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# Dairy manure nutrient recovery reduces greenhouse gas emissions and transportation cost in a modeling study

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Technologies that separate manure or digestate into fractions with different solids and nutrient contents present interesting options to mitigate manure storage emissions (by reducing the quantity of carbon stored anaerobically) and to improve nutrient distribution (by reducing the quantity of water transported with nutrients). In this study, the dairy farm model, DairyCrop-Syst, was used to simulate storage emissions of methane (CH<sub>4</sub>), nitrous oxide (N<sub>2</sub>O), and ammonia (NH<sub>3</sub>), and to simulate nutrient distribution for a case-study farm in Canada. The farm used several types of manure processing, including: anaerobic digestion (AD), solid-liquid separation (SLS), and nutrient recovery (NR). Simulations were done with combinations of the above technologies, i.e., a baseline with only AD that produced a single (unseparated) effluent, compared to AD+SLS, and AD+SLS+NR that produced two separate fractions. With AD+SLS+NR, the processing system isolated a solid fraction with a high concentration of N and P, and a liquid fraction containing less nutrients. Compared to the baseline system, the addition of solid liquid separation and nutrient recovery (i.e. SLS+NR) reduced CH<sub>4</sub> emissions from outdoor liquid digestate storage by 87%, with only a small offset from higher N<sub>2</sub>O and NH<sub>3</sub> emissions from storing the solid fraction. The solid fraction was simulated to be transported to fields at least 30 km away from the dairy barns, while the liquid fraction was transported by dragline to fields adjacent to the barn. The advanced nutrient separation system resulted in much lower transport costs for manure nutrients and the ability to transport N and P to greater distances.

## KEYWORDS

manure separation, greenhouse gas emissions, liquid manure, nutrient distribution, dairy farm modeling, manure transportation

## 1 Introduction

The livestock sector is a significant source of greenhouse gas (GHGs) emissions (IPCC, 2014). Manure management contributes an increasingly large proportion to GHG emissions due to the industrialization of animal agriculture and contributes about 12-41% of methane (CH<sub>4</sub>) and 30-50% of nitrous oxide (N<sub>2</sub>O) to the total global agricultural

emissions (Chadwick et al., 2011; Li et al., 2020). Thus there is an interest in understanding the effects of manure management on direct and indirect GHGs emissions.

Besides emission considerations, manure contains valuable nutrients for crops. Most livestock excrete more than 70% of dietary N and 65% of dietary P in feces and urine (Reijs et al., 2007; Van der Meer, 2008). Hence, the efficient recovery and recycling of livestock manures to fertilize crops and improve soil fertility is an important option for minimizing the reliance on fossil-fuel-derived synthetic N and the depletion of non-renewable P resources (Desmidt et al., 2015; Sharpley et al., 2018).

The distribution of manure nutrients is an important consideration because surplus manure-derived nutrients are a waste of natural resources and can be harmful to water quality and biodiversity. A Canadian study illustrated that the imbalanced distribution of P in agricultural lands occurs in many regions in Canada and this trend was continuing (Reid et al., 2019). They noted about 10% of agricultural regions accumulated significantly high P and were continuously increasing, while 50% of soils were deficient in P and becoming more depleted. The over-accumulation of P in most high soil test P areas was dominated by livestock manure which highlights the need to develop strategies to disperse and rebalance the manure P to land that is low in P. However, due to the high water content of manure, the cost of manure transport is generally more expensive than commercial fertilizers. This transportation issue restricts manure-derived fertilizer application to only those areas located near livestock farms.

New technologies may provide opportunities to mitigate emissions and balance nutrients in manure for more efficient nutrient use. Manure treatment may induce changes to manure properties and therefore influence GHG emissions throughout the management chain (Hou et al., 2017). Manure treatment by anaerobic digester (AD) have demonstrated the potential to reduce GHG emissions (Hou et al., 2017; VanderZaag et al., 2018; Sigurnjak et al., 2020). Compared to untreated slurry, the CH<sub>4</sub> emissions with AD treatment can be reduced by 24 to 66% (Amon et al., 2006; Clemens et al., 2006; Chadwick et al., 2011; Battini et al., 2014). The biogas generated from AD can be used as renewable natural gas, or used to produce electricity and heat, thus offsetting fossil energy sources and further reducing GHG emissions. Solid-liquid separation (SLS) can be combined with AD, thereby separating the manure into two fractions, and partitioning some carbon and nutrients to the solid fraction and thus reducing total GHG emissions (Aguirre-Villegas et al., 2019). Compared to untreated dairy manure, SLS has the potential to reduce GHG emissions by 20 – 37% and increasing SLS efficiency can further reduce GHG by 46% (Jayasundara et al., 2016; Guest et al., 2017; Aguirre-Villegas et al., 2019). In doing so, liquid manure storage capacity is increased, and the solid fraction can be used to reduce expenses by providing bedding material or compost for soil amendment. Other technologies such as nutrient recovery by physical and/or chemical processes have been investigated in recent years and have shown the potential to further partition nutrients contained in the liquid manures and digestate (Shi et al., 2018; Porterfield et al., 2020; Camilleri-Rumbau et al., 2019; Camilleri-Rumbau et al., 2021).

