



Self-Healing and Damage Resilience for Soft Robotics: A Review

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Advances in soft robotics will be crucial to the next generation of robot–human interfaces. Soft material systems embed safety at the material level, providing additional safeguards that will expedite their placement alongside humans and other biological systems. However, in order to function in unpredictable, uncontrolled environments alongside biological systems, soft robotic systems should be as robust in their ability to recover from damage as their biological counterparts. There exists a great deal of work on self-healing materials, particularly polymeric and elastomeric materials that can self-heal through a wide variety of tools and techniques. Fortunately, most emerging soft robotic systems are constructed from polymeric or elastomeric materials, so this work can be of immediate benefit to the soft robotics community. Though the field of soft robotics is still nascent as a whole, self-healing and damage resilient systems are beginning to be incorporated into three key support pillars that are enabling the future of soft robotics: actuators, structures, and sensors. This article reviews the state-of-the-art in damage resilience and self-healing materials and devices as applied to these three pillars. This review also discusses future applications for soft robots that incorporate self-healing capabilities.

Keywords: soft robotics, self-healing, damage resilience, soft actuators, soft sensors

INTRODUCTION

Soft robots are often inspired by key aspects of biological systems, such as their near-infinite degrees of freedom, dexterity, environmental adaptability, and power output (Kim et al., 2013; Rus and Tolley, 2015; Balasubramanian et al., 2016). Taking inspiration from the soft, deformable, and adaptable bodies found in nature, soft roboticists develop robotic systems with capabilities beyond those achievable by traditional rigid robots (Pfeifer et al., 2012; Majidi, 2013). Because of their materially soft nature, soft robotic technologies are often considered to be potentially safer for interaction with humans, both as human-assisting actuators and as wearable sensory skins (Hammock et al., 2013; Laschi and Cianchetti, 2014; Lu and Kim, 2014; Amjadi et al., 2016; Abidi and Cianchetti, 2017; Wang et al., 2017). However, in order to be commercially viable for everyday use in these applications, soft robots should be robust enough to function alongside their self-healing, damage resilient biological companions (Bauer et al., 2014).

This article reviews current examples of self-healing and damage resilient materials that have been integrated into soft robot technologies (actuation, structure, and electronics). This review also has the goal of showing that there is an open field of research in the future of self-healing, damage resilient soft robots. We exclude from this review the details of the chemistry behind self-healing materials, as many recent reviews and books are already dedicated to this subject

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(Wool, 2008; Wu et al., 2008; Ghosh, 2009; Hager et al., 2010, 2016; Murphy and Wudl, 2010; Ahner et al., 2015; Kuhl et al., 2015; Li and Meng, 2015; Roy et al., 2015; Huynh et al., 2017).

For the purpose of this article, we distinguish damage resistance from damage resilience. We define damage *resistance* as the ability to withstand an unexpected external stressor without damage, i.e., getting hit with a hammer, run over by a car, or exposed to open flame (Martinez et al., 2014; Tolley et al., 2014). Soft robots are almost always assumed to be damage resistant, an ideal characteristic for robots intended to function alongside biological systems in uncontrolled, unpredictable environments. We define damage *resilience* as the ability to be materially damaged (permanently deformed through crack propagation, fracture, mechanical failure, or puncture) and then continue functioning. Self-healing is an obvious subset of this overarching definition, yet it is a critical ability for next-generation soft robots and holds equal importance to general damage resilience. The idea that robots can self-heal, self-repair, or correct for damage that has occurred like biological systems is a concept that is still relatively new (Frei et al., 2013), but one that would continue to distinguish soft robots from their rigid-bodied counterparts (Bauer et al., 2014).

Among the many potential advantages of soft robotic systems is the opportunity to bypass functional partitions. While traditional robots are usually comprised of components with a single function (e.g., actuators, sensors, structures, and controllers), emerging multifunctional materials are enabling components that can fulfill two or three different functions simultaneously. In the sections that follow, we review the use of self-healing materials in soft actuators, soft structures, and soft sensing devices. However, we note that material systems often appear across these categories as researchers have solved different functional problems using the same materials. **Table 1** provides a summary detailing some of the material applications and damage resilience systems presented in this review.

DAMAGE RESILIENT AND SELF-HEALING SOFT ACTUATION

Soft actuation comes in many forms, using specially designed material bodies or systems to convert an energy source into forces and displacements. Energy sources include (but are not limited to) electricity and electric fields, magnetic fields, pressurized gasses and liquids, thermal energy, and chemically induced mass transfer, each capable of providing kinematic motion (Madden et al., 2004; Hines et al., 2017). Though different in their underlying physics, soft actuators all allow for large strains (sometimes greater than 100%) in a flexible or stretchable material. In this section, we look at the current research that has gone into making these actuators damage resilient.

Dielectric Elastomer Actuators (DEAs)

Dielectric elastomer actuators are a promising actuation mechanism for soft robots (Gu et al., 2017; Hines et al., 2017). DEAs are capable of high strain deformations at high frequencies (<1 s), reliable blocking forces, and rapid controllability, all of which are

valuable qualities for actuation (Choi et al., 2007; Kofod, 2008; Kornbluh et al., 2009; Brochu and Pei, 2010; Anderson et al., 2012; Rosset and Shea, 2012; Carpi, 2016; Madsen et al., 2016a; Naficy et al., 2016). By sandwiching a highly stretchable dielectric layer between two stretchable electrodes, DEAs operate on a simple fundamental principle: charging the electrodes causes an attraction that squeezes the elastomer-based dielectric layer in between them, decreasing the actuator thickness and increasing its area. DEAs can be solid-state or semi-solid (where either the electrodes or the dielectric layer have fluidic elements), and their dielectrics can be made of silicones, acrylic elastomers, and other types of highly deformable, non-conductive materials (Romasanta et al., 2015). Very high electric potentials (in the range of kV) are often necessary to induce significant shape change, despite the dielectric typically being a thin film (<1 mm). For greater details, the reader is recommended these recent reviews (Wang and Qu, 2016; Zhu et al., 2016; Zhang and Serpe, 2017).

The thin nature of DEAs makes them susceptible to defects from physical damage and manufacturing imperfections. These defects are often undetectable until the electric potential is applied (Zurlo et al., 2016), and they can create a continuous conductive bridge or a sudden spark between the electrodes, effectively ending the life of the actuator. Since this defect-induced failure occurs at potentials much lower than required for a general dielectric breakdown, the whole actuator is rendered useless by a single flaw. Identifying this critical issue with DEAs, researchers have begun to search in earnest for effective solutions.

