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Robust optimal power flow considering uncertainty in wind power probability distribution

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This paper proposes an optimal power flow model that takes into account the uncertainty in the probability distribution of wind power. The model can schedule controllable generators under any possible distribution of wind power to ensure the safe and economic operation of the system. Firstly, considering the incompleteness of historical wind power data, the paper models the uncertainty of wind power using second-order moments of probability distribution and their fluctuation intervals. Subsequently, a robust optimal power flow model based on probability distribution model and joint chance constraints is established. The Lagrangian duality theorem is then employed to eliminate random variables from the optimization model, transforming the uncertainty model into a deterministic linear matrix inequality problem. Finally, a convex optimization algorithm is used to solve the deterministic problem, and the results are compared with traditional chance-constrained optimal power flow model. The feasibility and effectiveness of the proposed method are validated through case study simulations.

KEYWORDS

wind power uncertainty, fluctuation interval, robust joint chance constraints, convex optimization, optimal power flow

1 Introduction

As the penetration rate of intermittent renewable energy sources, such as wind and solar power, continues to rise, the shortcomings of existing operating modes in the power system may limit the integration of new energy sources. The intermittency and incomplete controllability of renewable energy generation pose significant challenges to the safe and economic operation of the power system.

Traditional power systems mainly rely on thermal power generation to meet electricity demand, with no renewable energy generation units in the system. Therefore, traditional optimal power flow models proposed in (Bacher and Van Meeteren, 1988; Hua et al., 1998; Zhang et al., 2020; Kardoš et al., 2022) are not suitable for scenarios considering the uncertainty of new energy output. With the gradual development of low-carbon power construction, the significant injection of new energy has huge impacts on the safe and economic operation of the power system, demanding a reform in the power system's operational control mode. The volatility of wind power output (Ela and O'Malley, 2012) can be addressed at the planning level by configuring energy storage to smooth out output fluctuations (Wang et al., 2013; Angizeh et al., 2023; Fan et al., 2023). On the operational level, controllable generators can be scheduled to absorb fluctuations. In recent years, research on optimal power flow problems considering the stochastic nature of wind power has attracted considerable attention (Morales and Perez-Ruiz, 2007; Bienstock et al., 2012;



TABLE 1 Wind farm parameters

Parameter	Installed capacity (MW)	Predicted output (MW)
Wind farm in node 2	200	99
Wind farm in node 3	90	45

Shi et al., 2012; Li et al., 2015; Gao et al., 2017; Sun et al., 2019; Angizeh et al., 2023; Xiao et al., 2024a; Xiao et al., 2024b).

Reference (Li et al., 2015) establishes an optimal power flow model considering wind power uncertainty using stochastic programming. The paper obtains an estimated distribution of wind power output based on observed samples and generates a discrete scenario set based on this estimated distribution. However, the accuracy of the results depends on the number of observed samples and discrete scenarios, which can lead to the "curse of dimensionality." Reference (Morales and Perez-Ruiz, 2007) proposes a probability optimal power flow algorithm based on

three-point estimation, but the computational complexity of point estimation algorithms is high. Additionally, probabilistic power flow analysis should consider the correlation between realistically existing injection amounts, or it may result in significant errors (Sun et al., 2019). Reference (Bienstock et al., 2012) introduces the chance-constrained OPF (CC-OPF) model and proposes a cut-plane algorithm for solving it, assuming that wind power forecast errors follow a Gaussian distribution. To address the issue of modeling wind power stochastic errors with a single deterministic distribution, Reference (Gao et al., 2017) innovatively proposes the robust chance-constrained OPF (RCC-OPF) model, describing wind power forecast errors as random variables with uncertainty in both variance and expectation. However, Reference (Gao et al., 2017) does not provide a modelsolving algorithm.

Against this background, this paper proposes a power system optimal power flow calculation method considering the uncertainty of wind power probability distribution. The paper first models the uncertainty of wind power output using partial statistical information (Bofinger et al.). It then describes the optimal power flow problem of a wind farm system with distributionally robust joint chance constraints (DRJCC-OPF) (Zymler et al., 2013; Bian et al., 2014) and employs the Lagrangian duality to eliminate random variables in the model (Ding, 2014), transforming the uncertainty model into a deterministic linear matrix inequality (LMI). Furthermore, convex optimization methods are used to solve the deterministic LMI. This approach, based on partial statistical information of wind power in the power system, innovatively considers the uncertainty of the probability distribution of wind power forecast errors, obtaining generation scheduling plans that can meet the requirements of safe and economic operation of the power system under arbitrary wind power distributions. The feasibility and effectiveness of the method are verified through an IEEE 5-node case study.