A recent measurement study at a dairy farm with AD, SLS, and nutrient recovery (NR) showed the technologies greatly reduced CH<sub>4</sub> emissions from liquid storage (VanderZaag and Baldé, 2022). The NR technology used in this case study is based on the case-study farm and local environmental conditions and is consistent with some of the system designs identified by Sobhi et al. (2022). VanderZaag and Baldé (2022) also showed the system partitioned P in the solid fraction, and identified that emissions from the solid fractions should be considered to understand whether those emissions offset the reductions of CH<sub>4</sub> from liquid storage. Further analysis of nutrient transport costs with nutrient recovery was also suggested. The present study aims to address these gaps, using the same facility as a case study. The specific objectives were: 1) to evaluate the impacts of anaerobic digestion, solid liquid separation and nutrient recovery on multiple GHG emissions including CH<sub>4</sub>, NH<sub>3</sub>, and N<sub>2</sub>O from both liquid and solid fractions using a modeling approach; and 2) to investigate the cost implications of transporting manure P with separated liquid and solid fractions.

## 2 Materials and methods

### 2.1 Case study farm information and manure characteristics

This case study was based on the dairy farm and manure processing facility described in VanderZaag and Baldé (2022). The farm was located in British Columbia, Canada, and utilized an anaerobic digester, SLS, and NR system. Emissions of CH<sub>4</sub> from the liquid storages were measured over one year. The present case study does not exactly reflect the real farm conditions; rather, the facility was used as a reference point providing general farm information as inputs for building the case-study. The farm had 375 milking cows and 350 replacement animals on site. The manure management system included an anaerobic digester (AD) receiving the manure and food wastes (source separated organics, fats-oils-grease) and producing upgraded and compressed natural gas. Digestate was first processed through a solid-liquid separator (SLS) to produce bedding for the cows. The liquid fraction was then processed into a nutrient rich “cake” and a liquid fraction “tea”, using a nutrient recovery (NR) system including a dissolved air flotation (DAF) system and a moving disc separator (Trident Processes Inc., Abbotsford, BC).

### 2.2 Manure treatment and transportation scenarios

Three scenarios with different manure treatment systems were developed and analyzed for nutrients budgets, and GHG emissions. In Scenario A (SA), manure is processed by AD and the digestate is stored until field application. In scenario B (SB), the manure processing includes both an AD and a screw press (SLS). In this case digestate passes through a SLS, and the liquid fraction is stored, while the solid fraction is recycled back to the barn as bedding

material. In Scenario C (SC), manure is processed by an AD, a SLS and a nutrient recovery (NR) system in series. The NR system includes a dissolved air flotation system and press that produces a solid fraction (“cake”) and the liquid fraction (“tea”) has very low solids and is stored. The flow chart of treatment scenarios is shown in Figure 1.

Four transportation scenarios were considered for potential nutrient redistribution strategies, including a baseline reference scenario. The scenarios consider a farm that owns 250 ha of cropland adjacent to the barns, and has 100 ha of land located 30 km away. This is similar to the case study farm in the Fraser Valley, BC where available farmland is rare due to agricultural, commercial, and urban competition. Surplus manure in excess of crop requirements is sold to other farmers located at least 30 km away. The digestate application rate is limited by the N and P requirement for the crop, for which we used values of 300 kg N/ha and 60 kg P/ha (Kowalenko and Bittman, 2000; Sawyer and Mallarino, 2008). In the reference scenario (T0), unprocessed digestate of treatment SA is transported through a dragline pipe and directly applied on a local field of 250 hectare within 1 km distance. The remaining liquid manure is transported by truck to a 100-hectare field that is 30 km away from the farm for application.

The remaining three transportation scenarios are based on the nutrient flows from manure treatment scenario SC (Figure 2) in which solid and liquid fractions are transported separately. In transportation scenario 1 (T1), the liquid fraction is transported and applied by dragline to the same local field as described in T0, in this case the local 250 ha field receives less than 58.7 kg P/ha and is assumed to utilize soil P reserves. The solid fraction is transported by truck to a distant fields located 30 km away. Surplus solid manure is sent to additional fields at the same distance (30 km) by truck. Local transportation and application of the liquid fraction (1 km) and distant transportation and application of the solid fraction (30 km) of transportation scenarios 2 (T2), and scenario 3 (T3), are the same as T1. For T2, surplus solid manure is

transported to fields as far as possible by truck (farther than 30 km) while keeping the total transportation cost the same as T0. For T3, the surplus solid manure is transported the same distance as for T2, however, solid manure is transported by train rather than by truck. Transport costs were given in tonne × km, or tkm, the cost to transport one tonne a distance of one km. The unit transportation price (application cost not included) for dragline (liquid), truck for solid, truck for liquid, and train (solid) were \$0.06/tkm for dragline, \$0.28/tkm for truck, \$0.04/tkm for train. Due to inflation these values are higher than those in previous studies (Fleming et al., 1998; Ribaud et al., 2003; Mahmudi & Flynn, 2006).

