



# Drag Force for Asymmetrically Grafted Colloids in Polymer Solutions

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We consider the situation in which a colloidal particle modifies locally the solvent leading to a spatially dependent viscosity. This situation is typical for colloidal particles in crowded environment, for example DNA-grafted particles in a polymer solution, or a hot particle which implies a temperature gradient to a viscous liquid. By means of suitable approximations we calculate the dependence of the friction force on the profile of the local viscosity. Our results show that in the case of axially symmetric viscosity profile the friction force is sensitive to the anisotropy of the viscous profile whereas it is not sensitive to for-ahead asymmetries. Our results are crucial for active microrheology measurements where tracer particles are pulled through complex fluids.

Keywords: crowded environments, polymer solution, drag force, anisotropic viscosity, transport phenomena and fluid mechanics, functionalized colloids

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# **1. INTRODUCTION**

Particles in the nanometer size range coated with polymers are of growing importance for rather diverse applications [1]. In hybrid materials such as nanocomposites, the use of polymers grafted to nanoparticles is widely exploit to suppress aggregation of particles and to enhance their dispersion and mixing into solvent or matrix. The nanoparticles coated with DNA are used for building highly sensitive probes or drug carriers in biological systems [2, 3] and to assemble crystals and other structures of numerous morphologies [4].

In the absence of external driving, the transport of nanobjects in the fluid environment is dominated by diffusion, a process due to random molecular motion excited by thermal fluctuations [5–7]. Diffusion of isolated spherical nanoparticle in the simple molecular liquids is well-described by the Fick's law, which says that the mean-square displacement changes linearly in time. The rate of this change, the translational diffusion coefficient  $D_t$ , is related to the macroscopic viscosity of the solvent  $\eta_m$  (as measured rheometer) via Stokes-Sutherland-Einstein (SSE) relation [6, 8];  $D_t = k_B T/\zeta_m$  where  $\zeta_m$  is the hydrodynamic drag coefficient given by the Stokes equation  $\zeta_m = 6\pi \eta_m R$ . In this equation R is the hydrodynamic radius of diffusing particle,  $k_B$  is the Boltzmann constant and T is the temperature.

However, various experiments [9–20] and simulation studies [21–23] show that diffusion of nano-sized particles in complex fluids is not accurately described by Fick's law and that the SSE relation is violated in certain regimes of parameters. For polymer solutions, these parameters involve the size of the particle and the polymer length scales [24, 25]. For example, if the particle size is comparable to or smaller than the characteristic length scale in a polymer solution, its diffusion is significantly faster than the one predicted based on the macroscopic viscosity [13, 17, 18]. This is because on such length scales the nanoparticle does not experience the homogeneous continuum medium with high viscosity, rather, the individual polymer chains or blobs and their fluctuations as well as entanglements influence its dynamics.

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Grafting nanoparticles with macromolecules, such as polymers or DNA, complicates their interactions with the complex medium and, therefore, stronger deviations from the SSE relation are expected. These deviations can be tested in rheological experiments [26] by measuring the drag force. The experiments for a bare (non-grafted) colloid in DNA solutions demonstrated that by using optical tweezers it is possible to move a particle through a highly monodispersed polymer solution at a given velocity as well as to measure the drag force on the colloid with piconewton resolution at the same time [26].

Here we provide a theoretical prediction for a drag force based on the assumption that interactions between grafted particle and the complex medium result in an effective spatially dependent viscosity. A similar idea was used by Tuinier et al. [27], Fan et al. [28, 29], and Feng et al. [30] to calculate the hydrodynamic resistance force for a bare spherical particle in a non-adsorbing polymer solution, where polymer depletion results in a reduced polymer concentration near the particle surface. Using the concept of local viscosity [31], the polymer concentration profile was related to the viscosity profile near a spherical particle. Hydrodynamics was formulated by the modified Stokes equation with non-uniform spherically symmetric viscosity, which was solved by a regular perturbation approximation using the Green function method.

In the present paper, we extend this analysis to account for anisotropic viscosity profile around a spherical particle, which may result from anisotropically grafted nanoparticles in a nonadsorbing polymer solution (see **Figure 1**). Such anisotropically grafted nanoparticles, e.g., DNA-grafted Janus particles can be manufactured [33–35]. They provide a basic structural element that can be used to produce useful nanoparticle clusters of different topologies through DNA-based self-assembly [33–35]. The concept of anisotropic viscosity might also be applicable for describing the transport of protein through the nuclear pore complex, where the transporting protein encounters heterogeneous polymer brush or gel like environment [36–38].

Because the concentration profile of free polymers in the solution depends on the length of grafted macromolecules and on the grafting density [32], an anisotropic grafting changes the depletion zone around the particle, which leads to anisotropic polymer concentration and thus to anisotropic effective viscosity. We assume that the particle is dragged slow enough such that the polymer solution can adiabatically follow the motion of the colloid. This means that the advective transport rate must be smaller than the diffusive transport rate of the polymers, which can be expressed via the Peclét number  $Pe = l_p u/D_p \ll 1$ , where  $l_p$  is the characteristic length scale of the polymer, uthe characteristic velocity of the solvent u, and  $D_p$  diffusivity of the polymers. Further, we assume that the characteristic length scale of the variation of polymer concentration is bigger than the length of an effective statistical chain element. This assures a sufficiently large number of chain elements in small volume element to apply the concept of local viscosity [31]. Solving the modified Stokes equations with a spatial-dependent viscosity of a general form is not easy-even within a regular perturbation approximation. However, for the axisymmetric systems some simplifications occur. For axisymmetric Stokes equations with constant viscosity, translational and rotational motion are decoupled. For translational motion a scalar stream function, which transforms vectorial equations to the scalar ones is well-established. We demonstrate that these properties also hold for the modified Stokes equations with axisymmetric viscosity profile and provide a formalism to calculate the drag force experienced by a translating particle.