Fault-Tolerant Electrodes in DEAs

Fault-tolerant DEAs are a subcategory of DEAs whose electrodes are resilient to damage caused by dielectric breakdown or puncture. The group led by Dr. Qibing Pei has been working for the past decade to develop “self-clearing” electrodes. They first demonstrated the basics of this idea in 2007 (Yuan et al., 2007), but it was not until their pioneering paper in 2008 that they showed that this type of fault-tolerant electrode could operate after damage, even with a solid foreign object piercing the entire actuator (**Figure 1A**) (Yuan et al., 2008). The researchers made a flexible, stretchable electrode from spray-coated single-walled carbon nanotubes (CNTs) that degrades locally around any spark caused by dielectric breakdown, outside sources of electricity, or physical piercing. This degradation breaks the local continuity, and therefore conductivity, of the electrode, preventing further loss of energy through the damaged area, though also locally increasing the stiffness of the electrode. Initial results demonstrated self-clearing damage resilient electrodes fabricated by spray-coating onto dielectrics made of acrylic elastomers, and further work demonstrated self-clearing CNT electrodes on silicone dielectric layers as well (Yuan et al., 2010). Silicone as the dielectric material enables tunability of the speed of the self-clearing response by changing the thickness of the dielectric layer. Furthermore, the self-clearing electrodes enhance the overall lifespan of a DEA, operating for tens of thousands of cycles while experiencing and overcoming periodic breakdowns during operation (Stoyanov et al., 2013).

Another research group led by Dr. Dorina Opris has investigated damage resilient DEAs, altering both the electrode

TABLE 1 | Summary of self-healing and damage resilience mechanisms in the current soft robotic literature.

Damage resilience system	Application	Active material	Modulus of elasticity	Damage resilience mechanism	Self-healing stimulus	Recovery time scale	Recovered material property	Resilience cycles	Recovery efficiency per cycle	Reference
Damage isolation	Actuators (DEAs)	Carbon nanotubes	N/A	Electrode degradation	–	0–10 s	Area strain	>30	0.99	Stoyanov et al. (2013)
		Modified PMVS	80–200 kPa	Dielectric buffering	–	0–10 s	Area strain	5	0.99	Dünki et al. (2015)
Material elasticity	Actuators (inflatable)	Kevlar/silicone composite	0.4 MPa	Elastomer pressure	–	0–10 s	Curvature change	1	–	Shepherd et al. (2013)
	Electronics (RTLTM)	Silicone (PDMS)	1.84 MPa	Encapsulating elastomer pressure	–	0–10 s	Conductivity	2	0.99	Li et al. (2016b)
Physical self-healing (fluidic reflow)	Actuators (DEAs)	RTLTM	N/A	–	Applied voltage	10–20 s	Area strain	1	0.8	Liu et al. (2013)
		Silicone oil	N/A	–	Voltage reduction	0–5 s	Area strain	6	0.99	Hunt et al. (2014)
	Structures (low melting temperature materials)	Low melting temperature alloy	9.25 GPa/0.54 MPa	–	Joule heating	5–10 min	Tensile strength	3	0.78	Van Meerbeek et al. (2016)
		Wax	68–125 MPa	–	Thermal	10–20 min	Compressive strength	2	0.9	Cheng et al. (2014)
	Electronics (RTLTM)	RTLTM	N/A	–	Thermal	0–10 s	Conductivity	2	0.99	Li et al. (2016b)
Chemical self-healing (solid bonding)	Actuators (inflatable)	S-H polymer	7.85 MPa	–	Thermal	25 h	Contraction force	3	0.98	Terryn et al. (2017a)
		S-H elastomers	6–287 kPa	–	UV	30 s	Curvature change	1	0.99	Wallin et al. (2017)
	Actuators (hydrogel)	S-H hydrogel	240–770 kPa	–	Thermal	20 min	Tensile strength	1	0.99	Liu and Li (2017)
	Actuators (DEAs)	S-H elastomer	0.54 MPa	–	Thermal	72 h	Area strain	1	–	Li et al. (2016a)
	Structure (shape memory material)	Shape memory, S-H polymer	10–650 MPa	–	Thermal	5 h	Bending load	5	0.75	Nji and Li (2012)
			0.3–0.4 MPa	–	Pressure Joule Heating	–	Curvature change	>1	–	Huang et al. (2010)
	Electronics (RTLTM)	S-H polymer	240 kPa	–	Thermal Pressure	10–60 min	Conductivity	1	0.75	Palleau et al. (2013)
	Electronics (composites)	S-H elastomer	0.4–2 MPa	–	Thermal Pressure	15–30 s	Conductivity	3	0.98	Tee et al. (2012)
			0.67–0.8 MPa	–	Thermal	30–60 s	Conductivity	1	0.96	Darabi et al. (2017)
0.1 MPa 0.1 MPa			–	Thermal	5 min 24 h	Conductivity Fracture toughness	1 1	0.99 0.95	Liu et al. (2017) Cao et al. (2017b)	

PDMS, polydimethyl siloxane; RTLTM, room temperature liquid metal; S-H, self-healing; PMVS, polymethylvinylsiloxane; DEA, dielectric elastomer actuator.