### 2.3 Dairy-CropSyst model and inputs

Effects of the management scenarios on gaseous emissions and nutrient budgets were modeled using Dairy-CropSyst, a comprehensive dairy farm and manure management modeling tool developed by Khalil et al. (2019). The model was developed based on standards such as IPCC and ASABE, mass balance, and empirical equations which can be found in the Appendix A of Khalil et al. (2019). The Dairy-CropSyst model considers the impacts from manure treatment processes including AD, SLS, and NR to separate nutrients and fine solids. The model was developed based on integrating existing equations describing the biochemical transformations (e.g., C, N, P) and gas emissions (CO<sub>2</sub>, CH<sub>4</sub>, N<sub>2</sub>O, NH<sub>3</sub>), as well as performance parameters of manure treatment technologies. In this study, the default model settings for weather input were modified (R. Nelson, personal communication), to represent the target site described in VanderZaag and Baldé (2022). Site-specific inputs to the model included site location and dimensions, dairy characteristics, diet components, manure digestion, treatment, and storage processes (Table 1).

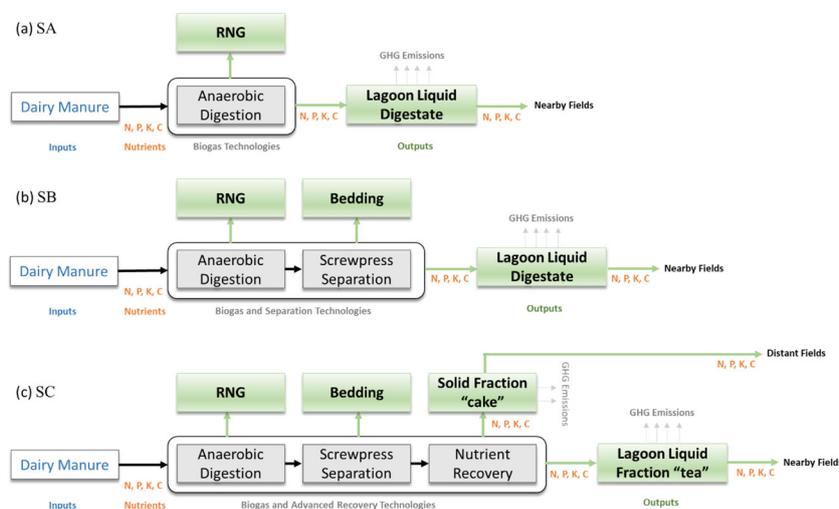


FIGURE 1 Manure management technologies of three treatment scenarios: (A) Treatment scenario SA; (B) Treatment scenario SB; (C) Treatment scenario SC.

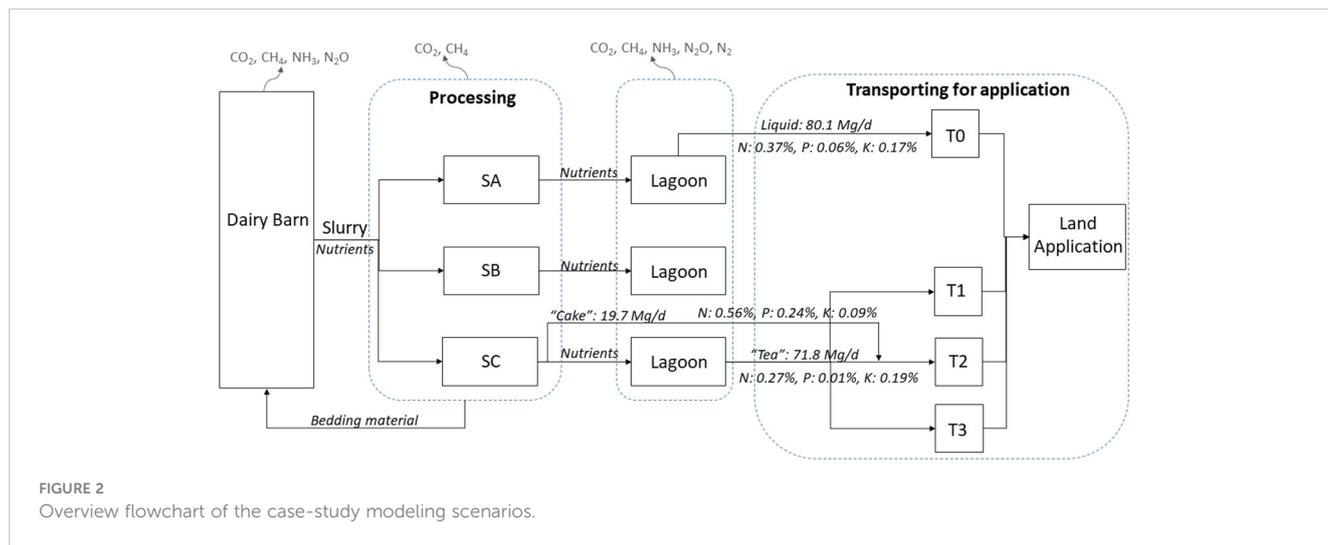


FIGURE 2 Overview flowchart of the case-study modeling scenarios.

At the facility described in VanderZaag and Baldé (2022), the manure stream was mixed with off-farm feedstocks (e.g. food waste) and the mixture was fed to the AD. The Dairy-CropSyst model, however, can only consider manure produced on the farm as the feedstock for AD. Therefore, to produce a similar mass flow of digestate, the number of dairy cows was doubled in the model simulations, to 750 head (N1;

Table 1). This assumption of a manure-only digester likely changes the C, N, and P allocations compared to a digester receiving food-waste as co-feedstocks. The model simulated biogas production of 980 kg/d (CH<sub>4</sub>), which is about 1/3 the amount produced at the case-study farm. The differences is likely due to the lower biogas potential of manure compared to off-farm co-feedstocks used at the case-study farm.