Our paper is structured as follows. In section 2, we present the extended Stokes equations with the spatially dependent viscosity and introduce the perturbation calculation scheme. In section 3 the drag force for the axisymmetric systems is calculated and analyzed for various grafting geometries. We conclude in section 5.

## 2. MODEL

#### 2.1. Extended Stokes Equation

The Stokes equations are valid for small Reynolds numbers  $Re = \rho u l / \eta \ll 1$ , where  $\rho$  is the density of the fluid, u is the characteristic velocity of the flow, and l is the characteristic length scale of the particle. This assures that viscous forces dominate the inertial forces. The stationary incompressible Stokes equations with spatially dependent viscosity  $\eta(\mathbf{r})$  are given by

$$\nabla \cdot \boldsymbol{\tau} = 0, \qquad \nabla \cdot \boldsymbol{\nu} = 0, \qquad (1)$$

where  $\tau = -pI + 2\eta(r)\Delta$  the stress tensor, *p* is a pressure and  $\Delta = [\nabla v + (\nabla v)^T]/2$  is the strain rate. The superscript *T* denotes the transposed of a tensor, *I* is the identity matrix. Expanding the divergence in the momentum equation one obtains an additional term, which is proportional to the gradient of the viscosity

$$0 = -\nabla p + \eta (\nabla^2 \boldsymbol{\nu}) + (\nabla \eta) \cdot \left[ \nabla \boldsymbol{\nu} + (\nabla \boldsymbol{\nu})^T \right].$$
 (2)

We consider a quiescent, unbounded fluid which is dragged by a particle with no-slip and vanishing far-field boundary conditions:

$$\mathbf{v} = \mathbf{U} + \mathbf{\Omega} \times (\mathbf{r}_p - \mathbf{r}_c), \qquad \mathbf{r} \in \Sigma_p$$
 (3a)

$$\mathbf{v} \to 0, \quad p \to 0, \qquad |\mathbf{r}| \to \infty.$$
 (3b)

where  $\Sigma_p$  is the particle surface and  $r_p$  is a point on the particle surface  $\Sigma_p$ . The particle is translating with velocity U and rotating with angular velocity  $\Omega$ , which requires a force F and a torque T acting on the particle. The angular motion of the particle is described in a coordinate system fixed to the particle at  $r_c$ .

The drag force on the particle is determined by the force acting on the particle surface  $\Sigma_p$ , which corresponds to the momentum flux through the surface

$$F = \int_{\Sigma_p} \mathrm{dS}\,\boldsymbol{\tau} \cdot \boldsymbol{n}\,,\tag{4}$$

where *n* is the surface normal vector. In the following all quantities are represented in dimensionless units:  $\mathbf{v} \propto U$ ,  $\mathbf{\Omega} \propto U/a$ ,  $\mathbf{\tau} \propto \bar{\eta}U/a$  and  $\mathbf{p} \propto \bar{\eta}U/a$ , where *a* is the particle radius and  $\bar{\eta}$  is the bulk viscosity. Accordingly, the drag force and viscosity are also dimensionless.



## 2.2. Small Viscosity Variations

We consider an expansion of the system in small viscosity perturbations of order  $\mathcal{O}(\epsilon)$ 

$$\eta = 1 + \epsilon \eta_1 + \epsilon^2 \eta_2 + \mathcal{O}(\epsilon^3) \tag{5a}$$

$$\mathbf{v} = \mathbf{v}_0 + \epsilon \mathbf{v}_1 + \epsilon^2 \mathbf{v}_2 + \mathcal{O}(\epsilon^3) \tag{5b}$$

$$p = p_0 + \epsilon p_1 + \epsilon^2 p_2 + \mathcal{O}(\epsilon^3).$$
(5c)

The fluid velocity at the surface of the particle is determined by the leading order velocity field  $v_0$ . Thus, the higher order fluid velocity fields at the surface must vanish. The far-field condition of the quiescent fluid requires that both the pressure and the velocity fields have to vanish at infinity.

We expand the stationary Stokes equations in small viscosity variations of order  $\epsilon$ . The leading order system  $\mathcal{O}(\epsilon^0)$  is given by

$$-\nabla p_0 + \nabla^2 \boldsymbol{v}_0 = 0, \qquad 0 = \nabla \cdot \boldsymbol{v}_0 \tag{6a}$$

$$\mathbf{v}_0 = \mathbf{U} + \mathbf{\Omega} \times (\mathbf{r}_p - \mathbf{r}_c), \qquad \mathbf{r} \in \Sigma_p$$
 (6b)

$$\mathbf{v}_0, \, p_0 \to 0 \,, \qquad |\mathbf{r}| \to \infty \tag{6c}$$

and the first order system  $\mathcal{O}(\epsilon^1)$ 

$$-\nabla p_1 + \nabla^2 \boldsymbol{v}_1 = -\eta_1 \nabla^2 \boldsymbol{v}_0 + \nabla \eta_1 \cdot \left[ \nabla \boldsymbol{v}_0 + (\nabla \boldsymbol{v}_0)^T \right] \quad (7a)$$

$$0 = \nabla \cdot \boldsymbol{v}_1 \tag{7b}$$

$$\boldsymbol{v}_1 = 0, \ \boldsymbol{r} \in \Sigma_p$$
 (7c)

$$\mathbf{v}_1, \, p_1 \to 0, \, |\mathbf{r}| \to \infty$$
 (7d)

The leading order solutions fulfill common Stokes equations with constant viscosity.

