; Hosoya et al., 2005; Huang et al., 2018; Han et al., 2020), PrFeO₃ (Ma et al., 2018), HoFeO₃ (Song et al., 2020), NdFeO₃ (Sheng et al., 2022), YCoO₃ (Addabbo et al., 2015), BaSnO₃ (Cerdà et al., 2002), ZnSnO₃ (Yin et al., 2020), and YMnO₃ (Balamurugan and Lee, 2015). For H₂S, commonly used gas-sensing materials include Pt–ZnO (Zhou et al., 2022), Pd–ZnO (Bae et al., 2022), CuO/SnO₂ (Fan et al., 2019), Pt–WO₃ (Yao et al., 2022), WO₃ (Wang et al., 2018; Akamatsu et al., 2021; Li et al., 2022b), Pt–Fe₂O₃ (Guo et al., 2018), CuO/CuFe₂O₄ (Lim et al., 2021), Ag–SnO₂ (Senapati and Sahu, 2020), LaFeO₃ (Xiangfeng and Siciliano, 2003), YMnO₃ (Balamurugan and Lee, 2015), and Sn–NiO (Gao et al., 2017), among others. MOSs—especially ABO₃ perovskite materials—have the unique advantages of large specific surface area and abundant active sites, which can promote the diffusion path and increase the adsorption of target gas molecules, thus enhancing the sensing ability. There are other ways to detect a target gas, such as Tamm plasmon resonance (Mehaney et al., 2021) and photonic crystal (Ahmed et al., 2021; Ameen et al., 2021; Alrowaili et al., 2022). In particular, these two methods have high accuracy in detecting the gases in exhaled breath, and have good development prospect.

In recent years, sensors based on Graphene and MWCNT have been widely reported, especially for gases in exhaled breath or aromatic gases (Behi et al., 2020, 2022; Thamri et al., 2021). Such sensors display high response and selectivity to target gases; moreover, they have good development prospect due to their low preparation costs.

The aim of this study is to obtain a gas-sensing material with high response, high selectivity, low detection limit, and high long-term stability. PrFeO₃ with different Au doping levels was synthesized using an electrospinning method and sintered at 800°C. It has high specific surface area and high porosity, which are two important factors for improving the gas response of gas-sensing materials. Compared with PrFeO₃, Au–PrFeO₃ shows a higher response and high selectivity for H₂S. In addition, Au doping, as a catalyst, can greatly enhance the surface activity of gas-sensing materials, thus shortening the response-recovery time. Finally, the H₂S concentration in the air around shrimp is detected using the gas sensor designed in this study, which was compared with the data obtained by GC-MS, showing that the error was within 15%. The experimental results prove that Au

doping can greatly improve the response of PrFeO₃ to H₂S gas, providing a feasible and effective way to detect H₂S gas using a gas sensor.

Materials and methods

Preparation of nanocrystalline Au–PrFeO₃

First, samarium oxide, ferric nitrate, palladium chloride, DMF (99.5%), PVP (Mw = 1,300,000), C₂H₅OH (99.7%), and HNO₃ in a stoichiometric ratio were weighed and mixed in deionized water (Figure 1A). The mixed solution was heated in the water bath at 60°C with magnetic stirring until it became transparent, in order to obtain the electrospinning precursor solution (Figure 1B). Then, the as-prepared precursor solution was transferred into a 10 mL syringe. The voltage was maintained at 12 kV during the spinning process, the distance between needle tip and the collector was about 20 cm, and the injection rate of the syringe was 0.4 mL/h (Figure 1C). The obtained nanofibers were sintered at 800°C for 6 h in a muffle furnace (Figure 1D). Finally, the X (0, 1, 3, 5) wt% Au–PrFeO₃ powder was obtained.

Fabrication and measurement of sensor

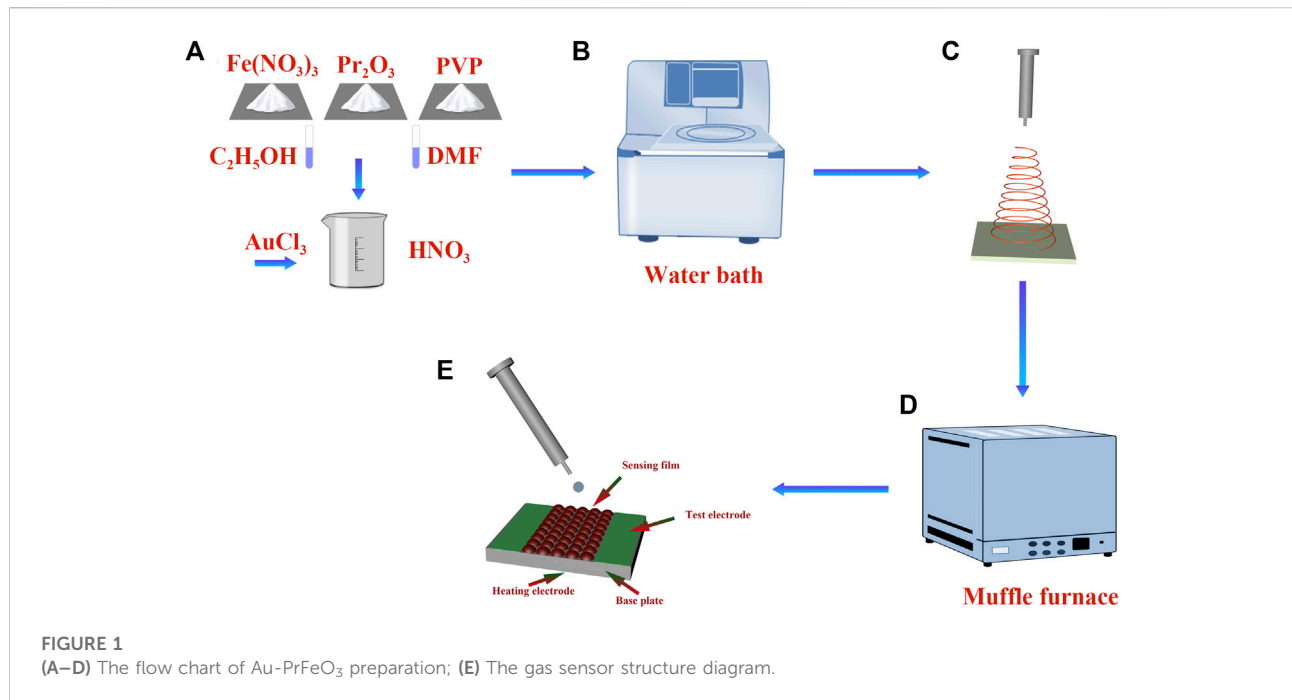
The Au–PrFeO₃ powder was mixed with deionized water to make a paste, which was then placed on gas-sensing film (Figure 1E). The as-prepared plane electrode plate was aged on an aging platform for 48 h, in order to dry it out. At this time, a qualified sensor was ready. The front side of the electrode plate has two electrodes, which are used to detect the resistance value of the gas-sensing material. On the back of electrode plate is a heating plate, which enables the gas-sensing material to reach a higher operating temperature.