TABLE 1 Site information and model inputs, either based on the case-study in VanderZaag and Balde 2022, or estimated.

Parameter	Description	Unit	Value	Source
Latitude	site location	°	49.1	Case study farm
Longitude	site location	°	-122.9	Case study farm
BW	body weight	kg	700	Estimated
DMI	dry matter intake	kg/d	26	Estimated
MP	milk production	kg/d	35	Case study farm
CP	crude protein	%	16	Estimated
Starch	Starch in diet	%	30	Estimated
ADF	acid detergent fiber in diet	%	18.9	Estimated
NDF	neutral detergent fiber in diet	%	32.8	Estimated
ME	metabolizable energy in diet	MJ/d	479.7	Estimated
pH	pH of manure		7.0	Case study farm
A1	area of manure alley	m <sup>2</sup>	750	Case study farm
N1	number of milking cows	head	750	Modified from case study
Nc	cleaning frequency	#/d	6	Case study farm
A2	surface area of lagoon	m <sup>2</sup>	4260	Case study farm
Vmax	max volume of lagoon	m <sup>3</sup>	11997	Case study farm
Nd	day of year for fertigation	d	180	Modified from case study
a1	% amount removed	%	50	Estimated
n	repeats every	d	90	Modified from case study
A3	field area (nearby, <2 km)	ha	100	Estimated
A4	field area (far away, >30 km)	ha	200	Estimated

The model calculated urine and manure production and nutrients in manure slurry as functions of milk production and body weight (Khalil et al., 2019). Manure produced in the barn was assumed to be periodically scraped and flushed out from the floor with water in milking parlors (Khalil et al., 2019). Manure mass flow rates, total solid contents of manure (TS), nutrient concentrations of total nitrogen (TN), total phosphorous (TP), and total potassium (TK) of each manure treatment process were predicted for each liquid and solid stream. Default separation efficiencies (nutrient content in the solid fraction/liquid influent) of the coarse SLS separator are 40%, 12%, 10%, 5%, and 9% for TS, TKN, TON, TP, and TK, respectively. Nutrient concentrations of TN, TP, and TK in the liquid “tea” were estimated for the NR system in treatment SC using the separation efficiency of 36% for N, 85% for P, and 11% for K, respectively based on a previous study (Porterfield et al., 2020).

The Dairy-CropSyst model simulates emissions from the animals and barn surfaces including CH<sub>4</sub>, N<sub>2</sub>O and NH<sub>3</sub> (biogenic CO<sub>2</sub> is simulated but was excluded in our analysis as it is not a net GHG). Biogas produced by the AD was predicted by the model, and fugitive emissions were assumed to be 1% of the total CH<sub>4</sub> production (IPCC, 2019). Literature values of volatile solid (VS) to TS ratios are used to estimate VS contents for liquid and solid storage which are 71% and 91%, respectively (Fillingham et al., 2017; VanderZaag & Baldé, 2022). Direct and indirect N<sub>2</sub>O (via NH<sub>3</sub>) emissions from lagoon, bedding materials, and solid “cake” were predicted following the IPCC procedures (IPCC, 2019), specifically the Tier 2 method of methane emissions from solid and liquid manure management was used for estimating CH<sub>4</sub> emissions. Methane conversion factors (MCF) for solids (bedding and cake) was 2% (IPCC, 2019). The maximum methane-producing capacity of dairy manure (B<sub>0</sub>) was assumed to be 0.24 m<sup>3</sup> CH<sub>4</sub>/kg VS (IPCC, 2019). Nitrogen loss due to volatilization of NH<sub>3</sub> (and NO<sub>x</sub>) as a fraction of total N excreted for uncovered anaerobic lagoon systems and solid storage systems are 0.35 and 0.30, respectively (IPCC, 2019). Emission factors (EFs) for direct N<sub>2</sub>O

emissions from solid and liquid manure storage are 0.02 and 0.001 kg N<sub>2</sub>O-N/kg N, respectively (Kebreab et al., 2006).

## 3 Results

### 3.1 Nutrient budget

According to estimates from Dairy-CropSyst the daily manure produced in the barn was 97.6 Mg/d with 8.12% total solids (TS) content. This is approximately double the observed manure production rate at the case study farm (VanderZaag and Baldé, 2022) which makes sense because we assumed the herd size was doubled to make-up for the lack of off-farm feedstocks. Simulated water flow out of the barn (89.65 Mg/d) was slightly greater than the total water excreted by cows (41.69 Mg/d) and water used in the parlor (44.18 Mg/d) and the difference was the amount of water consumed for other cleaning. The liquid manure was subject to further processing using different technologies (Table 2). The initial nutrients in the out-flow stream leaving the barn contained 0.37% N, 0.06% P, and 0.17% K, and the N/P ratio was 6.1:1, which is similar to the observed ratio of 6.7:1 (VanderZaag and Baldé, 2022). Therefore, a total of 2890 Mg of TS per year was generated in the barn with annual production of N, P, and K of 131 Mg/yr, 22 Mg/yr, and 62 Mg/yr, respectively.