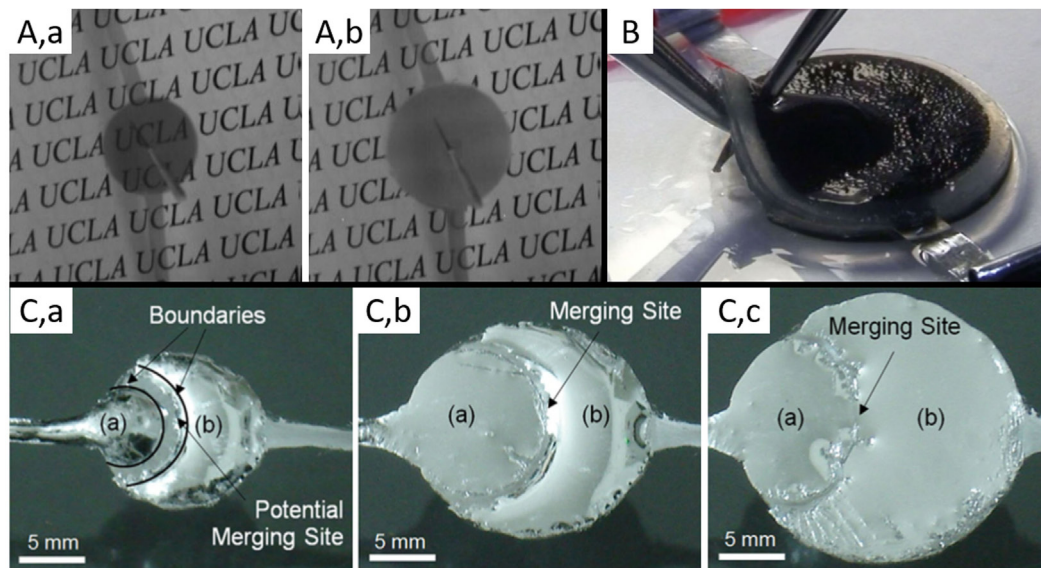


FIGURE 1 | (A) A damage resilient dielectric elastomer actuator (DEA) (via self-clearing carbon nanotube electrodes) is pierced with a foreign object [(A), a] and can still actuate [(A), b]. **(B)** A self-healing, silicone oil-based DEA is pierced with a needle. **(C)** Liquid-metal alloy is used as a self-repairing electrode layer in a DEA. **[(C), a]** The electrode is completely severed into two parts via separation of the liquid alloy. **[(C), b]** Upon application of the high voltage, the active side (a) expands, but the disconnected side does not (b). **[(C), c]** The electric potential disparity causes the liquid metal to flow from the active side to the inactive side, repairing the electrode and activating the rest of the DEA. **(A)** Reproduced from Yuan et al. (2008), ©2008 John Wiley & Sons Inc. **(B)** Adapted from Hunt et al. (2014), 2014 AIP Publishing LLC. **(C)** Reproduced from Liu et al. (2013), ©2013 AIP Publishing LLC. All figures are used with permission.

materials and dielectric materials to develop fault tolerance. In one work, a reduced-graphite electrode layer was used to achieve self-clearing (Michel et al., 2012). Although the original conductivity and stiffness of the undamaged electrode was higher than that of the CNT electrodes presented previously (Yuan et al., 2008), the electrode layer self-cleared without any increase in stiffness. In a separate work, damage resilience was embedded into the dielectric layer instead of the electrode through implementation of a chemically altered polymethylvinylsiloxane silicone. In the high heat of a spark, this dielectric material rapidly reacts to increase the local impedance, blocking further charge loss through the initial fault (Dünki et al., 2015).

Self-Healing DEAs

Moving beyond “fault tolerance,” several other works introduce fully self-healing systems into DEAs. This has been done by creating both self-healing dielectric layers and electrodes. Yu et al. (2015) first demonstrated a silicone dielectric elastomer that could self-seal holes in the dielectric layer created by a high-energy discharge spark. Li et al. (2016a) developed a highly stretchable, self-healing silicone elastomer and used it as the dielectric layer in a DEA to withstand both electrical and physical damage. A flat sample of the self-healing elastomer was punctured with a hole, allowed to heal for 72 h at room temperature, and then used as a DEA. The damaged site experienced no dielectric breakdown, even with application of an 11-kV charge on the electrodes. This research was followed up by Madsen et al., who presented a whole family of self-healing, stretchable dielectric silicones for use in DEAs (Madsen et al., 2016b).

Two other recent works have focused on harnessing the intrinsic healing of fluidic systems to build self-healing dielectric layers and electrodes. Hunt et al. (2014) created a dielectric layer from an open-cell silicone foam filled with silicone oil, with an electrode made out of a solidified carbon grease. When this DEA was punctured repeatedly with a needle (Figure 1B) or cut with scissors, the DEA rapidly self-healed and continued to function. Since the dielectric layer was a two-phase system, the dielectric oil flowed into the damaged sites, restoring the dielectric barrier between the two electrodes without any loss of flexibility or actuation potential in the DEA. Liu et al. used room-temperature liquid metals (the same used in self-healing electronics, see Self-Healing Electronics for Soft Robotics) to create a highly deformable thin-film fluidic electrode for a DEA (Liu et al., 2013). This liquid-metal electrode was able to self-heal from a break introduced by squeezing the liquid metal out from between two sections and sealed with the liquid metal’s non-conductive oxide skin (Figure 1C, a). With simple application of the same potential used to cycle the actuator, the liquid metal mechanically bridged the electrical block, reconnecting the rest of the electrode and restoring full functionality to the DEA (Figure 1C, b,c).

Damage resilient DEAs have been demonstrated using a variety of techniques. In the context of soft robotics, however, there are still challenges to overcome. DEAs made with self-clearing electrodes often must be operated at a reduced voltage in order to maintain the viability of the DEA during cyclic use (Stoyanov et al., 2013). An electric breakdown at higher voltages can cause catastrophic failure in the elastic dielectric layer, regardless of the self-clearing electrode. Furthermore, due to limitations in pre-straining and elastic response of self-healing dielectric materials

(Hunt et al., 2014), self-healing DEAs do not experience strains as large as their non-healing, counterparts. Self-healing DEAs also take a significant amount of time to heal, compared to their self-clearing counterparts (Li et al., 2016a). In the future, damage resilient DEAs might benefit from combining the various methods employed above: self-clearing or self-repairing electrodes with self-healing dielectrics, to create fully healing, highly resilient actuation systems.