## 3. AXISYMMETRIC SYSTEMS

Axisymmetric systems possess at least one axis of rotational symmetry, which we choose to be parallel to  $e_z$ . We use spherical coordinates  $\{r, \theta, \phi\}$  with the corresponding orthonormal basis  $\{\hat{r}, e_{\theta}, e_{\phi}\}$  and the origin located at the center of the particle. Due to the rotational symmetry the system is independent of the azimuthal angle  $\phi$ . Thus, the viscosity  $\eta(r, \theta)$  is a function of radial distance r and the polar angle  $\theta$ . Accordingly, the  $\hat{r}$ - and  $e_{\theta}$ -components of the extended Stokes equations Equation (1) depend on the components  $v_r$  and  $v_{\theta}$  of the fluid velocity, whereas

the  $e_{\phi}$ -component of Equation (1) depends only on  $v_{\phi}$ . The velocity field of the fluid for translational motion of the particle  $U \parallel e_z$  is determined by  $\{v_r, v_{\theta}\}$  and for rotational motion  $\Omega \parallel e_z$  is determined by  $v_{\phi}$ . These properties are summarized in **Figure 2**.

For axisymmetric Stokes equations translational and rotational motion are decoupled. For translational motion a scalar stream function formalism is well-established to simplify the vectorial equation to a scalar one (see, e.g., Happel and Brenner [39]). This formalism can be extended to a non-uniform viscosity as long as it is axisymmetric (see **Appendix A**). In the following we focus on translational motion of a particle in an axisymmetric system which is characterized by the particle velocity U.

## 3.1. Leading Order Solution

The leading order axisymmetric momentum equation [see (A5) in the **Appendix A**] is the same as for the homogeneous system. So the stream function (see Equation A1) for the leading order system is [39]

$$\psi_0(r,\theta) = \frac{1}{4}r^2\sin^2\theta \left[\left(\frac{1}{r}\right)^3 - \frac{3}{r}\right].$$
 (8)

The corresponding velocity field is given by

$$\nu_{r0} = \cos\theta \left[\frac{3}{2r} - \frac{1}{2}\left(\frac{1}{r}\right)^3\right]$$
(9a)

$$v_{\theta 0} = -\sin\theta \left[\frac{3}{4r} + \frac{1}{4}\left(\frac{1}{r}\right)^3\right].$$
 (9b)

As expected, the leading order decay of the velocity is  $\propto 1/r$ . The pressure is determined by integration

$$\nabla p_0 = \nabla^2 v_0$$
,  $\Rightarrow p_0(r, \theta) = \frac{3}{2} \frac{\cos \theta}{r^2}$ 

## 3.2. First Order Solution

For the first order velocity field we use Equations (B3) (see **Appendix B**), which correspond to the stream function ansatz (B2). In order to determine the first order pressure contribution



**FIGURE 2** | Short summary of the decoupling of translational and rotational motion of the extended Stokes equations for an axisymmetric system. The velocity field of the fluid for translational motion of the particle  $U \parallel e_z$  is determined by  $\{v_r, v_\theta\}$  and for rotational motion  $\Omega \parallel e_z$  is determined by  $v_\phi$ .

 $p_1(r = 1, \theta)$  at the particle surface, we exploit the  $e_{\theta}$ -component of the stationary Stokes equation

$$\nabla \cdot \boldsymbol{\tau}_{|\boldsymbol{e}_{\theta}} = 0 \quad \Rightarrow \quad \frac{1}{r} \frac{\partial p}{\partial \theta} = \nabla \cdot \left( \eta(r=1,\theta) [\nabla \boldsymbol{\nu} + (\nabla \boldsymbol{\nu})^{T}] \right)_{|\boldsymbol{e}_{\theta}}.$$
(10)

Using the stream function relations for  $v_0$  (9) and  $v_1$  (B3) we integrate over  $\theta$  to obtain the pressure at the surface r = 1

$$p_{1}(r=1,\theta) = \sum_{n\geq 3} f_{n}^{(3)}(r=1) \int \frac{\mathscr{I}_{n}}{\sin\theta} d\theta - \frac{1}{2} f_{2}^{(3)}(r=1) \cos\theta$$
$$-\frac{3}{2} \int \left(\eta_{1}(r=1,\theta) - \frac{\partial\eta_{1}(r,\theta)}{\partial r}\right)_{r=1} \sin\theta d\theta + c(r).$$
(11)

The integration constant c(r) does not contribute to the drag force. Here, superscript (*i*) defines the *ith* derivative.