As manure was processed in the AD, organic matter (OM) was decomposed to produce biogas (CH<sub>4</sub>, CO<sub>2</sub>) and the mass of total solids in manure dropped from 7.92 Mg/d in barn out-flow to 4.45 Mg/d in AD effluent which was beneficial for reducing CH<sub>4</sub> emission during digestate storage (Table 2). Parts of the organic N (TON) was converted to ammoniacal N (TAN) in the digester, but the total N (TN) was unchanged. Total P (TP) and total K (TK) were all retained in the digestate and flowed into the screw press separator.

After passing through SLS, 8.95 Mg/d solid mass was separated from the liquid fraction accounting for 9.5% of the total mass input

TABLE 2 Mass and nutrient composition of manure at the out-flow of different treatment stages as estimated by Dairy-CropSyst.

Operation	Manure product	Mass Mg/d	%TS	%N	%P	%K	TS Mg/d	Water Mg/d	TN kg/d	TP kg/d	TK kg/d
Barn	Cow	49.26	15.36	0.37	0.11	0.31	7.57	41.69	332.61	54.65	153.90
	Parlor	44.59	0.91	0.06	0.01	0.04	0.41	44.18	26.93	4.49	15.71
	Flow-out	97.57	8.12	0.37	0.06	0.17	7.92	89.65	358.64	59.14	169.60
After anaerobic digestion											
AD	Digestate	94.11	4.73	0.38	0.06	0.18	4.45	89.65	358.64	59.14	169.60
After separation											
SLS	Liquid	85.15	3.14	0.37	0.07	0.18	2.67	82.48	315.53	56.46	154.34
	Solid	8.95	19.90	0.48	0.03	0.17	1.78	7.17	43.11	2.68	15.26
After nutrient recovery											
NR	Liquid	76.98	1.42	0.26	0.01	0.18	1.10	75.88	201.94	8.47	137.36
	Solid	8.18	19.29	1.39	0.59	0.21	1.58	6.60	113.59	47.99	16.98

AD, anaerobic digestion; SLS, solid liquid separation; NR, nutrient recovery.

and the TS content in the liquid fraction was decreased to 3.1%. According to the separation efficiencies of the screw press separator, the TN, TP, and TK remaining in the liquid fraction were 315.5, 56.5, and 154.3 kg/d, respectively. The N/P ratios of liquid and solid fractions were 16:1 and 5.6:1, respectively.

Finally, the nutrient recovery system separated 19.7 Mg/d of mass from the liquid manure to the solid fractions (Table 2). The TS content in the liquid was further reduced to 1.4%, which was somewhat higher than the observed value at the case-study farm (0.8%, VanderZaag and Baldé, 2022). As a result of NR, the liquid “tea” contained only 64% of TN and 15% of TP, compared to the unseparated digestate. Conversely, the solid fraction contained 85% of the TP with only 8% of the mass of water. The majority of K remained in the liquid fraction and only 11% of TK was recovered into the solid “cake” by NR. In general, these simulated results are comparable to the observed values at the case-study farm (VanderZaag and Baldé, 2022). The simulated N/P ratio in the liquid “tea” was 23.8:1 which was significantly higher than that in the solid “cake” of 2.4:1, and this was because most of the P was recovered in the solid “cake” by NR treatment.

### 3.2 GHGs

Simulated GHG emissions for each treatment scenario is listed in Table 3. Emissions from the dairy barn were primarily in the form of CH<sub>4</sub> from enteric fermentation, which are constant across all manure treatment scenarios. In SA, enteric emissions account for less than half of the total emissions from the whole facility, owing to higher emissions from the manure processing and storage. In SC, enteric emissions account for the over 75% of the total due to lower emissions from manure processing. Fugitive emissions from AD are

also constant across all scenarios and contribute <2% of the total CO<sub>2</sub>e in all scenarios.

In SA, the majority (59%) of the total GHG emissions were from the storage of digestate in the lagoon (Table 3). These emissions were primarily due to CH<sub>4</sub>, with indirect N<sub>2</sub>O from ammonia emissions having a small contribution and direct N<sub>2</sub>O being negligible (Figure 3). Guest et al. (2017) also simulated that emissions from conventional manure storage tanks on a farm in Ontario were high and contributed more than half of the carbon footprint of the farm.

In SB, the addition of SLS led to reduced overall GHG emissions by 24% (including barn emissions), and reduced lagoon emissions by 45%. These reductions were due to less solids (carbon) entering the lagoon resulting in lower CH<sub>4</sub> emissions, offset by small increases in emissions from solid storage. Emissions from the solid fraction were mainly direct N<sub>2</sub>O emissions; however, the contribution of N<sub>2</sub>O from the solid fraction was small relative to the CH<sub>4</sub> emitted from the liquid fraction (Figures 3, 4). Thus, overall liquid and solid manure storage GHG emissions were 42% lower in SB compared to SA (Figure 4).

In SC, the addition of NR technology further reduced overall GHG emissions by 44%, and lagoon emissions by 87%. The simulated CH<sub>4</sub> emissions from the lagoon were 83.8 kg/d on average, which is somewhat higher than the observed average of 56 kg/d at the case-study farm (VanderZaag and Baldé, 2022). This difference is reasonable given the differences in feedstocks to the AD, and the higher simulated TS in the liquid tea compared to observed. The simulated CH<sub>4</sub> emissions from the lagoon in SC were 75% lower than SB, and 87% lower than SA. Reduced emissions from the liquid fraction were due to much greater carbon and nitrogen content in the solid fraction. This, in-turn, led to higher emissions from the solid fraction. In fact, the solid fraction

TABLE 3 Estimated gas emissions from each treatment stage and the total gas and GHG emissions (CH<sub>4</sub>, N<sub>2</sub>O, indirect NH<sub>3</sub>) of the treatment scenarios using Dairy-CropSyst.