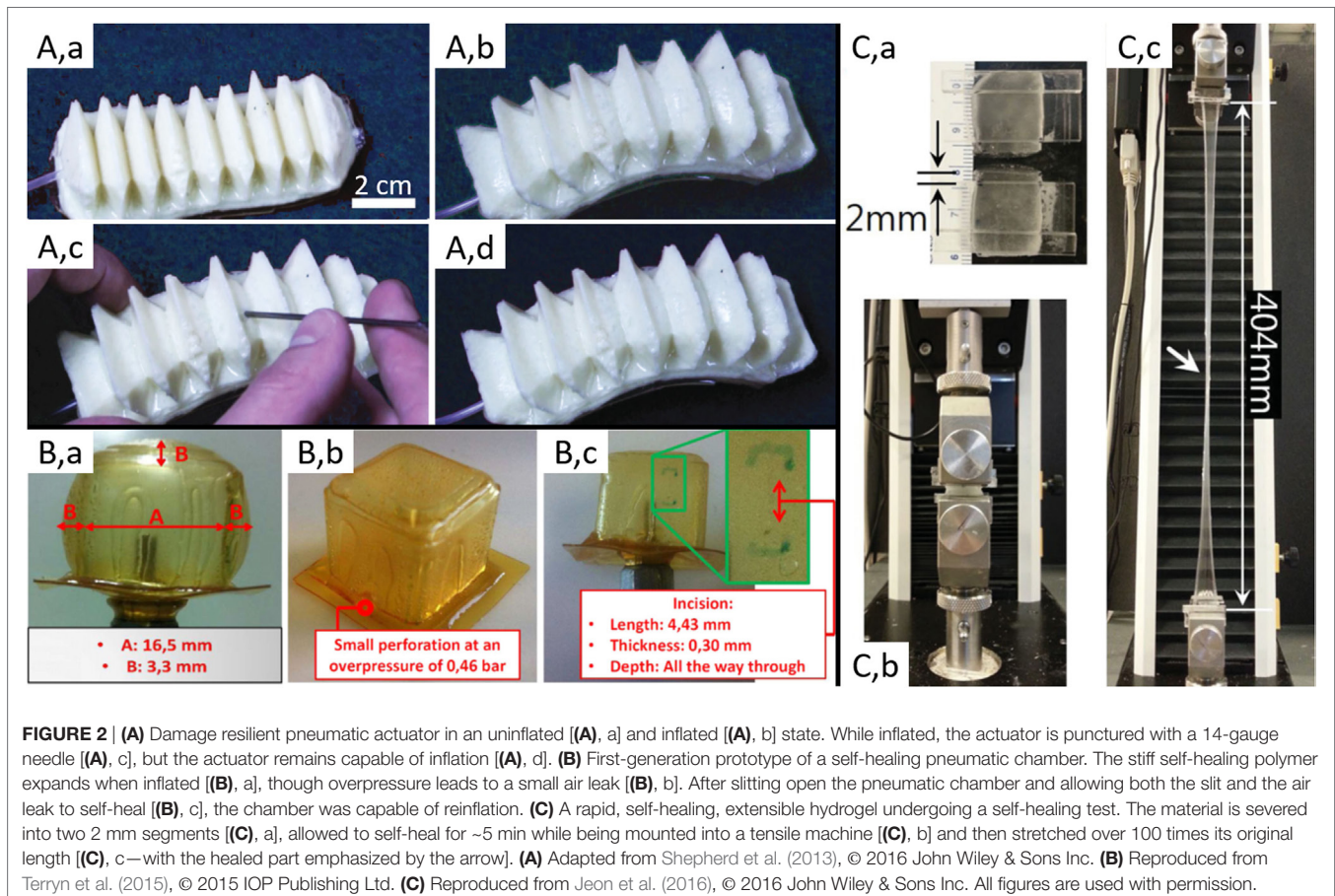
Inflatable Actuators

Pneumatic or hydraulic actuators created out of soft elastomeric silicone materials have become ubiquitous in the soft robotics community (Hughes et al., 2016; Lee et al., 2017). These actuators are made by casting the elastomer to create channels that, when inflated, cause the body to bend (or twist) in a manner dependent on the channel design. Their soft, highly deformable elastomer bodies inherently resist damage: absorbing impacts, twisting and compressive loads and more (Martinez et al., 2014), and can even survive being run over with a car (Martinez et al., 2014; Tolley et al., 2014). There is a key problem with this damage resistance: like a balloon, if the actuators pop from overpressure or puncture, they lose all functionality.

Shepherd et al. (2013) presented a potential opportunity to correct this deficiency, wherein they demonstrated a pneumatic actuator that could be punctured with a 14-gauge needle and continued to function. The molded silicone elastomer actuator

was reinforced with polyaramid fibers (Kevlar) dispersed into the silicone before curing (**Figure 2A**). This composite pneumatic arm was punctured with a needle while under positive pressure and maintained its internal pressure, even after the needle was removed (**Figure 2A**, b–d). Though the reason behind the damage resilience was never fully discovered, the current theory is that the damage resilience stems from a combination of the polyaramid fibers preventing crack propagation (Geethamma et al., 2005) and the silicone's natural tendency to self-adhere when elastically returning to its original molded shape (after removal of the needle). In another recent example, Wallin et al. (2017) developed a self-healing elastomer-based soft robot, wherein UV cure elastomer resins were used to stereolithographically 3D print hydraulic actuators. The 3D printing process trapped liquid resin in the elastomer; when the robot was punctured, the excess resin was able to seal up the holes if given sufficient UV stimulus (such as direct sunlight).

Terryn et al. (2015, 2017a,b) have taken a different approach to resilient pneumatic actuators by shaping self-healing polymers into inflatable chambers. In their early work, they molded a single, thin-walled cube out of a thermally responsive self-healing polymer and demonstrated its inflation capacity, even after catastrophic failure (Terryn et al., 2015). Although the pneumatic cube was made out of a stiff polymer (when compared to elastomers), it deformed with a 40% increase in side-to-side dimension when inflated (**Figure 2B**, a). To test its self-healing, the cube



was inflated with positive pressure until the chamber popped. To enhance the failure of the actuator, the cube was also cut through with a blade before being heated to instigate self-healing (**Figure 2B**). After undergoing this puncture and self-healing cycle, the cube inflated the same way it did before it received any damage (both in force produced and displacement achieved). Most recently, Terryn et al. (2017b) demonstrated that by patterning these cubes adjacent to one other, the extended system could be utilized as a soft robotic bending actuator capable of grasping objects. In another recent work, the researchers utilized this same self-healing material to create a pneumatically actuated artificial muscle that can contract over 10% of its length (Terryn et al., 2017a).

Inflatable actuators have seen initial forays into self-healing and damage resilience, and these initial works open possibilities for future development. For example, self-healing inflatable robots open up possibilities in actuator reconfigurability, as the inflatable actuator material can be cut and rearranged as necessary. To achieve such goals, the limitations of the state-of-the-art must be addressed, from long healing times to a need for an intense source of stimulus for self-healing. Since inflatable actuator systems have yet to show any stimuli-independent healing, it will be particularly important in future research to integrate the self-healing stimulus into the soft actuator.

Hydrogel Actuators

Hydrogels are a type of extremely hydrophilic thermoset polymer matrix that absorb water molecules into the bulk material. By pulling water molecules in between the long polymer chains, a hydrogel's polymer matrix expands, enabling a change in size many times that of the original structure. This diffusion-limited process has been used repeatedly in soft robots as a potential actuation method (Gerlach and Arndt, 2009; Richter, 2009; Kim et al., 2013). Self-healing hydrogels are their own field of research for materials scientists, as can be seen in recent reviews (Phadke et al., 2012; Taylor and Marc in het Panhuis, 2016). Yet, despite this field of research, hydrogel self-healing has yet to enter the soft robotics community, so this section is mostly forward-looking based on presently developed systems.