Ready-made sensor

The gas sensor structure diagram is shown in Figure 1E. The Au–PrFeO₃ is coated onto the sensing film. The V_C is the supply voltage, which was kept constant at 5 V. The R_g is calculated by the following formula:

$$R_g = \frac{U}{I} = V_i/R_i \quad (1)$$

The gas-sensing response, S , is defined as R_g/R_a , where R_a is the resistance of the sensor in air and R_g is that when in the tested gas. The response time is defined as the time taken to attain 90% of the maximum value in ascending phase, while the recovery time is the time taken to regain 10% of the base value



in the descent phase. For the experimental environment, the RH was 20% and the temperature was 20°C.

Gas concentration control

The whole experiment was carried out in a closed glass chamber, into which H₂S gas was injected with a microinjector. The injection amount of H₂S liquid was calculated as follows (Deng et al., 2013):

$$V_{liquid} = \frac{V_s C_{gas} M}{22.4 \rho d} \quad (2)$$

where V_{liquid} is the volume of the injected H₂S liquid; V_s is the volume of the test chamber; C_{gas} (ppm) is the concentration of the target gas; and M , ρ , and d are the molecular weight, density, and purity of the injected liquid, respectively. When a gas with PPM concentration is obtained, the gas with PPB concentration can be obtained by diluting it ten times using a microinjector.

Results

Material characterization

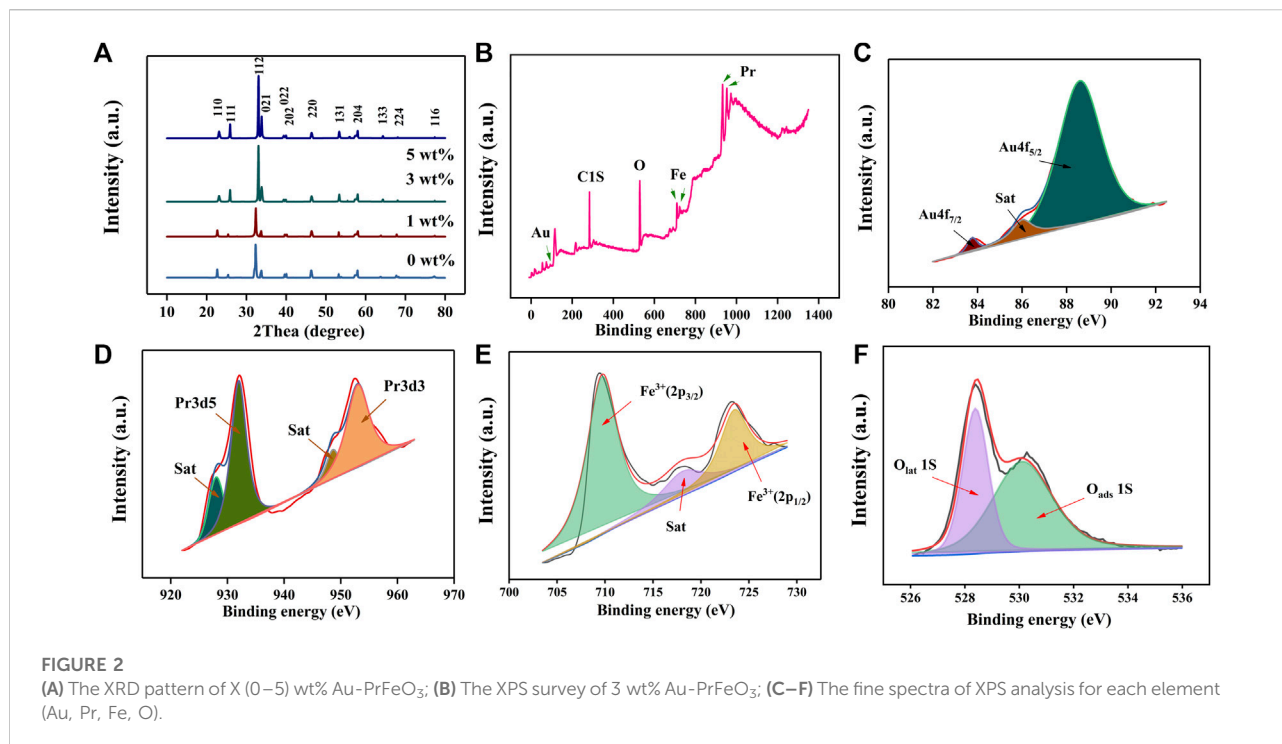
Figure 2A shows the X-ray diffraction analysis (XRD; Bruker D8 ADVANCE with the CuK α amount of 1.5405 Å at 40 kV and 40 mA) results of X (0, 1, 3, 5) wt% Au-PrFeO₃.