#### 3.3. Drag Force

The drag force on the particle is calculated by integrating the stress tensor over the particle surface (see Equation 4). First, we derive an expression for the forces  $f_s(r, \theta)$  at the particle surface r = 1

$$f_{s}(r=1,\theta) = \boldsymbol{\tau} \cdot \hat{\boldsymbol{r}} = -p\,\hat{\boldsymbol{r}} + 2\,\eta(r=1,\theta)\,\boldsymbol{\Delta}\cdot\hat{\boldsymbol{r}} \qquad (12)$$

( $\hat{r}$  is a vector normal to the surface denoted in Equation 4 by  $\boldsymbol{n}$ ). Up to the first order, the surface force can be expressed as  $f_s = f_{s0} + \epsilon f_{s1}$ . Using solutions for zero and first order velocities and pressures derived above, we find

$$f_{s} \mid_{\hat{r}} = f_{0s} \mid_{\hat{r}} -\epsilon \left\{ \underbrace{\sum_{n \ge 3}^{\text{vanish under surface integration}}}_{n \ge 3} f_{n}^{(3)}(r=1) \int \frac{\mathscr{I}_{n}}{\sin \theta} d\theta + \frac{1}{2} f_{2}^{(3)}(r=1) \cos \theta \right\}$$

$$+ \frac{3}{2} \int \left( \eta_1(r=1,\theta) - \frac{\partial \eta_1(r,\theta)}{\partial r} |_{r=1} \right) \sin \theta d\theta \bigg\}$$
(13a)

vanish under surface integration

$$f_{s}|_{e_{\theta}} = f_{0s}|_{e_{\theta}} + \epsilon \Big\{ \sum_{n \ge 3} f_{n}^{(2)}(r=1) \frac{\mathscr{I}_{n}}{\sin \theta} \\ + \frac{1}{2} f_{2}^{(2)}(r=1) \sin \theta + \frac{3}{2} \eta_{1}(r=1,\theta) \sin \theta \Big\}.$$
(13b)

In the leading order,  $f_{s0} |_{\hat{r}} = -3/2 \cos \theta$  and  $f_{0s} |_{e_{\theta}} = 3/2 \sin \theta$ . It turns out that the orthogonal component  $f_s \cdot \hat{r}$  of the surface force is determined by the pressure whereas the tangential component  $f_s \cdot e_{\theta}$  is determined by the shear force contribution.

The last step to calculate the drag force F is to integrate the surface forces over the whole surface of the particle  $F = \int_{\Sigma_p} dS f_s$ . Due to the symmetry of the system the drag force is aligned parallel to the symmetry axis  $e_z$ . The resolved part of the surface force  $f_s$  in  $e_z$  direction is obtained by using  $e_z = \hat{r} \cos \theta$  and  $e_z = -e_\theta \sin \theta$ . Performing partial integration and applying the orthogonality of Gegenbauer functions (C2) as well as relation (C3) (see **Appendix C**) the drag force can be expressed as

$$\Rightarrow \qquad F_z = -6\pi + \epsilon 2\pi \left\{ \frac{f_2^{(3)}(r=1)}{3}$$
(14a)  
$$-\frac{3}{4} \int_0^\theta \left( \eta_1(r=1,\theta) - \frac{\partial \eta_1(r,\theta)}{\partial r} \Big|_{r=1} \right) \sin^3 \theta d\theta$$
(14b)  
$$+ \epsilon 2\pi \left\{ -\frac{2f_2^{(2)}(r=1)}{3} - \frac{3}{2} \int_0^\pi \eta_1(r=1,\theta) \sin^3 \theta d\theta \right\}$$

The first line (14a) is the leading order drag force corresponding to a sphere and a homogeneous viscosity. The negative sign shows

that the force is opposite to the particle moving direction. It turns out that in the leading order, the pressure contributes 1/3 and the shear force 2/3 of the total drag force. The last two lines (14b) and (14c), give the first order correction to the drag force. The contribution of the first order pressure at the surface is shown in line (14b) and the first order shear force contribution is shown in line (14c). Equation (13) implies that only the second Gegenbauer coefficient  $f_2$  is needed to calculate the first order drag force. A general solution for  $f_2$  can be provided by the Green function of the ODE (14) with n = 2, which has a form

$$\left(\frac{\partial^4}{\partial r^4} - \frac{4}{r^2}\frac{\partial^2}{\partial r^2} + \frac{8}{r^3}\frac{\partial}{\partial r} - \frac{12}{r^4} + \frac{4}{r^4}\right)f_2(r) = R_2(r).$$
(15)

For a sphere in an unbounded quiescent fluid with vanishing velocity at the sphere surface, this Green function has been calculated by Tuinier et al. [28]:

$$G_{1}(r,r') = \left(\frac{-r'^{4}}{30r} + \frac{r}{6}r'^{2} + \frac{1}{12}\left(\frac{r'}{r} + \frac{r}{r'}\right) - \frac{r}{4}r' - \frac{1}{20rr'}\right), \ 1 < r' < r$$

$$G_{2}(r,r') = \left(\frac{-r^{4}}{30r'} + \frac{r'}{6}r^{2} + \frac{1}{12}\left(\frac{r}{r'} + \frac{r'}{r}\right) - \frac{r'r}{4} - \frac{1}{20r'r}\right), \ r < r' < \infty.$$
(16)