The absolute deviation of line power flow from the thermal stability limit.

TABLE 2 Sin	nulation results	of TCC-OPF	and DRJCC-OPF.
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Models	Generation units output/MW	Generation cost (*10 ³)
TCC-OPF	5.33\1.97	7.33
DRJCC- OPF	5.00\2.30	7.53

2 Traditional chance-constrained optimal flow model

Deterministic optimal power generation scheduling results are based on renewable energy output forecasts and do not take into account fluctuations in new energy output, which often results in frequent line overloads and power system security risks (Zhang et al., 2018). Traditional chance-constrained optimal flow model (traditional-chance-constrained TCC-OPF) can correct this problem and buffer critical renewable energy fluctuations to ensure secure and economic operation of the power system (Ma et al., 2019)

$$\min\sum_{i\in GB} c\left(\overline{P_i}\right) \tag{1}$$

$$s.t.B\bar{\theta} = P_g + \mu - d \tag{2}$$

$$\mathbf{P}_i^{\min} \le \overline{\mathbf{P}_i} \le \mathbf{P}_i^{\max} \quad \forall i \in GB \tag{3}$$

$$P_L = T\left(\overline{P_g} + \mu - d\right) \tag{4}$$

$$|\mathbf{P}_L| \le P_L^{\max} \tag{5}$$

$$\Pr\left(\overline{\mathbf{P}_{i}} - \Omega \alpha_{i} \le \mathbf{P}_{i}^{\max}\right) \le \gamma \quad \forall i \in GB$$
(6)

$$\Pr\left(\mathbf{P}_{i} - \Omega \alpha_{i} \ge \mathbf{P}_{i}^{\min}\right) \le \gamma \quad \forall i \in GB \tag{7}$$

$$\Pr\left(\Omega\alpha_i \le \mathrm{RD}_i\right) \le \gamma \quad \forall i \in GB \tag{8}$$

$$\Pr(\Omega\alpha_i \ge -R \cup_i) \le \gamma \quad \forall i \in GB \tag{9}$$

$$\Pr(P_{Li} \le P_{Li}) \le \gamma \quad \forall i \in t \tag{10}$$
$$\Pr(P_{i} > -P_{i}^{\max}) \le \gamma \quad \forall i \in t \tag{11}$$

$$\sum_{i=1}^{n} a_{i} = 0 \quad \forall i \in CP \tag{12}$$

$$\sum_{i \in GB} a_i - 1, a_i \ge 0 \quad \forall i \in GD \tag{12}$$

$$\Omega = \sum_{j} w_{j} \quad j \in WB \tag{13}$$

Where: $\overline{P_i}$ is Generator i power generation at desired wind power output, $c(\overline{P_i})$ is generation cost of generator i, P_g , μ and d are generation power vector, wind power expected output vector and load power vector respectively; B is node susceptance matrix, $\overline{\theta}$ is node phase angle vector, P_L and P_{Li} are line power flow vector, line power flow random variable vector under expected wind power output considering wind power random fluctuation, T is power distribution coefficient matrix, w_j is wind power prediction error of wind farm i; α is generator dispatch factor, GB, ℓ , WB are sets of generator nodes, power lines, and wind farm nodes respectively. P_i^{max} and P_i^{min} are upper and lower limits of generator i, RD_i and RU_i







are upper and lower ramping limits of generator i. $P_L^{\rm max}$ are thermal limits of power lines, y is confidence level of safe operation of the system. Pr () in Eqs 6–11 stands for the probability of the probabilistic event in the parenthesis.

Equation 2 and 4 are nodal power balance equation and line flow equation; Eqs 3 and (6) and 7 are generation output limits of generators. Eqs 5, 10, 11 are the thermal limits of power lines. Eqs 8–9 are ramping limits of generators. The objective function is



minimization of generation costs. TCC-OPF model ensures safe operation of the system at a given confidence level while minimizing power generation costs_o

The TCC-OPF model is based on a single accurate probability distribution of wind power prediction errors, and is therefore only suitable for situations where a definite and comprehensive description of wind power or wind speed stochasticity exists.