Compared with the standard card (PDF card: 37-1493), it shows a single-phase. The average particle size can be calculated using the Scherrer method. The Scherrer equation is as follows:

$$D = \frac{k\lambda}{\beta \cos\theta} \quad (3)$$

where λ is the X-ray wavelength, β is the integral width of diffraction peaks, and θ is the Bragg diffraction angle. The average particle size of 3 wt% Au-PrFeO₃ is about 73.8 nm. Due to the low Au doping amount, its characteristic peak could not be reflected in the XRD pattern; therefore, X-ray Photoelectron Spectroscopy (XPS; Thermo Scientific™ K-Alpha™⁺ spectrometer equipped with a monochromatic Al K α X-ray source at 1486.6 eV operating at 100 W) was performed on 3 wt% Au-PrFeO₃ to confirm the presence of Au. As can be seen from Figure 2B, the Au element was doped in the material. Figures 2C–F show the fine spectra obtained by XPS analysis for each element. In Figure 2C, the peaks located at about 84.0 and 88.3 eV can be assigned to Au 4f_{7/2} and Au 4f_{5/2}; in Figure 2D, the peaks located at about 932.2 and 953.1 eV can be assigned to Pr 3d₅ and 3d₃; in Figure 2E, the peaks located at about 708.6 and 724.1 eV can be assigned to 2p_{3/2} and 2p_{1/2} of Fe³⁺; and, in Figure 2F, the peaks located at about 528.6 and 530.8 eV can be assigned to lattice O1s and adsorbed O1s.

Figures 3A,B shows the Scanning Electron Microscope (SEM; Japan HITACHI SU8010, 8.0 kV) images of 3 wt% Au-PrFeO₃ under different magnifications (PrFeO₃ was synthesized by a sol-gel method and sintered at 800°C; Supplementary Figure S1). The



pure PrFeO₃ presented a common perovskite structure, while 3 wt% Au-PrFeO₃ presented a nanotube-like microstructure. In the material preparation stage, after sintering, the surface of the material becomes rough and the nanotubes become hollow as the PVP decomposes at high temperature.

In order to understand which microstructure provides more favorable properties to the gas-sensing material, it is necessary to figure out which structure has higher specific surface area and porosity. The specific surface area and porosity of the 3 wt% Au-PrFeO₃ hollow nanofibers were further analyzed by nitrogen adsorption-desorption analysis. Figure 3C shows the BET curves for 3 wt% Au-PrFeO₃ and the corresponding Barrett-Joyner-Halenda (BJH) pore size distribution (inset). The specific surface area of 3 wt% Au-PrFeO₃ was 23.67 m²/g and the average pore size was 10.2 nm. The specific surface areas of PrFeO₃ with different amounts of Au element doping are shown in Figure 3D. It can be seen that, when the doping amount of Au element was 3 wt %, the composite powder presented the largest specific surface area. This occurred as Au doping can inhibit the growth of MOS grains (the smaller the grain size, the larger the specific surface area); however, when the Au doping amount is too high, the particles will appear in a small range of agglomeration, and the specific surface area of the material will decreased. Considering the sensing properties of materials, the specific surface area is an important factor. A high specific surface area can provide

more adsorption sites, which can enhance the reactions between the sensing material and gas molecules, leading to a high response to the test gas.

Gas sensing performance

Figure 4A and Supplementary Figure S2 show the response curves of PrFeO₃ with different amount of Au doping to 1 ppm H₂S at various operating temperatures. For all samples, the highest responses were obtained at 120°C. The highest responses to 1 ppm H₂S were 6.93 (0 wt% Au), 38.16 (1 wt% Au), 72.86 (3 wt% Au), and 56.29 (5 wt% Au). It can be seen that the response was more than 10 times higher when using the best Au-doped sample, compared with the pure sample. Moreover, Table 1 shows the H₂S sensing properties of some typical gas-sensing materials for reference. By comparison, 3 wt% Au-PrFeO₃ exhibited an extremely high response value while ensuring a short response-recovery time.

The relationship between the material's sensitivity and the gas concentration is very important, and a good fitting relationship can be used to predict the response value at a given gas concentration. Figure 4B and Supplementary Figure S3 show the relationship between the response of Au-PrFeO₃ and multiple H₂S concentrations. It can be seen that, for both undoped and Au-doped PrFeO₃, the response had a good linear relationship with the gas concentration, with all R² values greater than 96%.