The coefficient  $f_2$  is obtained via integration of the Green function and the second Gegenbauer mode of the inhomogeneity  $R_2(r)$ 

$$f_2(r) = \int_1^r G_1(r, r') R_2(r') dr' + \int_r^\infty G_2(r, r') R_2(r') dr'.$$
 (17)

It satisfies the following boundary conditions: at the sphere surface  $f_2(r = 1) = 0$ ,  $f_2^{(1)}(r = 1) = 0$ , and in farfield  $\lim_{r\to\infty} : f_2(r)/r^2 = 0$ ,  $f_2^{(1)}(r)/r = 0$ . All integrands in (17) are smooth functions, therefore, even if for a given *r*-dependence of the viscosity an analytical solution does not exist, the integrals can be easily calculated using the standard quadrature method. For the first order drag force, also the derivatives  $f^{(2)}(r = 1)$  and  $f^{(3)}(r = 1)$  at the surface of the sphere are needed. Considering the Leibnitz rule and the continuity of the given Green function up to the second derivative, the derivatives of  $f_2$  at the surface are

$$\lim_{r \to 1} f_2^{(k)}(r) = \int_1^\infty G_2^{(k)}(r=1,r') R_2(r') \mathrm{d}r'$$
(18)

$$G_2^{(3)}(r=1,r') = -\frac{1}{2r'} - \frac{r'}{2}, \quad G_2^{(2)}(r=1,r') = -\frac{1}{2r'} + \frac{r'}{2}$$

#### 3.3.1. Multipol Representation

In order to proceed, we represent the first order viscosity variation in Equation (5a) as a multipole expansion with r-dependent coefficients

$$\eta_1(\mathbf{r}) = m(\mathbf{r}) + d(\mathbf{r}) \cdot \hat{\mathbf{r}} + Q(\mathbf{r}) : \frac{3\hat{\mathbf{r}}\hat{\mathbf{r}} - \mathbf{I}}{2} + \dots$$
 (19)

In the above, the symbol ":" denotes the double dot product. The projections of the viscosity variation are: the monopole  $m(r) = \frac{1}{4\pi} \int \sin\theta d\theta d\phi \eta_1(r)$ , the dipole  $d(r) = \frac{3}{4\pi} \int \sin\theta d\theta d\phi \hat{r}\eta_1(r)$  and the quadrupole  $Q(r) = \frac{5}{8\pi} \int \sin\theta d\theta d\phi \eta_1(r)(3\hat{r}\hat{r} - I)$ . The quadrupole matrix Q is traceless and symmetric by definition. It follows that the second Gegenbauer coefficient  $R_2(r)$  of the inhomogeneity  $h_1(r,\theta)$  in Equation (B4) depends on the monopole and quadrupole contributions to the axisymmetric viscosity but does not depend on the dipole contribution. Thus, for the total drag force F one has

$$F_{z} = -6\pi \left\{ 1 + \epsilon \left[ \frac{1}{2} m(r=1) - \frac{1}{6} m^{(1)}(r=1) \right] - \frac{\epsilon}{6} \left[ Q_{33}(r=1) - Q_{33}^{(1)}(r=1) \right] + \frac{\epsilon}{12} \int_{1}^{\infty} dr' \mathscr{G}(r') \left[ -r' \left( 1 + 3r'^{2} \right) m^{(1)}(r') + r'^{2} Q_{33}^{(2)}(r') \right] + \frac{\epsilon}{12} \int_{1}^{\infty} dr' \mathscr{G}(r') \left[ r' \left( 1 + 3r'^{2} \right) Q_{33}^{(1)}(r') - r'^{2} Q_{33}^{(2)}(r') - 18Q_{33}(r') + 9r'(1 - r'^{2}) Q_{33}^{(1)}(r') \right] \right\}.$$
(20)

In the above

$$\mathscr{G}(r') \equiv \left(\frac{1}{r'^6} - \frac{3}{r'^4}\right), \quad \int_1^\infty \mathrm{d}r' \mathscr{G}(r') = -\frac{4}{5}$$

This result includes the solution of Tuinier et al. [28] for isotropic viscosity variations  $\eta_1(r)$ .

#### 4. ANALYSIS

We start the analysis of our result for the drag force with the general case of viscosity variations that decay beyond a certain length scale. The decay of viscosity variations is expected because the overall polymer concentration profile approaches its bulk value sufficiently far away from the grafted particle. Specifically, we assume that each multipole mode n of  $\eta_1$  decays beyond the (possibly different) length scale  $d_n$ . Since merely the first three multipoles are relevant, we have

$$m(r) = Z_0(r; d_0) \cdot m \tag{21}$$

$$\boldsymbol{d}(r) = Z_1(r; d_1) \cdot \boldsymbol{d} \tag{22}$$

$$\mathbf{Q}(r) = Z_2(r; d_2) \cdot \mathbf{Q} \,. \tag{23}$$

In order to grasp the basics of the role of the viscosity profile on the drag force on the colloid, we follow Tuinier and Taniguchi [31] and consider the decay profile of the following functional form:

$$Z_n(r; d_n) = 1 - \tanh^2\left(\frac{r-1}{d_n}\right) , \qquad (24)$$

with the properties  $Z_n(r = 1; d_n) = 1$ ,  $Z_n^{(1)}(r = 1; d_n) = 0$ , and  $\lim_{r \to \infty} Z_n(r; d_n) = 0$ . An example of the decay profile is shown in **Figure 3** for different values of *d*.