3 Probabilistic distribution robust joint chance-constrained optimal power flow model and solution

Due to significant wind power fluctuations, we often can only obtain partial information about the probability distribution of wind power or wind power prediction errors (Bienstock et al., 2012). Without loss of generality, this paper assumes knowledge of the second-order moment information of the probability distribution of the wind power prediction error vector $\tilde{\omega}$. Let the empirical estimate of the expectation of the wind power prediction error be denoted as μ_{w0} and the empirical estimate of the covariance matrix as Γ_0 . In real-world applications, due to limitations in prediction technology, obtaining precise second-order moment information is challenging. Therefore, this paper considers using empirical estimates of the second-order moments and their fluctuation intervals to describe the randomness of wind power prediction errors, as shown in Eqs 14, 15:

$$\mu_0 - \eta \le \mathbf{E}[\omega] \le \mu_0 + \eta \tag{14}$$

$$\Gamma_{0} + (\mu_{0} - \eta)(\mu_{0} - \eta)^{T} \le \mathbb{E}(ww^{T}) \le \Gamma_{0} + (\mu_{0} + \eta)(\mu_{0} + \eta)^{T}$$
(15)

Where, μ_0 and Γ_0 represents the empirical estimate of the second moment of wind power prediction errors; η denotes the extent of deviation between the actual second moment and its estimated value, reflecting the accuracy of wind power predictions.

Based on the above assumptions, this paper proposes a method of using a series of probability distribution functions that satisfy the given second moment information to describe the uncertainty of wind power prediction errors. Let the probability distribution set formed by the series of probability distribution functions be denoted as $\Phi(\mu_w,\Gamma)$.

This section first establishes a robust joint chance-constrained optimal power flow model. Subsequently, the robust joint chance-constrained model is transformed into a deterministic Linear Matrix Inequality (LMI) problem, which does not involve random variables. Finally, a convex optimization algorithm is employed to solve this problem.

3.1 Probabilistic distribution robust joint chance-constrained optimal power flow model

In response to the uncertainty associated with the probability distribution of wind power prediction errors, and in order to obtain a generation scheduling scheme that satisfies system safety



constraints under any probability distribution in $\Phi(\mu_w,\Gamma)$. Based upon the TCC-OPF models, the DRJCC-OPF is employed to describe the optimal power flow problem considering wind power uncertainty. The specific model is as follows:

$$\min \sum_{i \in GB} \left\{ c_{i2} \left(\overline{P_i}^2 + \operatorname{var}\left(\Omega\right) \alpha_i^2 \right) + c_{i1} \overline{P_i} + c_{i0} \right\}$$
(16)

$$s.t.B\bar{\theta} = P_g + \mu - d \tag{17}$$

$$P_i^{\min} \le \overline{P_i} \le P_i^{\max} \quad \forall i \in GB$$
(18)

$$P_L = T\left(\overline{P_g} + \mu - d\right) \tag{19}$$

$$|P_L| \le P_L \tag{20}$$

$$\left(P_i^{\min} \le \overline{P_i} + \Omega \alpha_i \le P_i^{\max} \quad \forall i \in GB \right)$$

$$\inf_{\Phi(\mu_{\omega},\Gamma)} \Pr\left\{ \begin{array}{c} -\mathrm{RU}_{i} \leq \Omega \alpha_{i} \leq \mathrm{RD}_{i} \quad \forall i \in GB \\ |P_{Li}| \leq P_{Li}^{\max} \quad \forall i \in \mathscr{C} \end{array} \right\} \geq 1 - \varepsilon \quad (21)$$

$$\sum_{i \in GB} \alpha_i = 1, \alpha_i \ge 0 \quad \forall i \in GB$$
(22)

$$\Omega = \sum_{j} w_{j} \quad j \in WB \tag{23}$$

Where Eq. 16 represents the objective function, indicating the generation cost considering the regulating output of thermal power units (the specific transformation process of the objective function is detailed in the appendix); var(Ω) represents the variance of Ω . ε denotes the confidence level of violating the robust joint chance constraints; $\inf_{\Phi(\mu_{\omega},\Gamma)} (A)$ represents the minimum probability of event

A occurrence under all possible distributions; other variable definitions are the same as in Eqs 1–13.