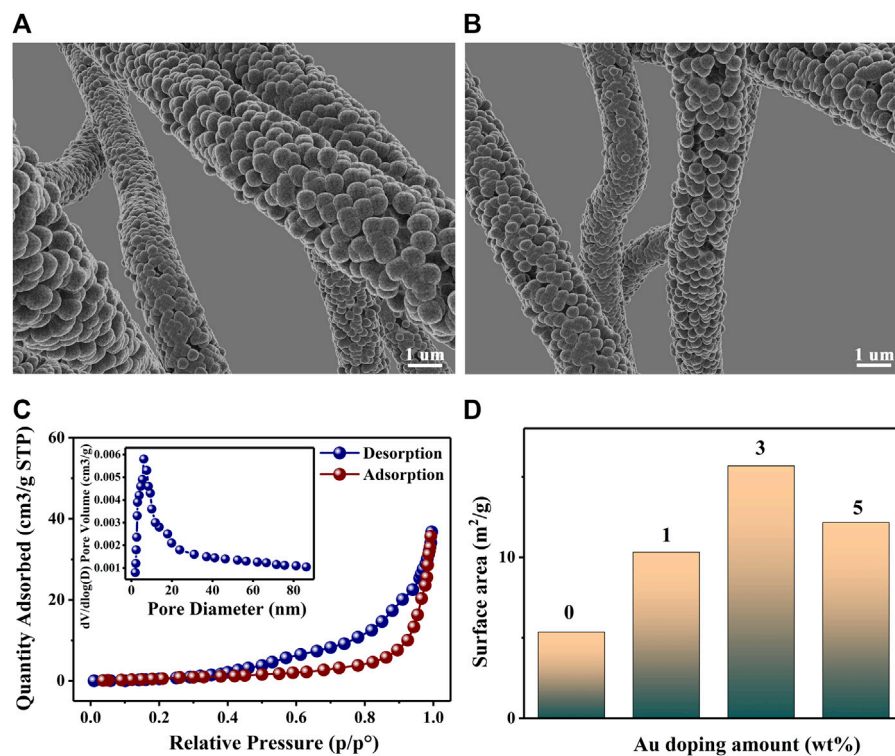


FIGURE 3

(A,B) The SEM of 3 wt% Au-PrFeO₃; (C) N₂ adsorption-desorption isotherms and pore size distributions (the inset) for Au-PrFeO₃ nanocomposite; (D) The surface area of PrFeO₃ with different amount of Au doping.

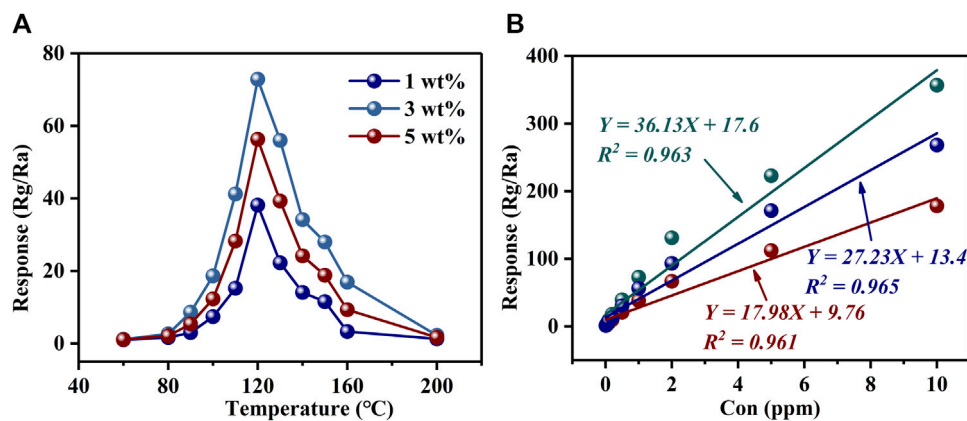


FIGURE 4

(A) The response of PrFeO₃ with Au doping; (B) The relationship between the response of Au-PrFeO₃ and multiple H₂S concentration.

Additionally, the response values of Au-doped PrFeO₃ to H₂S are given in Table 2. It can be seen that the detection limit of pure PrFeO₃ was 50 ppb; meanwhile, after Au doping, the Au-PrFeO₃ could detect a much lower concentration (10 ppb) of H₂S.

Repeatability is another important property that determines whether a gas-sensing material is excellent or not. For Au-PrFeO₃, the repeatability of responses to different concentrations of H₂S gas are shown in Figures 5A–C and

TABLE 1 The H₂S sensing performance of materials in the literature and this work.

Materials	T (°C)	S (ppm)	T _{res} /T _{rec} (s)	Detection limit (ppm)	Ref
rGO/WO ₃	300	22.9 (100)	23/75	1	Mehta et al. (2021)
Fe ₂ O ₃ /MoSe ₂	25	42.5 (10)	50/53	1	Pan et al. (2021)
WO ₃ /Bi ₂ WO ₉	92	84.18 (100)	2/582	0.01	Zhang et al. (2020)
CuO/WO ₃ -x	99	171.5 (10)	45/60	0.1	Peng et al. (2020)
Pt-Co ₃ O ₄ @NiO	200	250.0 (100)	213/135	20	Wang et al. (2021)
Pt-WO ₃	200	1638.2 (10)	42/37	0.005	Yao et al. (2022)
3 wt% Au-PrFeO ₃	120	72.86 (1)	28/18	0.01	This work

TABLE 2 The response of Au-PrFeO₃ to H₂S gas.

Con (ppm)	Doping amount	0.01	0.02	0.05	0.1	0.2	0.5	1	Detection limit (ppm)
0 wt%				1.21	1.62	2.38	4.06	6.93	0.05
1 wt%		1.18	1.58	2.94	5.45	9.93	20.85	38.16	0.01
3 wt%		1.26	2.43	4.78	9.32	17.9	39.38	72.86	0.01
5 wt%		1.21	1.98	3.68	7.56	13.56	30.59	56.29	0.01