Scenario	Technology	Stage	CH <sub>4</sub> (kg/d)	Indirect N <sub>2</sub> O (kg/d)	N <sub>2</sub> O (kg/d)	GHGs (Mg CO <sub>2</sub> e)
All	All	Barn	454.44	1.07	0.02	11.78
SA	AD	AD	9.80			0.24
		Lagoon	650.70	2.64	0.27	17.37
		Total	1114.94	3.71	0.29	29.39
SB	AD+SLS	AD	9.80			0.24
		Lagoon	342.01	2.51	0.24	9.59
		Bedding	5.21	0.22	1.35	0.60
		Total	811.47	3.80	1.62	22.22
SC	AD+SLS+NR	AD	9.80			0.24
		Lagoon	83.8	0.86	0.32	2.45
		Bedding	5.21	0.22	1.35	0.60
		Solid cake	4.61	0.57	3.57	1.35
		Total	557.88	2.72	5.27	16.42

AD, anaerobic digestion; SLS, solid liquid separation; NR, nutrient recovery.

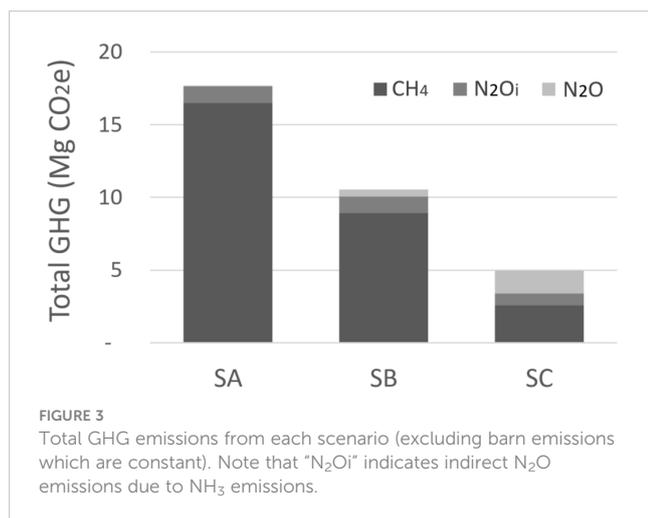


FIGURE 3  
Total GHG emissions from each scenario (excluding barn emissions which are constant). Note that “N<sub>2</sub>O<sub>i</sub>” indicates indirect N<sub>2</sub>O emissions due to NH<sub>3</sub> emissions.

contributed 44% of the total storage emissions (Figure 4), owing primarily to N<sub>2</sub>O emissions from the solid cake (Figure 3).

### 3.3 Transportation to fields

Annual cost of manure transportation and field application for separated liquid and solid fractions in scenario SC was evaluated and compared to transporting unseparated liquid digestate in SA. In the reference transportation scenario, T0, liquid was transported to a nearby 250-ha field through a dragline, and transported 30 km by truck to a 100-ha field to meet the P requirement. Surplus manure in excess of the P requirements of those 300-ha was applied to other fields 30 km-away (Table 4). In this case the total cost of transporting manure for field application was \$97,253, due to the relatively high cost of transporting water in the liquid fraction 30 km by truck.

The first transport scenario with separated fractions, T1, the liquid “tea” fraction stored in the lagoon was transported by dragline to the nearby 250 ha field, while the solid “cake” fraction was transported 30 km by truck. The total applied area of T1 was 30 ha greater than T0 to distribute the mass of P in the solid fraction

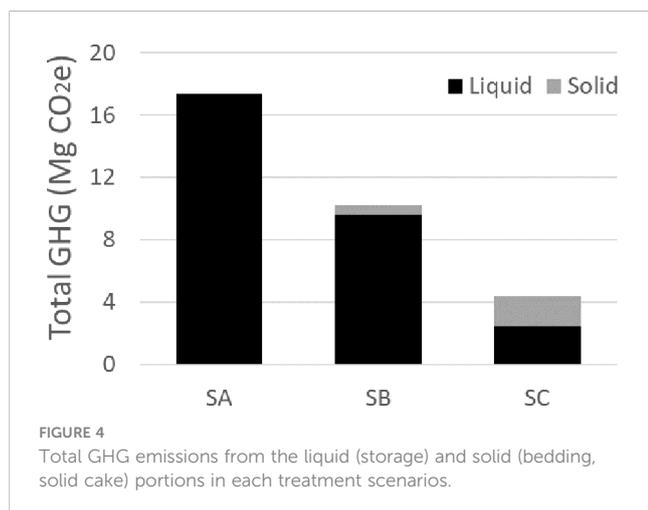


FIGURE 4  
Total GHG emissions from the liquid (storage) and solid (bedding, solid cake) portions in each treatment scenarios.

according to P requirements of the soil (Table 4). Nevertheless, despite transporting P to more land, the total transportation cost of T1 dropped more than 72% to \$26,638 because the mass of water transported by truck was reduced by 8,071 tonnes compared to T0 (from 10,479 to 2,408). The dramatic cost reduction shows that dewatered solid manure offers a promising opportunity to reduce manure transportation cost by distributing water *via* dragline rather than by truck.