In the above model, the probability distribution of wind power prediction errors is uncertain and can take any form of probability distribution in $\Phi(\mu_{\omega}, \Gamma)$. Therefore, the robust joint chance constraint Eq. 21 indicates that, under all possible probability distributions, the probability of satisfying system safety constraints is not less than $1 - \varepsilon$. Consequently, the DRJCC-OPF model can obtain scheduling strategies for generation power units that ensure the economic operation of the power system under the worst-case wind power distribution.

The decision variables of the DRJCC-OPF model are represented by $\overline{P_i}$, α , $\overline{\theta}$ and P_L , denoted as:

$$x = \left(\overline{P_i}, \alpha, \overline{\theta}, P_L\right) \tag{24}$$

Eqs 17-20, 22, 23 are deterministic constraints, while Eq. 21 represents the uncertainty constraint. The challenge in solving the DRJCC-OPF model lies in handling the probability distribution robust joint chance constraint equation.

3.2 Deterministic transformation of probability distribution robust joint chance constraints

Express the constraints in Eq. 21 in the form of unilateral constraints and separate the decision variables from the random variables, as shown below:



$$P_i - P_i^{\max} + (-\alpha_i e^T) \tilde{w} \le 0$$
⁽²⁵⁾

$$P_i^{\min} - P_i(\alpha_i e^T) \tilde{\omega} \le 0$$
(26)

$$-RD_i + (\alpha_i \mathbf{e}^T)\tilde{w} \le 0 \tag{27}$$

$$-RU_i - (\alpha_i e^T)\tilde{w} \le 0$$
(28)

For line power flow P_{Li} , it can be written in the following form (proof process is provided in the appendix):

$$\overline{P_{Li}} - P_{Li}^{\max} + \left(T_i' - T_i \alpha e^T\right) \tilde{w} \le 0$$
⁽²⁹⁾

$$-\overline{P_{Li}} - P_{Li}^{\max} - \left(T_i' - T_i \alpha e^T\right) \tilde{w} \le 0$$
(30)

Where e^{T} is the unit vector with all elements equals to 1. After replacing the expression in Eq. 21 with Eqs 25–30, the result is:

$$\inf_{\substack{\phi_{\omega} \in \Phi(\mu_{\omega}, \Gamma)}} \Pr \left\{ \begin{array}{l} \overline{P_{i}} - P_{i}^{\max} + (-\alpha_{i}e^{T})w \leq 0 \quad \forall i \in \wp \\ P_{i}^{\min} - \overline{P_{i}} + (\alpha_{i}e^{T})w \leq 0 \quad \forall i \in \wp \\ -RD_{i} + (\alpha_{i}e^{T})w \leq 0 \quad \forall i \in \wp \\ -RU_{i} - (\alpha_{i}e^{T})w \leq 0 \quad \forall i \in \wp \\ \overline{P_{Li}} - P_{Li}^{\max} + (T_{i}' - T_{i}\alpha e^{T})w \leq 0 \quad \forall i \in \ell \\ -\overline{P_{Li}} - P_{Li}^{\max} - (T_{i}' - T_{i}\alpha e^{T})w \leq 0 \quad \forall i \in \ell \end{array} \right\} \geq 1 - \varepsilon$$

$$(31)$$

Furthermore, by eliminating the random variables in Eq. 31 and transforming it into a deterministic problem (the detailed proof process is provided in the appendix), the resulting deterministic problem corresponding to the DRJCC-OPF model is expressed as follows:

$$\min \sum_{i \in p} \left\{ c_{i2} \left(\overline{P_i}^2 + \operatorname{var}(\Omega) \alpha_i^2 \right) + c_{i1} \overline{P_i} + c_{i0} \right\}$$

$$s.t. y_0 \in \mathbb{R}, y_1, y_2 \in \mathbb{R}^{n_w}, Y_1, Y_2 \in S^{n_w},$$

$$\beta + \frac{1}{\varepsilon} \left(\left\langle \Omega_+, \begin{pmatrix} Y_1 & \frac{1}{2}y_1 \\ \frac{1}{2}y_1^T & y_0 \end{pmatrix} \right\rangle - \left\langle \Omega_-, \begin{pmatrix} Y_2 & \frac{1}{2}y_2 \\ \frac{1}{2}y_2^T & y_0 \end{pmatrix} \right) \right\rangle \right) \le 0,$$