The drag force can be represented in terms of an isotropic viscosity contribution  $\epsilon m \alpha_i(d)$  and the anisotropic viscosity contributions  $\epsilon Q_{33} \alpha_a(d)$  as follows:

$$\frac{F_z}{-6\pi} = 1 + \epsilon \Big[ m \,\alpha_i(d_0) + Q_{33} \,\alpha_a(d_2) \Big]$$
(25)

with

$$\alpha_{i}(d) = \frac{1}{2} + \frac{1}{12} \int_{1}^{\infty} dr' \mathscr{G}(r') \Big[ -r' \left(1 + 3r'^{2}\right) Z_{0}^{(1)}(r', d) \quad (26)$$
$$+ r'^{2} Z_{0}^{(2)}(r', d) \Big]$$
$$\alpha_{a}(d) = -\frac{1}{6} + \frac{1}{12} \int_{1}^{\infty} dr' \mathscr{G}(r') \Big[ r' \left(10 - 6r'^{2}\right) Z_{2}^{(1)}(r', d) \quad (27)$$
$$- r'^{2} Z_{2}^{(1)}(r', d) - 18 Z_{2}(r', d) \Big].$$

In **Figure 4** we plot the forces  $\alpha_i$  and  $\alpha_a$  as function of the decay length  $d \in [10^{-3}, 10^3]$ . As expected, for variations very quickly decaying with the distance from the sphere, i.e., for  $(d \ll 1)$ , both functions vanish and the drag force is similar to a particle in a homogeneous solution. Thus, in this limit the viscosity variation is negligible. On the other hand, in the limit of very slow decays  $(d \gg 1)$ 

$$\lim_{d \to \infty} \alpha_i = 1 , \quad \lim_{d \to \infty} \alpha_a = \frac{7}{25}$$
(28)

the solution correspond to the case of viscosity variations that depend only on the angle  $\theta$ .

In between there is a transition region from short length scales to long length scales. The isotropic viscosity variation is the main contribution to the drag force. The contribution from the anisotropic viscosity variation is weaker. At  $d \approx 1$  the anisotropic contribution becomes negligibly small because  $\alpha_a$  shows a zero crossing in that region. Thus, up to the first order the drag force is independent of anisotropic viscosity variations that decay on the length scale of the particle. In order to get a better understanding



of the zero crossing we look at the specific quadrupole like viscosity variation  $\mathbf{Q} = [(-1, 0, 0), (0, -1, 0), (0, 0, 2)]/2$ , which is shown in **Figure 5** for  $d_2 \in \{0.3, 7\}$ . This specific viscosity variation does not change the net viscosity. The viscosity in front and at the back of the particle is increased whereas at the waist it is decreased. The corresponding drag force is increased for  $d_2 > 1$  and decreased for  $d_2 < 1$ . In a more general context this indicates that higher viscosity at the back and front of a particle leads to larger drag force if the viscosity variation decays on a longer length scale compared to the length scale of the particle.

#### 4.1. Analysis of the Velocity Mode v<sub>d</sub>

Our formalism allows us to analyze how the velocity field adapts to modulations in the local viscosity. In the following we focus on the dependence of the local velocity field on the local viscosity for anisotropic viscosity profiles (isotropic profiles have been analyzed in Fan et al. [28]). In this case only the quadrupolar component of the viscosity profile (with magnitude given by  $Q_{33} = l_2$ , where  $l_2$  is the coefficient of the projection of  $\eta_1$  on the second Legendre mode<sup>1</sup>) affects the translational friction, thus we study the velocity field variations which are related to those viscosity variations and call them  $\mathbf{v}_d \propto \epsilon l_2$ .

In **Figure** 7 we show the velocity field variation  $v_d$  (calculated using Equation 16) for different decay length of the quadrupolar contribution  $d_2 \in \{0.1, 1, 8, 20\}$  (in units of  $\epsilon l_2$ ). For each decay  $d_2$  two figures are shown. The semi-logarithmic plot gives information about the long ranged velocity field  $v_{dz}$  along the lines  $\theta = 0$  and  $\theta = \pi/2$  whereas the vector-density-plot indicates the absolute value of the velocity component  $|v_d|$  and the arrows give additional information about the direction of the velocity variation. For comparison the leading order velocity field is shown in **Figure 6**.

<sup>&</sup>lt;sup>1</sup>A function *f* defined on the interval [-1,1] can be represented in Legendre's polynomials  $f(x) = \sum_{n\geq 0} l_n P_n(x)$ . The coefficients  $l_n$  are the projections onto the corresponding Legendre's mode  $\frac{2n+1}{2}\langle f | P_n \rangle_P = l_n$ .



**FIGURE 5** | Axisymmetric, quadrupolar viscosity variation  $\mathbf{Q} = [(-1, 0, 0), (0, -1, 0), (0, 0, 2)]/2$  around a spherical particle with length scale decay (A)  $d_2 = 0.3$  and (B)  $d_2 = 7$ .



sphere in the middle of the plot and it is moving to the right parallel to  $e_z$ .