In the second transportation scenario, T2, the parameters of T1 were kept the same except that the transportation distance for the solid fraction was increased so that the total transportation cost was equal to T0. In this case the solid manure in excess of the requirements for 350 ha was transported by truck to 198 ha of land located over 150 km away.

In the third transportation scenario, T3, the parameters of T2 were kept the same, except that long distance transportation of the excess solid fraction was done by train instead of by truck. Since the transport by rail has a much lower cost than truck, the overall cost in this scenario was more than 75% lower than T0. Further calculation were done to maximize transport distance while maintaining the same transport cost from T0. In this case, the surplus solid fraction could be transported 1,100 km by train for the same overall cost as T0. This illustrates the potential for nutrient recovery to enable transport of manure P out of a manureshed with a high level of manure P, to another agricultural landscape where there is a P deficit (Reid et al., 2019).

## 4 Discussion

Application rates based on N and P generally limit the ability to appropriately distribute digestate or manure without exceeding crop requirements or environmental limits (Feinerman et al., 2004; Carreira et al., 2007; MPCA, 2011; Hanserud et al., 2017). The geographic location of this study – the Fraser Valley, BC – is an intensive agricultural area with a net import of nutrients (mainly in feed, forages, and fertilizer) with a limited amount of land for redistribution due to being constrained by mountains, ocean, and the border. Presently, very little nutrients are recycled back to distant cropland where the imported feed originated. Improving the efficacy of recycling nutrients has been identified as crucial for the reduction of net nutrient imports and sustainability in this area (Franzuebbers et al., 2021; Bittman et al., 2023).

In this study, model simulations showed separation considerably changed the N/P ratio in each fraction. After nutrient recovery, the liquid fraction N/P ratio was reduced in the solid fraction (where P was concentrated) and greatly increased in the liquid. These results were partially consistent to the findings by Hou et al. (2017) who reported that the N/P ratios in liquid fractions with separation treatments were higher than with untreated manure.

At the same time, nutrient recovery resulted in the solid fraction having a much higher concentration of solids and P, with less water. Reduced mass enabled the longer distance of solid fraction. Meanwhile, the higher N/P ratios in liquid fraction can be applied on nearby fields with lower requirements of P fertilizer due to

TABLE 4 Annual cost of reference and four transportation scenarios.

Scenario	Land	Fraction	Area (ha)	Distance (km)	Method	N applied (kg/ha)	P applied (kg/ha)	N transported (t/y)	P transported (t/y)	Water (t/y)	Mass (t/r)	Cost (\$/y)	Cost change	Unit cost (\$/tkm)
T0	nearby	liquid	250	1	dragline	264.51	58.69	66.1	14.7	22244	24209	97253	0.0%	0.27
	distant	liquid	100	30	truck	264.51	58.69	26.5	5.9	8898	9684			
	surplus	liquid	18	30	truck	264.51	58.69	4.7	1.0	1581	1721			
T1	nearby	liquid	250	1	dragline	286.42	12.36	71.6	3.1	25895	26215	26638	-72.6%	0.23
	distant	solid	100	30	truck	27.31	58.69	2.7	5.9	807	1000			
	surplus	solid	198	30	truck	27.31	58.69	5.4	11.6	1601	1984			
T2	nearby	liquid	250	1	dragline	286.42	12.36	71.6	3.1	25895	26215	97253	0.0%	0.26
	distant	solid	100	30	truck	27.31	58.69	2.7	5.9	807	1000			
	surplus	solid	198	157	truck	27.31	58.69	5.4	11.6	1601	1984			
T3	nearby	liquid	250	1	dragline	286.42	12.36	71.6	3.1	25895	26215	22441	-76.9%	0.06
	distant	solid	100	30	truck	27.31	58.69	2.7	5.9	807	1000			
	surplus	solid	198	157	train	27.31	58.69	5.4	11.6	1601	1984			

having received manure and digestate for many years. Due to the lower volume of P-rich solid fraction, this material was able to be transported long distances at a lower cost. This is because the majority of the mass of unseparated digestate is in the form of water. After separation, most of the water can be transported to the local field by dragline, which is the most efficient and economical transport method. The use of trucks is then more efficient because less money is used to transport water. For example, transporting the mass of digestate produced in a single day would require five trips for a tanker truck with a 20-tonne capacity. In contrast, after separation and nutrient recovery, the mass of solid cake produced can be transported by a single 20-tonne dump truck taking one load every-other-day. Not surprisingly, therefore, annual transport costs were reduced by more than 90%. Efficient manure dewatering and nutrient recovery technologies show the potential of concentrating the nutrients and reducing the cost of long-distance transport to reduce reliance on mined P in areas farther from livestock. This approach may enable new opportunities for manure trading among different farm types. For example, [Franzluebbers et al. \(2021\)](#) provided an example of using dairy manure solids for fertilizing a newly planted high-bush blueberry field.