$$\left(\begin{pmatrix} Y_1 & \frac{1}{2}y_1 \\ \frac{1}{2}y_1^T & y_0 \end{pmatrix} - \left(\begin{pmatrix} Y_2 & \frac{1}{2}y_2 \\ \frac{1}{2}y_2^T & y_0 \end{pmatrix} \right) \ge 0,$$

$$\left(\begin{pmatrix} Y_1 & \frac{1}{2}y_1 \\ \frac{1}{2}y_1^T & y_0 \end{pmatrix} - \left(\begin{pmatrix} Y_2 & \frac{1}{2}y_2 \\ \frac{1}{2}y_2^T & y_0 \end{pmatrix} \right) = 0,$$

$$\left(\begin{pmatrix} Y_1 & \frac{1}{2}y_1 \\ \frac{1}{2}y_1^T & y_0 \end{pmatrix} - \left(\begin{pmatrix} Y_2 & \frac{1}{2}y_2 \\ \frac{1}{2}y_2^T & y_0 \end{pmatrix} - \left(\begin{pmatrix} 0 & \frac{1}{2}L_i(x)^T \\ \frac{1}{2}L_i(x) & L_i^0(x) - \beta \end{pmatrix} \right) \ge 0, \forall i = 1, ..., m,$$

$$(32)$$

Where $L_i(x)$ and $L_i^0(x)$ correspond to the left side of Eqs 25–30 (details are explained in the appendix); *m* represents the total number of individual chance constraints in the robust joint chance constraint Eq. 31; *x* is the decision variable as in Eq. 24; Ω_+ and Ω_- is given by Eqs 33, 34:

$$\Omega_{+} = \begin{pmatrix} \Gamma_{0} + (\mu_{0} + \eta)(\mu_{0} + \eta)^{T} & \mu_{0} + \eta \\ \mu_{0}^{T} + \eta_{0}^{T} & 1 \end{pmatrix}$$
(33)

$$\Omega_{-} = \begin{pmatrix} \Gamma_{0} + (\mu_{0} - \eta)(\mu_{0} - \eta)^{T} & \mu_{0} - \eta \\ \mu_{0}^{T} - \eta_{0}^{T} & 1 \end{pmatrix}$$
(34)

3.3 Solution algorithm

Eq. 32 represents a convex optimization problem with LMI constraints, and a convex optimization algorithm can be employed to obtain the global optimal solution.

4 Case study

This paper conducts simulation tests using a modified 5-node system as shown in the diagram. The power system topology is illustrated in Figure 1, and specific data can be found in reference (Wang, 2003). Nodes 2 and 3 are connected to a wind farm, and the wind farm data is provided in Table 1. Optimization modeling is performed on the MATLAB platform, and the YALMIP solver is invoked to solve the LMIs in the model.

For simplicity in analysis, this paper assumes that the output of each wind farm is independent of each other. The expected value of wind power prediction error is denoted as μ_{ω} µ, and the variance is denoted as Γ . For μ_0 the empirical estimate of wind power prediction error, it is generally assumed that the predicted output of wind power is equal to the expected output of wind power (Baharvandi et al., 2018). Therefore, it can be assumed that $\mu_0 = 0$. In cases $\mu_0 \neq 0$ or where wind power outputs are not mutually independent, the problem can still be solved after appropriate transformations (Calafiore et al., 2009).

4.1 Comparison of simulation results between TCC-OPF and DRJCC-OPF

Let $\mu_0 = 0$, $\Gamma_0 = 0.003$ and $\varepsilon = 0.0105$ (Bian 2015). The simulation results comparison between TCC-OPF and DRJCC-OPF is illustrated in Figure 2 and Table 2.

According to Table 2, it is evident that the generation cost in DRJCC-OPF is higher than that in TCC-OPF. This is because DRJCC-OPF represents a more conservative estimate, ensuring system compliance with safety requirements under the worst-case distribution. Additionally, from Figure 2, it can be observed that under DRJCC-OPF, the absolute deviation of line power flow is higher than that under TCC-OPF. This indicates a more uniform distribution of line power flow, making it less prone to overloads.

4.2 Simulation results for robust joint chance-constrained OPF

This section analyzes the impact of system operating parameters and wind power uncertainty parameters on the system generation cost. The system operating parameters include the confidence level of safe operation, which is the probability $1 - \varepsilon$ of satisfying the robust joint chance constraints. The wind power uncertainty parameters consist of the prediction reliability η and the empirical estimate Γ_0 reflecting the volatility of wind power forecasting errors.