In the semi-logarithmic plot we see the algebraic decay of the velocity field and at the surface r = 1 the dimensionless velocity of the particle  $\nu \propto 1$ . Thus, a positive sign in the semilogarithmic plot as well as arrows with positive z-component corresponds to an increase of the velocity field. On the other hand, a negative sign in the semi-logarithmic plot as well as arrows with negative z-component corresponds to a decrease of the velocity field. For short ranged viscosity variations  $d_2 \lesssim 1$  the semi-logarithmic plot is negative as shown in the top right panel of Figure 7. Thus, the velocity variation decreases the velocity field. For viscosity variations of the particle length scale  $d_2 \approx$ 1 (middle left panel of Figure 7) the semi-logarithmic plot is mainly positive except close to the particle surface. Hence, the velocity variation increases the velocity field. This property is maintained in the far-field for long ranged viscosity variations. Finally, in the bottom right panel of Figure 7 the vector-densityplot shows two velocity regions which are separated by a crossover area (blue area) with very small velocity variations. The first region is close to the particle surface. Here the fluid velocity is reduced compared to the homogeneous case. The second region is outside the crossover area and increases the velocity field. With increasing length scale of the viscosity variation *d* the layers get stretched.

## 4.2. Janus and Quadrupole Particles

We consider a spherical particle that is anisotropically grafted with polymer chains in a polymer suspension. The grafted polymers induce an anisotropic depletion zone of suspended polymers whose width is controlled by the mutual interaction between the grafted and suspended polymers. In the following we assume that the motion of the particle occurs on time scales  $\tau_{\text{particle}}$  that are much larger than the relaxation time of the polymers ( $\tau_{\text{particle}} \gg \tau_{\text{polymer}}$ ), i.e., the Peclét number  $Pe = l_p u/D_p \ll 1$ .

Under these conditions the semi empirical Martin Equation [40] can be used to relate the local polymer concentration to a local viscosity:

$$\eta_p / \eta_s = 1 + [\eta] c_b \rho(\mathbf{r}) \, \mathrm{e}^{k_H[\eta] c_b \rho(\mathbf{r})} \,. \tag{29}$$

where  $\rho$  is the dimensionless, normalized total polymer (i.e., grafted plus suspended polymers) concentration profile,  $\eta_s$  is the viscosity of the solvent,  $k_H$  is the Huggins coefficient, which is specific for a given polymer-solvent combination. The intrinsic viscosity  $[\eta]$  is approximately the inverse of the polymer overlap concentration  $1/c_b^*$  in the bulk, which corresponds to the hydrodynamic volume of a polymer chain in solution per unit



**FIGURE 7** | Velocity profiles. The velocity field variation  $v_d$  is shown for different decays of the viscosity variation  $d_2 \in \{0.1, 1, 8\}$  top to bottom, respectively. Each velocity field is shown in two plots. The first one is a semi-logarithmic plot which gives information about the long ranged velocity field  $v_{dz}$  decay parallel to the symmetry axis. Therefore we calculated  $v_{dz}$  along the lines  $\theta = 0$  and  $\theta = \pi/2$ . The second one is a vector-density-plot which indicates the absolute value of  $|v_d|$  and the arrows give additional information about the direction of the velocity variation. The particle is denoted by the white sphere in the middle of the plot and it is moving to the right parallel to  $e_z$ .

mass. We expand the Martin equation for small variations of the polymer concentration profile  $c_b\rho(\mathbf{r})$ , which is in the dilute regime  $\epsilon = c_b[\eta] \ll 1$ 

$$\eta_p/\eta_s = 1 + \epsilon \rho(\mathbf{r}) + \epsilon^2 k_H \,\rho(\mathbf{r})^2 \,. \tag{30}$$

We identify  $\eta_1 = \rho$ .

Now, we discuss the following (physically realizable) grafting geometries [33–35]:

- **isotropic:** bare particle index '*i*';
- dipolar grafting: a Janus like particle index 'j';
- quadrupolar grafting two cases
  - dominant length scale at back and front index 'q';
  - dominant length scale at the waist index  $'q'_2$ ;

which are defined by the following concentration profiles

$$\rho_i = R(r, d) \tag{31}$$

$$\rho_{j} = \frac{\left(R(r, d_{1}) + R(r, d)\right)}{2} + \frac{\left(R(r, d) - R(r, d_{1})\right)}{2}\cos\theta \qquad (32)$$

$$\rho_q = \frac{\left(R(r,d_1) + R(r,d)\right)}{2} + \frac{R(r,d) - R(r,d_1)}{2} (3\cos^2\theta - 1)/2$$
(33)

$$\rho_{q2} = \frac{\left(R(r,d_1) + R(r,d)\right)}{2} + \frac{R(r,d_1) - R(r,d)}{2} (3\cos^2\theta - 1)/2.$$
(34)

The lowest monopoles of the viscosity corresponding to these concentration profiles are:

$$m_i(r) = R(r, d) \tag{35}$$

$$m_{j,q}(r) = \frac{\left(R(r,d_1) + R(r,d)\right)}{2}$$
(36)

$$d_j(r) = \frac{R(r,d) - R(r,d_1)}{2} \cdot d$$
 (37)

$$\mathbf{Q}_{q}(r) = \frac{R(r,d) - R(r,d_{1})}{2} \cdot \mathbf{Q}$$
(38)

$$Q_{q2}(r) = \frac{R(r, d_1) - R(r, d)}{2} \cdot Q.$$
(39)

We assume that near a surface of the bare particle polymers are depleted, which corresponds to the polymer concentration profile [41]

$$R(r,d) = \tanh^2\left(\frac{r-1}{d}\right).$$
(40)

The polymer concentration profile  $\rho_j$  next to a Janus like colloidal particle is shown in **Figure 8A**. The polymer concentration profile for the two cases  $\rho_q$ ,  $\rho_{q2}$  of quadrupolar grafting are shown in **Figures 8A**,**C**.