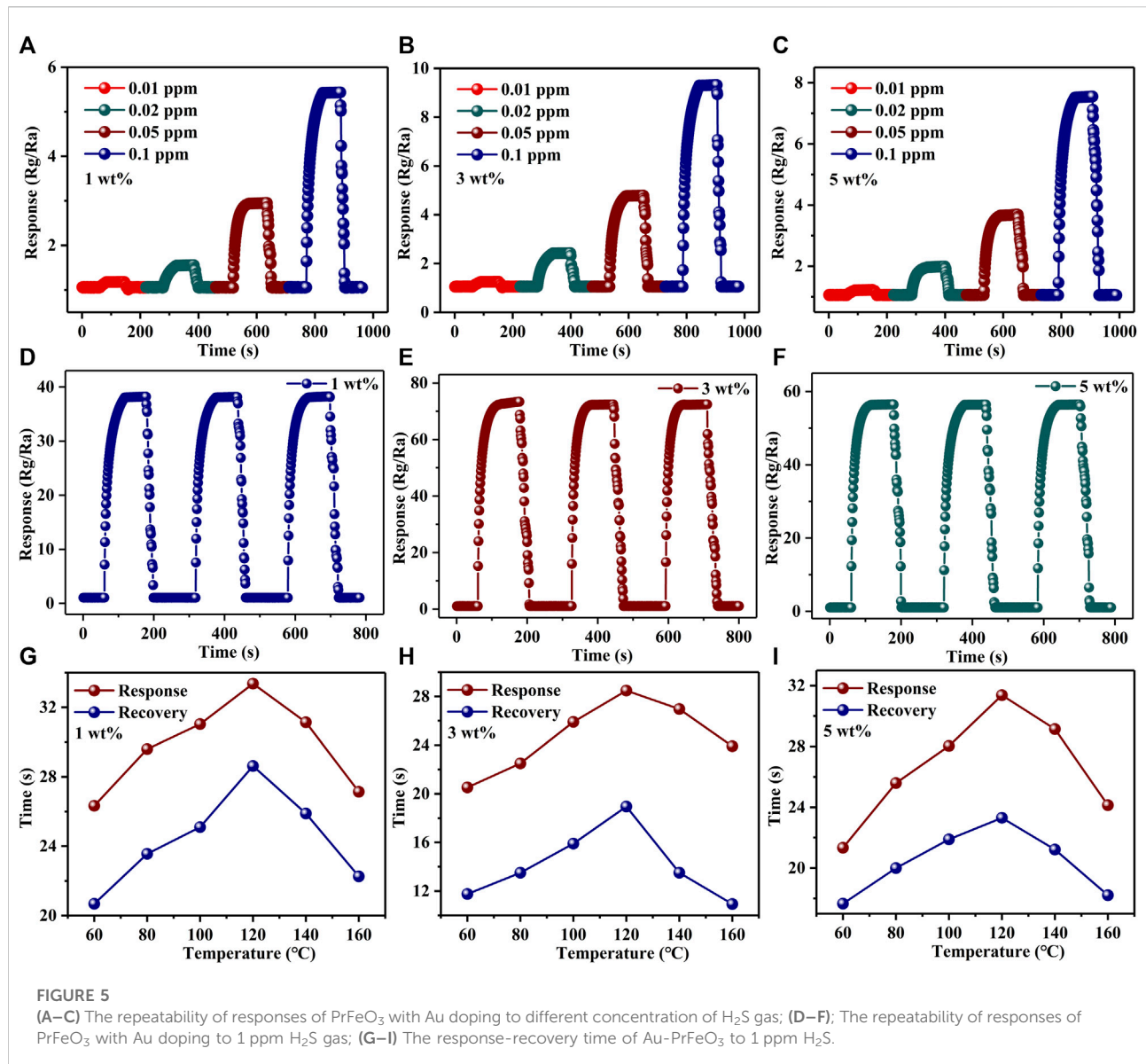
Supplementary Figure S4. The repeated processes were carried out as follows: when the resistance value of the gas-sensing material had stabilized, the H₂S gas was injected into the reaction chamber, and the resistance of the material increased immediately. After a period of time, the resistance stabilized, following which the H₂S gas is removed and the resistance of the material decreased immediately, restoring it to the initial state. It can be seen that, for H₂S gas at different concentrations, the resistance of the gas-sensing material could be restored to the initial value every time after the H₂S gas was removed, indicating that the material has excellent repeatability. Additionally, the response of all samples changed upon exposure to 1 ppm H₂S gas, as shown in Figures 5D–F. It can be seen that the gas response of samples had no obvious change after a 3-cycle response–recovery test, indicating the high operating stability of the designed Au-PrFeO₃ sensor. Additionally, the gas-sensing reproducibility of Au-PrFeO₃ is about 38.16 ± 4% (1 wt%), 72.86 ± 2% (3 wt%), 56.29 ± 3.6% (5 wt%).

The response–recovery time of all samples differed at different operating temperatures, indicating that the operating temperature affects the chemical reaction on the material's surface. The response–recovery times of all samples are shown in Supplementary Table S1, Figures 5G–I, and Supplementary Figure S5. It can be seen that the response–recovery time increased with the operating temperature up to 120°C; then, after 120°C, the response–recovery time decreased with any further increase in the operating temperature. This may be due to the fact that, before the optimum operating temperature, the adsorption rate of gas molecules is higher than the desorption rate, and the number of oxygen ions and H₂S gas molecules adsorbed on the material's surface are

increased, leading to an increased reaction time. With an increase in the operating temperature, the adsorption and desorption rates are balanced at the optimum operating temperature, and the number of H₂S gas molecules and adsorbed oxygen ions on the material's surface reach a maximum. At this operating temperature, the reaction time also reaches its maximum. With a further increase in operating temperature, the desorption rate of gas molecules is higher than the adsorption rate, the reaction reactants become less, and the reaction time is shortened. In addition, Au doping can increase the surface activity of the material and improve the reaction rate; therefore, the response–recovery time of Au-PrFeO₃ was shorter than that of pure PrFeO₃.

In practical application, it is very common to detect a certain gas in a mixture, such as H₂S gas in an individual's exhaled breath. Therefore, the selectivity of a gas-sensing material to a certain gas determines its practical application value. The selectivity comparison of Au-PrFeO₃ to 1 ppm H₂S and several other common gases in a person's exhaled breath is shown in Figures 6A–C and Supplementary Figure S6. It can be seen that, compared with other gases, Au-PrFeO₃ presented high selectivity for H₂S gas. In particular, for N₂, O₂, NO, CO₂, CO, and other common gases present in exhaled breath, the response was negligible, such that the H₂S in the exhaled breath can be detected more accurately.