Responsive hydrogels have not generally been used in actuators (inflatable or otherwise) like silicones and other inert elastomers. Yuk et al. recently broke this trend in their novel application of hydrogels as an inflatable robotic gripper (Yuk et al., 2017). The hydraulic gripper was built with a highly deformable hydrogel that was simultaneously gentle and robust, capable of trapping a live fish without harming it. Highly stretchable, self-healing hydrogels such as the one recently presented by Jeon et al. (2016) could potentially be used to create these types of hydrogel grippers. Their hydrogel can self-heal very quickly (in under 30 s, given ideal conditions) and can strain over 1,000% its original length (**Figure 2C**). Similar work has recently been presented by Liu and Li (2017) whose tough, self-healing hydrogel requires slightly more healing time but is also ionically conductive.

There is much to gain by further exploring self-healing hydrogels in soft robots. For example, by adding hygroscopic ions to the hydrogel, the hydrogel could self-hydrate by pulling water

out of the ambient environment (Bai et al., 2014; Chen et al., 2014), ensuring that the actuator is always ready to self-heal. The high water concentration in hydrogels (when compared with the humidity of the surrounding air) can enable hydrogel polymers to heal much more rapidly than normal self-healing polymers, as demonstrated by Jeon et al. (2016). However, one constant challenge that hydrogels face is ensuring that they remain sufficiently hydrated. Further advantages gained through the use of conductive hydrogels will be discussed briefly in Section "Shape Memory Materials" in the context of self-healing electronics.

SELF-HEALING SOFT ROBOT STRUCTURES

Given the goals of environmental adaptability and large degree-of-freedom operation for soft robots, it is not surprising that structure is of deep interest to soft robotic design (Bar-Cohen and Breazeal, 2003; Mazzolai et al., 2007; Case et al., 2016). Designing with materials that support actuation and sensing is crucial to enable functionality and adaptability in soft robots. Passive structures, material backbones that hold together a series of actuators and sensors, can easily be enhanced by adding self-healing functionality (Ghosh, 2009; Li and Meng, 2015; Huynh et al., 2017). Of particular interest to soft roboticists are stiffness changing materials that enable soft robotic structures to have low stiffness for adaptation or actuation, and high stiffness to increase output forces or provide stability. A recent review covers this topic in more detail in its application to soft robotics (Manti et al., 2016). It is with this idea of structural materials that we continue our investigation of self-healing and damage resilience in soft robotics.

Low Melting Temperature Materials

Materials that have been employed in purely functional structural cases are primarily those that can undergo phase changes at low temperatures, such as low melting point alloys (LMPAs) or wax. This is because the low-temperature phase change alters the material stiffness by many orders of magnitude, with relatively small amounts of energy input. These materials are also ideal for self-healing, since they can change to a liquid form that readily flows to fill cracks, holes, or other damage. Once the system has healed the damage, the materials can be cooled again to restore a continuous solid body.

Low melting point alloys have been used in variable stiffness applications in order to provide a stiffening or morphable element in the robot (Nakai et al., 2002; Shan et al., 2013; Shintake et al., 2015), typically display melting points below 70°C and are solid at room temperature. Dr. Dario Floreano's lab has demonstrated the value of LMPAs as self-healing, variable-stiffness soft robotic components (**Figures 3A,B**) (Schubert and Floreano, 2013). The researchers started by showing that the solid LMPA encapsulated in an elastomer provides structural stiffness until overloaded, causing the metal to crack and break. When this happens, the load is removed, allowing the encapsulating silicone to restore its original shape and pushing the