4.2.1 Impact of wind power prediction reliability on cost

Let $\varepsilon = 0.01$ and $\Gamma_0 = 0.003$. Since it is assumed that the predicted output of wind power is equal to the expected output of wind power, this paper only considers the case of a smaller value of η , with values ranging from 0.02 to 0.03. The results of DRJCC-OPF are as follows:

Figure 3 shows that as the prediction reliability decreases (or increases), the generation cost increases. This is because when the prediction accuracy decreases, the system needs to dispatch generators, especially Generator 2 with greater regulating capacity, to cope with the fluctuations in uncertain parameters, leading to an increase in generation cost.

4.2.2 Impact of system safety operation confidence level on generation cost

Let $\eta = 0$ and $\Gamma_0 = 0.003$, ε ranging between 0.01 and 0.5, the results of DRJCC-OPF model are as follows:

Figure 4 indicates that with the relaxation of the system's safety operation constraints, the generation cost decreases. In Figure 5, as the safety constraints increase, the controllable output of the generating units decreases to reserve more regulating capacity to cope with the fluctuations in wind power output. When the confidence level of violating chance constraints is greater than 0.1, the impact of safety constraints on the output of generating units is relatively small. This is because, in this case, the less strict system's safety constraints demands less regulating capacity for the generating units. The generating units can operate under optimal conditions with lower impact. When the confidence level of violating chance constraints is less than 0.1, the safety constraints become more stringent, and further increasing the safety constraints significantly affects the output of generating units.

Moreover, combining Figures 5, 6, it can be observed that when $\varepsilon \le 0.2$, the regulation coefficient of Generator 1 is constrained by its regulating capacity, leading to a decrease in the regulation coefficient. In contrast, when $\varepsilon \ge 0.2$, the regulation coefficient of Generator 1 increases to reduce the generation cost. This demonstrates that the DRJCC-OPF model can flexibly adapt to different operational requirements of the system.

4.2.3 Impact of wind power output fluctuations on generation cost

Let $\eta = 0$ and $\varepsilon = 0.01$, When the variance of wind power prediction errors Γ_0 varies between 0.0 and 0.009, the results of DRJCC-OPF are as follows:

Figure 7 indicates that after an increase in wind power fluctuations, the system needs to increase the planned output of Generator 2 to maintain safe operation, leading to an increase in generation cost. Additionally, from Figure 8, it can be observed that considering wind power fluctuations, the system decreases the planned output of Generator 1 and increases the output of Generator 2 to enhance the system's ability to cope with wind power fluctuations. At the same time, the regulation coefficient for Generator 1 rapidly decreases and then gradually increases. This is because when wind power fluctuations start to increase from zero, Generator 1 is constrained by the output limit, leading to a rapid decrease in its regulation coefficient. As Generator 1 deviates from the output limit due to a decrease in output, if wind power fluctuations continue to increase, the system gradually decreases the regulation coefficient for Generator 2 and increases the regulation coefficient for Generator 1 to reduce generation cost. This indicates that DRJCC-OPF can ensure safe and economic operation even when wind power fluctuations are significant.

5 Conclusion

The large-scale integration of new energy sources, especially wind power, poses significant challenges to the secure operation of power systems. This paper focuses on the uncertainty in wind power prediction errors and proposes a probabilistic distribution robust joint chance-constrained optimal power flow model for wind power systems. This model can obtain scheduling schemes for thermal power units that ensure safe and economic operation under the worst-case wind power distribution. The analysis also explores the impact of factors such as prediction reliability, confidence level for safe system operation, and wind power fluctuations on system generation cost and unit dispatch strategies. This approach provides a new perspective for the economic dispatch of power systems incorporating renewable energy sources. The findings can serve as a reference for system operators and control personnel in managing power systems with renewable energy integration.

Data availability statement

The raw data supporting the conclusion of this article will be made available by the authors, without undue reservation.

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Author contributions

LD: Investigation, Methodology, Writing-original draft. HX: Software, Validation, Writing-review and editing. PY: Data curation, Resources, Supervision, Writing-review and editing.

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Author LD was employed by Guangzhou Power Supply Co. Ltd.

The remaining authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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