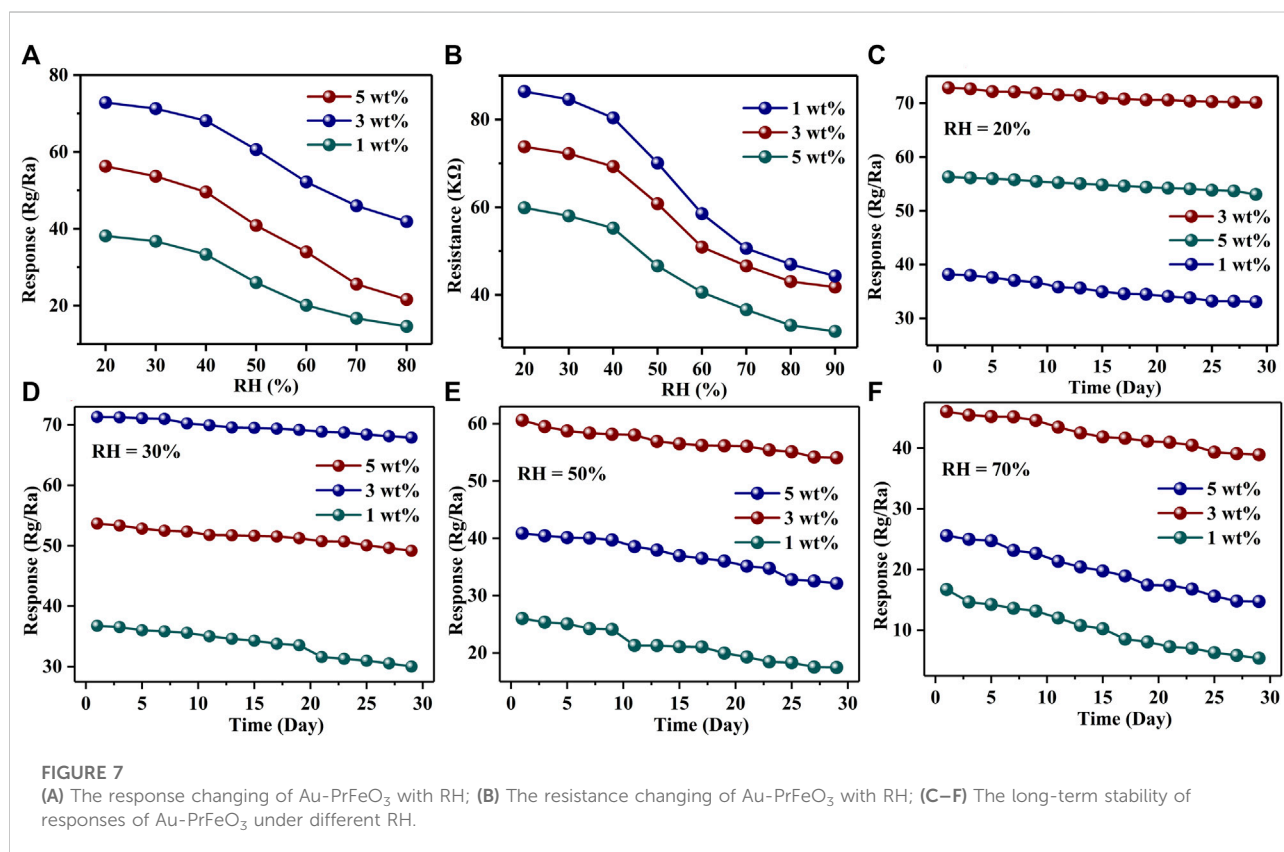
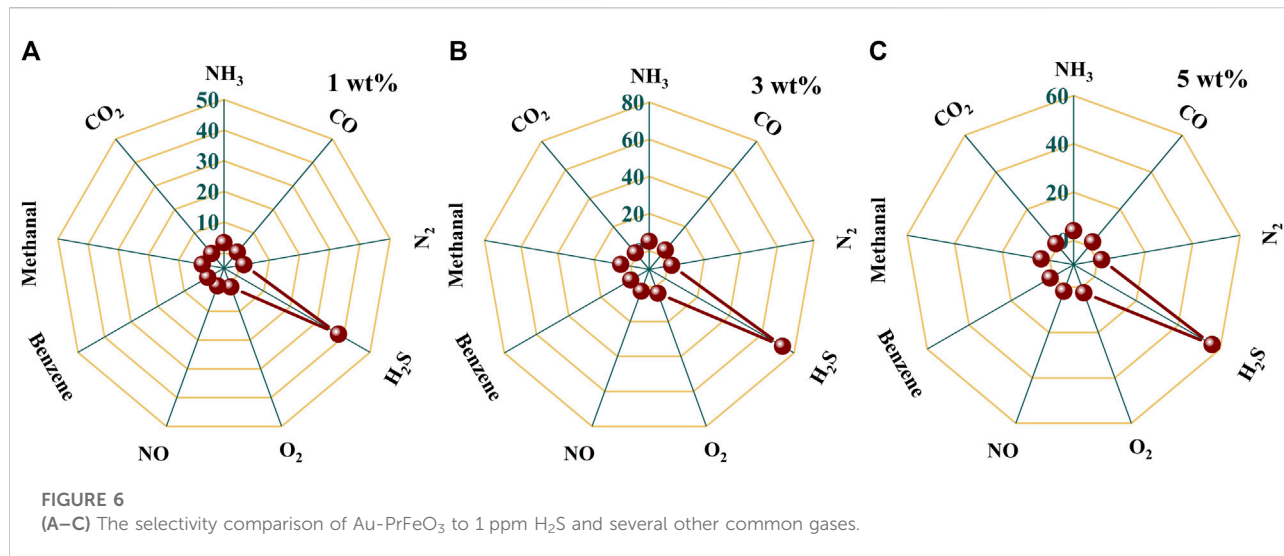
The relative humidity (RH) in the environment is also a factor that cannot be ignored in the application of gas sensors. Figures 7A and Supplementary Figure S7 show the responses of Au-PrFeO₃ to 1 ppm H₂S with varying RH. It can be seen that the response decreased with increasing RH: before 50% RH, the response was little affected by it; however, above 50% RH, the



responses decreased sharply. This means that the gas sensor in this study can be used in a low-RH environment without considering the influence of RH. This will greatly expand its practical application field. Figures 7B and Supplementary Figure S8 show the resistance change of Au-PrFeO₃ with RH. For Au-PrFeO₃, the resistance decreased with RH, but the proportion of decrease differed. In the 20–90% RH range, the proportion of decreases were 53.21% (0 wt% Au), 48.6% (1 wt% Au), 41.8% (3 wt% Au), and 47.09% (5 wt% Au). Thus, the resistance of 3 wt% Au-PrFeO₃ presented the highest RH adaptability.