Emissions of CH<sub>4</sub> from the liquid storage were reduced by half through simple separation with SLS (SB) relative to the baseline (SA). In SB, emissions of N<sub>2</sub>O were increased; however, this had little impact on the overall GHG emissions from manure management which were reduced by 42% relative to SA. Overall farm GHG emissions were reduced 25% in SB relative to SA. This closely agrees with previous analyses where a 24% reduction in total farm GHG emissions were estimated from a dairy farm with a screwpress separator and composter ([Guest et al., 2017](#)), and 25 to 31% for AD and SLS ([Holly et al., 2017](#)).

Further treatment with nutrient recovery (SC) resulted in greater CH<sub>4</sub> emission reductions from liquid storage, being 87% less than SA. Transferring C and N to the solid cake, however, resulted in much greater N<sub>2</sub>O and NH<sub>3</sub> emissions compared to the baseline condition in SA. Nitrous oxide emitted from solid cake storage in SC were high, which is consistent with previous studies comparing N<sub>2</sub>O emissions from solid and liquid storage ([Pattey et al., 2005](#); [Fangueiro et al., 2008](#); [Petersen et al., 2013](#)). Nevertheless, after considering the global warming potential of each gas, the reduction of CH<sub>4</sub> emissions outweighed the increase in N<sub>2</sub>O and NH<sub>3</sub> because CH<sub>4</sub> was the main contributor to emissions. Therefore, the overall effect of the nutrient recovery system was beneficial, reducing the total GHG emissions from manure storage. This is an important finding as the potential for pollution-swapping is always a concern in agricultural emission mitigation. Therefore, although N<sub>2</sub>O emissions from the solid fraction were small compared to the original CH<sub>4</sub> emissions that were reduced, there is potential to further improve the GHG balance of nutrient recovery systems by developing technologies or techniques to reduce N<sub>2</sub>O and NH<sub>3</sub> emissions from the solid fraction.

Methane produced by the AD was estimated to be 980 kg/d (1485 m<sup>3</sup>/d). This is a conservative estimate because the AD was using only manure as feedstock. Like most on-farm AD systems in Canada, the AD at the case-study farm produces ca. 3-times more methane (150-250 m<sup>3</sup>/h) due to the use of high-yielding co-feedstocks from other sectors (e.g. fats, oils, grease, food waste).

This methane is injected on a natural gas pipeline and displaces fossil fuels. Displaced emissions adds GHG benefit that were not considered in the present analysis.

The Dairy-CropSyst model used to simulate the treatment scenarios is a user-friendly tool to assist in decision making of dairy farm nutrient management. However, it was unable to include off-farm streams, customize the treatment process, or easily modify site specific factors such as the recovery rates of N-P-K nutrients. We suggest the model be expanded to include off-farm organic matter addition, enable the use of more site and treatment specified parameters and add more flexibility for simulating mass flow of nutrients and GHG emissions for different technologies.

Although, manure management technologies can be efficient to decrease the transportation cost for redistributing manure P to distant land, the capital cost, maintenance, and operation cost have not been considered in this study. The nutrient recovery system implemented on the case-study farm cost in the range of \$650,000 in 2015 and roughly \$5,000 per month for operation and purchase of polymer. Meanwhile, this manure treatment system produced valuable bedding materials and greatly reduced manure transport costs, and reduced fossil fuel emissions from trucking liquid manure. Energy produced from AD can replace heat and electricity generated by fossil fuels and therefore reduce CO<sub>2</sub> emissions from fossil energy. Economic analysis of cost and revenue, and returns on investment is an area for further research. With greater research, there may be opportunities to reduce costs for this type of nutrient recovery system, or to develop other technologies to achieve similar results.

Distribution of manure nutrients N-P-K could also be economically beneficial provided it is used to substitute chemical fertilizers. Moreover, there is value in viewing P recycling as the recovery and careful use of a precious essential nutrient rather than a waste to manage. It is important to recognize the greater resilience through circular re-use of P and the need to balance net P imports within intensive agricultural regions like the Fraser Valley ([Bittman et al., 2017](#)). At a broader scale, effective re-use of P is important for Canada which is completely reliant on import of non-renewable rock P ([Nicksy and Entz, 2021](#)). Alternative transportation methods such as pipeline, barge, and other innovative hauling plans may be beneficial for specific regions and should be evaluated for the possibility of manure nutrients redistribution.

## 5 Conclusions

Scenario analyses demonstrated that combined manure management technologies can substantially reduce total GHG emissions during manure processing and storage. Using SLS alone reduced liquid storage emissions by 45%, while the combination of SLS and NR partitioned most of the carbon to the solid fraction and reduced CH<sub>4</sub> emissions from the lagoon by 87%. There was a modest trade-off with higher emissions of N<sub>2</sub>O from the solid fraction, the mitigation of which could be an area for further study. With these technologies most of the water in digestate was kept in the liquid fraction and could be applied by dragline, thus reducing the cost associated with long-distance hauling of water. As a result it

was economical to transport the P-rich solid fraction long-distance to redistribute nutrients (especially P) from the dairy farm to farther away fields.

## Data availability statement

The raw data supporting the conclusions of this article will be made available by the authors, without undue reservation.

## Author contributions

XF: Formal analysis, data curation, investigation, methodology, software, writing original draft. WS: Funding acquisition, methodology, resources, conceptualization, revision. AV: Conceptualization, funding acquisition (lead), investigation, visualization, resources, supervision, validation, revision. All authors contributed to the article and approved the submitted version.

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## Conflict of interest

The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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