We calculate the drag force for different length scales  $d \in [0.01, 50]$  of the depletion zone at the grafted sides and compare it to the isotropic case. The length scale of the depletion zone at one hemisphere of the dipolar grafted particle, the waist of the quadrupolar back-front grafted particle 'q' as well as the back and front of the waist grafted particle  $('q'_2)$  are fixed at  $d_1 = 1$  or at  $d_1 = 0.01$ .

The results for the first order correction to the drag force  $F_{z,1} = (F_z - 1)/(-6\pi)$  (in units of  $\epsilon$ ) are shown in **Figure 9** for two cases: (1)  $d_1 = 1$  and (2)  $d_1 = 0.01$ . One can see that for all cases  $F_{z,1}$  is positive, i.e., the total drag force always increase, and that the first order correction decays monotonically upon increasing the decay length *d*. Because the dipolar part of the axisymmetric viscosity variations does not contribute to the first order correction to the drag force, for the Janus like grafting  $F_{z,1}$  is determined by the monopol part (36). For the quadrupolar grafting both monopol and quadrupole viscosity variations contribute to  $F_{z,1}$ . By the choice of the polymer concentration profiles, at  $d_1 = d$  the drag force  $F_{z,1}$  for all cases of grafted particles equals the one for the bare particle. If  $d_1 < d$ , i.e., when the grafting induce a larger depletion zone, the first order correction to the drag force is

smaller than that for a bare particle. If  $d_1$  or d are <1,  $F_{z,1}$  is almost the same for all three cases of grafting. For  $d > d_1$ , the back-front grafting leads to a weaker  $F_{z,1}$  than the waist grafting.

#### **5. CONCLUSIONS**

We have characterized the friction force of colloidal particles dragged across a fluid that show an inhomogeneous and anisotropic viscosity profile. We have derived closed formulas for both the drag force as well as for the velocity profile. In order to rationalize our results we have expressed the local viscosity profile in terms of its multipole expansion. As expected, we found that the drag force is sensitive to the amplitude of the monopole, i.e., the drag force increases upon increasing the average viscosity. Interestingly, higher order multipoles have quite different roles. In fact, our results show that the drag force is insensitive to the amplitude of the dipole, i.e., for a fore-and-aft asymmetric particle pulling it back and forwards leads to the same drag force. In contrast, the drag force is sensitive to the amplitude of the quadrupole. In particular, we found that a proper choice of the quadrupole orientation (i.e., with higher viscosity on the waist and lower on the axis of motion) with a long decay,  $d \gg 1$  leads to a net reduction of the drag force. We emphasize that such a reduction occurs with "fixed" average viscosity, i.e., at fixed monopole contribution. Hence this is a genuine effect of the anisotropic viscosity distribution and cannot be reduced to a simple reduction of the average drag. Moreover, the sign of this contribution can be switched by changing either the sign of the quadrupole, i.e., moving the higher viscosity from the waist of the particle to the axis of motion, or by reducing the decay length,  $d \ll 1$ .

We have analyzed the cases of physically plausible grafting shown in **Figure 7** in more detail. Interestingly, we found that the net drag force can be controlled by tuning the relative magnitude of the monopole and quadrupole contribution to the density of the grafted polymers (see **Figure 8**). In particular, our results show that for the Janus grafting the anisotropic grafting can both reduce and enhance the drag force as compared to the isotropic case. In contrast, for the







case of back-front grafting the net effect of the anisotropic contribution is to enhance the drag force as compared to the isotropic case.

Concerning the velocity profile, we have shown that the inhomogeneous and anisotropic viscosity profile induces quite involved modulations in the velocity field. Interestingly, the modulations of the velocity profile can oppose t the main flow. Due to our perturbation approach, the magnitude of these modulations are tiny. In this perspective, our results are pinpointing the relevance of the modulations in the viscosity that, possibly, may persist also for stronger variations of the viscosity. We have truncated our expansion at first order since, typically, this is also the leading order when the perturbation parameter is small. Indeed this is the case for monopole and quadrupole contributions to the density of grafted polymers. Interestingly, dipole contributions to the density distribution, at linear order, do not affect the effective friction. Therefore, for the dipolar contribution a higher order expansion is required. Since this quadratic contribution is relevant only when the monopole and quadrupole are vanishing small, we have decided to disregard this contribution in the present manuscript and to focus on the leading contributions, namely monopole and quadrupole. We plan to investigate higher order contribution (and hence also dipole ones) in forthcoming works. Results of

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Fan et al. [28] suggest that they may be relevant for variations at short length scales.

# DATA AVAILABILITY

The datasets generated for this study are available on request to the corresponding author.

# **AUTHOR CONTRIBUTIONS**

MW, PM, and AM contributed conception and design of the study. MW wrote the first draft. AM rewrote several sections. All authors contributed to manuscript revision.

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# SUPPLEMENTARY MATERIAL

The Supplementary Material for this article can be found online at: https://www.frontiersin.org/articles/10.3389/fphy. 2019.00122/full#supplementary-material

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**Conflict of Interest Statement:** The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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