Long-term stability is another important property for gas-sensing materials. The higher the long-term stability, the longer

the replacement cycle of the gas-sensing material and, so, the more economic and energy advantages it has. Figures 7C–F show the long-term stability of Au-PrFeO₃ under different RH over 30 days. The experimental data were obtained every 2 days. It can be seen that all of the responses decreased slightly with time, but the proportion of decrease was lowest when the sensor was kept at under 20% RH. The proportions of decrease when the sensor was kept at under 20% RH were 34.9% (0 wt% Au), 13.3% (1 wt% Au), 3.7% (3 wt% Au), and 5.7% (5 wt% Au). It can be seen that the long-term stability of 3 wt% Au-PrFeO₃ was more than 9 times that of pure PrFeO₃. Therefore, Au-doped PrFeO₃ demonstrated advantages, in terms of long-term stability. Other types of sensors, such as MOX (Pashami et al., 2012; Li



et al., 2021) and MWCNT (Pistone et al., 2013; Barthwal and Singh, 2020) have been shown to have good stability under high RH environments. However, MOS, MOX, and MWCNT gas sensors are affected by RH in practical applications; therefore, improving their RH adaptability is a keyway to broaden their application field.

Sensing mechanism analysis

Figure 8 shows the reaction mechanism for the experiment conducted in this work. At room temperature (20°C), for a p-type semiconductor, the main carrier of Au-PrFeO₃ is the hole (*h*⁺; Figure 8A). According to Kröger-Vink defect notation, the holes

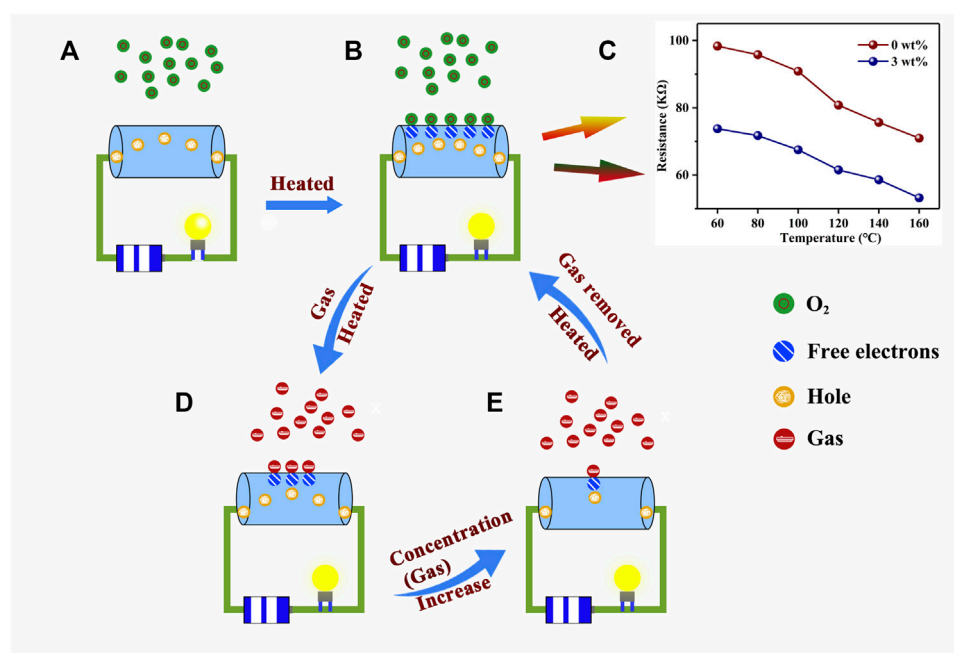


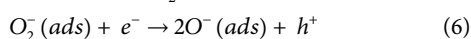
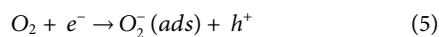
FIGURE 8

The reaction mechanism of the whole experiment in this work. (A) The hole is the main carriers in Au-PrFeO₃; (B) At high operating temperatures, the oxygen molecules capture electrons from the surface of the Au-PrFeO₃; (C) The resistance changing of Au-PrFeO₃ at any operating temperature; (D) At high operating temperatures, the H₂S gas molecules react with oxygen ions on the surface of the Au-PrFeO₃; (E) At high operating temperatures, the response increase with the concentration of H₂S gas molecules.

are mainly produced by the ionization of $[V_{Pr}^x]$, the reaction may like this:



Before Au doping, few oxygen molecules capture the free electrons from the material, resulting in the formation of oxygen ions on the material's surface and few holes are created in this process at the same time. As the work function of Au is larger than that of PrFeO₃, electrons will transfer from PrFeO₃ to the surrounding Au nanoparticles after Au doping, resulting in an increase in the number of holes in PrFeO₃ (Figure 8B). This reaction may look like:

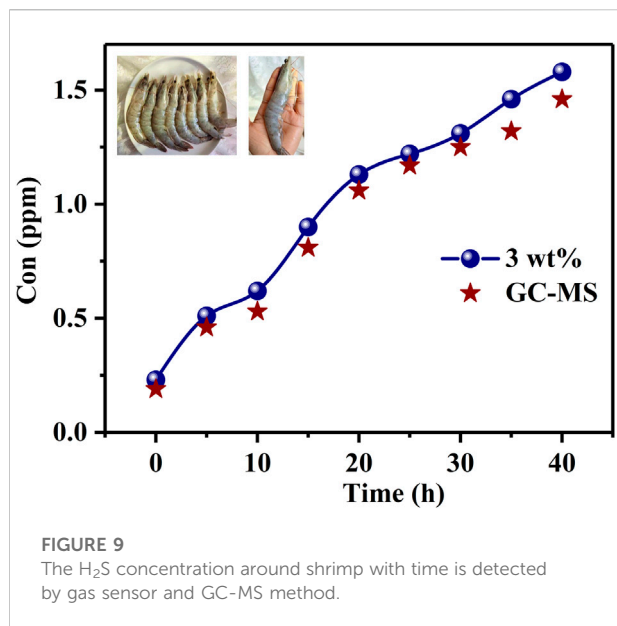


where *ads* denote the state where oxygen is adsorbed on the material surface.