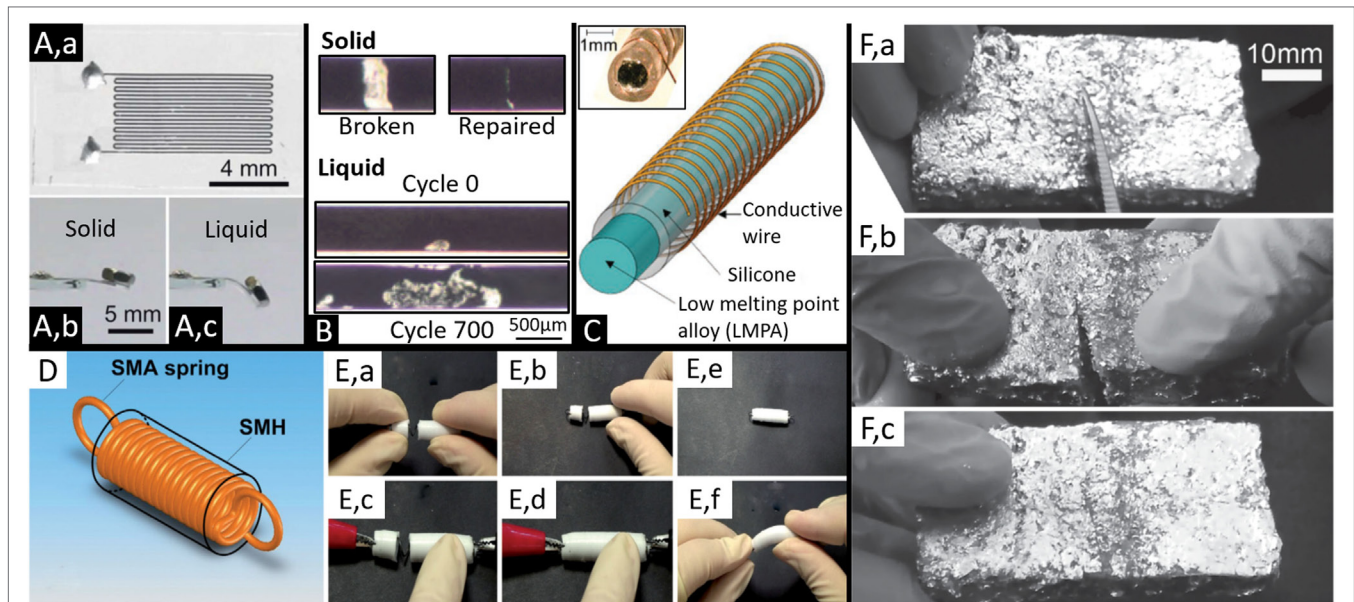


FIGURE 3 | (A) A planar variable stiffness material made of a self-healable low melting point alloy microchannel in silicone. Top view [(A), a] and side views in a stiff [(A), b] and soft [(A), c] state. **(B)** Photographs of a low melting point alloy (LMPA) microchannel that has been fractured then Joule-heated to self-repair, as well as photographs of an LMPA microchannel in a liquid state showing degradation after 700 strain cycles. **(C)** Self-healing variable-stiffness fiber comprised of LMPA in a compressive silicone sleeve, with a cross section photo inset. **(D)** Diagram of self-healing hybrid with shape memory alloy (SMA) coils in a self-healing polymer exterior [labeled as a shape-memory hybrid (SMH)]. **(E)** A Self-healing cycle of the hybrid. Pulling the SMH apart [(E), a,b]; Joule heating the SMA to restore shape and encourage self-healing [(E), c,d]; the SMH after healing [(E), e] and bent to show restoration of material flexibility [(E), f]. **(F)** Self-healing of an LMPA-foam composite. Damaging the LMPA-foam composite with scissors [(F), a], showing the damage [(F), b] and resealing the damage [(F), c]. **(A,B)** Adapted from Schubert and Floreano (2013), © 2013 The Royal Society of Chemistry. **(C)** Adapted from Tonazzini et al. (2016), ©2016 the authors. **(D,E)** Reproduced from Huang et al. (2010) ©2010 Elsevier Ltd. **(F)** Reproduced from Van Meerbeek et al. (2016), ©2016 John Wiley & Sons Inc. All figures are used with permission.

cracked metal together. By Joule-heating the metal, it melts and reforms a continuous structural system (Figure 3B). Though this process breaks down after several hundred cycles (Figure 3B), it is possible to completely replace the damaged LMPA. Later work advanced this concept by sealing LMPA into a silicone tube that was pre-stretched (see Figure 3C) (Tonazzini et al., 2016). The pre-stretched tube added a constant internal compression to the LMPA, improving the self-healing process when compared to a system using the exact same setup and materials without the pre-stretch.

Polyurethane and silicone foams have been previously used as structural elements in soft robotics, as they are usually easy to deform, compress well, and often can sustain large extensions (Shimoga and Goldenberg, 1992; Lipson, 2014; Yuen et al., 2014, 2016). By impregnating porous foams such as these with low-melting point materials, variable stiffness materials are formed. This structure differs significantly from the above examples of encapsulated LMPA, as the low-melting point materials adhere to the foam (even in a liquid state) using capillary forces and wetting adhesion. Van Meerbeek et al. (2016) mixed LMPA into pre-cured silicone to create an open-celled, foam structure (see Figure 3F). Not only does the LMPA provide stiffening to the foam structure but also enables damage repair by welding the foam block back together with the LMPA post damage (Figure 3F, c). Mirroring the use of LMPAs, Cheng et al. (2014) filled a polyurethane foam lattice with wax which they broke repeatedly though over-compression. This foam-wax structure

can self-heal back to nearly full-strength by melting the wax, even after multiple over-compressions. Although not conductive like LMPAs, wax does hold an advantage over LMPA since careful tuning of the molecular structure of the wax will separate out the softening temperature (for physical shape change) from the solid-to-liquid phase change temperature (for self-healing).

Characterization and implementation of soft robotic variable-stiffness, self-healing structures has only just begun. There is much opportunity for research into structural materials that can change shape and heal from mechanical damage by phase changing and reflooding in a soft structure. Finding ways for a soft robotic system to auto-detect damage in a phase-changing structure and initiate the self-repair process is one possible future step that could be taken in this area.

Shape Memory Materials

Shape memory materials are a type of material, including both metallic shape memory alloys (SMAs) and shape memory polymers (SMPs), that can be plastically deformed from a pre-programmed state and self-return to their programmed shape upon controlled heating. SMAs and SMPs are common actuator tools that have been used frequently in soft robotics applications (Ionov, 2011; Albu-Schäffer and Bicchi, 2016; Hou, 2016; Rodrigue et al., 2017), but they have only occasionally been used as variable-stiffness structural materials (Manti et al., 2016). Their ability to autonomously restore form after plastic deformation

parallels the motivations of self-healing and damage resilience as presented thus far. However, since their common use as actuators does not strictly fall into our definition of damage resilience (the plastic deformation is expected during operation), we will not explore this idea further.

With the common use of SMAs and SMPs as actuators, it would not be difficult to implement them as reinforcing structural elements in damage resilient soft robots (Kirkby et al., 2008; Ferreira et al., 2016). Huang et al. (2010) demonstrated the feasibility of this by embedding a coiled SMA wire inside of a semi-flexible, self-healing polymer (**Figures 3D,E**). When the polymer structure was stretched beyond its fracture limit, the SMA coil prevented the two segments from separating completely. After failure of the encapsulating polymer, the SMA wire was Joule heated, simultaneously pressing the two fractured halves of the polymer together and heating them so that they could self-heal, thus restoring the polymer flexibility (see **Figure 3E**, a–f). Xiao et al. (2010) presented a self-healing SMP which could heal its surface after being scratched, which has initiated research into self-healing coatings (Luo and Mather, 2013; Dalmoro et al., 2016; Lutz et al., 2016). SMPs have also been used in two-step self-healing processes where the SMP can close whole cracks using the shape memory effect then self-heal the cracks through internal chemistry (Nji and Li, 2010, 2012; Rodriguez et al., 2011). Such hybrid systems that allow both crack closure and crack healing show much promise, though the biggest challenge will be demonstrating this capacity while simultaneously controlling the soft robot using these same materials. For more details on self-healing and shape memory materials, we highly recommend the first chapter of this book: Li and Meng (2015) or this recent review: Meng and Li (2013).

SELF-HEALING ELECTRONICS FOR SOFT ROBOTICS

For any robot to have closed-loop control, it will require some form of sensory feedback combined with an on-board computer to control its actuation. Toward this goal, sensory skins have been sought by soft roboticists as their flexibility suggest excellent integration of complex electronic components into soft-bodied robots (Lu and Kim, 2014). There is an entire class of materials and devices with numerous arrays of sensors (or even actuators) designed to be either compatible with human skin so that they can adhere to a person (Kim et al., 2011), or be generally stretchable (McCoul et al., 2016). Integration of self-healing into electronics that are both flexible and stretchable is key to a fully controllable, self-healing soft robot.

A simple example of self-healing, flexible electronics comes from over a decade ago when Carlson et al. (2006) demonstrated a flexible sensor skin using standard copper-based electronics encapsulated in a self-healing polymer. The polymer body was thin enough to be flexible, but when cracked by over-bending, it could heal completely. This basic body-healing could not restore damaged electronic components; however, once the metal-based sensor was damaged, the sensor ceased to function. Since then, a recent progress report has highlighted work done in polymer

chemistry and physics to develop self-healing polymers and flexible electronic components, specifically with a focus on wearables applications (Huynh et al., 2017). In it, self-healing polymers find applications in a number of sensory-skin devices such as flexion sensors (D'Elia et al., 2015), strain sensors (Wu and Chen, 2016), capacitors, supercapacitors, batteries, and solar cells (Wang et al., 2013, 2014; Sun et al., 2014, 2016; Banerjee et al., 2015; Huang et al., 2015; Zhao et al., 2016). Even though research into these devices continues, we have yet to see many integrated into soft robotic systems.

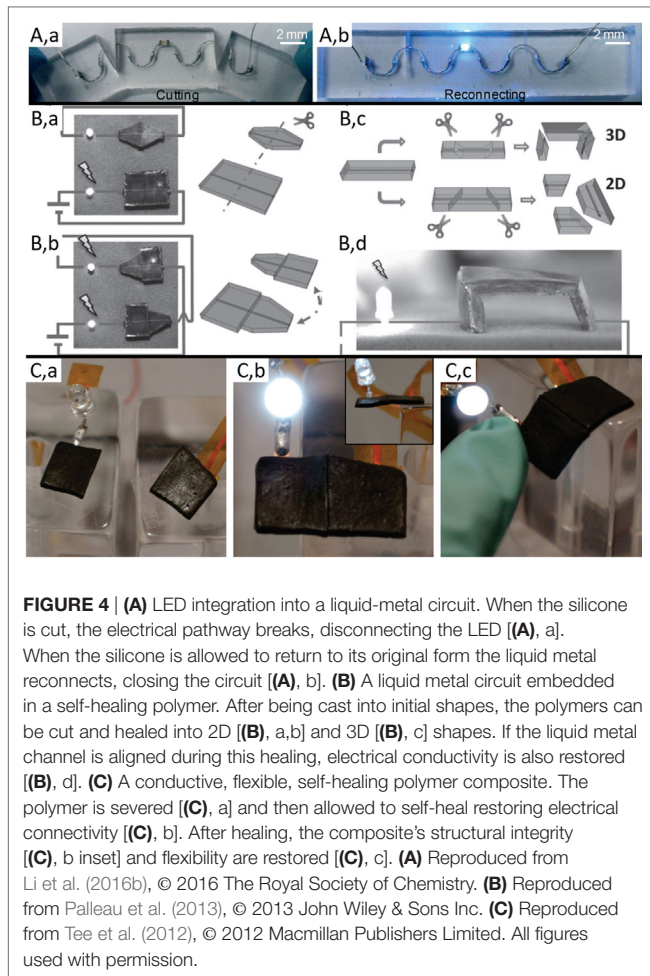
Two different approaches have been taken by researchers to develop fully self-healing, flexible (and sometimes highly stretchable) electronics implementable in soft robotics. The first uses room temperature liquid metals encapsulated in a self-healing structure, and the second uses a composite self-healing bulk polymer mixed with conductive filler.

Room Temperature Liquid Metal-Based Electronics

Gallium-based room temperature liquid metals (eutectic gallium-indium, or eGaIn, and eutectic gallium-indium-tin, or galinstan, alloys) are often used in highly stretchable and flexible soft electronics (Dickey, 2016, 2017). Their unique properties allow for a variety of soft systems to be developed that are not available in solid-metal electronics. First, when encapsulated in channels in a silicone elastomer, the liquid metal flows readily, maintaining continuity as the channel changes geometry due to external extension or compression. Furthermore, when gallium-based liquid metals are exposed to air, the liquid metal forms a stabilizing oxide layer that prevents unwanted flow (Dickey, 2014). These two properties make these alloys ideal for use in damage resilient electronics: the stabilizing oxide prevents the conductive liquid from leaking out any punctures/holes, but the liquid-like behavior allows it to seal circuit breaks.

The effectiveness of room-temperature liquid metals in damage resilient circuitry was recently demonstrated by Li et al. (2016b). In this work, liquid metal channels encapsulated in PDMS silicone were cut and pulled apart, thereby breaking the circuit (**Figure 4A**, a). When released, the material elastically returned to its original form and the liquid metal reconnected the electrical path (**Figure 4A**, b). Palleau et al. (2013) used a self-healing, stretchable polymer as an encapsulating body around a room-temperature liquid metal conductive circuit. This combination was used in both flexible self-healing wires and bulk planar materials with liquid-metal channels. The bulk planar material could mechanically and electrically self-heal after being separated into two parts (**Figure 4B**, a,b). Furthermore, the self-healing enabled reconfigurability in the material, as a 2D electronic pathway could be cut and then reconfigured into a 3D electrically conductive shape (**Figure 4B**, c,d). This powerful demonstration shows separate self-healing mechanisms for the bulk material and the electrical components, and how to combine the two mechanisms to create a fully self-healing system.

Though self-healing electronics based on liquid metals have been demonstrated in their initial forms, we have yet to see integration of these demonstrations into more complex devices.



One potential challenge facing this system is the non-conductive oxide layer that builds up each time the liquid metal is exposed to air (during multiple self-healing events), which results in overall decreasing conductance. However, liquid metal oxidation has also been shown to prevent the liquid metal from leaking during healing events by creating an encapsulating seal at the location of failure (Dickey, 2014). Therefore, while highly advantageous in simple applications, implementation of liquid metal as a self-healing conductor may be limited in applications where stable conductance is necessary, such as resistive sensors.