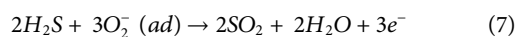
In order to verify this theoretical assumption, the resistances of pure PrFeO₃ and 3 wt% Au-PrFeO₃ were tested, and the results are shown in Figure 8C. It can be seen that the resistance of 3 wt% Au-PrFeO₃ was lower than that of PrFeO₃ at any operating temperature, consistent with the above theoretical assumption.

When the H₂S gas molecule is introduced, it will be adsorbed onto the surface of the PrFeO₃ to react with the oxygen ions

(Figure 8D). The adsorption and desorption on the surface of Au-PrFeO₃ of H₂S gas molecules exist simultaneously. The rates of adsorption and desorption increase with the operating temperature, where the rate of adsorption is greater than the rate of desorption before the operating temperature reaches the optimum temperature. Therefore, the count of adsorbed H₂S molecules on the surface of the material increases, and the reaction between H₂S molecules and oxygen ions is more intense, resulting in an increased response. When the operating temperature exceeds the optimum temperature, the rate of adsorption of Au-PrFeO₃ with respect to H₂S molecules is lower than the rate of desorption and the intensity of the reaction between H₂S molecule and oxygen ions is reduced, causing the response to decrease. Furthermore, at the optimum temperature, as the concentration of H₂S gas molecule increases, the number of H₂S molecules adsorbed on the surface of the Au-PrFeO₃ will increase, causing the response to increase (Figure 8E). However, the number of free electrons on the surface of the Au-PrFeO₃ is not infinite, and the energy required to make an electronic transition within Au-PrFeO₃ is also increasing. Therefore, the response (R_g/R_a) increases with the concentration of H₂S gas molecules, but the rate of increase declines. In addition, when the free electron is released from oxygen ions adsorbed onto the Au-PrFeO₃, the PrFeO₃ in the depletion layer width narrowing caused by Au, resulting in a greater resistance change.



The reaction between H₂S molecules and oxygen ions may as follows:



Additionally, it is well-known that the oxygen in air can be adsorbed onto the surface of semiconductor metal oxides to become oxygen ions, for which Au is a good catalyst. In this work, with the assistance of Au, oxygen molecules can more easily be adsorbed onto the surface of PrFeO₃, due to the spillover effect (Kung et al., 2007; Wang et al., 2013). For this reason, more oxygen gets adsorbed and captures free electrons to form oxygen ionic species (Liu et al., 2011). This process increases both the quantity of adsorbed oxygen and the molecule-ion conversion rate, resulting in a high gas response (Wang et al., 2012).

Application in the detection of H₂S

Accurately and quickly assessing whether meat and seafood have decomposed or not is very important. H₂S is thought to be one of the most important gases released in the decomposition of food. The H₂S concentration around shrimp with time was detected using the gas sensor designed in this study and GC-MS, as shown in Figure 9. Eight shrimps were placed in the experimental apparatus, each about 10–16 cm in length. It can be seen that the concentration of H₂S increased with death-time, and the concentration of H₂S measured by the designed gas sensor was greater than that measured by GC-MS at any time, which indicates that there were other gases in the surrounding air of the shrimp, which can have an effect on the gas sensor;

TABLE 3 The concentration of H₂S obtained by gas sensor and GC-MS method.

Time(h) Method	0	5	10	15	20	25	30	35	40
Gas sensor	0.23	0.51	0.62	0.9	1.13	1.22	1.31	1.46	1.58
GC-MS	0.20	0.46	0.53	0.81	1.06	1.17	1.25	1.32	1.46

however, this effect was very small. By comparing the H₂S concentrations measured by the two methods, the error was within 10%. The results are provided in Table 3.

Conclusion

In this study, Au-modified PrFeO₃ was synthesized using an electrospinning method. It has a large specific surface area and high porosity, which improved the response to a certain extent. Our experimental results demonstrated that the optimum Au doping content was 3 wt%. The response of 3 wt% Au-PrFeO₃ to H₂S was more than 10 times higher, and its long-term stability was more than 9 times that of pure PrFeO₃. Moreover, the response-recovery time of 3 wt% Au-PrFeO₃ was more than 10 s shorter than that of the pure PrFeO₃. In addition, the doping of Au, as a catalyst, greatly improved the RH adaptability and selectivity of the material. Finally, the designed Au-PrFeO₃ was shown to be very accurate for detecting the concentration of H₂S gas in the air around shrimp, with an error of less than 15%, when compared to the results obtained by GC-MS. Our experimental results fully demonstrate the advantages of noble metal doping in improving the performance of gas-sensing materials and the great potential of Au-PrFeO₃ in H₂S detection.

Data availability statement

The raw data supporting the conclusions of this article will be made available by the authors, without undue reservation.

Author contributions

HZ, YZ, LZ, JC, and JX designed the study. HZ performed experiments and analyzed data. HZ, JC, JX, and PJ wrote and revised the manuscript. HZ, JC, JX, and PJ provided an experimental resource.

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Conflict of interest

The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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Supplementary material

The Supplementary Material for this article can be found online at: <https://www.frontiersin.org/articles/10.3389/fbioe.2022.969870/full#supplementary-material>

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