Composite Polymer Electronics

A second approach to developing fully self-healing electronic systems uses conductive polymer composites formed out of a self-healing polymer matrix and a conductive filler. Appropriate mix ratios can allow for strong electrical conductivity through the bulk material, while maintaining the self-healing properties of the polymer bulk (Tee et al., 2012; Gong et al., 2013). Any cut or puncture in the polymer will self-heal, reconnecting the conductive filler material and rejoining the circuit, much like the material demonstrated by Tee et al. (2012) (Figure 4C). In this work, a polymer composite was demonstrated that could withstand moderate flexing and twisting (withstanding strains of up

to 20%), while also being highly conductive and self-healing. The untreated material can withstand significantly higher strains, but when sufficient conductive filler is added (31% vol) to enable high conductivity (10 S/cm), the material's strain-to-failure is reduced. Alternatively a self-healing elastomer can be coated with a layer of conductive particles, as demonstrated by Cao et al. (2017a). As long as the conductive coating is aligned during the self-healing process, the material regains its conductivity. It is also worth noting that the elastomer presented in this work is able to self-heal in seconds (on the same order of magnitude as hydrogel self-healing, but without the need to be hydrated), which represents a step forward for self-healing elastomeric materials.

Conductive hydrogels that are self-healing at room temperature, robust, and elastically stretchable have begun to emerge in simple composite-polymer sensory applications. A common thread among recent examples is the use of metal ions as a key to both the self-healing chemistry and the conductive element (Darabi et al., 2017; Lei et al., 2017; Liu and Li, 2017; Liu et al., 2017). Though adding metal ions increases the conductivity of the hydrogels, researchers have carefully tuned the concentration: too low and the hydrogel does not conduct, too high and either the flexibility of the hydrogel is reduced or it ceases to self-heal. Cai et al. (2017) took a mixed approach by developing a self-healing, stretchable hydrogel and adding conductive filler (CNTs), much like the composite elastomers previously mentioned. This conductive hydrogel composite can self-heal in 60 s and recover 98% of its electrical conductivity (demonstrated multiple times on the same sample). A third approach to conductivity in self-healing, flexible hydrogels is demonstrated from previous work, wherein the polymer network itself provides the conductivity (Shi et al., 2015).

There are many challenges to overcome as conductive composite soft polymers become more incorporated into damage resilient soft robotic systems. Though the relative electrical stability of many conductive composite polymers has been demonstrated over a few strain cycles, a long-term fatigue cyclic test has yet to prove that these materials do not suffer from electrical drift. The few examples of long-term testing on ionically conductive hydrogels have shown that hydrogel systems can lose water through evaporation during use outside of a solvent environment, and when this happens, their performance drops significantly (Cai et al., 2017). Also, hydrogel composites tend to have higher resistances (greater than 1 k Ω for small samples), limiting their use to mostly strain sensing rather than conductive pathways. For a more comprehensive look at self-healing composite polymers (both bulk composites and conductive composites), readers are referred to these other recent, in-depth reviews/book chapters: Gibson (2010), Benight et al. (2013), Zhu et al. (2014), Ahner et al. (2015), Zhong and Post (2015), Zhang et al. (2017).

FUTURE PROSPECTS AND CHALLENGES

There are many open possibilities for the future of self-healing and damage resilience in soft robotics. Since multifunctional materials that bridge functional partitions drive innovation in the soft robotics field, it is worth pointing out how the

self-healing materials discussed in the previous sections could continue to break down functional barriers. Recently, Cao et al. (2017b) demonstrated the use of high-resistive, ionic, self-healing hydrogels as DEA electrodes, showing how work toward improving self-healing ionic hydrogels is also improving damage resilience in soft robotic actuation. Likewise, DEAs have also been used as sensory components in soft electronics (Iskandarani and Karimi, 2012; Xu et al., 2016), so progress made toward fault-tolerant and self-healing DEAs can also be applied to soft sensors and electronics. Looking to the future, LMPAs could potentially be used in place of room-temperature liquid metals in self-healing soft electronics, thereby adding additional structural function, although simultaneously introducing the need for thermal control. Furthermore, using the mixing techniques already demonstrated in liquid metal-filled silicone foams (Kazem et al., 2017), current self-healing LMPA foams could be enhanced by replacing the non-self-healing silicone elastomer with a self-healing elastomer. These are only a few examples from the large range of applications for self-healing materials that will enhance the innovation capacity in future soft robotic systems.

Though we have presented materials and work already done by researchers in the soft robotics field, along with some of the near-future prospects, there are broad challenges that must be overcome for this field to continue to grow. While self-healing materials are prevalent in the literature, it is not always possible to simply import already-existing materials into the soft robotics community. For example, we discussed the potential of using self-healing elastomers and hydrogels in inflatable actuators (see Inflatable Actuators and Hydrogel Actuators); however, the materials that are currently available for use are not the ideal solution. Current self-healing elastomers tend to rapidly stress-relax (Li et al., 2016a), losing their ability to snap back to their original form. Despite this, immediate application of currently available materials would enable an exploration of how self-healing impacts and improves various facets of soft robotics, leading to clearer material requirements for self-healing elastomers and encouraging research into these materials. Other challenges that must be overcome include determining the nature of interfaces between materials, especially those that may be chemically active and simplifying the synthesis of self-healing materials for bulk applications (i.e., mass-producing these materials to enable ubiquitous implementation).

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Regardless of the challenges being faced, exciting possibilities are on the horizon for self-healing soft robots. For example, DEA rolls and stacks are powerful actuators that are highly susceptible to premature failure from a single manufacturing defect (O'Halloran et al., 2008). Self-healing and self-correcting DEAs would no longer suffer from this fundamental flaw and provide future soft robots with hundreds of hours of high-deformation, high-strength actuation. Recent efforts have shown exciting progress using DEAs to blur the lines between soft robot logic control and actuation (Wilson et al., 2016). Blending actuation and control in fully integrated self-healing soft robotic systems may enable a new form of materials based logic where logic and actuation components can be cut apart and physically reprogrammed without any need for software, similar to other recent developments (Zhang and Soh, 2017). Furthermore, creative applications of materials that restore physical continuity could make soft robotics outperform their biological inspirations. We envision soft robots that can not only self-repair, but also leverage self-healing to enable reconfigurability, whereby parts can be cut apart and reassembled to tune overall function or performance.

In conclusion, the work presented in this review demonstrates the exciting possibilities at the intersection of self-healing materials and soft robotics. We expect that as these research communities continue to intermix, emerging soft robots will have the ability to heal from damage, similarly to their biological inspirations. Further, this confluence of material breakthroughs and novel application will enable the next generation of reconfigurable soft robots with tunable gait, function, and body morphology, all on-demand.

AUTHOR CONTRIBUTIONS

RB and RK conceived of the review topic and wrote the text. RB gathered the citation base for the review. Both agree to be accountable for the content of the work.

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Conflict of Interest Statement: The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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